APPENDIX F: GEOTECHNICAL INVESTIGATION REPORT

# Report of Geotechnical Investigation and Analysis

## Slope Stability Evaluation Pickles Butte Sanitary Landfill Expansion Canyon County, Idaho

Tetra Tech Project No. 114-571040-2022

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## **ACRONYMS/ABBREVIATIONS**

Acronyms/ Abbreviations	Definition
AASHTO	American Association of State Highway and Transportation Officials
ASTM	ASTM International (formerly known as American Society for Testing and Materials)
bgs	Below ground surface
CFR	Code of Federal Regulations
IDEQ	Idaho Department of Environmental Quality
EPA	U.S. Environmental Protection Agency
FS	factors of safety
ksf	kips per square foot
MCE	Maximum Credible Earthquake
mm	millimeter
MSWLF	Municipal Solid Waste Landfills
PBSL	Pickles Butte Sanitary Landfill
PGA	Peak Ground Acceleration
PSHA	Peak spectral horizontal acceleration
SPT	Standard Penetration Testing
USGS	United States Geological Survey

## **EXECUTIVE SUMMARY**

The Pickles Butte Sanitary Landfill is developing a plan for the expansion of the landfill to include an additional four phases, (Phase 5 through Phase 8). The proposed expansion consists of approximately 231 acres of unlined cells pending the approval of an arid exemption. Proposed permanent excavation slopes are planned to be on the order of 3H:1V to 4H:1V, with maximum cut depths on the order of 150 to 165 feet.

Tetra Tech previously completed a slope stability evaluation that included static and seismic stability evaluations for Phases 2 through 4 of the Canyon County Landfill (October 7, 2015). Tetra Tech also reviewed the previous evaluations conducted by Holladay Engineering Company for the Pickles Butte Sanitary Landfill, dated 1998, and conducted a seismic survey that was dated February 21, 2022 titled, 'Pickles Butte Sanitary Landfill 3D Seismic Survey Report'. The survey was designed to image and delineate a suspected fault in support of the proposed expansion program at the PBSL.

For this stability evaluation, Tetra Tech incorporated the following information: 1) the soils strength data available from previous analysis, 2) materials strength properties assigned based on the laboratory testing of the geotechnical samples collected in 2021 and also correlated from the Standard Penetration Testing (SPT) N-value (blow count) data collected during the geotechnical drilling and previous well installation reports.

Based on findings from former and 2021 site investigations, the subsurface conditions beneath the areas of proposed landfill expansion are assumed to generally consist of silty and clayey sand, clay, and gravel overlying the Glenns Ferry Formation (300 to 950 feet thick), which includes younger lacustrine and fluvial sediments. The surrounding local geology includes an igneous basalt group of the Hat Butte-McElroy Butte type<sup>1</sup> that was not encountered in area of the proposed expansion.

Slope stability and pseudo-static analyses were performed using the computer program Slide2 (2020), developed by Rocscience, Inc., to determine the factors of safety (FS) of critical slip surfaces using both circular (rotational) and block failure analyses and vertical slice limit equilibrium methods. Circular failures can be viewed as a soil 'slump' with a remnant head 'scarp' or drop in elevation where the slide started, and a resultant 'hump' or bulge at the slide terminus. A block failure represents a large mass or 'chunk' of soil failing outwardly as a larger intact mass. Where the pseudo-static analysis indicated a factor of safety of equal to or less than 1.3 (industry standard for pseudo-static factor of safety for landfills), the internal slope of the landfill cell prior to waste emplacement was evaluated using the Newmark displacement analysis method to determine a range of potential seismic-induced deformations of the refuse mass.

Results of the slope stability evaluations indicate that the preliminary design for the expansion phases will meet the requirements of the Idaho Administrative Rules IDAPA 58.01.06 for the Idaho DEQ's administration of municipal solid waste landfills (MSWLF). The analyses indicate static FS values on the order of 1.38 to 2.43, and 1.83 to 3.11 for circular and block failure respectively, while the pseudo-static FS values were on the order of 0.99 to 1.88, and 1.45 to 2.16 for circular and block failure, respectively. Subsequent seismic deformation analyses indicate maximum probable displacements on the order of 0.25 to 3.19 inches (0.5 to 8 cm) for the anticipated peak ground acceleration of 0.12g generated during the design seismic event at the project site. In general, the seismic displacement analyses indicate permanent seismic-induced displacements within the tolerances 6 to 12 inches (15 to 30 cm) that are typically considered acceptable for design of landfill systems with no liner.

Multiple slope angles were considered for Tetra Tech's slope analyses, ranging from 2.5:1 to 4:1 depending on the soil and bedrock types at each location. Based on Tetra Tech's analysis and the required FS's, the following two slope angles are recommended for the preliminary landfill site grading plans:

3H:1V: for the majority of the site slopes

4H:1V: where silt is encountered (Section F discussed below)

<sup>&</sup>lt;sup>1</sup>Mancos - Macrostrat.org

The 4:1 slope was analyzed and recommended for Section F because silt was interbedded between poorly-graded sand and fine sand and created a weakened soil profile. In areas where a high concentration of silt is predominant during construction, a slope of 4H:1V is recommended for cut areas. The soil profile within Section F was identified as having a high concentration of silt in the upper 135 feet of the proposed slope cut, thus decreasing the factor of safety. There are other areas where the silt was present; however, based on the analysis the proposed cut slope of 3H:1V was allowable for the silts as they were interbedded into stronger soil deposits. As the stratification is exposed during excavation of future cells, it is recommended that the soil conditions be reviewed to verify they match the design criteria.

The slope with compacted refuse were modeled to confirm the slope angles that were allowable during the backfilling process. Slopes of 3H:1V are recommended as a maximum angle for the backfill process. A steeper slope of 2.75H:1V was modeled as an iteration to confirm the recommendations, and in this situation the pseudo static conditions produced a factor of safety below 1.3 and is not recommended.

Portions of the soil profile were defined as claystone, and have unconfined compression strengths higher than the site soils; however, the claystone had interbedded layers of softer soils, and for this reason Tetra tech has treated these areas as a soil rather than a rock and also recommends a slope cut of 3H:1V for the claystone zones.

This executive summary has been prepared solely to provide a general overview and should not be relied upon for any purpose except for that for which it was prepared. The full geotechnical report must be referenced for information about findings, recommendations, and other concerns.

## 1. INTRODUCTION AND BACKGROUND

The following report is the geotechnical evaluation of the slope stability that provides recommendations for the planned lateral expansion of the landfill. The Pickles Butte Sanitary Landfill (PBSL) is located at 15500 Missouri Ave. in Nampa, Idaho. The landfill is located approximately 6-miles south of Nampa, north of Missouri Avenue, south of Deer Flat Road, and ¼- mile west of Farner Road. Canyon County (County) owns approximately 1,180 acres of land in the area, which includes the active area of the PBSL. The County has operated the landfill since it began accepting waste in April 1983. PBSL currently services the residents of Canyon and Owyhee Counties.

The Idaho Department of Environmental Quality (DEQ) approved the original design and operating plan for the PBSL in June 1973, and reconfirmed approval in May 1975 (Holladay, 1994). The Southwest District Health Department approved the landfill in December 1979. Then when Subtitle D was implemented, the County obtained a site certification for the landfill from the DEQ in August 1993 for 116.7 acre. The County applied to modify the site certification boundary in 2020 and received approval from DEQ in February 2021 for approximately 600 acres. The current waste disposal area occupies the original footprint of approximately 116.7 acres, which has a natural soil liner. The Site Certification for the planned lateral expansion was approved on February 26, 2021.

The DEQ Site Certification approval included a request that engineering design considerations be evaluated for resisting peak ground accelerations, prior to the design and construction of containment structures. This report addresses that request and discusses the seismic considerations and slope stability. After the approval was received, a data gaps analysis was conducted in 2021 to identify missing or additional data required for the design focusing on geotechnical and seismic considerations. The evaluation identified locations where additional data would be beneficial and proposed a geotechnical drilling program that was initiated in November 2021 to collect additional data for the analysis.

This report is organized as follows: **Section 1** presents the introduction and background; **Section 2** presents the purpose and the scope; **Section 3** provides information on the proposed expansion; **Section 4** provides highlights of the field exploration; **Section 5** provides information on the geotechnical laboratory testing; **Section 7** discusses the engineering analysis and recommendations; **Section 8 Section 9** provides limitations of the study; and **Section 10** provides references. **Appendix A** provides miscellaneous figures and details, **Appendix B** provides exploratory boring logs, **Appendix C** provides the laboratory testing, **Appendix D** provides slope analysis, **Appendix E** provides deformation analysis, and **Appendix F** provides previous boring logs.

## 2. PURPOSE AND SCOPE OF STUDY

Tetra Tech performed stability analyses and seismic evaluations of the proposed expansion cell geometries to verify adequate stability or to indicate if flatter slopes are required to achieve stability. The analyses were performed in accordance with Tetra Tech's proposal and contract with Canyon County Solid Waste.

The regulatory requirements for the stability analysis are discussed in the administrative rules for the Idaho Solid Waste Facilities Act (Idaho Statutes, Title 39 – Health and Safety, Chapter 74, Section 39-7407) for the Idaho Department of Environmental Quality's (IDEQ) administration of municipal solid waste landfills (MSWLF) and are discussed further in **Section 7.1**.

The purpose of this study is to demonstrate that slope stability requirements are met for the conceptual design of the following containment structures:

- Phase 5-1, 5-2, 5-3 Temporary Cut Slope, Maximum Section (Section E)
- Phase 6-1, 6-2, 6-3 Temporary Cut Slope, Maximum Sections (Sections C and F)
- Phase 7-1, 7-2, 7-3 Temporary Cut Slope, Maximum Section (Sections B, C, D, F, G)
- Phase 8-1, 8-2, 8-3 Temporary Cut Slope, Maximum Section (Sections B, C, D, F, G)

• Final Slope with Waste Backfilled (Section A was used to represent final slope criteria).

This report details and summarizes the analyses, the material properties selected for the analyses, the seismic design criteria, and presents conclusions based on the existing subsurface conditions and proposed landfill design and construction.

## 3. PROPOSED EXPANSION

The proposed area for the expansion has been sectioned into smaller units and labeled as the phases listed in Figure 1040-1, Data Gap Areas & Proposed Boring Plan (**Appendix A**). The proposed conceptual expansion of Phases 5 through Phase 8 will consist of approximately 231.4 acres of unlined cells. Proposed fill slopes are planned to be on the order of 5.3H:1V (horizontal to vertical) to 4H:1V, with maximum waste fill depths on the order of 254 feet. Proposed excavation slopes are planned to be on the order of 3H:1V to 4H:1V, with maximum cut depths on the order of 150 to 165 feet. The finished fill slopes will consist of a sequence of slopes with 20-foot-wide storm water/erosion-control benches for every 40 to 60 feet of elevation gain. The purpose for selecting flatter slopes includes more effective erosion and stormwater control on the final slopes.

If the design, locations, or conditions are significantly different from those described above, Tetra Tech should be notified to reevaluate the recommendations contained in this report.

## 4. FIELD EXPLORATION

Tetra Tech conducted a field investigation for Phases 5 through 8 between the dates of November 15 and December 19, 2021. The field investigation consisted of drilling eight boreholes to explore subsurface conditions at the locations shown on Figure 1040-1 (Data Gap Areas & Proposed boring Plan, **Appendix A**). Figure 1040-1 includes the conceptual expansion cells for the landfill, the locations of the exploration borings, and the location of borings drilled in previous phases. Prior to mobilization, Tetra Tech contacted Idaho One Call to request the location and clearance of public underground utilities before performing drilling. Well logs from the previous well installations are included in **Appendix F**, and they include extracted pages from the Geotechnical Evaluation by Holiday Engineering Company (Holiday), Borehole Logs GT-1 through GT-5, and the combination of Well Driller's Reports and Well Logs PB logs 5 through 15 by Holiday and Daniel B. Stephens & Associates, Inc. The logs provide general descriptions and depths of the site soils at each location.

Canyon County's drilling subcontracted with Holt Drilling to advance the borings through overburden soils with a track-mounted TS150 Crawler drilling rig equipped with auger, 6-inch diameter outer casing and core barrel. The TS150 Crawler provides very accurate and detailed soil profiles when compared to other drilling methods like auger. Tetra Tech's field engineer provided technical oversight during the field investigation, logged the borings, and obtained samples. The borings were backfilled with grout.

Sampling of the borings included determination of the N values, collection of split spoon samples, and bulk samples. Split-spoon samplers were driven into the various strata using a 140-pound hammer falling 30 inches. Sampling was done every 2 feet in the first 10 feet to obtain accurate soil strengths in the depths most critical to the evaluation of the dust control system and landfill gas flare pad. After 10 feet sampling was done every 5 feet to the final depth. For the expansion design sampling was done every 5 feet done to a depth of 50 feet and every 10 feet to 170 feet to collect information about the relative densities of the soil stratum.

The number of blows required to advance the sampler each of three successive 6-inch increments was recorded. When using the split-spoon sampler, the total number of blows required to advance the sampler the second and third 6-inch increments is the penetration resistance (N value), as described by ASTM International (ASTM) Method D1586. Penetration resistance values generally indicate the relative density or consistency of the subsurface soils.

Samples of the subsurface materials were obtained with both 2-inch and 2.5-inch outside- diameter split-spoon samplers. Bulk, Shelby tube and modified California samples were collected at various layers by the field engineer under the direction of a senior geotechnical engineer. More specific drilling and subsurface information regarding individual borings is listed below. Bulk samples of soil were obtained from cuttings based on visual observations in the field.

#### B2021-1/B2021-2

- Geotechnical borings for dust control system drilled to 30 ft
- Deep layer of poorly graded sand

#### B2021-3

- Geotechnical boring for landfill expansion
- Winch line snapped imbedding sampling rod deep into a clay layer at 170 feet.

#### B2021-4

- Geotechnical boring for landfill expansion
- Thick layers of loose sand extended to 90 feet, which created an issue with keeping the hole open. The hole collapse was especially problematic between 50 90 feet.
- The deep clay layers were not encountered as in all other deep borings.

#### B2021-5

- This boring was sited after geophysical seismic testing
- Samples were collected for analysis in the zone geophysics indicated the fault splay was located
- No visual evidence was found during drilling to confirm the existence of a fault plane

#### B2021-6

- Geotechnical boring for landfill expansion
- Altering layers silt and sand were encountered till 75 feet
- Dense clay to 200 feet with occasional silt seams between 100 110 feet

#### B2021-7

- Geotechnical boring for landfill expansion
- Altering layers of dense sand and silt were encountered till approximately 65 feet followed by dense clay with varying amounts of silt to 145 feet.
- Dense blue-gray clay continued to 200 feet.

#### B2021-8

- Geotechnical boring for Landfill Gas Flare Station
- Type II cement should be used for concrete in contact with silt soils

Boring logs were prepared noting the borehole location, equipment and drill methods used, subsurface profile and descriptions per ASTM D2487. Groundwater was not encountered in any of the borings. Boring depths are referenced to the existing ground surface elevation. Depths at which the samples were obtained along with the penetration resistance values are shown on the logs of exploratory borings, presented in **Appendix B** (Figures 1-B through 8-B).

## 5. LABORATORY TESTING

Samples obtained during the field exploration were taken to Tetra Tech's accredited laboratory, where they were observed and visually classified in accordance with ASTM Method D2488, which is based on the Unified Soil Classification System.

Following the field exploration, a senior Tetra Tech geotechnical engineer reviewed all the boring logs and samples obtained and created an inventory of samples available for testing. The senior engineer reviewed the potential depths of cut, and locations of fill, and selected samples along the depths of each boring for testing. The tests assigned in each boring were intended primarily to identify the precise type of soil at each depth, as well as the associated strength properties of each soil type, with the ultimate goal of incorporating all of the strength testing directly into the slope stability models in each cross section analyzed. The laboratory testing data was directly utilized in the slope stability models to determine the resultant factor of safety at each cross-section location.

The laboratory testing was performed in general accordance with the Idaho Materials Manual of Test Procedures, American Association of State Highway and Transportation Officials (AASHTO), ASTM, or other approved procedures. Tetra Tech's laboratory is an AASHTO Materials Reference Laboratory (AMRL) and Concrete and Cement Reference Laboratory (CCRL) accredited facility conforming to ASTM E 329 - Standard Specification for Agencies Engaged in Construction Inspection, Testing, or Special Inspection.

**Table 1** describes laboratory testing performed for this investigation, and their purpose:

Test Conducted:	To Determine:	Test Procedure:
Natural Moisture Content	Moisture content representative of field conditions at the time samples were taken.	ATM D2216
Grain-size Distribution	Size and distribution of soil particles (i.e., clay, silt, sand, and gravel).	ASTM D6913
Natural Moisture Content	Moisture content representative of field conditions at the time samples were collected.	ATM D2216
Atterberg Limits	The effect of varying water content on the consistency of fine- grained soils.	ASTM D4318
Moisture-Density Relationship	The optimum moisture content for compacting soil and the maximum dry unit weight (density) for a given compactive effort.	MT 210-16 MT 230-16
Unconfined Compression	Unconfined compressive strength of soil and rock.	ASTM D2166 ASTM D7012
Direct Shear	Standard Test Method for Direct Shear Test of Soils Under Consolidated Drained Conditions	ASTM D3080
Triaxial Shear	Consolidated-Undrained soil strength properties.	ASTM D4767
Resistivity and pH	The combination of these characteristics determines the potential of soil to corrode metal.	ASTM G187/D4972 MT 232-16
Consolidation	The amount a soil sample compresses with loading and the influence of wetting on its behavior. For use in settlement analysis, determining expansive potential and foundation design.	ASTM D2435

#### Table 1. Laboratory Testing Completed by Tetra Tech

Field and laboratory test results are presented graphically and summarized in **Appendix C**. This data, along with the field information, were used to prepare the exploration boring logs in **Appendix B**.

## 6. SUBSURFACE CONDITIONS

Subsurface soil conditions are variable throughout the boring depths; elevations ranged between 2956.6 to 2436.6 feet. The borings contained interbedded layers of poorly graded sand, poorly graded sand with silt, silty sand, silty with sand, silt, lean clay with sand, and silty clay. One layer of fat clay was observed in boring B2021-6 as described below. Given the variability of the site soils, other variations in the soil classifications are entirely possible. The top elevation of the individual borings varied, so the boring descriptions were broken into sections based on elevation for a more defined classification throughout the proposed cells.

Subsurface soils were classified in accordance with standards set by AASHTO. Descriptive terms were obtained using the ASTM Soil Classification System. Both the AASHTO and ASTM classifications are noted on the logs and laboratory data presented in **Appendix C** for each soil sample. **Appendix C** includes a summary of all the soil types and properties obtained in the borings drilled along the project length. Each soil type encountered is briefly described below.

#### 6.1 Sand

Sand was encountered in all borings, B2021-1 through B2021-7, at depths ranging in elevations on the order of 2799 to 2470 feet. The sand gradations included poorly-graded sand, poorly-graded sand with silt, and silty sand. The poorly-graded sand generally consisted of a fine to medium-grained matrix, while the silty sand was fine-grained. In Boring B2021-8, the sand included 10 feet of fine-grained, silty sand, and 2.5 feet of a poorly-graded fine to medium grained sand.

Penetration resistance values in the sand ranged from 2 to greater than 50 blows per foot which indicates a potentially very loose to very dense soil stratum. The looser densities were encountered near the surface, with an increase in density at depths of approximately 10 feet and deeper. The natural moisture contents in the sand ranged from 2 to 22 percent at the time of drilling.

Laboratory testing performed on bulk and split spoon samples of the sands indicated a range of maximum dry density between 100.2 and 111.7 pcf, and an optimum moisture content between 11 and 16 percent. (**Appendix C**). Results of the Unconfined Compression Test for boring B2021-3 between 61 and 65 feet indicates an unconfined compression strength on the order of 0.143 kips per square foot (ksf). Direct shear testing of the sand in Boring B2021-3 between 60 to 62 feet indicates a cohesion of 0.282 ksf and a friction angle of 20.2 degrees, and between 80 and 82 feet a cohesion of 0.413 ksf, and a friction angle of 32.81 degrees. Consolidation testing indicated an under-consolidated soil in with preconsolidation pressure 3.0 ksf and a swell pressure of 2.6 percent. (**Appendix C**).

In Boring B2021-4 between 90 and 91 feet, the direct shear testing indicated a cohesion of 0.198 ksf, and a friction angle of 22.83 degrees, and between 120 and 120.9 feet, the cohesion was on the order of 0.588 ksf, with a friction angle on the order of 29.51 degrees. Direct shear testing in Boring B2021-5 between 90 and 91.5 feet indicated a cohesion of 0.260 ksf, and a friction angle of 31.18 degrees.

In Boring B2021-3 between 25 and 27 feet, the triaxial shear testing indicated a cohesion of 0 ksf, and a friction angle of 25.86 degrees. Triaxial shear testing of the soil in Boring B2021-5 between 50 and 51.5 feet indicated a cohesion of 0.123 ksf, and a friction angle of 27.04 degrees.

#### 6.2 Silt

Silt was encountered in Borings B2021-3 through B2021-7 at depths ranging in elevations from 2,784 to 2,490 feet. The silt classifications varied between silt and silt with sand. The silt and silt with sand layers varied in thickness between 1 and 28 feet.

Generally the silt was tan to gray and had low plasticity. Penetration resistance values in the silt ranged from 10 to greater than 50 blows per foot which indicates a potentially stiff to hard matrix soil stratum.

Laboratory testing performed on bulk and split spoon samples of the silt soils indicated natural moisture content of samples ranged from 4 to 29 percent at the time of drilling. Boring B2021-5 was sited to attempt to intersect the suspected fault in the area. In Boring B2021-5 at 70 feet, the liquid limits were on the order of 27 with a plastic index of 21 and a dry density of 112 pounds per cubic feet (pcf). The soils and soil matrix in this boring did not differ substantially from the other borings, and therefore there was not conclusive evidence to indicate the presence of a fault. In Boring 2021-8 at 100 feet the liquid limits were non plastic, and the dry density was 97 pcf.

In Boring the B2021-5 between 69 and 70 feet, the triaxial shear testing indicated a cohesion of 0.037 ksf, and a friction angle of 19.09 degrees (**Appendix C**).

#### 6.3 Lean Clay

Lean Clay and lean clay with sand was encountered in Borings B2021-5 through B2021-7, at depths ranging in elevations on the order of 2,615 to 2,456 feet. The clay layers varied between 1 foot and 54 feet thick. Penetration resistance values in the lean clay ranged from 45 to greater than 50 blows per foot which indicates a potentially hard to very hard soil stratum. The clay color was gray to tan to blue and had high plasticity.

Laboratory testing performed on bulk and split spoon samples of the clay soils indicated natural moisture content of samples ranged from 20 to 21 percent at the time of drilling. In Boring B2021-5 between 80 and 81.5 feet, the liquid limits were on the order of 35 with a plastic index of 14. In Boring 2021-6 at 106 feet the liquid limit was 47 with a plastic Index of 25, with a maximum dry density of 100.0 pcf and an optimum water content of 20.5 percent.

In Boring the B2021-7 between 120 and 121.3 feet, the triaxial shear testing indicated a cohesion of 0.053 ksf, and a friction angle of 18.02 degrees (**Appendix C**).

#### 6.4 Silty Clay

Silty clay was encountered in Borings B2021-4 through B2021-7, at elevations on the order of 2,774 to 2,510 feet. The layers of silty clay were not as prevalent as the other soil types and averaged in thicknesses between 2 and 15 feet.

Generally, the silt clay was tan to gray and has higher plasticity. Penetration resistance values in the silt ranged from 26 to greater than 50 blows per foot which indicates a potentially hard to very hard soil stratum.

Laboratory testing performed on Shelby, bulk and split spoon samples of the silt soils indicated natural moisture content of samples ranged from 16 to 24 percent at the time of drilling. In Boring B2021-5 at 50 feet, and in Boring B2021-7 at 120 feet, the consolidation testing indicated an under-consolidated soil in with pre-consolidation pressures of 4.8 and 1.5 ksf. Boring B2021-5 had a swell pressure of 2.8 percent.

In Boring B2021-5 between 50 and 51.5 feet the triaxial shear testing indicated a cohesion of 0.489 ksf, and a friction angle of 14.95 degrees (**Appendix C**).

Boring B2021-5 was sited to attempt to intersect the suspected fault in the area. The soils and soil matrix in this boring did not differ substantially from the other borings, and therefore there was not conclusive evidence to indicate the presence of a fault.

#### 6.5 Fat Clay

Silty clay was encountered in Boring B2021-6 from elevations 2,555 to 2,531 feet. The fat clay was very dark gray, had a high plasticity, and consolidated similar to claystone. It was identified in this single boring; however, may exist in surrounding areas. Penetration resistance values were greater than 50 blows per foot which indicates a potentially very hard soil stratum.

Laboratory testing performed on split spoon samples of the fat clay indicated liquid limits were on the order of 56 to 67 with a plastic index of 19 to 22. (**Appendix C**).

#### 6.6 Groundwater

Groundwater was not encountered in any of the previous or more current borings drilled at this site. Based on the well data presented in previous reports, the natural groundwater elevation is assumed to be below the proposed excavation depths of up to 200 to 250 feet for the proposed landfill expansion. Numerous factors contribute to groundwater fluctuations, and evaluation of such factors is beyond the scope of this report.

## 7. ENGINEERING ANALYSIS AND RECOMMENDATIONS

#### 7.1 Seismic Impact Zone Characterization

The seismic evaluation of the landfill was completed to comply with the Idaho Department of Environmental Quality's administration of municipal solid waste landfills. The Canyon County Landfill is located within a "seismic impact zone" as defined by the Administrative Rules for the for the Idaho Solid Waste Facilities Act (Idaho Statutes, Title 39 – Health and Safety, Chapter 74, Section 39-7407) that states:

"A MSWLF unit shall not be located: ...(ii)within seismic impact zones except as provided in 40 CFR §258.14;".

The United States Environmental Protection Agency (EPA) 40 CFR §258.14 defines a seismic impact zone as;

"...an area with a ten percent or greater probability that the maximum horizontal acceleration...will exceed 0.10g in 250 years."

The EPA requires that MSWLF units located within a seismic impact zone shall demonstrate that all landfill containment structures are designed to resist the maximum horizontal acceleration in lithified earth material for the site. Based on the United States Geological Survey (USGS) National Seismic Hazard Mapping application, the peak horizontal ground acceleration at the project site having a 10 percent probability of exceedance in any 250-year period is 0.12g, which exceeds the criteria above and therefore classifies or designates the site by rule definition to be within a seismic impact zone.

The results for the USGS National Seismic Hazard Mapping application were based on a risk category II, with the landfill as a moderate risk to human life determined based on the normal-day operations with human operators processing and covering the trash. The soil conditions were considered Site Class D for stiff soils with Standard penetration Resistance, N values, between 15 and 50.

Tetra Tech reviewed the most recent published USGS probabilistic earthquake hazard information for seismic events with a 10 percent probability of exceedance in a 250-year period (USGS 2008 NSHMP PSHA Interactive Deaggregation Web Application), as current state of practice warrants, to select a peak spectral horizontal acceleration (PSHA). Based on our review of the USGS probabilistic earthquake hazard information, including site specific deaggregation characteristics of the Maximum Credible Earthquake (MCE), including magnitude, distance, and probability, a PSHA of 0.23g was selected to represent the extreme seismic case.

Based on recommendations in the EPA's Seismic Design Guidance for Municipal Solid Waste Landfill Facilities (1995), the maximum horizontal acceleration was reduced by 50 percent to represent the average horizontal acceleration for the given slope. In this case, 50 percent of the maximum horizontal acceleration (0.23g) yields an average horizontal acceleration of 0.115g. An adjusted horizontal acceleration of 0.12g was applied for pseudo-static analysis of the modeled slope configurations. The above acceleration values were applied for pseudo-static analysis of the modeled slope configurations.

To model the proposed slope cuts an initial angle between 2.25H:1V to 2.75:H:1V was removed to the proposed base elevation and the factor of safety for slope stability was calculated. The slope angle was adjusted using iterations of the same process until a resulting factor of safety was established that was above the criteria of 1.5 for static, and 1.3 for pseudo-static. The proposed fill was then added into the cut section and iterations were used with varied slopes between 2.75H:1V and 3H:1V to achieve a long-term factor of safety as described.

#### 7.2 Material Strength Properties

Tetra Tech previously completed a slope stability evaluation that included static and seismic stability evaluations for Phases 2 through 4 of the Canyon County Landfill (October 7, 2015). Additionally, Tetra Tech reviewed the previous evaluations from Holladay Engineering Company for the Pickles Butte Sanitary Landfill, dated 1998.

For this stability evaluation, Tetra Tech incorporated the following information: 1) the soils strength data available from the previous analysis, 2) materials strength properties assigned based on the laboratory testing of the geotechnical samples collected in 2021 and correlated data from the SPT N-value (blow count) data collected during the geotechnical drilling and well installation.

As discussed in the laboratory testing section, Tetra Tech's senior geotechnical engineer specifically selected samples for testing in each boring to directly incorporate into the slope stability models at each cross-section location. An attempt was also made to provide duplicate or crossover testing to identify variations in strength parameters for similar soil types. Several different tests were also performed to obtain a range of soil strength properties for each soil type. **Tables 2** and **3** presents a detailed breakdown of some of the data utilized to analyze the cross sections.

Conservative (lower bound) shear strength values were used to evaluate slope stability for static and seismic conditions. The following **Tables 2** and **3** present the material values that were assumed for this analysis.

Material	ASTM Classification	Unit Weight (pcf)	Friction Angle (deg)	Cohesion (psf)
Waste Fill		75	28	300
Poorly-Graded Silty Sand	SP-SM	110	20	280
Poorly-Graded Silty Sand	SP-SM	110	27	123
Silt (B,C)	ML	110	19	37
Silt (D,E)	ML	110	0	908
Lean Clay	CL	130	14	2000
Lean Clay-Silty Clay	CL-ML	109	15	489
Clay (Hard)	CL	125	0	6211
Clay (Hard)	CL	125	10	7831
Silty Sand - B3	SP-SM	115	32	400
Silty SandB4	SP-SM	115	30	580
Sand B3	SP	110	36.2	0
Sand/Gravel Interbedded	GW	135	37	0
Clayey Gravel	GW	138	36	1

#### Table 2. Material Strength Properties - Soil

#### Table 3. Material Strength Properties - Rock

Generalized Hoek-Brown Material	UCS (ksf)	GSI	mi	Unit Weight (pcf)
Basalt	3,500	30	25	146
Claystone	7,000	10	4	135

### 7.3 Slope Stability Analyses

Slope stability and pseudo-static analyses were performed using the computer program Slide2 v.9.023, developed by Rocscience, Inc., to determine the factors of safety of critical slip surfaces using both circular and block failure searches and vertical slice limit equilibrium methods. Because the proposed expansion of the landfill would be unlined, the potential of a critical interface between the waste fill and the natural subgrade soil is low. Therefore, circular failure analyses were performed at the critical sections. A screening analysis for block failure was performed to verify the potential for failure along the waste-soil interface is low compared to circular failure through the waste fill.

The EPA recommends a minimum FS of 1.5 for static slope stability analysis and a FS of 1.3 for pseudo-static slope stability analysis, based on Table 2-4 of the EPA's Solid Waste Disposal Facility Criteria Technical Manual (1998). For temporary cut slopes, a minimum FS of 1.2 is typically considered acceptable. Tetra Tech did not analyze temporary slopes given that it is anticipated that most all of the cut slopes will be open for a minimum of 6 months to 1 year, which per geotechnical standard of practice, are considered permanent slopes for purposes of slope analyses. Higher values for the FS indicate that the design is less likely to fail.

The cross-sections were created in the areas with the highest proposed cut and fill slopes where the critical soil slope conditions were identified, and in the areas incorporating the existing landfill with the proposed additional cells. There are seven section profile views, A through G, shown on Figures 2D to 5D, and included in **Appendix D**. A summary of the slope stability analysis results are presented in **Table 4** below and the corresponding output plots are Figures 6D through 37D in **Appendix D**.

		Factor of Safety			
Section	Analyzed Slope Long term	Static Analysis, Circular Failure	Pseudo-Static Analysis, Circular Failure	Static Analysis, Block Failure	Pseudo-Static Analysis, Block Failure
А	3H:1V	2.3	1.53	2.85	2.02
A – Final Slope Configuration	2.75H:1V 3H:1V	1.73 1.94	1.28 1.40	- 2.21	- 1.68
В	2.27H:1V	2.43	1.88	2.52	2.00
С	2.85H:1V	1.85	1.35	2.16	1.63
D	2.87H:1V	1.93	1.37	3.11	2.33
E	2.27H:1V	1.96	1.51	-	-
E	1.87H:1V	1.66	1.34	1.77	1.45
F	3H:1V	1.38	0.99	-	-
F- 2 Tier	3H:1V on lower, and 4H:1V on upper	1.81	1.19	2.14	1.53
F	4H:1V	2.06	1.35	1.83	1.69
G	2.6H:1V	2.22	1.68	2.65	2.16

#### Table 4. Factors of Safety for Slope Stability Analyses

The analysis as represented above indicates FS values for the static determinate loading on the order of 1.38 to 2.43, and 1.83 to 3.11 for circular and block failure, respectively. The seismic FS values were on the order of 0.99 to 1.88, and 1.45 to 2.16 for circular and block failure, respectively. The silty soils within the proposed cut in Section F produced a FS below 1 for the seismic loading condition. The slope was modeled with 4H:1V slope cut and a FS of 1.35 was obtained which met the minimum requirements of 1.3. Various degrees of slope cuts were modeled in an iterative manner to define the most effective slope cut for the soil conditions. The final slope

configuration was modeled on Section A and was representative of the backfill method and slope for the remaining project area. An iterative process was used to define which slope complied with the required factor of safety criteria of 1.5 for static stability and 1.3 for pseudo-static stability.

#### 7.4 Pseudo-static

When the pseudo-static analysis indicates a factor of safety of equal to or less than 1.3, the containment structure is required to be evaluated utilizing at least two independent methods to estimate permanent seismic induced displacement of the refuse mass. The displacement analysis methods are typically used as a screening method to evaluate if the structure or slope under analysis is within the range of critical displacement. For design of municipal solid waste landfill facilities, a maximum displacement less than 0.5 to 1.2 inches (1 to 3 cm) is typically acceptable for design. Where the pseudo-static analysis indicated a factor of safety of equal to or less than 1.3, the containment structure was evaluated using the Newmark displacement analysis method to determine a range of seismic-induced deformation. There was one cross-section, Section F, where the pseudo-static analyses indicated a factor of safety below 1.3. Yield accelerations were performed using Slide2 and are provided in the **Table 5** below.

The Slide2 program calculates the Newmark displacement based on the program SLAMMER (2013), developed by the USGS. The Slide2 program allows the user to enter a seismic record directly (time and acceleration data) or choose from a database of available historical seismic records. For the seismic analysis, a historical earthquake record was selected based on comparison to the design seismic event stated above. The earthquake record selected was the Mammoth Lakes – 1 1980, CVK-090 record, with a magnitude of 6.1 and Peak Ground Acceleration (PGA) of 0.416g, and represents an average high magnitude earthquake in similar soil conditions.

The performance of landfills subjected to strong earthquake ground motions is an extremely complicated process for which all of the variables affecting the behavior are not yet fully understood or capable of being analyzed. The historical performance of landfills subjected to seismic events similar to the design earthquake generally indicates satisfactory performance for the landfills studied.

For Section F, a conceptual slope was evaluated based on the methods above. Two different slope angles were analyzed, 3H:1V (20.8- degrees) and 4H:1V (14-degrees) with the 0.12g peak ground acceleration and the section F geometry. A summary of the analyses results is presented in **Table 5** and the corresponding output plots (Figures 1E through 12E) are included in **Appendix E**.

	Static Analysis		Pseudo-static Analysis	
Slope 3H:1V	Circular Failure	Block Failure	Circular Failure	Block Failure
Factor of Safety	1.38	1.90	0.99	1.41
Yield Acceleration (%g)	-	-	-	0.12
Estimated Displacement (in)	-	-	-	3.19
Slope 4H:1V				
Factor of Safety	2.06	2.49	1.35	1.69
Yield Acceleration (%g)	-	-	-	0.23
Estimated Displacement (in)	-	-	-	0.25

#### Table 5. Section F Stability Analysis Results for Displacement

#### 7.5 Comprehensive Seismic Survey for Fault identification

Tetra Tech prepared a 3D Seismic Survey report dated February 21, 2022. The project site is located within the Western Snake River Plain (WSRP) fault system and a portion of an undifferentiated Quaternary aged northeastdipping WSRP normal fault is mapped within the project boundaries, extending northwest through the proposed expansion area. The mapped fault is labeled as a normal fault with an approximate slip rate of less than 0.2 mm/year. Proposed excavations within the fault areas are expected to extend up to 150 feet below ground surface, potentially intercepting this fault.

The report prepared by Tetra Tech presented the results from an active-source 3D seismic survey. The seismic survey was designed to image and delineate the suspected fault. Seismic imaging over the suspected fault area was attained by using 3D seismic velocity tomography and reflection processing. Seismic reflection is a reliable method for imaging faults when present and can help to orient the faults and subsurface structure. The 3D seismic tomography provides the information needed to accurately convert seismic reflection data in time to depth and elevation. The information gained from this survey was used to site the location of Boring B5 to aid in the evaluation of the fault.

The summary of the seismic investigation and report were as follows:

- 1) The USGS NW-striking NE-dipping WSRP normal fault that is mapped as extending into the project site from the northwest does not appear to displace ~100ka age sedimentary units.
- 2) From a probabilistic perspective there seems to be little possibility of significant shallow (< 200 feet) faulting within the project site southeast of the west edges of the mapped tip splay faults.
- 3) To best characterize the potential movement and absolute location of faulting would require geologic mapping during excavation of the future landfill cell. This area of the proposed landfill expansion would be constructed in >50 years in the future. When the area is excavated for cover material in the future before waste is placed in this area it is recommended that geologic mapping of the fault is conducted, with particular attention to identifying narrow fault zones with evidence of recent activity and areas of potential materials suitable to date the most recent age of fault activity to determine if any detected fault activity is recent (unlikely) or > 100 ka in age (most likely).

Tetra Tech's slope evaluation recommendations presented in **Section 7.3** are not affected or altered by the results of the results of the February Seismic Survey Report. We suggest that a geotechnical engineer observe the slope cuts in the future to determine the potential presence of a faulted area. Should a faulted area be identified, the geotechnical engineer should determine at that time whether further investigation or analysis is required for the specific cells in the suspect fault area.

#### 7.6 Conclusions and Recommendations

The material strength properties incorporated in the geotechnical analyses were based on lower bound shear strength values and are considered conservative estimates. The stability analyses performed are considered to be the worst-case slope configurations with conservative material strengths and resulted in the factors of safety and displacements indicated above.

Results of the geotechnical investigation and analyses indicate that the proposed excavation and design as shown on Figure 1D in **Appendix D** will meet the Factor of Safety requirements of the Idaho Administrative Rules for the Idaho Solid Waste Facilities Act for the Idaho DEQ's administration of MSWLF.

Multiple slope angles were considered for Tetra Tech's slope analyses, ranging from 2.5:1 to 4:1 depending on the soil and bedrock types at each location. Based on Tetra Tech's analysis and the required FS's, the following two slope angles are recommended for the preliminary landfill site grading plans:

3H:1V: for the majority of the site slopes

4H:1V: where silt is encountered (Section F)

The 4:1 slope was analyzed and recommended for Section F because silt was interbedded between poorly-graded sand and fine sand and created a weakened soil profile. In areas where a high concentration of silt is predominant during construction, a slope of 4H:1V is recommended for cut areas. For now, Section F is the only area identified as having a high concentration of silt.

If it can be confirmed that bedrock exists for the entire depth of cut during construction, a 2:1 slope may be utilized. However, if there are any soft silt or clay seams interbedded withing the bedrock layer at any location along the cut, a 3:1 slope must be used. If slope angles are proposed to be steepened to a 2:1 slope during construction, a licensed geotechnical engineer from Tetra Tech must observe and evaluate the slope prior to make the determination if the slopes can be steepened, otherwise the slope must remain at 3:1.

In general, the seismic displacement analyses indicate permanent seismic-induced displacements are within the tolerances of 6 to 12 inches (15 to 30 cm) that are typically considered acceptable for landfill design. The preliminary seismic evaluation presented above was performed in accordance with generally accepted standards of the geotechnical engineering profession.

Because it is anticipated that most all of the cut slopes will be exposed for a minimum of 6 months to 1 year, Tetra Tech analyzed all slopes as permanent, and did not consider reducing the factor of safety for temporary slopes.

Some states specify the maximum allowable steepness of landfill cut or fill slopes, sometimes also based on the height of the slopes. In Pennsylvania for example, the maximum allowable slope steepness is 3:1. Other states have varying specifications or slope steepness limits for short term or longer-term slope exposures. The requirements are based both on historical slope failure data and slope analysis data, along with added factors of safety. Therefore, states have somewhat calibrated requirements based on the soil types and rainfall. The 3:1 maximum slope steepness for Pennsylvania landfills matches that determined for this investigation.

## 8. CONTINUING SERVICES

Two additional elements of geotechnical engineering service are important to the successful completion of this project.

- Design Phase. During the design phase, it is essential to ensure that the intent of the recommendations is incorporated in design decisions related to the project and that changes in the design concept consider geotechnical aspects. If issues arise, Tetra Tech's geotechnical engineers should be consulted for clarification and additional analysis on an as needed basis.
- 2) Observation and monitoring during construction. PBSL Operations should be trained to observe the types of materials encountered during the earthwork phases of the project, including the site grading and landfill cell excavations, to determine that the subsurface conditions are compatible with those used in the analysis and design. If conditions change, a geotechnical engineer should be consulted to evaluate the stability or potential impact on the design. During site grading, placement of fill should be observed and tested to confirm that the proper compaction has been achieved. PBSL should continue the annual aerial evaluation of the site and performance analysis to verify that the compaction remains consistent.

### 9. LIMITATIONS

The subsurface conditions and recommendations presented in this document are based on conditions encountered at the boring locations and based on the laboratory analysis. Due to the complexity and variability of natural earth and rock formations and materials, significant variations may occur between and around these locations or with time. Because these data represent a very small statistical sampling of subsurface conditions, it is possible that conditions may be encountered that are substantially different from those indicated. In these instances, modification and adjustment to the recommendations presented may be warranted.

This study has been conducted in accordance with generally accepted geotechnical engineering practices in the region where the work was conducted. The conclusions and recommendations submitted in this report are based upon project information collected and provided to Tetra Tech. The nature and extent of subsurface variations across the site may not become evident until construction. Tetra Tech should be on site during construction, to verify that actual subsurface conditions are consistent with those described herein.

This report has been prepared exclusively for the client. This report and the data included herein shall not be used by any third party without the express written consent of both the client and Tetra Tech. Tetra Tech is not responsible for technical interpretations by others. As the project evolves, Tetra Tech or another qualified geotechnical engineer should provide continued consultation and field services during construction to review and monitor the implementation of the recommendations and verify that the recommendations have been appropriately interpreted. Significant design changes may require additional analysis or modifications of the recommendations presented herein. On-site observation of excavations and foundation bearing strata and testing of fill should be performed by a representative of the geotechnical engineer.

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## **APPENDIX A: MISCELLANEOUS FIGURES AND DETAILS**

Important Information About Your Geotechnical Engineering Report (Published by ASFE)

Tetra Tech Boring Log Descriptive Terminology Key to Soil and Rock Symbols and Descriptive Terms

**Classification of Soils for Engineering Purposes** 

**Tetra Tech Exploratory Boring Locatsions – Figure 1040-1** 

# APPENDIX B: LOGS OF EXPLORATORY BORINGS

Figures 1-B through 16-B

## APPENDIX C: LABORATORY TESTING

Summary of Laboratory Results - Table 1-C Sieve Analysis Results Moisture Density Relationship Results Consolidation Tests Unconfined Compressive Strength Results Triaxial Tests

# APPENDIX D: SLOPE ANALYSIS

Figures 1D through 43D

## APPENDIX E: DEFORMATION ANALYSIS

Figures 1E through 12E

Static and Pseudo-Static Slope Stability Stability Analyses with Associated Circular and Block Failure Factor of Safety, Newmark Displacement, and Critical Acceleration for Slope 3H:1V Figures 1E through 6E

Static and Pseudo-Static Slope Stability Stability Analyses with Associated Circular and Block Failure Factor of Safety, Newmark Displacement, and Critical Acceleration for Slope 4H:1V Figures 7E through 12E

# APPENDIX F: PREVIOUS BORING LOGS

Logs GT-1 through GT-8

Logs PB-5 through PB-15

## **APPENDIX A: Miscellaneous Figures and Details**

Important Information about Your Geotechnical Engineering Report (Published by ASFE/GBA)

Tetra Tech Boring Log Descriptive Terminology Key to Soil and Rock Symbols and Terms

Classification of Soils for Engineering Purposes

Figure No. 2001-1 – Location of Exploratory Borings

## IMPORTANT INFORMATION ABOUT YOUR GEOTECHNICAL ENGINEERING REPORT

More construction problems are caused by site subsurface conditions than any other factor. As troublesome as subsurface problems can be, their frequency and extent have been lessened considerably in recent years, due in large measure to programs and publications of ASFE/The Association of Engineering Firms Practicing in the Geosciences.

The following suggestions and observations are offered to help you reduce the Geotechnical-related delays, cost-overruns and other costly headaches that can occur during a construction project.

#### A GEOTECHNICAL ENGINEERING REPORT IS BASED ON A UNIQUE SET OF PROJECT-SPECIFIC FACTORS

A Geotechnical engineering report is based on a subsurface exploration plan designed to incorporate a unique set of project-specific factors. These typically include: the general nature of the structure involved, its size and configuration; the location of the structure on the site and its orientation; physical concomitants such as access roads, parking lots, and underground utilities, and the level of additional risk which the client assumed by virtue of limitations imposed upon the exploratory program. To help avoid costly problems, consult the geotechnical engineer to determine how any factors which change subsequent to the date of the report may affect its recommendations.

Unless your consulting Geotechnical engineer indicates otherwise, your Geotechnical engineer report should not be used:

- When the nature of the proposed structure is changed, for example, if an office building will be erected instead of a parking garage, or if a refrigerated warehouse will be built instead of an unrefrigerated one;
- when the size or configuration of the proposed structure is altered;
- when the location or orientation of the proposed structure is modified:
- when there is a change of ownership, or
- for application to an adjacent site.

Geotechnical engineers cannot accept responsibility for problems which may develop if they are not consulted after factors considered in their reports' development have changed.

#### MOST GEOTECHNICAL "FINDINGS" ARE PROFESSIONAL ESTIMATES

Site exploration identifies actual subsurface conditions only at those points where samples are taken, when they are taken.

Data derived through sampling and subsequent laboratory testing are extrapolated by Geotechnical engineers who then render an opinion about overall subsurface conditions, their likely reaction to proposed conditions, their likely reaction to proposed construction activity, and appropriate foundation design. Even under optimal circumstances actual conditions may differ from those inferred to exist, because no Geotechnical engineer, no matter how qualified, and not exploration program, no matter subsurface how comprehensive, can reveal what is hidden by earth, rock and time. The actual interface between materials may be fare more gradual or abrupt than a report indicates. Actual conditions in areas not sampled may differ from predictions. Nothing can be done to prevent the unanticipated, but steps can be taken to help minimize their impact. For this reason, most experienced owners retain their Geotechnical consultants through the construction stage, to identify variances, conduct additional tests which may be needed, and to recommend solutions to problems encountered on site.

#### SUBSURFACE CONDITIONS CAN CHANGE

Subsurface conditions may be modified by constantlychanging natural forces. Because a Geotechnical engineering report is based on conditions which existed at the time of subsurface exploration, *construction decisions should not be based on a Geotechnical engineering report whose adequacy may have been affected by time*. Speak with the Geotechnical consultant to learn if additional tests are advisable before construction starts.

Construction operations at or adjacent to the site and natural events such as flood, earthquakes or groundwater fluctuations may also affect subsurface conditions and, thus, the continuing adequacy of a geotechnical report. The geotechnical engineer should be kept apprised of any such events, and should be consulted to determine if additional tests are necessary.

#### GEOTECHNICAL SERVICES ARE PERFORMED FOR SPECIFIC PURPOSES AND PERSONS

Geotechnical engineers' reports are prepared to meet the specific needs of specific individuals. A report prepared for a consulting civil engineer may not be adequate for a construction contractor, or even some other consulting civil engineer. Unless indicated otherwise, this report was prepared expressly for the client involved and expressly for purposes indicated by the client. Use by any other persons for any purpose, or by the client for a different purpose, may result in problems. *No individual other than the client should apply this report for its intended purpose without first conferring with the* 

geotechnical engineer. No person should apply this report for any purpose other than that originally contemplated without first conferring with the geotechnical engineer.

#### A GEOTECHNICAL ENGINEERING REPORT IS SUBJECT TO MISINTERPRETATION

Costly problems can occur when other design professionals develop their plants based on misinterpretations of a geotechnical engineering report. To help avoid these problems, the geotechnical engineer should be retained to work with other appropriate design professionals to explain relevant geotechnical findings and to review the adequacy of their plans and specifications relative to geotechnical issues.

#### BORING LOGS SHOULD NOT BE SEPARATED FROM THE ENGINEERING REPORT

Final boring logs are developed by geotechnical engineers based upon their interpretation of field logs (assembled by site personnel) and laboratory evalution of field samples. Only final boring logs customarily are included in geotechnical engineering reports. *These logs should not under any circumstances be redrawn* for inclusion in architectural or other design drawings, because drafters may commit errors or omissions in the transfer process. Although photographic reproduction eliminates this problem, it does nothing to minimize the possibility of contractors misinterpreting the logs during bid preparation. When this occurs, delays, disputes and unanticipated costs are the all-too-frequent result.

To minimize the likelihood of boring log misinterpretation, give contractors ready access to the complete geotechnical engineering report prepared or authorized for their use. Those who do not provide such access may proceed under the *mistaken* impression that simply disclaiming responsibility for the accuracy of subsurface information always insulates them from attendant liability. Providing the best available information to contractors helps prevent costly construction problems and the adversarial attitudes which aggravate them to disproportionate scale.

#### READ RESPONSIBILITY CLAUSES CLOSELY

Because geotechnical engineering is based extensively on judgment and opinion, it is far less exact than other design disciplines. This situation has resulted in wholly unwarranted claims being lodged against geotechnical consultants. To help prevent this problem, geotechnical engineers have developed model clauses for use in written transmittals. These are not exculpatory clauses designed to foist geotechnical engineers' liabilities onto someone else. Rather, they are definitive clauses which identify where geotechnical engineers' responsibilities begin and end. Their use helps all parties involved recognize their individual responsibilities and take appropriate action. Some of these definitive clauses are likely to appear in your geotechnical engineering report, and you are encouraged to read them closely. your geotechnical engineer will be pleased to give full and frank answers to your questions.

#### OTHER STEPS YOU CAN TAKE TO REDUCE RISK

Your consulting geotechnical engineer will be pleased to discuss other techniques which can be employed to mitigate risk. In addition, ASFE as developed a variety of materials which may be beneficial. Contact ASFE for a complimentary copy of its publications directory.

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# Tetra Tech Boring Log Descriptive Terminology Key to Soil Symbols and Terms

## SOIL CLASSIFICATION CHART

MAJOR DIVISIONS		SYMBOLS		TYPICAL	
IVI			GRAPH	LETTER	DESCRIPTIONS
	GRAVEL	CLEAN GRAVELS		GW	Well-graded gravels, gravel sand mix- tures, little or no fines.
	AND GRAVELLY SOILS	(LITTLE OR NO FINES)		GP	Poorly graded gravels, gravel-sand mix- tures, little or no fines.
COARSE GRAINED SOILS	MORE THAN 50% OF COARSE	GRAVELS WITH FINES		GM	Silty gravels, gravel-sand-silt mixtures.
00120	FRACTION RETAINED ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		GC	Clayey gravels, gravel-sand-clay mixtures.
	SAND	CLEAN SANDS		SW	Well-graded sands, gravelly sands, little or no fines.
MORE THAN 50% OF MATERIAL IS LARGER THAN NO. 200 SIEVE SIZE	AND SANDY SOILS	(LITTLE OR NO FINES)		SP	Poorly graded sands, gravelly sands, little or no fines.
	MORE THAN 50% OF COARSE	SANDS WITH FINES		SM	Silty sands, sand-silt mixtures.
	FRACTION PASSING ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		SC	Clayey sands, sand-clay mixures.
				ML	Inorganic sits and very fine sands, rock flour, sity or clayey fine sands or clayey sits with slight plasticity.
FINE GRAINED	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.
SOILS	CLATS			OL	Organic sits and organic sity clays of low plasticity.
MORE THAN 50% OF MATERIAL IS				ΜН	Inorganic sits, micaceous or diatomaceous fine sandy or sity soils, elastic sitts.
SMALLER THAN NO. 200 SIEVE SIZE	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		СН	Inorganic clays of high plasticity, fat clays.
				ОН	Organic clays of medium to high plasticity, organic silts.
HIC	GHLY ORGANIC S	OILS	**************************************	PT	Peat and other highly organic soils.

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS

Notes

#### See Soil Boring Information Special Provision.

SPT (Standard Penetration Test-ASTM D1586): The number of blows of a 140 lb (63.6 kg) hammer falling 2.5 ft (750 mm) used to drive a 2 in (50 mm) O.D. Split Spoon sampler for a total of 1.5 ft (0.45 m) of penetration.

. Written as follows:

first 0.5 ft (0.15 m) - second 0.5 ft (0.15 m) - third 0.5 ft (0.15 m) (ex: 1-3-9)

Note: if the number of blows exceeds 50 before 0.5 ft (0.15 m) of penetration is achieved, the actual penetration rounded to the nearest 0.1 ft (0.03 m) follows the number of blows in parentheses (ex: 12-24-50 (0.09 m),

34-50 (0.4 ft), or 100 (0.3 ft)).WR denotes a zero blow count with the weight of the rods only.

WH denotes a zero blow count with the weight of the rods plus the weight of the hammer.

MC=Moisture Content, LL=Liquid limit, PL=Plastic Limit -200%=percent soil passing 200 sieve, DD=Dry Density

Soil Classifications are Based on the Unified Soil Classification System, ASTM D2487 and D2488. Also included are the AASHTO group classifications (M145). Descriptions are based on visual observation, except where they have been modified to reflect results of laboratory tests as deemed appropriate. Order of Descriptors

12/06/12

**TETRA TECH** 

- Group Name
- Consistency or Relative Density
- Moisture Condition - Color

ł

Dry Moist

Wet

- Particle size descriptor(s) (coarse grained soils only)
- Angularity of coarse grained soils
- Other relevant notes

### Criteria For Descriptors

Consistency of Fine Gra	ainea Solis
Consistency	N-Value (uncorrected)
Very Soft	< 2
Soft	2 <del>-</del> 4
Medium Stiff	5 - 8
Stiff	9 - 15
Very Stiff	16 - 30
Hard	> 30
Apparent Density of Coarse	Grained Soils
Relative Density	N-Value (uncorrected)
Very Loose	< 4
Loose	4 - 10

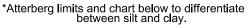
	• –
Loose	4 - 10
Medium Dense	11 - 30
Dense	31 - 50
Very Dense	> 50

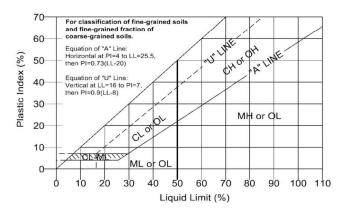
#### Moisture Condition

-Absence of moisture, dusty, dry to the touch. -Damp, but no visible water. -Visible free water.

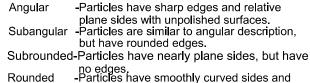
#### Definition of Particle Size Ranges Soil Component Size Range

Boulder	
Cobble	3 in (75 mm) - 12 in (300 mm)
Gravel	No. 4 Sieve (4.75 mm) to`3 in (75 mm)
Sand	No. 200 (0.075 mm) to No. 4 Sieves (4.75 mm)
Silt	No. 200 Sieve (0.075 mm)*
Clay	< No. 200 Sieve (0.075 mm)*
	, , , , , , , , , , , , , , , , , , ,





#### Angularity of Coarse-Grained Particles



well-rounded corners and edges.

Example soil description: Sandy FAT CLAY (CH), soft, wet, brown. (A-7) Page 1 of 2

# Tetra Tech Boring Log Descriptive Terminology Key to Rock Symbols and Terms

					I
Rock Type	Symbol	Rock Type	Symbol	Rock Type	Symbol
Argillite		Dolomite		Quartzite	
Basalt		Gneiss		Rhyolite	
Bedrock (other)		Granitic		Sandstone	
Breccia		Limestone		Schist	
Claystone		Siltstone		Shale	
		Conglomerate			

12/06/12 **TETRA TECH** 

#### Order of Descriptors

- Rock Type
- Color

С F

- Grain size (if applicable)
- Stratification/Foliation (as applicable)
- Field Hardness
- Other relevant notes

#### Criteria For Descriptors Grain Size

Description	Characteristic
oarse Grained	-Individual grains can be easily
	distinguished by eye
Fine Grained	-Individual grains can be dis-
	tinguished with difficulty

#### Stratum Thickness

Thickly Bedded	3-10 ft (1-3 m)
Medium Bedded	1-3 ft (300 mm - 1 m)
Thinly Bedded	2-12 in (50-300 mm)
Very Thinly Bedded	< 2 in (50 mm)

#### Rock Field Hardness

Very Soft Soft

Medium

Hard Very Hard -Can be carved with knife. Can be excavated readily with point of rock hammer. Can be scratched readily by fingernail. -Can be grooved or gouged readily by knife or point of rock hammer. Can be excavated in fragments from chips to several inches in size by moderate blows of the point of a rock hammer.

-Can be grooved or gouged 0.05 in (2 mm) deep by firm pressure of knife or rock hammer point. Can be excavated in small chips to pieces about 1 in (25 mm) maximum size by hard blows of the point of a rock hammer. -Can be scratched with knife or pick. Gouges or grooves to 0.25 in (6 mm) can be excavated by hard blow of rock Moderately hard hammer. Hand specimen can be detached by moderate blows.

-Can be scratched with knlfe or pick only with difficulty. Hard hammer blows required to detach hand specimen.

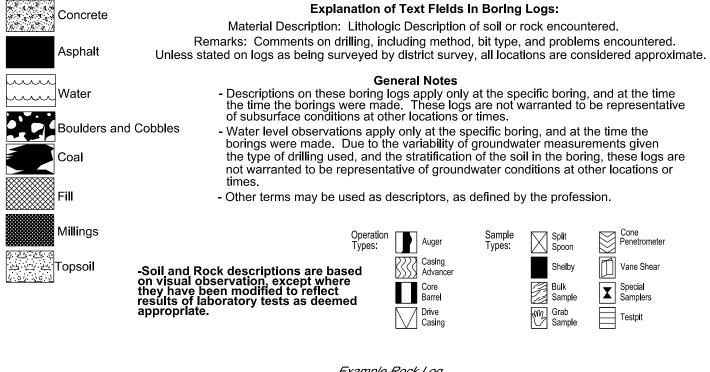
Cannot be scratched with knife or sharp rock hammer point. Breaking of hand specimens requires several hard blows of a rock hammer.

Notes:

UCS = Unconfined Compressive Strength obtained from laboratory testing at the given depth.

See Soil Boring Information Special Provision.

# Miscellaneous Soil/Rock Symbols and Terms



Example Rock Log SANDSTONE, gray, fine grained, thickly bedded, hard field hardness.



#### **CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES**

ASTM Designation: D 2487 – 83 (Based on Unified Soil Classification System)

	MAJ	OR DIVISIONS		GROUP SYMBOL	GROUP NAME
	Gravels	Clean Gravels	$Cu \ge 4 \text{ and } 1 \le Cc \le 3^{E}$	GW	Well graded gravel <sup>F</sup>
Coarse-Grained Soils More than 50% retained on No. 200	More than 50% coarse	Less than 5% fines	Cu < 4 and/or 1 > Cc > 3 <sup>E</sup>	GP	Poorly graded gravel <sup>F</sup>
	fraction retained on	Gravels with	Fines classify as ML or MH	GM	Silty gravel <sup>FGH</sup>
	No. 4 sieve	Fines More than 12% fines	Fines classify as CL or CH	GC	Clayey gravel <sup>FGH</sup>
sieve	Sands	Clean Sands	$Cu \ge 6 \text{ and } 1 \le Cc \le 3^{E}$	SW	Well-graded sand <sup>1</sup>
	50% or more of coarse	Less than 5% fines	Cu < 6 and/or 1 > Cc > 3 <sup>E</sup>	SP	Poorly graded sand <sup>1</sup>
	faction passes No. 4	Sands with Fines	Fines classify as ML or MH	SM	Silty Sand GHI
	sieve	More than 12% fines	Fines classify as CL or CH	SC	Clayey sand GHI
Fine-Grained Soils 50% or more passes the No. 200 sieve		Inorganic	PI > 7 and plots on or above "A" line	CL	Lean clay KLM
	Silts and Clays Liquid limit less	morganio	PI < 4 or plots below "A" line	ML	Silt <sup>KLM</sup>
	than 50	Organic	Liquid limit – oven dried Liquid limit – not dried <0.75	OL	Organic clay <sup>KLMN</sup> Organic silt <sup>KLMO</sup>
		Inorganic	PI plots on or above "A" line	СН	Fat clay <sup>K⊥M</sup>
	Silts and Clays Liquid limit 50 or	morganie	PI plots below "A" line	МН	Elastic silt KLM
	more	Organic	Liquid limit – oven dried Liquid limit – not dried < 0.75	ОН	Organic clay <sup>KLMO</sup> Organic silt <sup>KLMO</sup>
Highly organic soils	Primarily organic	c matter, dark in co	olor, and organic odor	PT	Peat

<sup>A</sup> Based on the material passing the 3-in. (75-mm) sieve.

- <sup>B</sup> If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.
- <sup>c</sup> Gravels with 5 to 12% require dual symbols:

GW-GM well-graded gravel with silt GW-GC well-graded gravel with clay GP-GM poorly graded gravel with silt GP-GC poorly graded gravel with clay

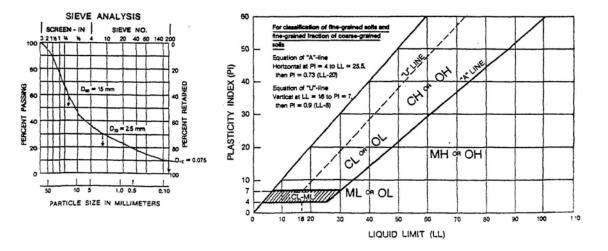
<sup>D</sup> Sands with 5 to 12% fines require dual symbols:

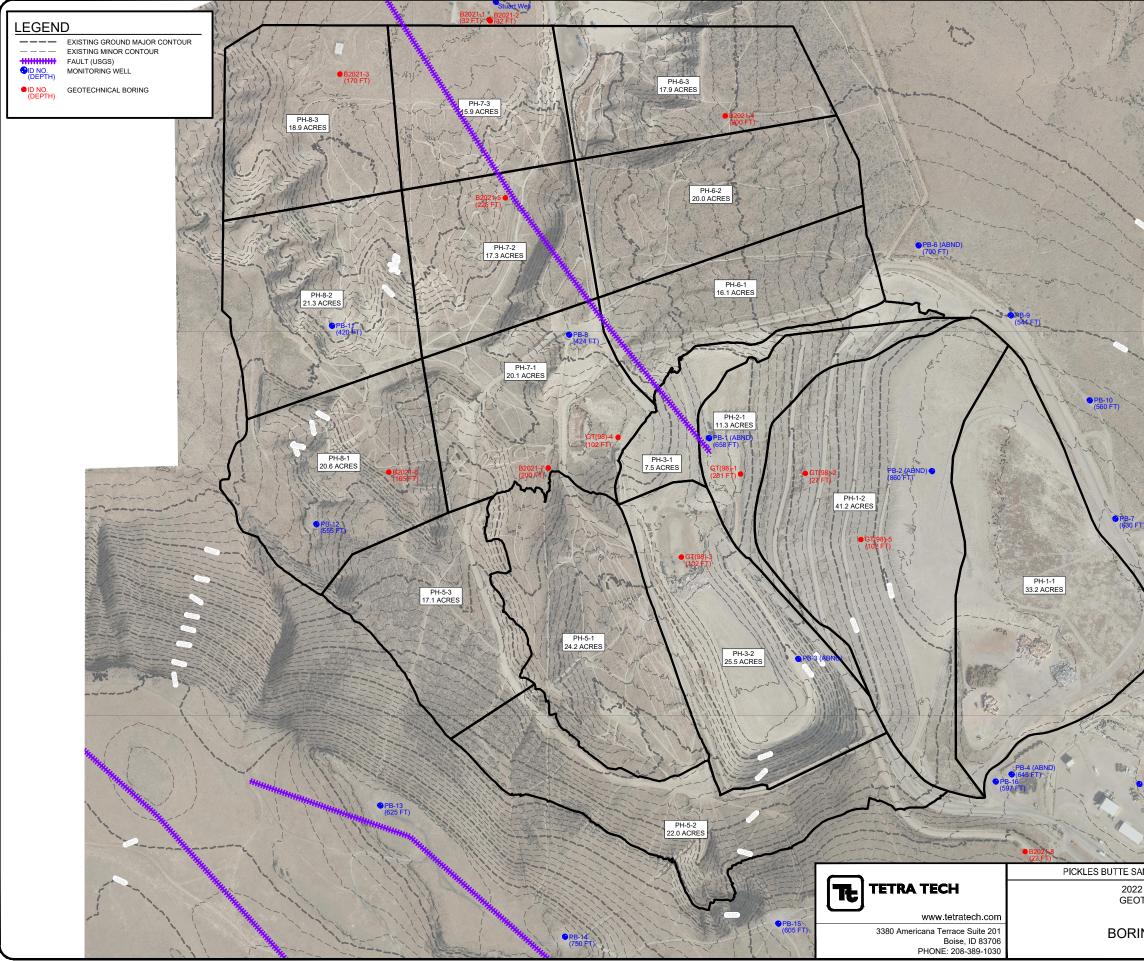
SW-SM well-graded sand with silt SW-SC well-graded sand with clay SP-SM poorly graded sand with silt SP-SC poorly graded sand with clay

- <sup>E</sup> Cu =  $D_{60}/D_{10}$  Cc= $(D_{30})^2$  /  $(D_{10} \times D_{90})$ <sup>F</sup> If soil contains ≥15% sand, add "with
- sand" to group name.
- <sup>G</sup> If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.
- <sup>H</sup> If fines are organic, add "with organic fines" to group name.
- If soil contains ≥15% gravel, add "with gravel" to group name.
- If soil contains  $\geq$  15% gravel, add "with gravel" to group name.

<sup>J</sup> If Atterberg limits plot in hatched area, soil is a CL-ML, silty clay.

- <sup>K</sup>. If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel", whichever is predominant.
- <sup>L</sup> If solid contains ≥ 30% plus No. 200, predominantly sand, add "sandy" to group name.
- <sup>M</sup> If soil contains ≥ 30% plus No. 200, predominantly gravel, add "gravelly" to group name.
- <sup>N</sup> PI  $\geq$  4 and plots on or above "A" line.
- <sup>o</sup> PI < 4 or plots below "A: line.
- <sup>P</sup> PI plots on or above "A: line.
- <sup>Q</sup> PI plots below "A: line.





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NITARY LANDFILL, CANYON COUNT	Y, IDAHO	Project No.: 114-571040-2022
2 CONCEPTUAL EXPANSION TECHNICAL INVESTIGATION		Project No.:         114-571040-2022         Particular           Date:         7/29/2022         Particular           Designed By:         SEF/MAM         Particular           Figure         10/10-1         Particular
IECHNICAL INVESTIGATION		Designed By: SEF/MAM
		Figure
NG LOCATIONS PLAN		1040-1 <sup>3</sup>
	L	Bar Measures 1 inch

# APPENDIX B: Logs of Exploratory Borings

Figures 1 through 8

#### Figure No. 1 LOG OF BORING \_ . \_ \_ . . .



Fax:								Boring B	B2021-1								Sheet 1 of 1
Projec					e Sanitary Lar	ndfill	-	Rig: TS150 Crawler	Boring Locatio								
Projec				Jou	inty, ID			Hammer: Auto Boring Diameter:	Coordinates System: Decir		-116.6		204			-	
Project Number: 114-571040-2022						6 in	Datum: NAD		1001000						o of Boring vation: 2740.4 ft		
Date Started: Date Finished:					Date Finishe	Drilling Fluid:	Abandonment		nod:								
11/15/2		<b>.</b>			11/15/21	<b>u</b> .		None	Grout								
Driller: Holt Services								Location: Refer to	site map.								
Logge	r:M	att /	Adaı	ns					•								
Depth (ft) <i>Elev.</i> (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology		Material Description			Depth (ft) <i>Elev.</i> (ft)	MC (%)	F	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
(-9		o ر	ц		_	. N 1., ·		DCOIL maint tan/k			0.3	2	-	-	<u> </u>		
		X	100		3-3-4			OPSOIL, moist, tan/b orly-Graded SAND v		/	2740.1						
			100		2-3-3		loc	ose, moist, brown to edium grained, subar	gray, fine to	,,		9	NV	NP	12	110	
5 2735.4			100		2-3-5		Po	orly-Graded SAND (			5.3						
		X	100		3-6-9	***** ***** *****	me	edium dense, moist, edium grained, subar	gray to tan,	ar.	2735.1	8					
201 – – R 10 –		X	100		9-13-13												
2730.4		X	100		8 - 11 - 13			ty SAND (SM), medi		st,	11.2 2729.2	6					
							pla	ay to tan, fine grained asticity, Pockets of cl	ay.		14.1						
5 2735.4         		X	100		10 - 13 - 15	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	de me	orly-Graded SAND ( nse, slightly moist, g edium grained, subar edium plasticity, Sma ly.	gray, fine to ngular to angula		2726.3	5					
 _ 20 2720.4 		X	100		10 - 12 - 13												
20 2720.4   25 2715.4          -			100				de	orly-Graded SAND v nse to very dense, s ay, fine to medium gr	lightly moist,	),	24.1 2716.3		NV	NP	6	113	Cc= 0.03
  _ 30 _			100		13 - 21 - 23												
2710.4			100		13 - 25 - 34		R	oring Depth: 31.5 ft,	Flevation: 270	8 0	<u>31.5</u> 2708.9						
								ft		5.5	2108.9						
<u> </u>										1							
		Wate	ər L	evel	Observations		l <u> </u>	ring illing: Not Encountered		Rem	arks:						
After	<b>g:</b> No	t Rec	corde	ł				ter illina: Not Recorded									

# Figure No. 2 LOG OF BORING



Elev. (ft)Image: Color of the second secon	<b>ng</b> 2739.0 ft									
Project Number: 114-571040-2022       Boring Diameter: 6 in       System: Decimal Degrees Datum: NAD83       Top of Bori Elevation:         Date Started: 11/16/21       Date Finished: 11/16/21       Date Finished: 11/16/21       Drilling Fluid: None       Abandonment Method: Grout         Driller: Holt Services Logger: Matt Adams       Location: Refer to site map.       Cocation: Refer to site map.         Depth (ft)       in transform       in transform       in transform         Difference       in transform       in transform       in transform         Difference       i	<b>ng</b> 2739.0 ft									
114-571040-2022     6 in     Datum: NAD83     Elevation:       Date Started:     Date Finished:     Drilling Fluid:     Abandonment Method:       11/16/21     11/16/21     11/16/21     Integration     Grout       Driller:     Holt Services     Location: Refer to site map.       Logger: Matt Adams     Material Description     Depth (ft)     Depth (ft)     Group       Depth (ft)     Image: Site Services     Site Services     Site Services     Site Services       Location: Refer to site map.     Image: Site Services     Site Services     Site Services       Image: Site Service	ng 2739.0 ft									
Date Started: 11/16/21       Date Finished: 11/16/21       Drilling Fluid: None       Abandonment Method: Grout         Driller: Holt Services Logger: Matt Adams       Location: Refer to site map.         Depth (ft)       gt       (%) (%)       (%) (%)       (%) (%)       (%) (%)       (%) (%)       (%) </td <td>2739.0 II</td>	2739.0 II									
Date Stated.     Date Finished.     Drining Find.     Grout       11/16/21     11/16/21     None     Grout       Driller: Holt Services     Location: Refer to site map.       Logger: Matt Adams     Material Description     Depth (ft)     Depth (ft)       Image: State of the sta										
Depth (ft)     use (ft)     use										
Logger: Matt Adams         Depth (ft)       wo free										
Depth (ft)       used (ft)       used (ft) <thuteu (ft)       used (ft)       <thutueu (ft)</thutueu </thuteu 										
100       2-1-3       Silty SAND (SM), very loose, slightly moist, brown to tan, fine grained, subangular to angular.       7         100       2-1-1       Poorly-Graded SAND with silt (SP-SM), very loose to very dense, slightly moist to moist, brown to gray, fine to medium       2.3										
100       2-1-3       Silty SAND (SM), very loose, slightly moist, brown to tan, fine grained, subangular to angular.       7         100       2-1-1       Poorly-Graded SAND with silt (SP-SM), very loose to very dense, slightly moist to moist, brown to gray, fine to medium       2.3	emarks									
100       2-1-3       Silty SAND (SM), very loose, slightly moist, brown to tan, fine grained, subangular to angular.       7         100       2-1-1       Poorly-Graded SAND with silt (SP-SM), very loose to very dense, slightly moist to moist, brown to gray, fine to medium       2.3	and									
100       2-1-3       Silty SAND (SM), very loose, slightly moist, brown to tan, fine grained, subangular to angular.       7         100       2-1-1       Poorly-Graded SAND with silt (SP-SM), very loose to very dense, slightly moist to moist, brown to gray, fine to medium       2.3	er Tests									
100     2-1-3     moist, brown to tan, fine grained, subangular to angular.     2.3       100     2-1-1     Poorly-Graded SAND with silt (SP-SM), very loose to very dense, slightly moist to moist, brown to gray, fine to medium     2.3										
100     2-1-1     Poorly-Graded SAND with silt (SP-SM), very loose to very dense, slightly moist to moist, brown to gray, fine to medium     2.3 2736.7										
2-1-1 Poorly-Graded SAND with silt (SP-SM), 2736.7 very loose to very dense, slightly moist to moist, brown to gray, fine to medium										
$ \rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$										
5     100     3-3-4     grained, angular to subangular.     3       100     2-4-6     3       100     7-10-14     3										
2734.0 2-4-6 3 100 7-10-14 3										
100     2-4-6       100     7-10-14										
$\begin{bmatrix} 2709.0 \\ 5 \end{bmatrix}$ 100 15-25-34										
المنظل المنظل المنظلة ا المنظلة المنظلة ا										
ft	Boring Depth: 31.5 ft, <i>Elevation:</i> 2707.5 2707.5 <i>ft</i>									
$ \frac{2}{2719.0} $ $ \frac{2}{2714.0} $ $ \frac{2}{2714.0} $ $ \frac{2}{2709.0} $ $ \frac{100}{15-25-34} $ $ \frac{11-16-21}{ft} $ $ \frac{31.5}{777.5} $ $ \frac{100}{ft} $ $ \frac{11-16-21}{ft} $ $ \frac{31.5}{777.5} $ $ \frac{11-16-21}{ft} $ $ \frac$										
After     After       Drilling: Not Recorded     Drilling: Not Recorded										



Fax:								Boring B	32021-3								Sheet 1 of 4
Project					e Sanitary La	ndfill -		Rig: TS150 Crawler	Boring Locati	on N:	43.500	)87	4				
				Οοι	inty, ID			Hammer: Auto	Coordinates	E:	-116.7	167	768				
Project								Boring Diameter:	System: Deci	imal D	egrees	;				Тор	o of Boring
114-57	104	10-2	022					6 in	Datum: NAD	83						Ele	vation: 2737.7 ft
Date S	tart	ed:			Date Finishe	d:		Drilling Fluid:	Abandonmen	t Met	hod:						
11/16/2					11/22/21			None	Grout								
Driller:		olt S	Serv	ices				Location: Refer to	site man								
Logge					-				Site map.								
								•				Ì					
Depth	_	8	Recovery (%)		Ę	≥					Depth						
(ft)	tio	Ę.	ery	18	Co			Material Des	cription		(ft)	1			(%	(bcf)	Remarks and
Elev.	Operation	Sample Type	No.	RQD (%)	Blow Count	Lithology		Material Des	cription		Elev.	0	F		-200 (%)	d 0	Other Tests
(ft)	0	S	Re	-	ā	-					(ft)	lĕ		립	Ŗ	B	
	$\overline{m}$	_				<u>N 17</u> . 3	Sli	ghtly moist, tan.			0.7	-					
	$\langle \rangle \rangle \langle \rangle$	Į						_T (ML), stiff, slightly	moist, light tar	/ 1.	2737.0						
	KK	{						v plasticity.		.,							
	\$\$\$\$	1															
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	KKK	arphi			2-0-1												
_ ]	5555	1									8.0						
		1				× × × ×		ty SAND (SM), loose			2729.7						
10 2727.7	KSSS-	$\leftarrow$	100		7-9-9			nse, slightly moist to nt tan, very fine grair									
	ß	КÅ	100		1-3-3		iigi	it tail, very line grail	icu.			1					
	<u>}</u> }}	}															
]	$\langle \rangle \rangle \langle \rangle$	{															
15 2722.7	KKK	$\leftarrow$			11 11 10	0 0 0 0 0 0											
	\$\$\$\$	ĮХ	100		11 - 11 - 12	00000 00000											
	KSSS-	{															
20	K	$ \vdash $				****** *****						3					
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	$\langle \rangle \rangle \langle \cdot \rangle$	ł															
		{															
_ 25 _	SSSS	<u> </u>											NIX /		~		Fristian Angles OF OC
2712.7	$\langle \rangle \rangle \langle \rangle$	17	80										NV	MP	29		Friction Angle= 25.86 degrees
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	\$\$\$\$	¥¥	100														Cc= 0.04
	$\rangle\rangle\rangle\rangle$																
2707.7	KK	łΧ	100		10 - 12 - 14							3					
	ß					000000 000000											
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_ 35 _	$\langle \rangle \rangle \langle \rangle$																
2702.7	KKK	$\bigtriangledown$	100		11 - 14 - 21	0.000 0.000											
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40	KKK	4				<u>0000000000000000000000000000000000000</u>											
2697.7	5555	$\square$	93		10 - 14 - 16						41.1						
		$\vdash$	1					T (ML), very stiff, sl	ightly moist, gr	ray, <sub>r</sub>	2696.6						
	<u>}</u>	{						v plasticity.			41.9						
45	KKK	1				0000	Sil	ty SAND (SM), medi	um dense to		2695.8						
2692.7	\$\$\$\$	$\bigtriangledown$	100		12 - 12 - 12			nse, slightly moist, t ained, subangular to		;							
. ]	$\langle \rangle \rangle \rangle$	$\vdash$					-	-	-		47.0						
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50	ß	1				°°°°°°°		v plasticity.			47.7 2690.0						
2687.7	5555	$\succ$	1			0000	Sil	ty SAND (SM), medi	um dense to		2090.0	3					
p		<u> </u>									·						·
		Wate	er L	.eve	Observations	'	∠ Du	ring Iling: Not Encountered		Rem	arks:						
After							Af	ter		1							
👱 Drilling	g:No	t Rec	corde	d		-	± Dr	illina: Not Recorded									



Sheet 2 of 4

Fax:							Boring	B2021-3								Sheet 2 of 4
Projec	t:P	ickl	es E	Butte	e Sanitary La	ndfill -	Rig: TS150 Crawle	er Boring Locati	on N:	43.50	)87	'4				
		-		Cou	inty, ID		Hammer: Auto	Coordinates		-116.7		768	}			
Projec							Boring Diameter:	System: Deci	mal D	egrees	;				Тор	o of Boring
114-57	7104	0-2	022				6 in	Datum: NAD							Ele	vation: 2737.7 ft
Date S	tart	ed:			Date Finishe	d:	Drilling Fluid:	Abandonmen	t Meth	nod:						
11/16/	21				11/22/21		None	Grout								
Driller		olt S	Servi	ices			Location: Refer to	site map								
Logge	r: M	att /	Ada	ms												
											T					
Depth	_	8	Recovery (%)		Ę	2				Depth						
(ft)	atio	Γ,	ery	(%) (	Ŝ		Material De	scription		(ft)	10			(%	(bcf)	Remarks and
Elev.	Operation	Sample Type	S	RQD	Blow Count	Lithology				Elev.	(%)		Ι.	-200 (%)	d d	Other Tests
(ft)	0	ଞ୍ଚି	Re	-						(ft)	R		2	Ŗ	8	
	m	$\geq$	100		4 - 18 - 19	00000 00000	dense, slightly moist,	tan to gray, fine		52.0	┝					
	RSSS						grained, subangular to		ſ	2685.7						
	ß						SILT (ML), very stiff, s									
55 2682.7	5555						to tan, low plasticity, I	lard consolidate	d							
	<u>}</u> }}						pieces. Poorly-Graded SAND	with all (CD)		56.2 2681.5						
z –	ß	1					medium dense to den		t	2001.5						
	<u>}}}}</u>						tan to gray, fine graine									
60 2677.7	KK		4.0-				angular.	-						19		Friction Angle= 20.21
	\$\$\$\$	14	100									ΝV	/NP	8	100	degrees
	$\langle \rangle \rangle \rangle$															Cohesion= 0.282 ksf UCS= 0.143 ksf
65	KK	1														
2672.7	6555	17-														
	$\geq >>>$															
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	£SSS:															
5 70 2667.7	$\sum$	$\vdash$	100		15 - 25 - 50											
	R	ho	100													
° 1 – –	SSSS															
- 75	$\sum$															
75 2662.7	RSSS															
	5555						Sandy SILT (ML), stiff	dry gray to re	d	76.5						
E	$\geq >>>$						fine grained, Broken s		u,	2661.2 78.5						
80	R					00000 00000	Silty SAND (SM), med			2659.2						
2657.7	<u>K</u>					<u>~~~~</u>	dense, slightly moist,	tan to gray, fine				Nν	NP	24		Friction Angle= 32.81
			75			0.0.0. 0.000	grained, subangular to			82.0						degrees Cohesion= 0.413 ksf
	KK	$ \times$	100		4 - 11 - 50		Poorly-Graded SAND	(SP), very dens	e,	2655.7	2					0.413 KSI
85	6555						dry, salt & pepper, fir grained, subangular to									
2652.7	<u>}</u> }}						granica, subanyular u	s angular.								
²	KK															
	\$\$\$\$															
90	<u>}}</u> }															
2647.7	KK	$\bigtriangledown$	100		23 - 40 - 50											
<u>-</u>	\$\$\$\$	$ \vdash$														
9. – –	₽>>>															
_ 95 _	KK	1								95.0						
2642.7	\$\$\$\$						Poorly-Graded SAND		1),	95.0 2642.7						
	$\langle \rangle \rangle \rangle$						very stiff, dry, tan, fin	e to medium								
	KK						grained, subangular, l	_arge amounts c	ot							
100	\$\$\$\$		_		E0/0 Cf		broken sandstone.			100.0						
2637.7	$\langle \rangle \rangle \rangle \langle \rangle \langle \rangle \langle \rangle \langle \rangle \rangle \langle $		0		50/0.2ft	00000 00000	Silty SAND (SM), very	/ dense, dry, gra	ay	2637.7						
	$\langle \rangle \rangle \langle \rangle$	1					to red, fine to coarse of	grained,								
5					<b>A A A</b>		7 During			- ul ( - )						
2637.7 2637.7		Wate	er L	.evel	Observations	<u>}</u>	- Drilling: Not Encountered		Rema	arks:						
	<b>g:</b> No	t Red	corde	d			After Drilling: Not Recorded									



Fax:		Boring	32021-3						Sheet 3 of 4
Project: Pickles Butt Canyon Cou Project Number:	e Sanitary Landfill - unty, ID	Hammer: Auto Boring Diameter:	System: Decimal D	: -116.7	167	4 '68		Тор	of Boring
114-571040-2022 Date Started: 11/16/21 Driller: Holt Service:	Date Finished: 11/22/21	6 in Drilling Fluid: None Location: Refer to	Datum: NAD83 Abandonment Met Grout	hod:				Elev	vation: 2737.7 ft
Logger: Matt Adams			site map.						
Debty (t) Recovery (%) RCD (%)	Blow Count Lithology	Material Des	cription	Depth (ft) <i>Elev.</i> (ft)	MC (%)	; F	РL -200 (%)	DD (pcf)	Remarks and Other Tests
105 2632.7 110 2627.7 110 2627.7 115	31 - 50/0.2/t	subangular, Mixed with siltstone.	large pieces of						
110 2627.7 2627.7 2622.7 2622.7 2617.7 2	47 - 50/0.3ft	Silty SAND (SM), very moist, salt & pepper to medium grained, subar Minimal pieces of sand with depth.	gray, fine to ngular to angular,	- 115.0 2622.7	4	NVR	IP 16	5 104	
130 2607.7 135 2602.7 2602.7 140 2597.7 140 140 140 140 140 140 140 140	14-33-50	Poorly-Graded SAND v very stiff, dry, tan, fine grained, subangular, La broken sandstone and Poorly-Graded SAND ( dry to moist, salt & per to medium grained, sub angular, Minimal pieces	to coarse arge amounts of siltstone. SP), very dense, oper to gray, fine bangular to	- 135.0 2602.7 138.6 2599.1					
145 2592.7 150 2587.7 100	16-33-50	Silty CLAY (CL-ML), ha gray, high plasticity.	ard, very moist,	- 146.5 2591.2					
Water Leve	l Observations	During	Rem	narks:					
⊈ After Drilling: Not Recorded		After Drilling: Not Recorded							



## Figure No. 3 LOG OF BORING



Phone: 406-543-30 Fax:	)45	Boring B				Sheet 4 of 4
	utte Sanitary Landfill			N: 43.500874		
Canyon C	ounty, ID	Hammer: Auto	Coordinates E	<u> </u>		
Project Number: 114-571040-2022		Boring Diameter: 6 in	System: Decimal	Degrees	Top of	f Boring
	Data Finiakask		Datum: NAD83 Abandonment Me	thod:	Elevat	ion: 2737.7 ft
Date Started: 11/16/21	Date Finished: 11/22/21	Drilling Fluid: None	Grout			
Driller: Holt Service		Location: Refer to	site man			
Logger: Matt Adam	IS		ono map.			
(tj) Peetation Sample Type Recovery (%)	RQD (%) Blow Count Lithology	Material Des	cription	Depth (ft) <i>Elev.</i> 00 ( <i>ft</i> ) JM	-200 (%) DD (pcf)	Remarks and Other Tests
155 2582.7 160 2577.7 160 160 2577.7 165 2572.7 165 165 165 170	16 - 24 - 36					
2567.7		Boring Depth: 170. 2567.7	0 ft, <i>Elevation:</i> 7 ft	2567.7		
	vel Observations	<b>⊈ During</b> <b>Drilling:</b> Not Encountered	Re	marks:		
After		After				
Drilling: Not Recorded		Drilling: Not Recorded				



Fax:			Boring B	32021-4							Sheet 1 of 4
Project: Pickles Bu		dfill -	Rig: TS150 Crawler		<b>n</b> N: 43.66	536	4				
Canyon Co	ounty, ID		Hammer: Auto	Coordinates	<u>E: -116.6</u>		388				
Project Number:			Boring Diameter:	System: Decim		5					of Boring
114-571040-2022	1		6 in	Datum: NAD8						Elev	ation: 2797.2 ft
Date Started:	Date Finished	:	Drilling Fluid:	Abandonment	Method:						
12/8/21	12/14/21		None	Grout							
Driller: Holt Service	es		Location: Refer to	site map.							
Logger: Matt Adam	S			-							
Debth     (ti)       Recovery (%)     Recovery (%)	Blow Count	Lithology	Material Des	cription	Depth (ft)				(%)	cf)	Remarks and
Elev. Operati (ft) (ft) (ft)	Blow			•	Elev. (ft)	MC (%)	Е	Ч	-200 (%)	DD (pcf)	Other Tests
5 2792.2 	2-9-7	Si Si	DPSOIL, moist, dark Ity SAND (SM), medi slightly moist, tan, fi ngular.	um dense, moist	0.7 2796.8	6					
10 2787.2 	5-9-7	4000 000 000 000 000 000 000 000									
15 2782.2	5 - 12 - 14		ILT (ML), very stiff, sl w plasticity.	ightly moist, tan	, 15.0 , 2782.2	2					
	18 - 37 - 48		lty SAND (SM), medi slightly moist, tan, fi		20.0 t 2777.2	5					
	16 - 35 - 48	m SI	lty CLAY (CL-ML), ve oist, tan, medium pla ILT (ML), very stiff, sl	asticity.	25.2 2772.0 27.7 , 2769.5						
30 2767.2 	16 - 27 - 33		w plasticity.								
35 2762.2 	15 - 30 - 34					8					
40 - 2757.2 100	11 - 23 - 18	to ar	Ity SAND (SM), medi slightly moist, tan, fi ngular to subangular.	ne grained,	40.0 2757.2 41.0 2756.2						
45 2752.2 50	9-13-13	m 🖌	Ity CLAY (CL-ML), ve oist, tan to black, me roken pieces of conso t.	dium plasticity,		16					
2747.2		<u> </u>	oorly-Graded SAND v	<u>vith silt (SP-SM)</u>	. 50.0		NV	NP	6		Friction Angle= 27.04
Water Lev	el Observations		uring rilling: Not Recorded		Remarks:						

## Figure No. 4 LOG OF BORING



Fax:							Boring	B2021-4							Sheet 2 of 4
Projec	ct: F	lickl	es E	Butte	e Sanitary La	andfill -		Boring Location	l: 43.66	536	4				
Droiod				Cou	inty, ID		Hammer: Auto		<u>: -116.6</u>		388				
<b>Projec</b> 114-5							Boring Diameter: 6 in	System: Decimal	Degrees	5				Тор	o of Boring
			022					Datum: NAD83 Abandonment Me	thod:					FIG	vation: 2797.2 ft
Date S		ed:			Date Finish	ed:	Drilling Fluid:	Grout	inou.						
12/8/2 Driller					12/14/21		None	-							
Logge					5		Location: Refer to	site map.							
Logge			luu							i					I
Depth (ft) <i>Elev.</i>	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Des	scription	Depth (ft) <i>Elev.</i>	(%)			-200 (%)	DD (pcf)	Remarks and Other Tests
(ft)	σ	S.	Rec	L.	B				(ft)	RC	F	2	Ŗ		
 - 55 - 2742.2			100		9-26-41		medium dense to very moist, tan to salt & pe medium grained, suba	pper, fine to	2747.2						degrees Cohesion= 0.123 ksf
60 2737.2 65 2732.2 70 70 770 770 772.2 772.2 7 775 7727.2 2722.2			80		2-5-18					2					
65 2732.2 															
70 727.2  75			67		6 - 13 - 23		Silty SAND (SM), med to slightly moist, tan, f	ine grained,	- 73.0 2724.2						
			80		2-7-23	ଽୢୄ୕୰ୄଡ଼ୄୢୄୢୄ୶ୄ୰୶ୄୢୄ୶୰ଡ଼ୄ୶ୄୢ୶ଡ଼ୄ୶୶ୄୢ୶ୄ୶ୄୢ୶ ଽୄୡୄ୰ୄଡ଼ୄ୰ଡ଼ୄୢଽ୶ୄ୰ଡ଼ୄୄଽ୶ୡୄୡୄୢୄ୵ଽୄ ଽୄୄୄୄୄ	angular to subangular.								
85 712.2  90 707.2			100		13 - 40 - 50	۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵۵	Poorly-Graded SAND to yellow, fine to mediu angular to subangular. Silty SAND (SM), hard	, moist, tan to	- 87.0 2710.2 90.0 2707.2		N∨	NP	38		Friction Angle= 22.83 degrees
 95 _ 2702.2						<mark>\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ </mark>	brown, fine grained, ar subangular, Broken pie consolidated clay.	ngular to eces of							Cohesion= 0.198 ksf
100 2697.2		įΧ	100		9 - 18 - 20	<u>~~~</u> ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~				22					
	15555														
		144.4			Ohan set		During	D	marke						
After		Wate	er L	evel	Observations	;	Drilling: Not Recorded		marks:						
	ng: No	ot Enc	ounte	ered			Drilling: Not Recorded					_			



Sheet 3 of 4

								Bonng	32021-4								Sheet 3 of 4
Projec					Sanitary La	ndfill -		Rig: TS150 Crawler		n N:	43.665	536	4				
				Cour	nty, ID			Hammer: Auto	Coordinates		-116.6		388				
Projec								Boring Diameter:	System: Decim		egrees						of Boring
114-57	7104	0-2	022					6 in	Datum: NAD8							Elev	vation: 2797.2 ft
Date S	tart	ed:			Date Finishe	ed:		Drilling Fluid:	Abandonment	Meth	od:						
12/8/2	1				12/14/21			None	Grout								
Driller								Location: Refer to	site map.								
Logge	er: M	att /	Adan	ns													
Depth (ft) <i>Elev.</i> (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology		Material Des	cription		Depth (ft) <i>Elev.</i> (ft)	MC (%)	LL	۲	-200 (%)	DD (pcf)	Remarks and Other Tests
(19	 	S	ц			0.0.0					(19	2	-	ш		-	
		× s	100		6-12-20		mo Sil bro	ndy SILT (ML), very pist, tan, low plasticit ty CLAY (CL-ML), ha pwn, medium plastici consolidated clay.	ty. ard, moist, tan to		104.0 2693.2 105.0 2692.2						
							Sa	ndy SILT (ML), very	stiff, slightly		117.5 2679.7						
THE	\$\$\$\$	m					mo	pist, tan, low plasticit	iy.		120.0						
Toto of Borling-MDT REVISED 2009+ 6DT - 712/122 09:44 - N/GEOTECHIREPORT 2022/NPCKTES BUTTE LANDFILLIAB LOGS/GP			100		31 - 70/0.4ft	<u></u>	de pe su	ty SAND (SM), medi nse, slightly moist, t pper, fine to medium bangular to angular.	an to salt & grained,		120.0		NV	NP	49		Friction Angle= 29.51 degrees Cohesion= 0.588 ksf
130 2667.12кке 2667.2 2667.2 26 267.2 2667.2 26 267.2 267.2 26 2662.2 26 2662.2 26 2662.2 26 2662.2 26 2662.2 26 2662.2 26 2662.2 26 2662.2 26 2662.2 26 2667.2 26 267.2 267.			100		9 - 21 - 26	\$ \$\$\$\$\$\$	ve fin	orly-Graded SAND ( ry dense, slightly mo e to medium grained bangular.	ist, salt & peppe	er,	2668.2						
			100		30 - 48 - 44		Sa	ndy SILT (ML), very	stiff, slightlv		145.0 2652.2	2					
150			111		31 - 50/0.4ft		m	ist, tan to brown, lo	w plasticity.								
ц U U		Wate	er Le	evel	Observations	7		ring		Rema	arks:						
After							Af	Iling: Not Recorded ter									
⊏ 💾 Drillin	<b>g:</b> No	t Enc	ounte	red		-	<u>₹</u> Dr	illing: Not Recorded									



Fax:								Boring B	32021-4								Sheet 4 of
Projec					e Sanitary La	ndfill -		Rig: TS150 Crawler	Boring Locati	on N:	43.665	536	4				
				Cou	nty, ID			Hammer: Auto	Coordinates	E:	-116.6	883	388				
Projec	t Nu	ımb	er:					Boring Diameter:	System: Deci	imal D	egrees					Тор	of Boring
114-57	7104	10-2	022					6 in	Datum: NAD	83							/ation: 2797.2 ft
Date S	tart	ed:			Date Finishe	d:		Drilling Fluid:	Abandonmen	t Meth	nod:						
12/8/2					12/14/21			None	Grout								
Driller:		olt S	Serv					Location: Refer to	aito mon								
Logge								Looution: Relei lo	site map.								
99-												-					
Depth		e	(%)		ŧ	>					Depth						
(ft)	Operation	Sample Type	N N	RQD (%)	Blow Count	Lithology		Material Dec			(ft)				ি	Ê	Remarks
Elev.	Dera	ble	No.	B	Ň	tho		Material Des	cription		Elev.	(%)			-200 (%)	(bcf)	and Other Tests
(ft)	ŏ	San	Recovery (%)	œ	Bic						(ft)	ы	F	2	Ŗ	B	
	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		_			+ +						<u> </u>					
155	\$\$\$\$	}									155.0						
2642.2	8333	4					Po	orly-Graded SAND (	SP), dense to		2642.2						
	KKK	<						ry dense, slightly mo		per, <sub>,</sub>	157.0						
· 4	\$\$\$\$	Kim						e to medium grained	, angular to		2640.2						
160	$\langle \rangle \rangle \rangle$	$\vdash$						bangular.		lr	159.0						
2637.2	K	$\bigtriangledown$	111		29 - 50/0.4ft			ndy SILT (ML), very			2638.2						
	ßsss	$\frown$	1					oist, tan to brown, lo orly-Graded SAND (									
	\$\$\$\$	1						orly-Graded SAND ( ry dense, slightly mo		ner							
·	$\rangle\rangle\rangle\rangle$	}						e to medium grained		per,							
_165 2632.2	RSSS	4						bangular.	, angular to								
2032.2	KKK	4						5									
· -	6555	1															
	$\langle \rangle \rangle \rangle$	}															
170	8	C.			50 50/0 01												
2627.2	KKK		88		50 - 50/0.3ft												
	\$\$\$\$	1															
	$\langle \rangle \rangle \rangle$	]															
175	2222	}									175.0						
2622.2	KKK	(m)	1				Sil	ty SAND (SM), very	stiff, dry, gray,	,	2622.2						
	\$\$\$\$	ſĽ				~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	fin	e grained, angular to	subangular.	_	177.0						
	$\langle \rangle \rangle \rangle$	}						orly-Graded SAND (			2620.2						
180	RSSS	m						ry dense, slightly mo		per,							
2617.2	K	$\vdash$						e to medium grained	, angular to								
	\$\$\$\$	1					su	bangular.									
. ]	$\langle \rangle \rangle \rangle$	Ì									183.0						
	KSSS	4						ty SAND (SM), very			2614.2						
185 2612.2	KK	1					gra	ay, fine grained, ang	ular to subangu	ılar.							
2012.2	6555	1															
·	$\langle \rangle \rangle \rangle$	}				° <u>°</u> °°°° °°°°°°											
	KSSS																
190	ß	( <sup>B</sup>				\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	_				190.0						
2607.2	\$\$\$\$	1						orly-Graded SAND v			2607.2						
	$\rangle\rangle\rangle$	}						edium dense to very bist, tan to salt & per									
· -	R	4						edium grained, subar		ar							
195	ßsss	1						alam grainea, easai	igular to arigun	ur.							
2602.2	\$\$\$\$	)															
	$\langle \rangle \rangle \rangle$	1															
	K	1															
200	6555	1									200.0						
2597.2		4		·l		1		Boring Depth: 200.			2597.2	•					
								2597.2									
	_																
		Wate	er L	.evel	Observations			ring Iling: Not Recorded		Rem	arks:						
	an Mir	+ E~ -		ored			Af	ter		1							
▲ Drilling	y: INC	n ⊏NC	JUUNI	erea		-	± Dr	illina: Not Recorded		1							



Fax:								Boring	B20	21-5								Sheet 1 of 5
Projec					e Sanitary La	ndfill	-	Rig: TS150 Crawle										
_ ·				Οοι	inty, ID			Hammer: Auto		ordinates		<u>: -116.7</u>		191				
Projec								Boring Diameter:	-	stem: Deci		egrees					Тор	o of Boring
114-57	104	0-2	022					6 in		tum: NAD							Ele	vation: 2661.6 ft
Date S	tarte	ed:			Date Finishe	d:		Drilling Fluid:		andonmen	nt Met	hod:						
12/14/2	21				12/19/21			None	-	out								
Driller	: Ho	olt S	Servi	ices	6			Location: Refer to	o site	map.								
Logge	r:M	att /	Ada	ms						-								
Denth			()		L .							Denth						
Depth (ft)	F	<u>Y</u> pe	V (9	(%)	uno	Lithology						Depth (ft)					~	Remarks
	Operation	le T	ver	RQD (	Ŭ	lolo		Material De	escrip	tion			%			%	pcf	and
Elev. (ft)	ð	Sample Type	Recovery (%)	8	Blow Count	Lit						Elev. (ft)	MC (%)	F	2	-200 (%)	DD (pcf)	Other Tests
(-9		S	Ŕ		_								2	_	-	'		
┢ −	8555							PSOIL, moist, bro		htly maint		0.7						
	$\langle \rangle \rangle \langle \rangle$							ndy SILT (ML), stiff n, fine grained, ang			ar							
 	KKK							i, into grantoa, ang		oodbarigar	ur.							
5 2656.6	\$\$\$\$	$\vdash$			0.0.5								4					
2000.0	$\langle \rangle \rangle \langle \rangle$	K	100		6-8-5								Ι.					
	KSSS																	
	\$\$\$\$	-000																
10 2651.6	<u>}</u> }}	K <sup>W</sup>			10 04 40			orly Gradad SAND		modium		10.0						
2001.0	KKK	K	100		12 - 21 - 43			orly-Graded SAND nse to very dense,			d.	2651.6						
	\$\$\$\$							e to medium graine			u,							
							su	bangular.	,	0								
15	KK	$\leftarrow$			5 7 40								3					
2646.6	6555	$\bowtie$	100		5-7-16								ľ					
	<u>}</u> }}																	
20	K	(M)																
2641.6	\$\$\$\$	$\boxtimes$	100		10 - 21 - 26													
	8555																	
	K																	
25 2636.6																		
2030.0	kkk											07.0						
	\$\$\$\$	3				ŴŴ	Sil	ty CLAY (CL-ML), r	mediu	um stiff, slig	ghtly	27.0 2634.6						
							m	oist, white to gray, l	high	plasticity.		29.0						
30 2631.6	KKK	$\leftarrow$	4.0-		10 27 40			orly-Graded SAND				2632.6						
2001.0	6555	ľХ	100		10 - 27 - 40			nse to very dense, pepper to red, fine t										
	<u>}}}}</u>							gular to subangular		aium grain	<del>c</del> u,							
	KK							Jana is casangalar	•									
35 _2626.6	\$\$\$\$	kz	100		10-22-35								4					
_020.0	8	$\bowtie$	100		10-22-30	ŇŇŇŇ						37.0	<sup>`</sup>					
	KKK	1						LT (ML), hard, sligh	ntly m	oist, tan to	)	2624.6						
- 40 -	\$\$\$\$	600					gra	ay, low plasticity.										
40 	8	K	150		27 - 33 - 45/0.0ft													
	KKK											42.0						
	SSSS:							orly-Graded SAND				2619.6						
	<u>}</u> }}							nse to very dense,				44.0						
45 2616.6	KKK	$\vdash$	100		23 - 39 - 42			pepper to red, fine t gular to subangular		aum grain	ed,	2617.6 45.0						
	\$\$\$\$	Ŕ	100		20100142	°°°°°°		LT (ML), hard, sligh		nist tan to		2616.6						
	$\langle \rangle \rangle \rangle$							ay, low plasticity.	iay 11	0.01, tan 10								
	KK	<000				<u>, , , , , , , , , , , , , , , , , , , </u>		ty SAND (SM), med	dium	dense to v	ery							
50 2611.6	6555					Ì		nse, slightly moist,				50.0		54	24			Friction Angle= 14.9
_0/1.0			I		1	<u>r////</u>	41					<u> </u>	L	<u> </u>	<u> </u>			
		Wate	ər L	eve	Observations			ring illing: Not Recorded			Ren	narks:						
After							🕳 Af	ter			1							
⊻ Drillin	g:No	t Enc	counte	ered			🖃 Dr	illina: Not Recorded										



Sheet 2 of 5

Fax:								Borir	ng E	32021-5								Sheet 2 of 5
Project					e Sanitary La	ndfill -	•	Rig: TS150 Crav	wler	Boring Locatio								
Project				Jou	nty, ID			Hammer: Auto Boring Diamete	·r·	Coordinates System: Decir		-116.7		191			-	
114-57								6 in		Datum: NAD		egrees					Top	of Boring vation: 2661.6 ft
Date St					Date Finishe	ed:		Drilling Fluid:		Abandonment		nod:						
12/14/2					12/19/21			None		Grout								
Driller:	Hol	t Se	ervi	ces				Location: Refe	r to	site map.								
Logger	:Ma	tt A	dar	ns														
Depth (ft) <i>Elev.</i> (ft)	Operation		Recovery (%)	RQD (%)	Blow Count	Lithology		Material	Des	cription		Depth (ft) Elev. (ft)	MC (%)	-	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
. ,	7777		ш 100		27 - 38 - 50		ara	ined, angular to	sub	angular		2611.6		_	_		_	degrees
SIREPORT 2022/PICKLES BUTTE LANDFILLILLA LOGSBORING LOGS GPU 26001 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			100		34 - 50/0.1ft 10 - 30 - 20		Sili tar Po de to sul Sili mc Po de to sul Po vei Va silt SII vh of Sili	y CLAY (CL-ML) i, high plasticity. orly-Graded SAN ise to very dense tan, fine to mediu bangular. by SAND (SM), m ist, tan, fine gra orly-Graded SAN ise to very dense tan, fine to mediu bangular. orly-Graded SAN orly-Graded SAN y dense, moist, rying amounts of y clay. T with sand (ML ite to gray, non p consolidated clay ty SAND (SM), v	), ha ND ( e, s um <u>g</u> nedi inec ND ( e, s UD ( gra f silt , ha blast y.	rd, slightly mois SP), medium ightly moist, gr grained, angular um stiff, slightly t. SP), medium ightly moist, gr grained, angular vith silt (SP-SM y, fine grained, . Thin viens of ard, slightly moi ic, Broken piec	ray r to / ray r to ]), ist, es	261.0 51.0 2607.6 55.0 2606.6 60.0 2601.6 65.5 2596.1 71.5 2590.1 73.5			'NP	• 77	112	Friction Angle= 19.09 degrees Cohesion= 0.037 ksf
			100		10 - 18 - 27	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	CL mc pie	, fine grained. AY with sand (Cl ist, white to gray ces of consolida ty SAND (SM), v ist, tan to red, fi	y, no ited	on plastic, Brok clay. dense, slightly		2588.1 86.0 2575.6		35	21	83	104	Friction Angle= 31.18 degrees Cohesion= 0.26 ksf
WDT REVISED 2009+.GDT - 7/27/22 09:4-6 071 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2581.6 2004 2581.6 2581.6 2581.6 2581.6 2004 2581.6 2571.6 2576.		1) 1)	100		49 - 50/0.3ft	হাৰ প্ৰত হৈ হ'ব প্ৰথম হ'ব হ'ব প্ৰথম হ'ব প্ৰত হ'ব		bangular.		Janeu, angula			11	NV	'NP	34		Friction Angle= 13.53 degrees Cohesion= 0.654 ksf
100 - 100 -	<u>}}}</u>	Źŀ	115	:	21 - 46 - 50/0.3ft													
BOR	1111												<u> </u>					
ЧО С	и	latei	r Le	evel	Observations	ŀ		ring			Rem	arks:						
							🕳 Afi	lling: Not Recorded er										
¦≓ <u>I Prilling</u>	: Not I	ncc	ounte	red		-	<u>-</u> ∎ Dri	llina: Not Recorded										



Sheet 3 of 5

Fax:			Boring B	32021-5						Sheet 3 of 5
Project: Pickles Butt	e Sanitary Lan	ndfill -	Rig: TS150 Crawler		N: 43.499	13	3			
Canyon Cou	unty, ID		Hammer: Auto		<u>E: -116.7</u>	134	91			
Project Number:			Boring Diameter:	System: Decimal	Degrees					of Boring
114-571040-2022	1		6 in	Datum: NAD83					Elev	vation: 2661.6 ft
Date Started:	Date Finished	d:	Drilling Fluid:	Abandonment Me	ethod:					
12/14/21	12/19/21		None	Grout						
Driller: Holt Service:	S		Location: Refer to	site map.						
Logger: Matt Adams										
Debth (t) Rample Type RQD (%)	Blow Count	Lithology	Material Des	cription	Depth (ft)	(%)		(%)	(pcf)	Remarks and
Elev. dd	Blow	Lith			Elev. (ft)	MC (°	리	0	DD (F	Other Tests
		m m	ilty CLAY (CL-ML), ve oist, gray to blue, hig roken pieces of conso	h plasticity,	102.0 2559.6					
110 2551.6 100 100 100 100 100 100 100 10	30 - 50/0.1ft	m su Si m	ilty SAND (SM), very oist, tan to red, fine g ubangular. ilty CLAY (CL-ML), ve oist, gray to blue, hig roken pieces of conso	grained, angular to ery stiff, slightly h plasticity,						
110       100         2551.6       100         100       100         110       100         110       100         110       100         110       100         110       100         110       100         110       100         12546.6       100         12541.6       100         12551.6       100         12551.6       100         12551.6       100         12551.6       100         12551.6       100         12551.6       100         12551.6       100	9 - 17 - 36	de gr Si gr	ilty SAND (SM), medi ense, slightly moist, g rained, angular to sub ilty CLAY (CL-ML), ha ray to blue, high plasti eces of consolidated	gray to brown, fine angular. ard, slightly moist, icity, Broken	116.5 2545.1					
13200.0 13200.0 13200.0 13200.0 13200.0 13200.0 13200.0 13200.0 13200.0 107 107 107 107 107 107 107 10	26 - 50 - 50/0.4ft	re V m Si gr i pi Si	andy SILT (ML), hard ed to brown, fine grain ery fine sand. Some c ixed. ilty CLAY (CL-ML), ha ay to blue, high plasti eces of consolidated ilty SAND (SM), very	ed, low plasticity, consolidated clay ard, slightly moist, icity, Broken clay. dense, slightly	126.0 2535.6 127.0 2534.6 129.5 2532.1 131.5 2530.1 134.5					
13-05 2526.6 2526.6 2526.6 140 2521.6 111 111 111 111 111 111 111	42 - 50/0.4ft 8 - 17 - 50/0.4ft	m sa Le Si gr pi Si ta si Si gr pi Si ta si Si Si Si Si Si Si Si Si Si Si Si Si Si	oist, tan, very fine gr and. Some consolidate ess clay with depth. iity CLAY (CL-ML), ha ay to blue, high plasti eces of consolidated andy SILT (ML), hard n, low plasticity, Som It. Seams of varying c iity CLAY (CL-ML), ha ay to blue, high plasti eces of consolidated andy SILT (ML), hard n, low plasticity, Som It. Seams of varying c iity CLAY (CL-ML), hard	ained, Very fine ed clay mixed. ard, slightly moist, icity, Broken clay. , slightly moist, e consolidated clay content. ard, slightly moist, icity, Broken clay. , slightly moist, e consolidated clay content. ard, slightly moist, ard, slightly moist,	140.0 2527.1 2527.1 2521.6 141.0 2520.6 143.0 2518.6 145.0 2516.6 147.0 2514.6					
К К К К К К К К К К К К К К К К К К К К		KAN gr	ray to blue, high plasti	icity, broken						
u 0 Water Leve	l Observations		uring	Re	marks:					
			rilling: Not Recorded							
Drilling: Not Encountered			Filling: Not Recorded							



Sheet 4 of 5

Fax:								32021-5								Sheet 4 of
Projec					e Sanitary La nty, ID	ndfill -	Rig: TS150 Crawler									
Projec				Jou	пцу, ID		Hammer: Auto Boring Diameter:	Coordinates System: Deci		-116.7		91			_	
114-57							6 in	-		egrees						of Boring ation: 2661.6 ft
			022		Dete Finish			Datum: NAD Abandonmen		nod:					Liev	alion: 2001.01
<b>Date S</b> 12/14/:		ea:			Date Finishe	ea:	Drilling Fluid:	Grout		loui						
Driller		olt S	ervi	ices	12/19/21		None Location: Refer to	oito mon								
Logge							Location. Relef to	site map.								
- 00-																
Depth (ft) <i>Elev.</i> (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Des	cription		Depth (ft) <i>Elev.</i> (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
155							pieces of consolidated Sandy SILT (ML), hard									
2506.6	<u>}</u> }}	}					tan, low plasticity, Som	e consolidated		156.0						
	<b>{</b> }}}}	1					silt. Seams of varying of	clay content.		2505.6 157.0						
· -	\$}}}	-000					Silty CLAY (CL-ML), ha gray to blue, high plast	ard, slightly mo icity, Broken	ist,	2504.6						
_160 2501.6	£\$\$\$\$		83		46 - 50/0.1ft		pieces of consolidated			160.0						
	<u>}</u> }}						Sandy SILT (ML), hard			2501.6						
	<u>}</u> }}	}					tan, low plasticity, Som silt. Seams of varying of			163.5						
165	<u> </u>	\$					Silty CLAY (CL-ML), ha	ard, slightly mo	ist,	2498.1						
2496.6	<u>}</u> }}	}					gray to blue, high plast		. I	164.5 2497.1						
-	<b>\$</b> \$\$\$	1					pieces of consolidated content than previous.	uay. nigher si		167.0 2494.6						
170	ß						CLAY (CL), hard, slight									
_170 2491.6	<b>{</b> }}}}	$\mathbb{K}$	100		9 - 17 - 50		blue, high plasticity, Broconsolidated clay.	oken pieces of	ł	170.0 2491.6						
· -	3333	$   \rightarrow $	100				Sandy SILT (ML), hard	, slightly moist,		2101.0						
	£\$\$\$						tan, low plasticity, Som									
175	3335	X					silt CLAY (CL), hard, slight	thy moist aray	to							
2486.6	<u>}</u> }}	}					blue, high plasticity, Br									
	<u>I</u> SSS:	\$					consolidated clay.									
180	$\approx$	EM2					Silty SAND (SM), slight grained, angular to sub		fine	400.0						
2481.6	\$\$\$\$						Silty CLAY (CL-ML), ha		ist,	180.0 2481.6						
	<u>}</u> }}	}					gray to blue, high plast	icity, Varying								
-	5555						levels of silt content. Silty SAND (SM), slight	tly moist tan t	fine							
	ß	{				0000 00000	grained, angular to sub	angular.								
2476.6	<b>\$</b> \$\$\$	1						-								
· -	<u>}}}}</u>	{				00000 00000										
190	£\$\$\$\$	m														
2471.6	ß					<u>00000</u> 0000000000000000000000000000000										
	<u>}</u> }}	}														
	\$\$\$\$	\$				0000 0000 0000										
_195 2466.6	RSSS	}														
	<u> ISSS</u>	1														
	$\langle \rangle \rangle \langle \rangle$	{				<u>~~~</u> ~										
200	\$\$\$\$	193				0.0000 0.0000				200.0						
2461.6	<u>}}}}</u>	{ ]					CLAY (CL), hard, slight gray to blue, high plast			2461.6						
· -	<u> </u>						clay.	icity, consolida	leu							
	<u> </u>	4					-									
		Wate	er L	evel	Observations	<u> </u>	7 <b>During</b> - <b>Drilling:</b> Not Recorded		Rem	arks:						
After							After		1							

2525 Pa	lmer St
59808	
Phone:	406-543-3045
Fax:	

## Figure No. 5 LOG OF BORING



Phone: 406-543 Fax:	-3043	2		Boring B	32021-5				C		Sheet 5 of 5
Project: Pickles Canyor			dfill -	Rig: TS150 Crawler Hammer: Auto	Boring Locatio	on N: 43.499 E: -116.71	133	1			
Project Number		inty, iD		Boring Diameter:	System: Decir		348	21		Ton	of Boring
114-571040-202				6 in	Datum: NAD	83				Elev	vation: 2661.6 ft
Date Started:		Date Finished	<b>1:</b>	Drilling Fluid:	Abandonment	t Method:					
12/14/21		12/19/21		None	Grout						
Driller: Holt Ser Logger: Matt Ad		5		Location: Refer to	site map.						
				4							
Coperation Coperation	RQD (%)	Blow Count	Lithology	Material Des	cription	Depth (ft) <i>Elev.</i> (ft)	MC (%)	L L	-200 (%)	DD (pcf)	Remarks and Other Tests
205X ★ 2456.6 2451.6 2451.6 2451.6 2451.6 2451.6 2444.6 220 2441.6 220 221 222 225 226 227 227 228 229 229 229 220 225						225.0					
Water		Observations		uring rilling: Not Recorded fter		Remarks:					
T After Drilling: Not Encour	ntered		Ţ,	rilling: Not Recorded							



Fax:								Boring I	B2021-6								Sheet 1 of 4
Projec	t: P	ickl	es E	Butto	e Sanitary La	ndfill -		Rig: TS150 Crawler	Boring Locati	ion N:	43.495	519	6				
Projec				Cou	inty, ID			Hammer: Auto Boring Diameter:	Coordinates System: Deci		-116.7		18				
114-57				,				6 in	Datum: NAD		eyrees					Top	o of Boring vation: 2636.7 ft
Date S			022	•	Date Finishe	d.			Abandonmen		nod:					LIG	741011. 2030.7 IL
11/22/2		ea:			12/2/21	a:		Drilling Fluid: None	Grout								
Driller		olt S	Serv	ices				Location: Refer to	site man								
Logge									Site map.								
Depth (ft)	ы	Sample Type	Recovery (%)	(%)	Blow Count	ogy					Depth (ft)				-	Ē	Remarks
Elev.	Operation	ple	ovel	RQD (%)	U ≩	Lithology		Material Des	cription		Elev.	MC (%)			-200 (%)	DD (pcf)	and Other Tests
(ft)	ð	Sam	Rec	2	Blo						(ft)	δ	Е	Ч	- 70	B	Other rests
	2777					· · · · · · · ·	Т	OPSOIL, very moist,	brown.	Г	0.6						
	ß						Si	ty SAND (SM), loose	e to medium	)	2636.1						
	\$\$\$\$					0.000 0.000		nse, slightly moist, 1 ained, subangular.	an to red, fine								
_ 5 _	<u>}</u> }}						gr	anieu, subarigular.									
2631.7	£\$\$\$\$	$\bowtie$	67		4-5-5	0000 0000 00000											
10 2626.7 2626.7 15 2621.7 2621.7 2611.7 2611.7 2611.7	ß					0.000 0.000 0.000											
- 10	£\$\$\$\$	000				\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$											
10 2626.7	ßß	$\mathbb{V}$	73		7-7-7							6					
	<b>}</b> }}?????	Ŕ	1			0,000 0,000 0,000											
8	ßß																
15	<u> </u>										15.0						
2621.7	ß							orly-Graded SAND		se,	2621.7						
	\$\$\$\$\$							ghtly moist,  gray, fin ained, subangular.									
j	ß						0	, <b>G</b>									
20 2616.7	£\$\$\$\$	$\vdash$	100		11 - 31 - 42						21.0						
	\$}}}	ightarrow						ty SAND (SM), loose			21.0						
	£>>>							nse, slightly moist, g bangular.	gray, fine graine	ed,							
_ 25 _	\$\$\$\$						50	bangalar.									
2611.7	$\approx$	$\boxtimes$	100		12 - 22 - 42	00000 000000						18					
	5555							orly-Graded SAND		se,	27.0 2609.7						
	<u>}</u> }}						sli	ghtly moist, gray, fin	e to medium								
30 2606.7	5555						gra	ained, subangular.									
F -	ß																
	\$\$\$\$						Si	ty SAND (SM), loose	e to medium		33.0 2603.7						
35	<u>}</u> }}					**************************************	de	nse, slightly moist to	moist, gray, fi	ne	2003.7						
30 2606.7 35 35     	<b>{</b> }}}}					00000		ained, Pieces of silts th depth.	tone increasing	9							
	<u>}</u> }}					<u>0000000000000000000000000000000000000</u>	vvi										
- 40 -	\$\$\$\$	-000				0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0 0,0,0,0 0,0,0,0 0,0,0,0 0,0,0,0,0,0,0 0,											
2596.7	ß	Ŵ	100		8 - 18 - 37	** <u>*</u> **						22					
E	£\$\$\$\$	ΥZ															
	ĸ					00000 00000											
45	<b>}</b> }}}	$\vdash$				° • • • • • • • • • • • • • • • • • • •											
2591.7	ł	Ж	100		39 - 42 - 50												
	<u>}</u> }}}						_				48.0						
2 50	£SSS:							andy SILT (ML), hard ay, fine grained.	, slightly moist,	I.	2588.7						
2586.7	<u>}}}}</u>	$\ge$					Yi	ay, mie grameu.									
						١.	D	iring									
50 2586.7		Wate	er L	.evel	Observations	-	≚ Dr	illing: Not Recorded		Rem	arks:						
<u> </u>	g: No	t Enc	counte	ered		-	<u> </u>	illing: Not Recorded									

## Figure No. 6 LOG OF BORING



Fax:		Boring E	32021-6						Sheet 2 of 4
Project: Pickles Butte Sanitary La Canyon County, ID	ndfill -	Rig: TS150 Crawler	Boring Locatio	on N: 43.495	519	6 1 9			
Project Number:		Hammer: Auto Boring Diameter:	System: Decir	<u>E: -116.7</u> nal Degrees		10		Tor	o of Boring
114-571040-2022		6 in	Datum: NAD8					Ele	vation: 2636.7 ft
Date Started: Date Finishe	ed:	Drilling Fluid:	Abandonment Grout	i Methoa:					
11/22/21 12/2/21 <b>Driller:</b> Holt Services		None Location: Refer to							
Logger: Matt Adams									
(tj.)     (tj.)       Operation     Operation       Recovery (%)     Recovery (%)       ROD (%)     Blow Count	Lithology	Material Des	cription	Depth (ft) <i>Elev.</i> (ft)	MC (%)	LL	PL 200 (0/)	-200 (%) DD (pcf)	Remarks and Other Tests
$\begin{array}{c} 100 \\ 14-26-43 \\ 55 \\ 2581.7 \\ \hline \\ 55 \\ 2581.7 \\ \hline \\ 60 \\ 2576.7 \\ \hline \\ 70 \\ 2576.7 \\ \hline \\ 70 \\ 2566.7 \\ \hline \\ 75 \\ 2561.7 \\ \hline \\ 75 \\ 75 \\ 2561.7 \\ \hline \\ 75 \\ 75 \\ 2561.7 \\ \hline \\ 75 \\ 75 \\ 75 \\ 75 \\ 75 \\ 75 \\ 75$					25				UCS= 7.246 ksf
75 2561.7 80 2556.7 85 2551.7 85 2551.7 85 2551.7 85 85 2551.7 85 85 2551.7		CLAY (CH), hard, sligh dark gray, high plasticit claystone very consolid	y, Almost	76.0 2560.7		67	19 9	1	
100 2536.7 Water Level Observations After Drilling: Not Encountered						56	22 9	0	UCS= 15.661 ksf
Water Level Observations		During		Remarks:					
		- Drilling: Not Recorded After							
<b>Prilling:</b> Not Encountered	<u> </u>	- Drilling: Not Recorded							



Sheet 3 of 4

							Boring B									Sheet 3 of 4
	С	any	on C	utte Cou	e Sanitary Lar nty, ID	ndfill -	Rig: TS150 Crawler Hammer: Auto	Boring Location Coordinates	n N: 43 E: -1	3.495 16.71	190  57	6 '18				
Projec	t Nu	ımb	er:				Boring Diameter:	System: Decim	al Deg	rees					Тор	of Boring
114-57	7104	10-2	022				6 in	Datum: NAD83							Elev	ation: 2636.7 ft
Date S	start	ed:			Date Finishe	d:	Drilling Fluid:	Abandonment I	Metho	d:						
11/22/2	21				12/2/21		None	Grout								
Driller	: Ho	olt S	ervi	ces	;		Location: Refer to	site map.								
Logge	er: M	att /	Adar	ns				•								
Depth (ft) <i>Elev.</i> (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Des	cription	E	epth (ft) Elev. (ft)	MC (%)	F	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
 105 - 2531.7   110		23 23 2 23					Sandy SILT (ML), hard gray, medium plasticity Silty CLAY (CL-ML), ha very dark gray, high pla claystone very consolid CLAY with sand (CL), h moist, gray, medium pl	ard, slightly moist isticity, Almost lated. nard, slightly lasticity.	2 t, 2 1 2 1 2	02.0 534.7 02.8 533.9 06.0 530.7 06.9 529.8		47	22	91	100	
2526.7  115 - 2521.7			100		9 - 19 - 28		Silty CLAY (CL-ML), havery dark gray, high pla claystone very consolid Sandy SILT (ML), hard gray, medium plasticity Silty CLAY (CL-ML), havery dark gray to blue, Almost claystone very of	asticity, Almost lated. , slightly moist, ird, slightly moist high plasticity,	2: 1 2:	10.8 525.9 12.0 524.7	21					
120 _2516.7   125 2511.7			100		10 - 18 - 33						22					
 			115		28 - 47 - 50/0.3ft											
			100		6 - 16 - 31											
135 - 2501.7 - 2501.7 - - 140 - - 2496.7 - - - 145 - - 145 - - 2486.7 - - - - - - - - - - - - - - - - - - -			107		11 - 19 - 50/0.4ft											
		۹				raavka										
		Wate	er Lo	evel	Observations	Z	7 <b>During</b> - Drilling: Not Recorded		Remark	(s:				_		
After			ounte				After Drilling: Not Recorded									

2525 Palmer St 59808 Phone: 406-543-3045 Fax:

## Figure No. 6 LOG OF BORING



Fax:		6-54					Boring B	32021-6							Sheet 4 of 4
Projec					Sanitary La	ndfill -	Rig: TS150 Crawler	Boring Location	on N: 43.	4951	96				
Projec				Cou	nty, ID		Hammer: Auto Boring Diameter:	Coordinates System: Decir	<u>E: -11</u>		5718	}			
114-57							6 in	Datum: NAD		663				Top	of Boring ation: 2636.7 ft
Date S			022	1	Date Finishe	d.	Drilling Fluid:	Abandonment						LIEV	alion. 2030.7 IL
11/22/2		u.			12/2/21	u.	None	Grout							
Driller:		lt S	ervi				Location: Refer to	site map.							
Logge								ono map.							
Depth (ft) <i>Elev.</i> <i>(ft)</i>	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Des	cription	Dej (f <i>Ele</i>	t)	MC (%) LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
155 		X	115		29 - 50 - 50/0.3ft										
✓ After Drilling		Wate			Observations	<u> </u>	uring rilling: Not Recorded		Remarks						



							Boring	B2021-7								Sheet 1 of 4
Projec					e Sanitary La	ndfill -	Rig: TS150 Crawle									
				Σοι	inty, ID		Hammer: Auto	Coordinates		-116.7		592				
Projec							Boring Diameter:	System: Deci	imal De	egrees					Тор	of Boring
114-57	7104	0-2	022				6 in	Datum: NAD							Elev	/ation: 2659.5 ft
Date S	Starte	ed:			Date Finishe	d:	Drilling Fluid:	Abandonmen	t Meth	od:						
12/2/2	1				12/7/21		None	Grout								
Driller		olt S	ervi	ces			Location: Refer to	site man								
Logge	er: M	att /	\dar	ns				ono map.								
	1										i –					
Depth	-	e	Recovery (%)	~	Ĕ	2				Depth						
(ft)	Operation	Sample Type	Ъ	(%)	Blow Count	Lithology	Material Des	scription		(ft)				(%	(bcf)	Remarks and
Elev.	pera	ple	Š	RQD	Ň	ithe	Waterial Des	scription		Elev.	(%)			-200 (%)	ġ	Other Tests
(ft)	o	San	Re		ā	-				(ft)	ВC	E	Ч	-50	B	
						N 17. N	Slightly moist, dark bro	าพท		0.6						
	2					× × × × × ×	Silty SAND (SM), loos		<u> </u>	2658.9						
	R						moist, tan, fine graine		,							
	-\$\$\$\$						subangular.									
5 2654.5	\$}}}	$\vdash$	60		2-2-3						4					
	KK	$\bowtie$	60													
	<b>}</b> }}?	1														
- 10 -	<u>}}}}</u>					0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0										
10 	$\langle \rangle \rangle$	$ \downarrow $			10-8-5											
	5555	igtarrow	67		10-8-5	00000 00000										
	\$\$\$\$															
	2000															
15 					0 40 40											
2044.5	-65555	$\bowtie$	80		8 - 18 - 18			( <b></b> )		16.4						
	\$>>>						Poorly-Graded SAND			2643.1						
	<u>}</u> }}						moist, tan, fine to mee angular to subangular									
20 2639.5	<u>-</u> 85559	3														
2039.5																
	£\$\$\$															
	K															
25 2634.5	\$\$\$\$									25.0						
2634.5	2002	$\mathbb{X}$	100		13 - 40 - 50		Silty SAND (SM), loos moist, tan, fine graine		У	2634.5						
	K						subangular.	angular to								
	\$\$\$\$						ouburigular.									
	2000		_		26 - 50/0.1ft					30.3						
2629.5	KK		0		20 000.11		Poorly-Graded SAND			2629.2						
	\$\$\$\$						moist, gray, fine to me		H	31.3						
-	<u>}</u> }})))/						angular to subangular			2628.2 32.3						
35	<u> </u>				35 - 50/0.3ft		Silty SAND (SM), loos moist, tan, fine graine		y	2627.2						
2624.5			0		33-300.3it		subangular.	a, angular to		33.8 2625.7						
	2					00000	Poorly-Graded SAND		[	2023.1						
	XXX					<u>~~~~</u>	moist, gray, fine to me	edium grained,								
40	<u> </u>	(B)					angular to subangular		I	39.6 2619.9		NV	NP	23	112	UCS= 0.511 ksf
2619.5	- <u>}</u> }}}	$\boxtimes$	107		16 - 28 - 50/0.4ft		Silty SAND (SM), loos		y	41.4	23					
	£\$\$\$						moist, tan, fine graine	d, angular to	Π	2618.1						
	<u>}</u>						subangular. Poorly-Graded SAND	(SP) dense	∥	43.6						
45	\$\$\$\$?						moist, gray, fine to me			2615.9						
2614.5	$\langle \rangle \rangle \rangle \langle \rangle \langle \rangle \langle \rangle \rangle \langle \rangle \langle \rangle \rangle \langle \rangle \langle \rangle \langle \rangle \rangle \langle \rangle \langle \rangle \langle \rangle \rangle \langle \rangle \langle \rangle \langle \rangle \langle \rangle \rangle \langle $	$ \times $	100		19 - 37 - 48		angular to subangular		Ļ	46.1						
	₭⋘						Silty CLAY (CL-ML), v	ery stiff, moist,		2613.4						
	\$\$\$\$						tan, high plasticity, Bro									
50		193					consolidated clay.			50.0						
2609.5	2222	$\boxtimes$					Silty SAND (SM), very	dense, slightly	ſ	00.0						
							7 During		1_							
		Wate	er L	evel	Observations	7	Drilling: Not Encountered		Rema	arks:						
After							After		1							



Sheet 2 of 4

Fax:								B2021-7								Sheet 2 of
Projec					e Sanitary Lar ınty, ID	ndfill -	Rig: TS150 Crawle Hammer: Auto	F Boring Locati Coordinates	on N: E:	43.498	528 125	592				
Projec					···· <b>,</b> , ·_		Boring Diameter:	System: Deci							Ton	of Boring
114-57	7104	0-2	022				6 in	Datum: NAD	83						Elev	vation: 2659.5 ft
Date S	starte	ed:			Date Finishe	d:	Drilling Fluid:	Abandonmen	t Meth	nod:						
12/2/2	1				12/7/21		None	Grout								
Driller					3		Location: Refer to	site map.								
Logge	er: M	att /	Adaı	ms							_					
Depth (ft) <i>Elev.</i> (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Des	scription		Depth (ft) <i>Elev.</i> (ft)	MC (%)	F	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
- 55 2604.5 - 2599.5 - 2599.5 - - - - - - - - - - - - - - - - - - -		23	100		<del>29 - 49 - 37</del> 21 - 41 - 50/0.4ft 9 - 23 - 35		moist, tan, fine graine subangular, Broken pi- and sandstone. Silty CLAY (CL-ML), h high plasticity, Broken consolidated clay. Silty SAND (SM), very moist, tan, fine graine subangular, Broken pi- and sandstone. Silty CLAY (CL-ML), h high plasticity, Broken consolidated clay Silty SAND (SM), very moist, tan, fine graine subangular, Broken pi- and sandstone. Sandy SILT (ML), hard plasticity, Broken piece clay CLAY (CL), hard, mois plasticity.	eces of siltstone ard, moist, tan, pieces of dense, slightly d, angular to eces of siltstone ard, moist, tan, pieces of dense, slightly d, angular to eces of siltstone d, moist, tan, hi es of consolidat	[	2609.5 54.0 2605.5 55.6 2603.9 58.5 2601.0 66.0 2593.5	12		NP	84	104	UCS= 1.817 ksf
80		(53)	0		78 - 70/0.2ft 70/0.3ft		Silty SAND (SM), very moist, tan, fine graine subangular, Broken pi and sandstone. Silty CLAY (CL-ML), h high plasticity, Broken consolidated clay	d, angular to eces of siltstone ard, moist, tan,		80.0 2579.5 85.0 2574.5						
95 2564.5  100 2559.5			100		28 - 28 - 28		CLAY (CL), hard, mois plasticity.	st, tan, high		97.7 2561.8	20					
		Wate	er L	.evel	Observations	7	During     Drilling: Not Encountered		Rem	arks:						
After			corde				After Drilling: Not Recorded		]							

## Figure No. 7 LOG OF BORING



Fax:		Boring	B2021-7						Sheet 3 of 4
Project: Pickles Butte Canyon Cou		- Rig: TS150 Crawler Hammer: Auto	Boring Locatio	n N: 43.495 E: -116.7	28 1259	2			
Project Number: 114-571040-2022		Boring Diameter: 6 in	System: Decin Datum: NAD8	nal Degrees 3				Top Elev	of Boring /ation: 2659.5 ft
Date Started: 12/2/21	Date Finished: 12/7/21	Drilling Fluid: None	Abandonment Grout	Method:					
Driller: Holt Services Logger: Matt Adams	5	Location: Refer to	site map.						
(t) Sample Type Recovery (%) RQD (%)	Blow Count Lithology	Material Des	cription	Depth (ft) <i>Elev.</i> (ft)	MC (%)	님	-200 (%)	DD (pcf)	Remarks and Other Tests
105 2554.5 107 2554.5 100 2549.5 100 100 100 100 100 100 100	6-12-22.								
	22 - 41 - 50/0.3ft	SILT (ML), hard, dry, t Broken pieces. Silty CLAY (CL-ML), ha high plasticity, Broken consolidated clay	ard, moist, gray	122.2	3	3 23	ł		Friction Angle= 18.0 degrees Cohesion= 0.053 ks Cc= 0.38
130 2529.5 100 100 135 2524.5	12-33-48	Sandy SILT (ML), hard plasticity, Broken piece Silty CLAY (CL-ML), ha high plasticity, Broken consolidated clay	es. ard, moist, gray	128.5 2531.0 129.1 2530.4	19				
140 2519.5 100 100 145 2514.5	9-18-50	CLAY (CL), hard, mois	t, gray to blue,	145.0 <i>2514.</i> 5	24				
150 2509.5	9-18-31	high plasticity.							
Water Level	Observations	∠ During     Drilling: Not Encountered		Remarks:					
Trilling: Not Recorded		After Drilling: Not Recorded							

# Figure No. 7 LOG OF BORING



Fax:		-304:			Boring I	32021-7						Sheet 4 of 4
Project: Pic	kles	Butte	e Sanitary La	ndfill -	Rig: TS150 Crawler	Boring Locati	on N: 43.495	28	-00			
Project Nun			nty, ID		Hammer: Auto Boring Diameter:	Coordinates System: Deci	<u>E: -116.7</u>		92			
114-571040					6 in	Datum: NAD					Top	o of Boring vation: 2659.5 ft
Date Started		2	Data Einiaha	<u>م</u> ا،		Abandonmen					LIG	valion. 2009.0 n
12/2/21	:נ		Date Finishe	a:	Drilling Fluid: None	Grout						
Driller: Hol	t Ser	vices			Location: Refer to							
Logger: Mai					Location: Relef to	site map.						
Depth (ft) Deration	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Des	cription	Depth (ft) <i>Elev.</i> (ft)	MC (%)	Ŀ	PL 202 mil	-200 (%) DD (pcf)	Remarks and Other Tests
160 _2499.5   165 165 2494.5 	10	7	21 - 48 - 50/0.4ft									
170 2489.5 175 2484.5 2474.5 180 2479.5 185 2477.5 190 2469.5 195 2469.5 195 2469.5 2469.5 2469.5	<b>K</b> 10	0	14 - 18 - 28									
18012479.512479.512479.512479.512479.512474	×											
	×											
- 195	x						200.0					
2459.5					Boring Depth: 200. 2459.5	0 ft, <i>Elevation:</i> 5 ft	2459.5		· · · ·			
И	later	Level	Observations	$\nabla$	During Drilling: Not Encountered		Remarks:					
				-	After		1					

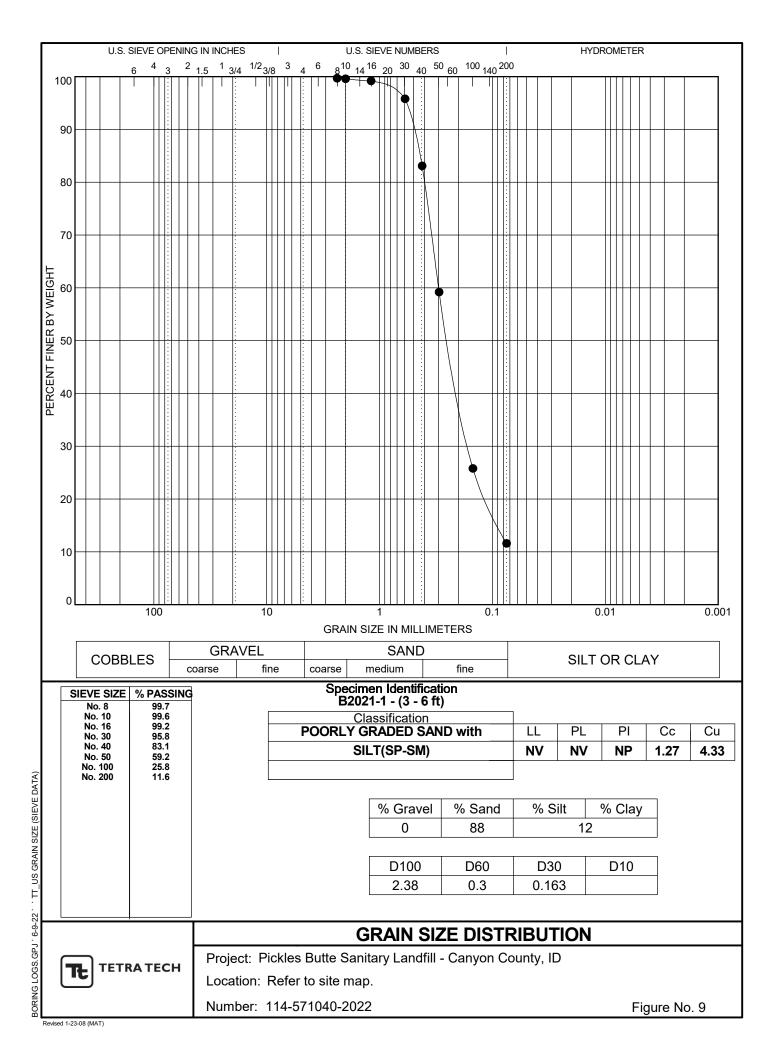
## Figure No. 8 LOG OF BORING

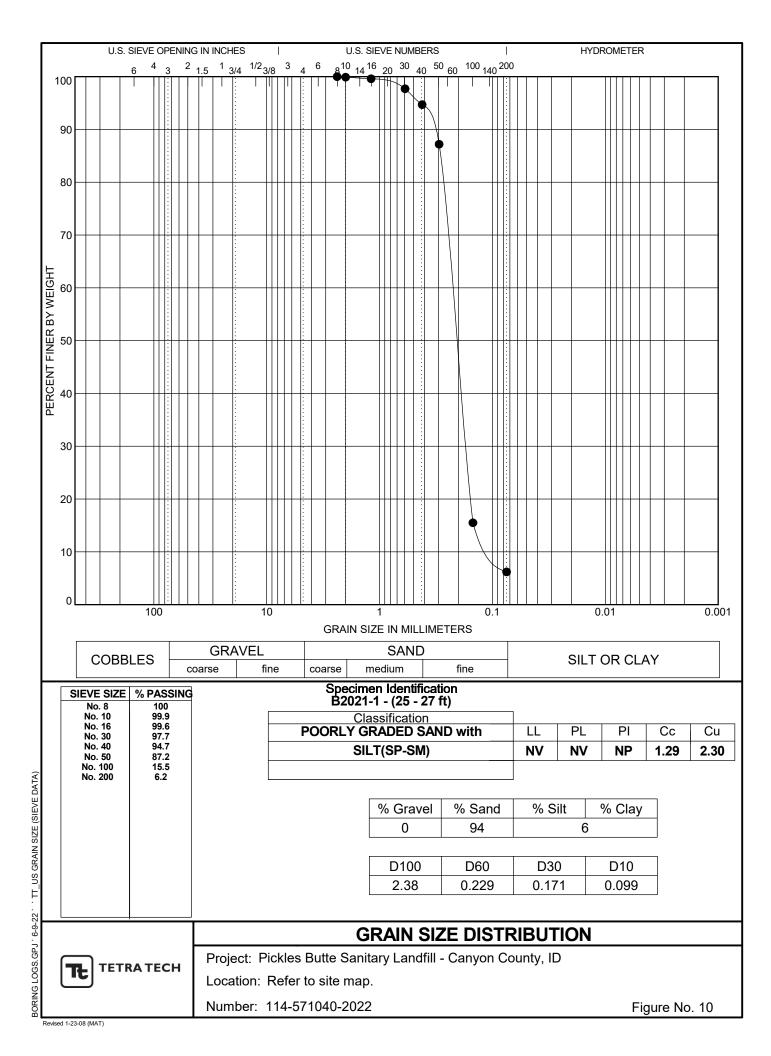


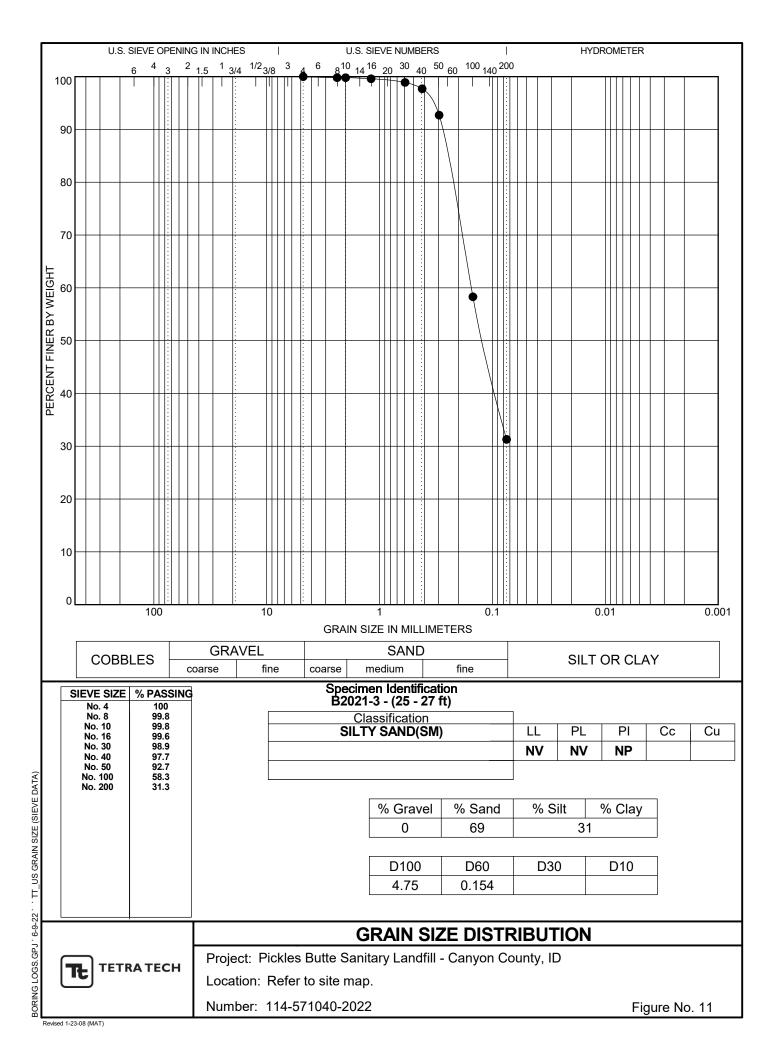
Fax:			10 0		,			Boring E	32021-8								Sheet 1 of 1
Projec	t: P	ickle	es B	utte	e Sanitary Lar inty, ID	ndfill -	•	Rig: TS150 Crawler	Boring Locatio	on N: ⊑·	43.489 -116.7	)88 02.	1/17	,			
<b>Projec</b> 114-57	t Nu	ımb	er:					Boring Diameter: 6 in	System: Decin Datum: NAD8	nal D 33	egrees		147			Top Elev	o of Boring vation: 2956.6 ft
<b>Date S</b> 11/15/2	21				Date Finishe 11/15/21	d:		Drilling Fluid: None	Abandonment Grout	Meth	nod:						
Driller: Logge					6			Location: Refer to	site map.								
Depth (ft) <i>Elev.</i> (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology		Material Des	cription		Depth (ft) <i>Elev.</i> (ft)	MC (%)	L	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
(19	<<<<	 N 7	₽ 100		5-5-12	<u></u>		DPSOIL, moist, brow			0.6	11			•		
-			100		0-0-12		SI mo	LT with sand (ML), ve pist to moist,  tan.	ery stiff, slightly		2956.0		NV	ΝP	84	97	
-		X	100		10 - 16 - 13												
5 2951.6			100		8-8-10							11					
-												12					
10 946.6			100 100		7-9-11	0,000 0,000 0,000	Si	ity SAND (SM), medi bist, tan to gray, fine	um dense, sligh	ntly	10.1 2946.5	6					
- - 15						<del>ေစ် ၀န္ခ်ီ စွာ စွေ စွေ စွေ စွေ စွေ ရွှ</del> စွေ စန္ဒ စွေ စွေ စွေ စွေ စွေ စွေ စွေ စွေ စွေ စွေ စွေ စွေ စွေ စွေ စွေ	su	bangular, scattered ç	jravel.								
2941.6 - - -		X	87		6-7-9	<u>୨୯୭୦ ୧୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦</u>						5					
20 936.6 -		X	87		9-13-15		de	oorly-Graded SAND ( onse, slightly moist, ta	an to yellow, fin	e	20.0 2936.6 21.5	5					
-							an	medium grained, sub gular. oring Depth: 21.5 ft,	•	[ 5.1	2935.1						
								ft									
		144.4			Olassa fi		, D	ring		Derri	orl/						
After		Wate	er L	evel	Observations		≚Dr	illing: Not Encountered		Rem	arks:						
Drilling	g:No	t Rec	ordeo	ł				rilling: Not Recorded									

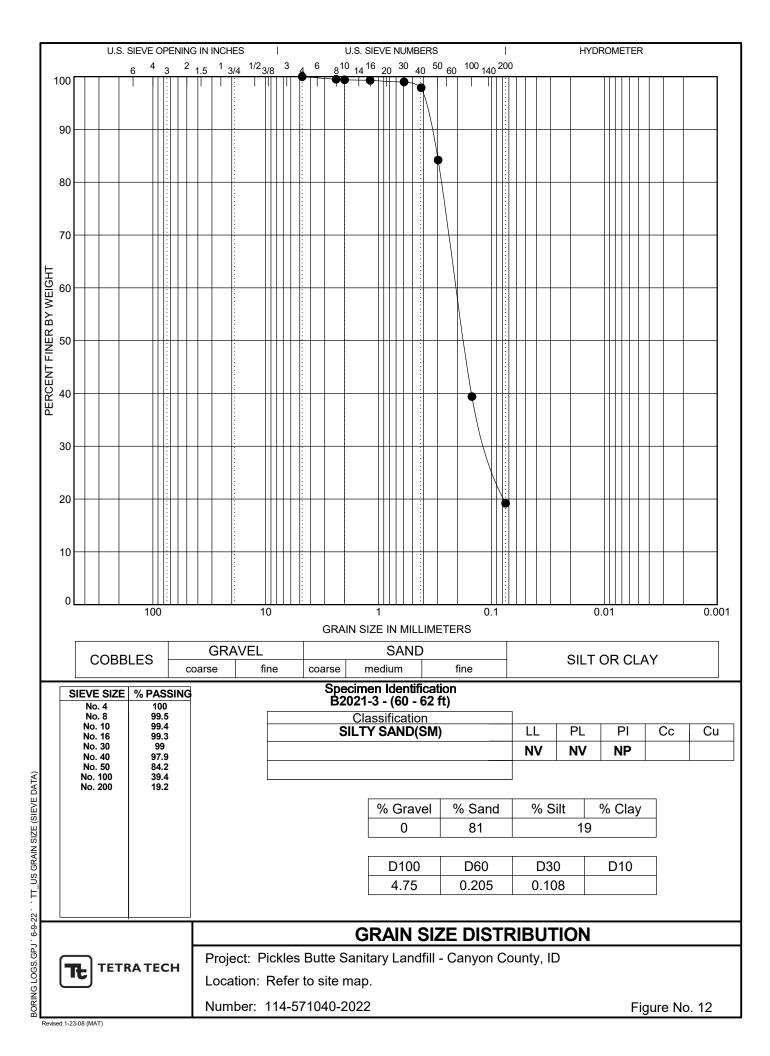
## APPENDIX C: Laboratory Testing

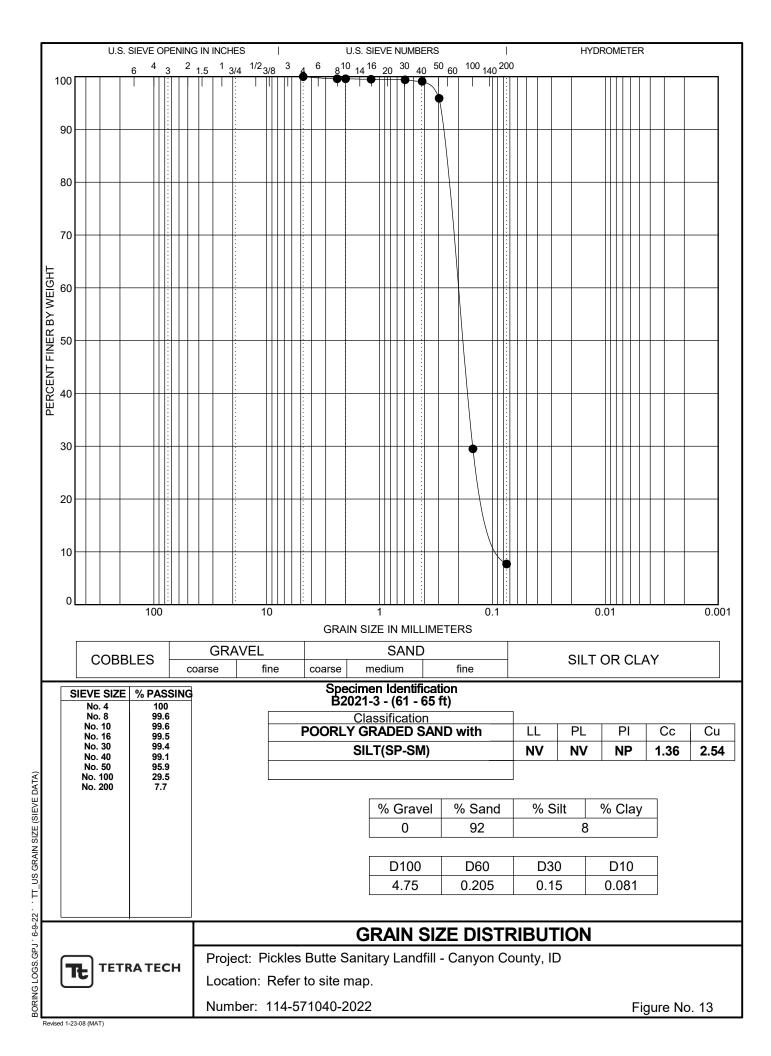
Figures 9 through 56

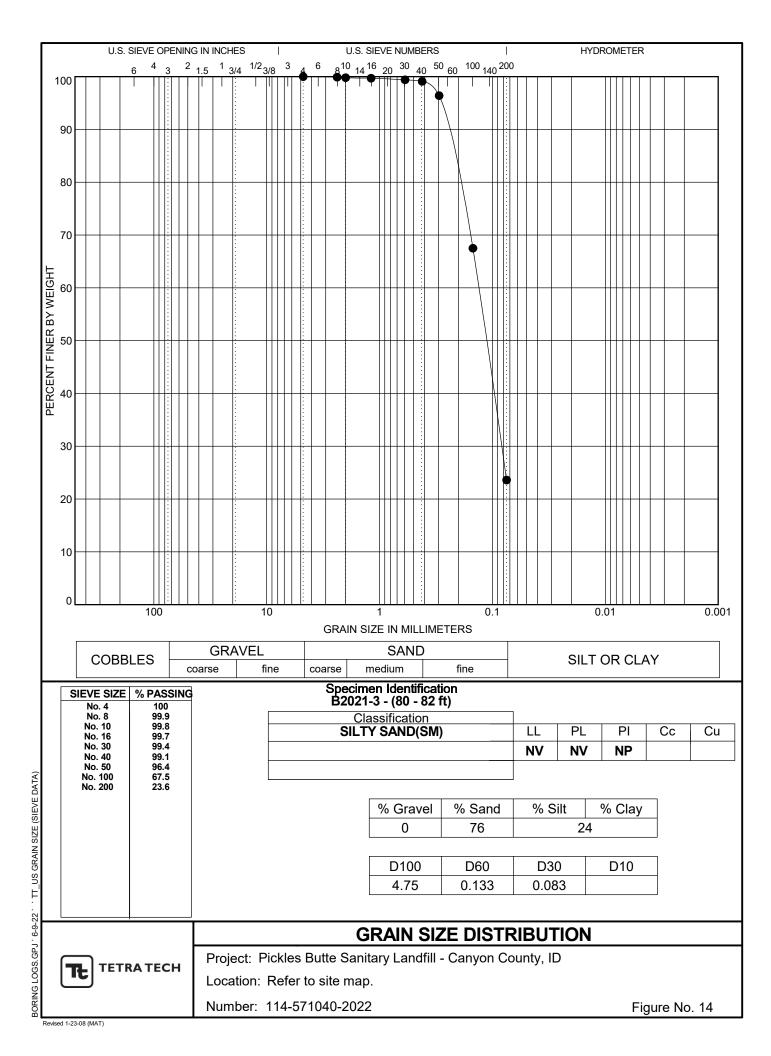


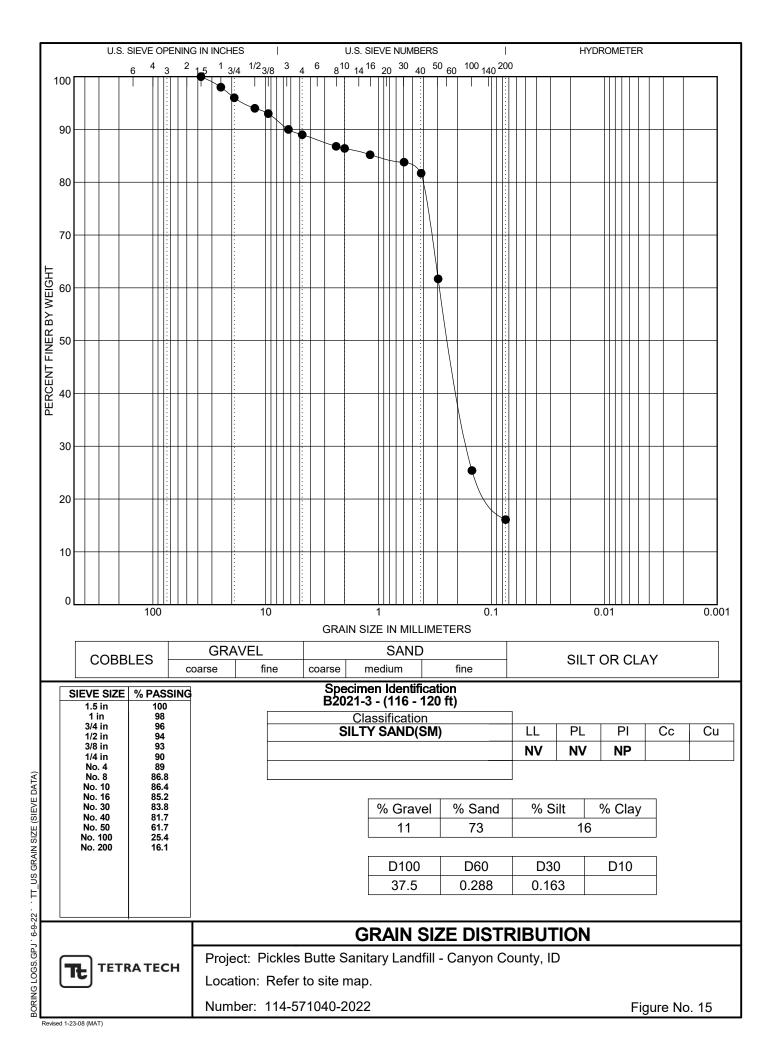


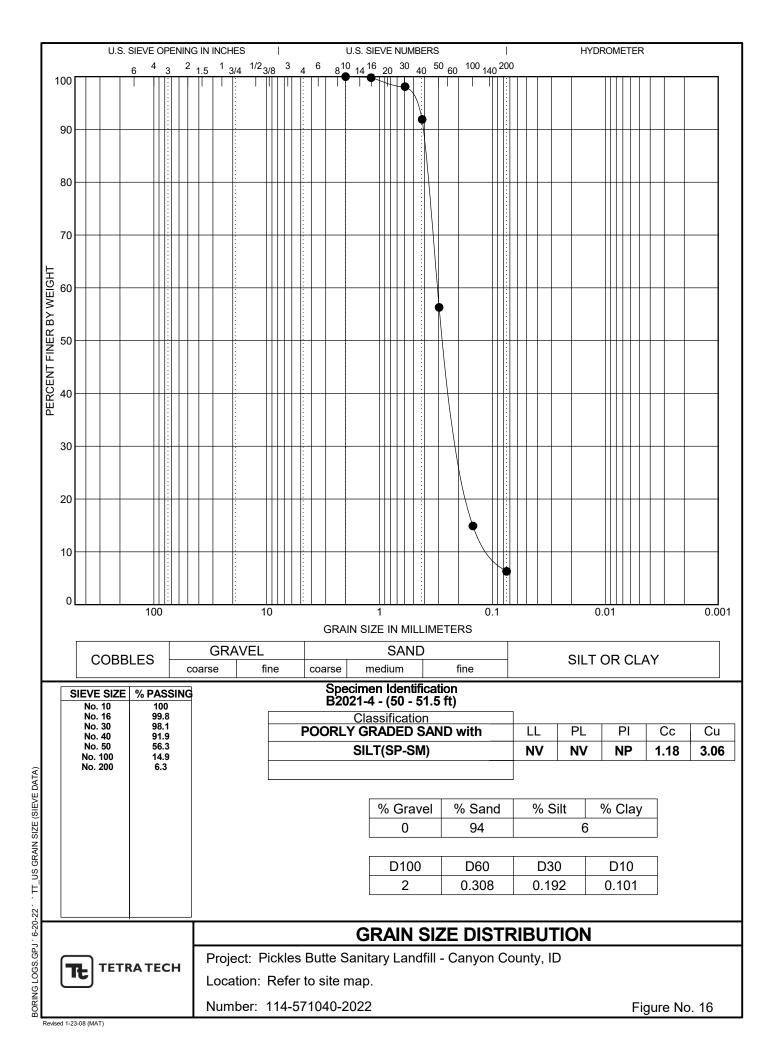


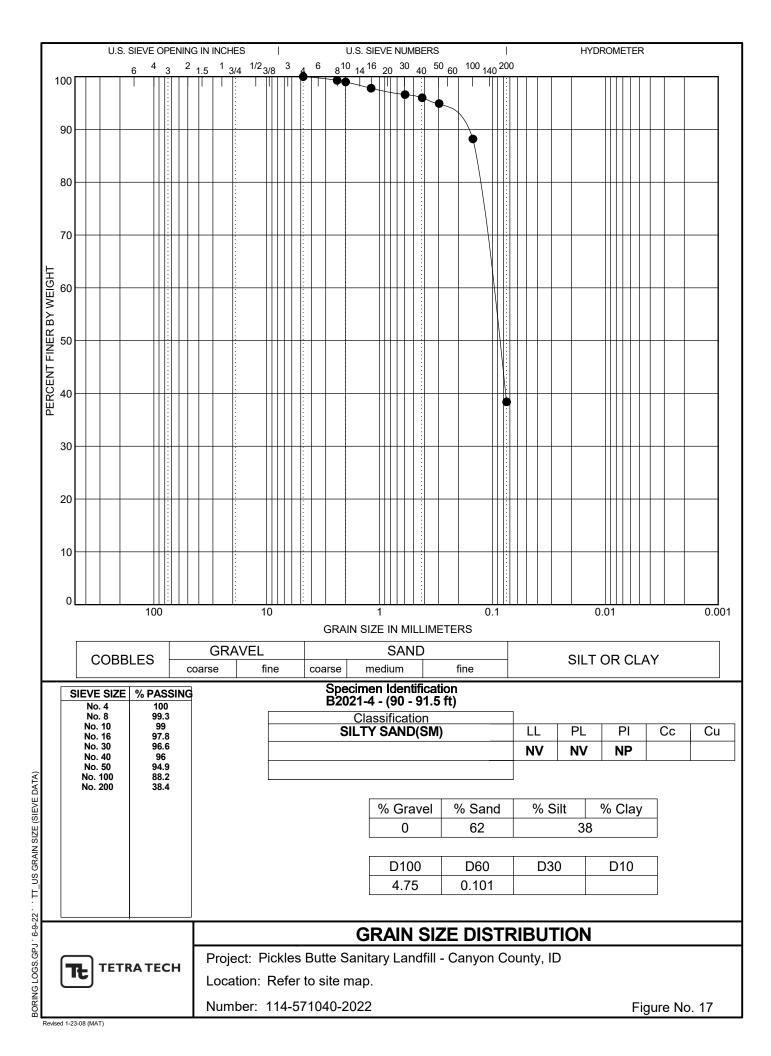


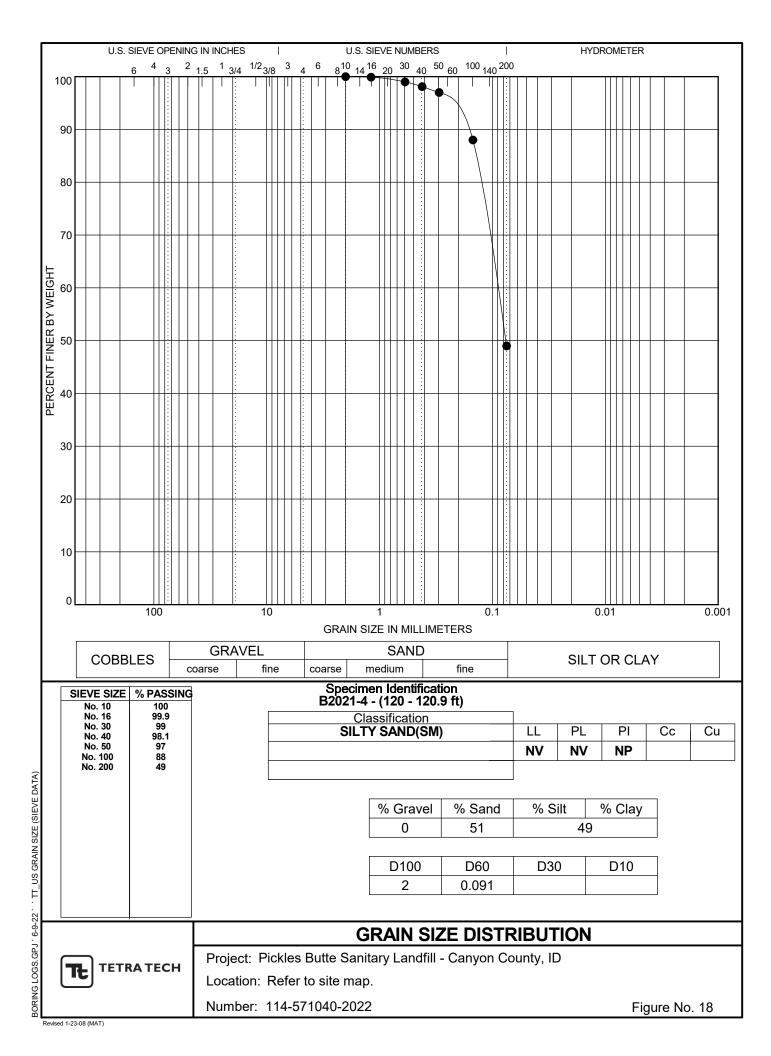


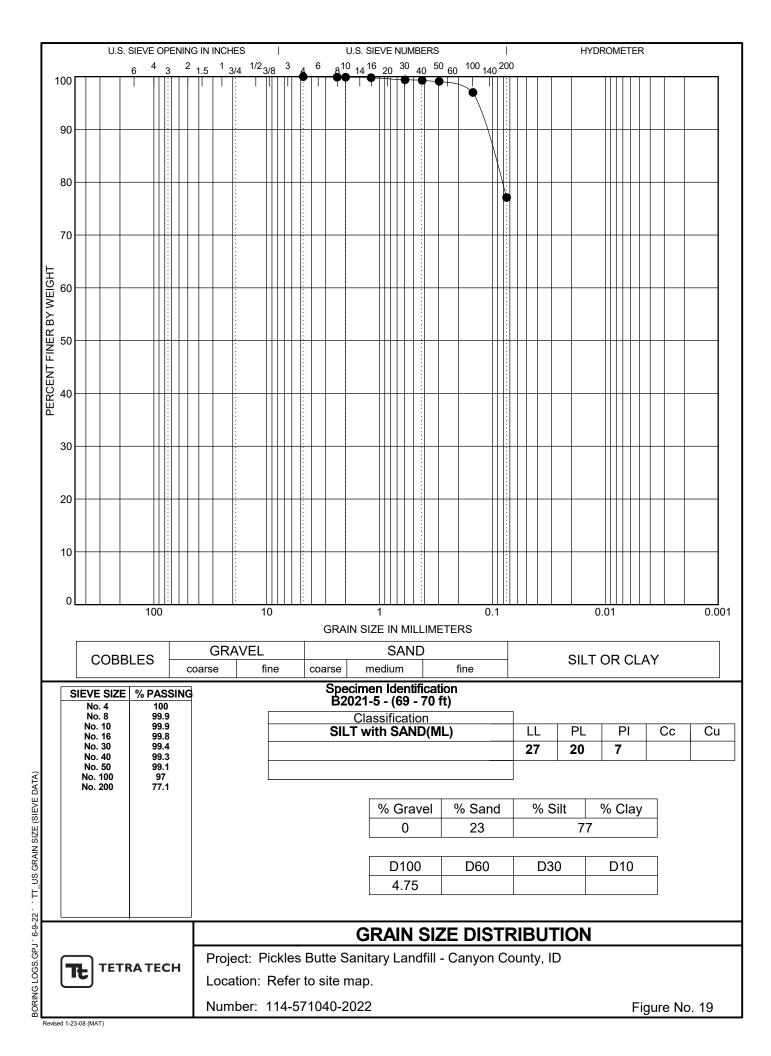


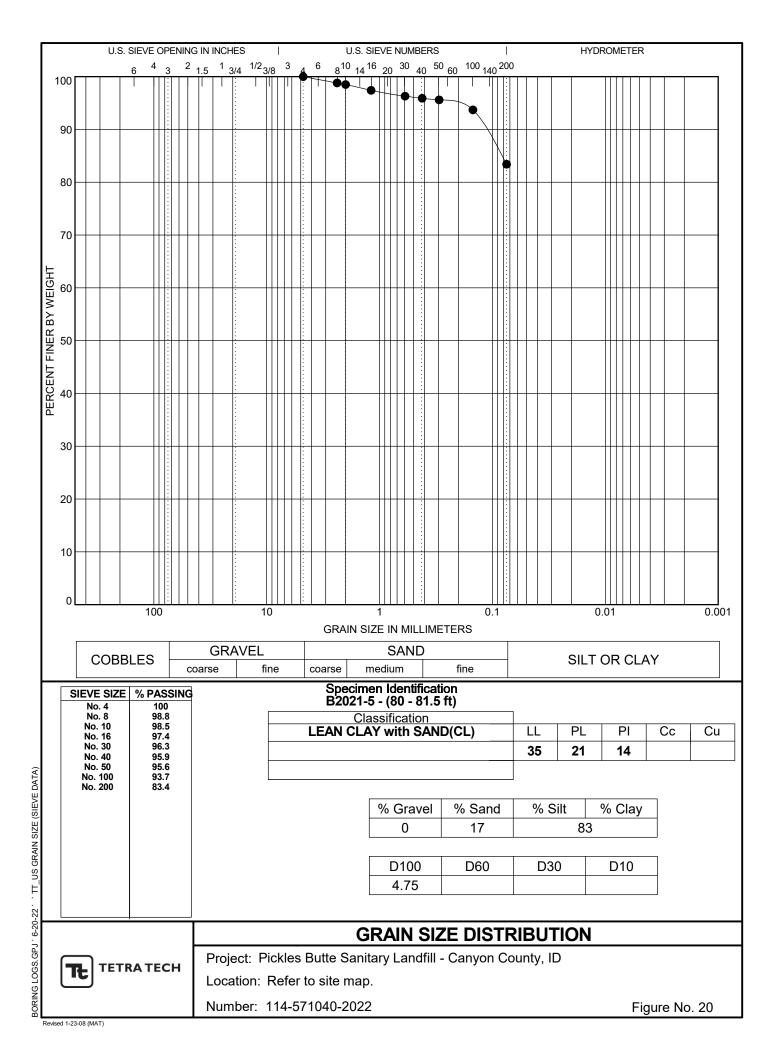


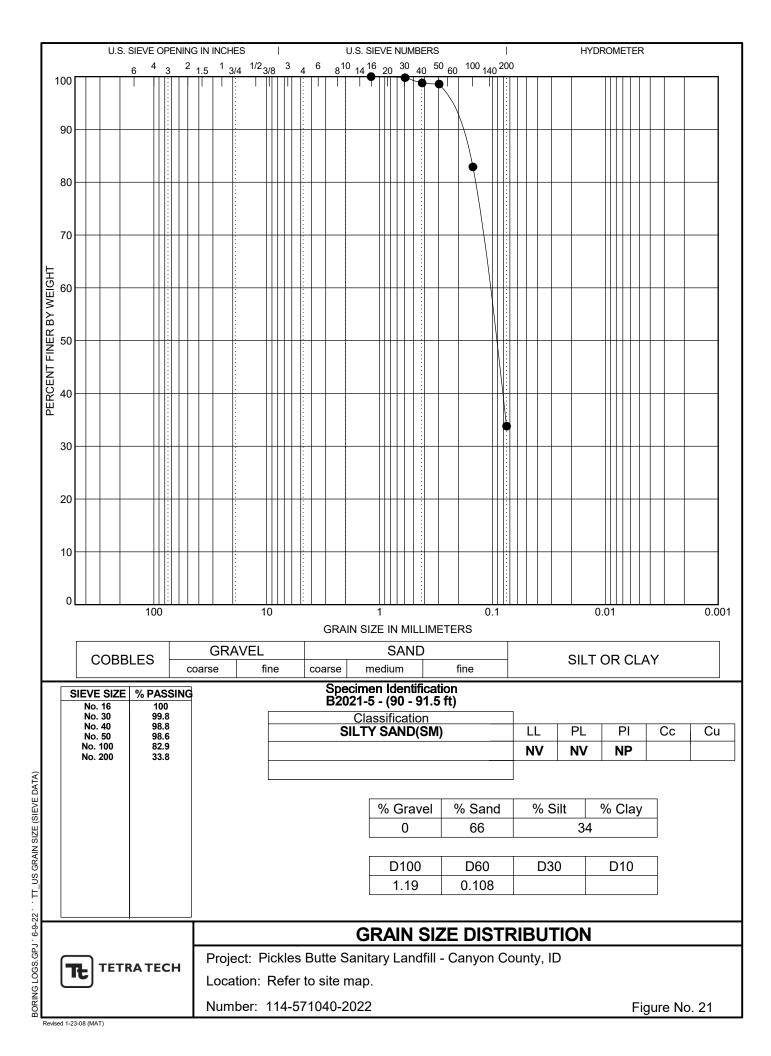


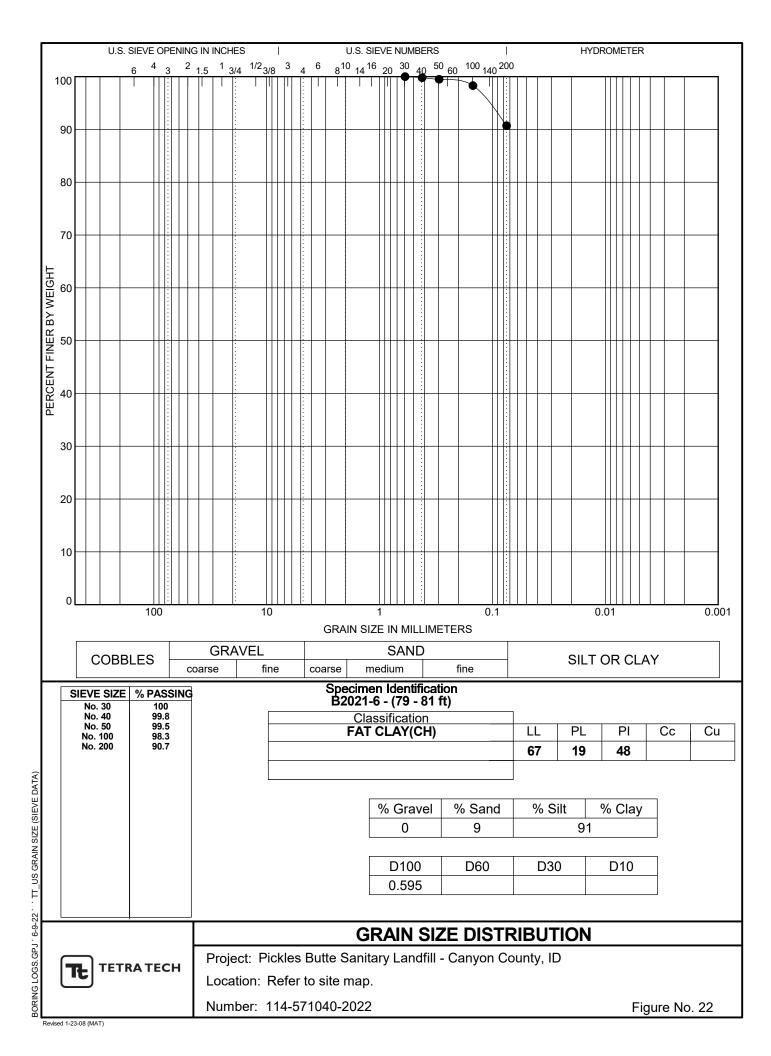


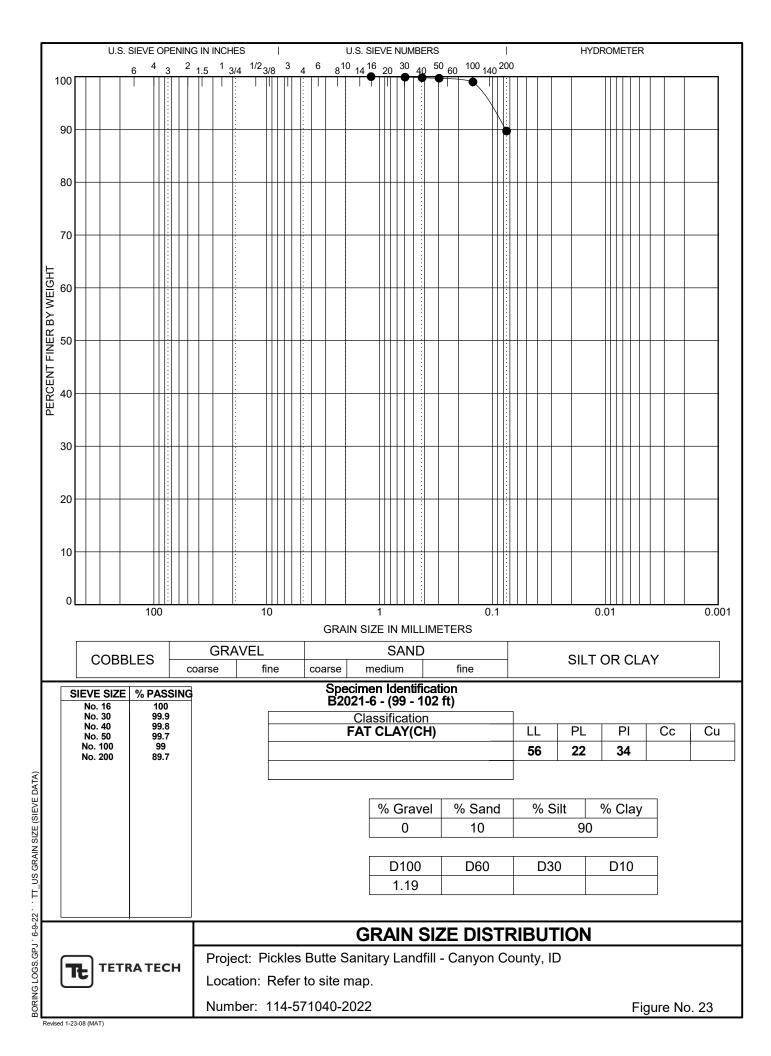


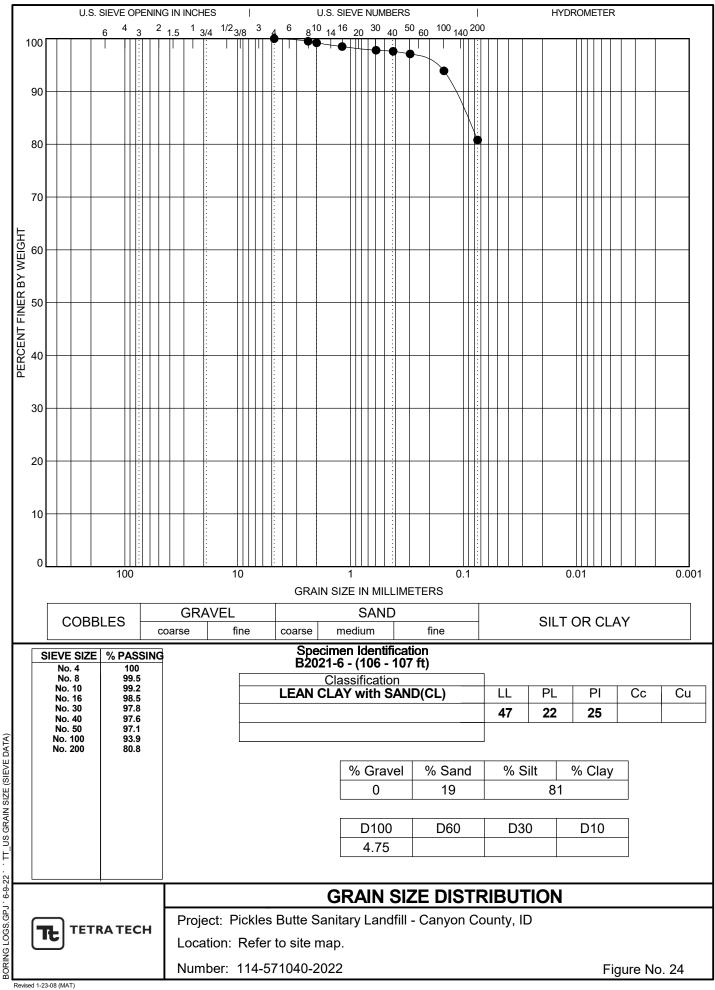


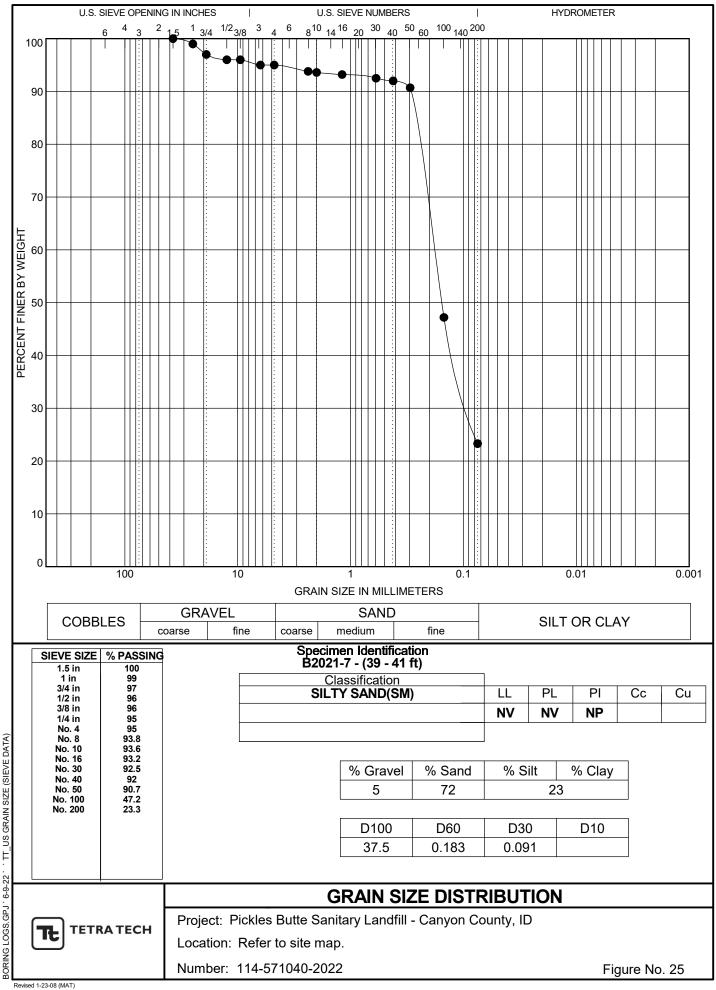


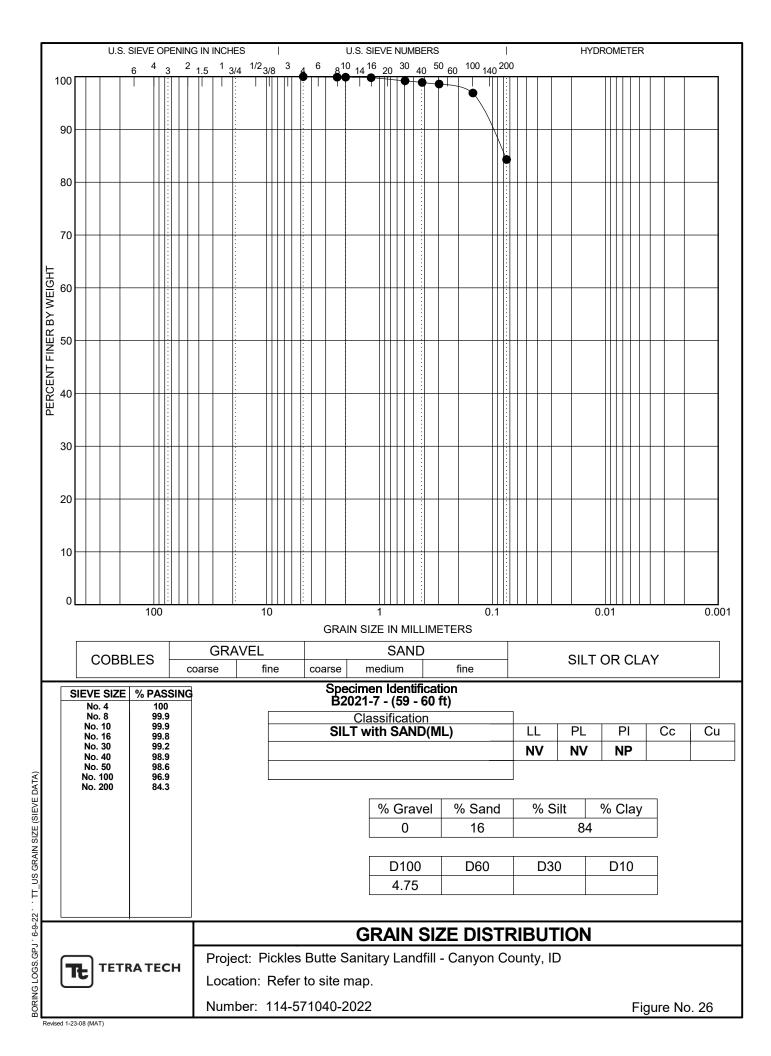


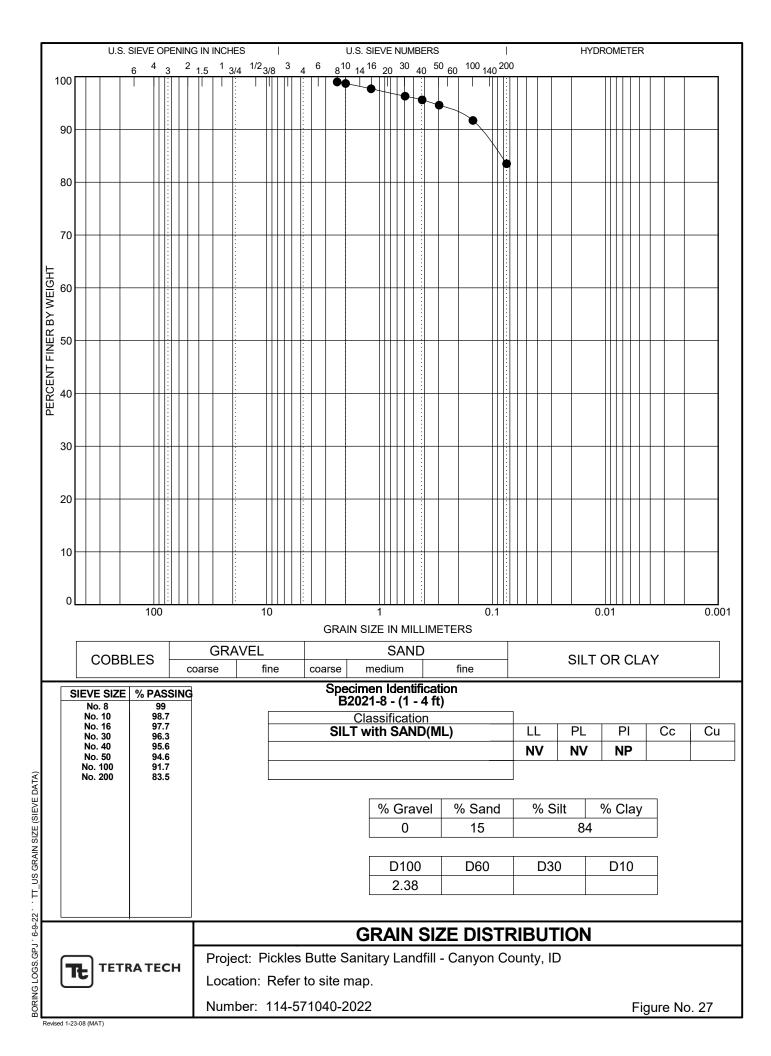


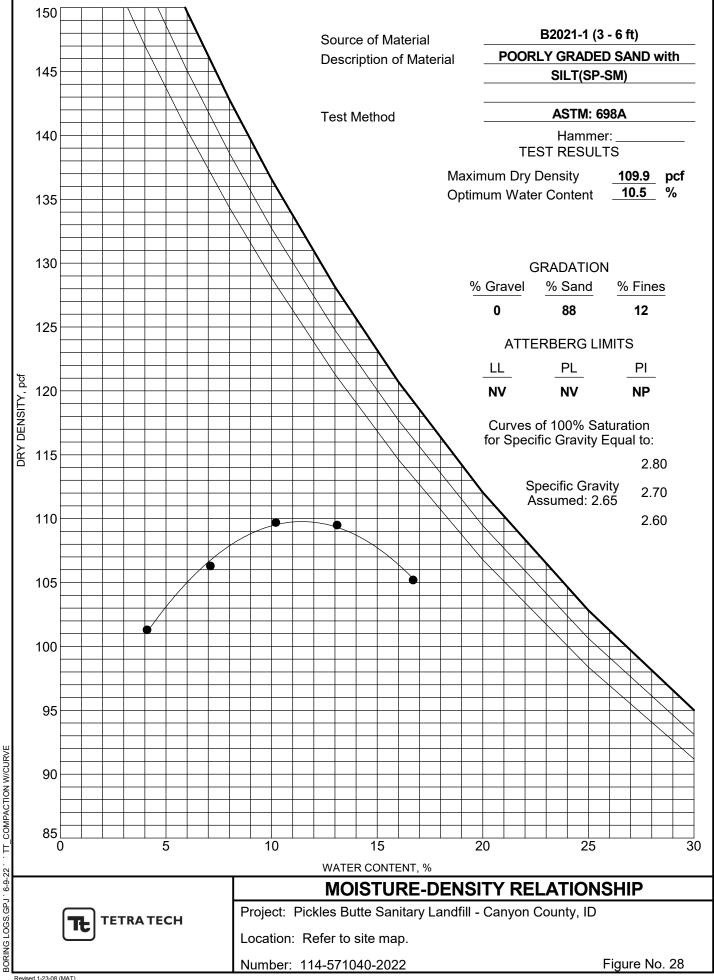




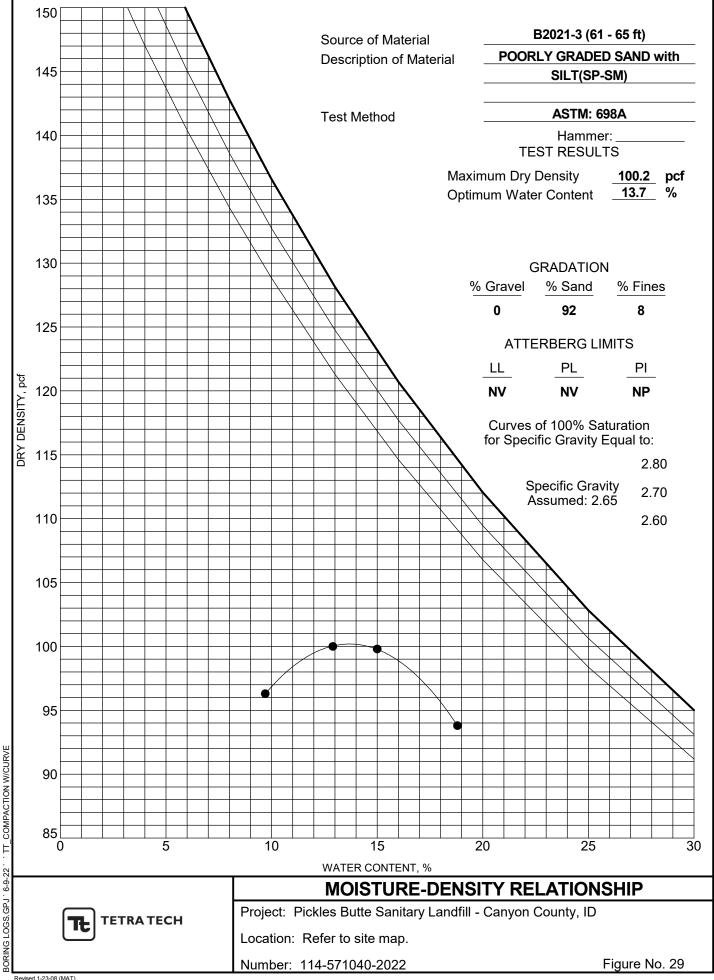




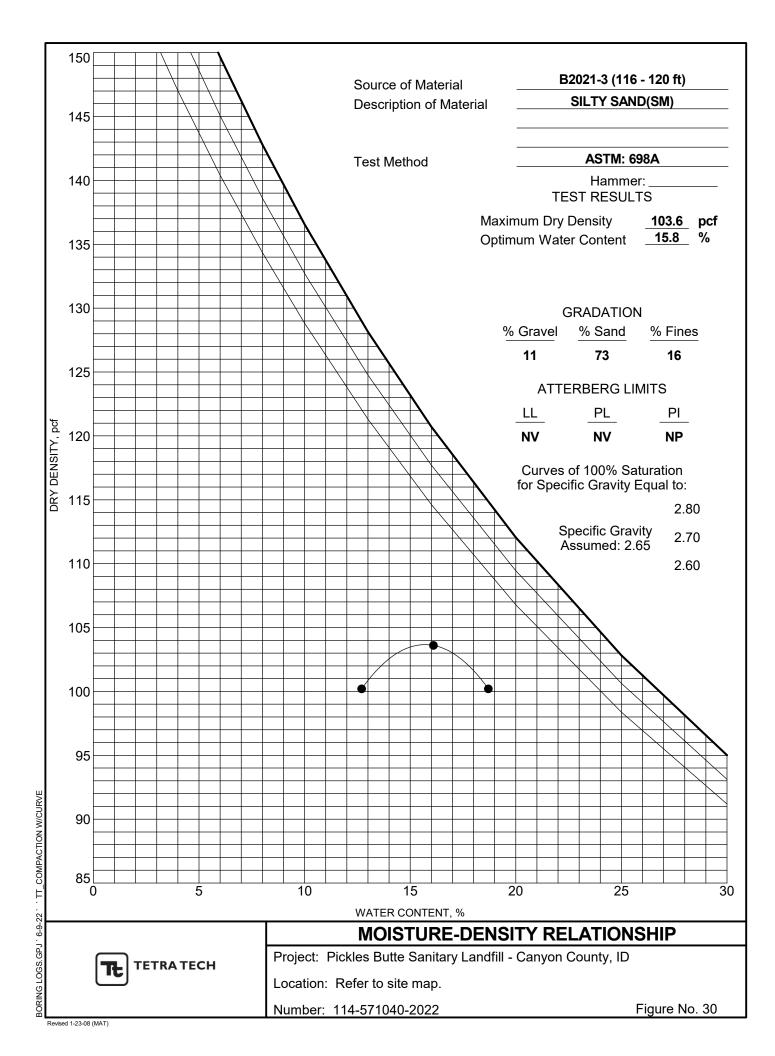


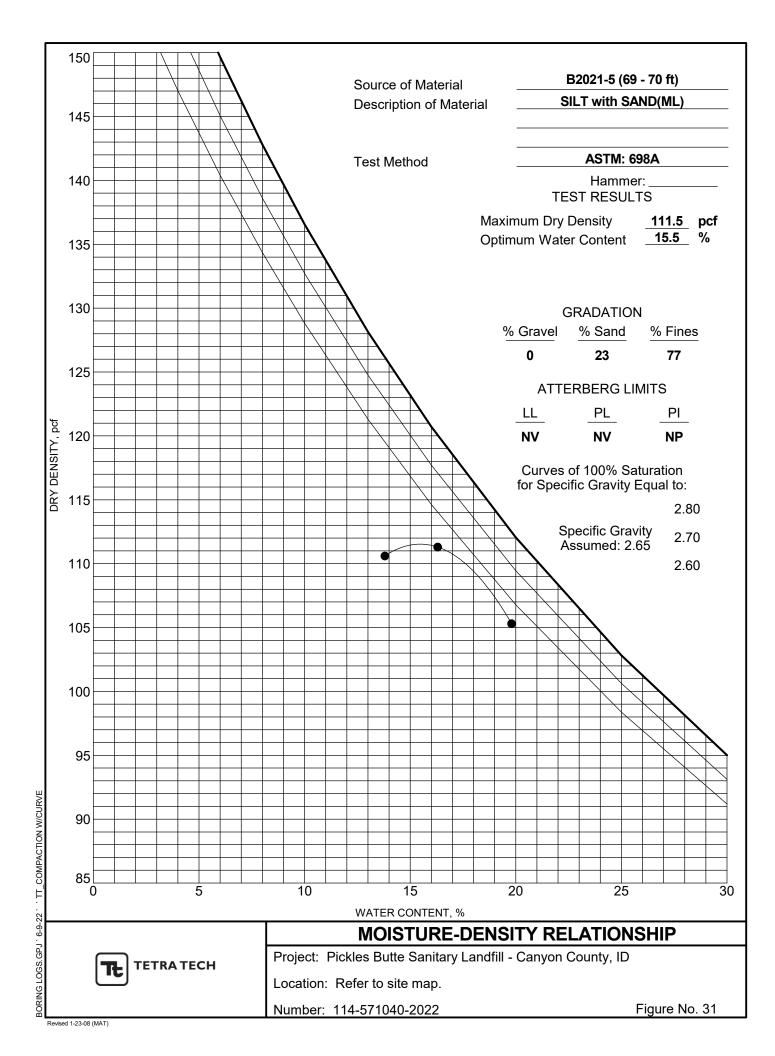


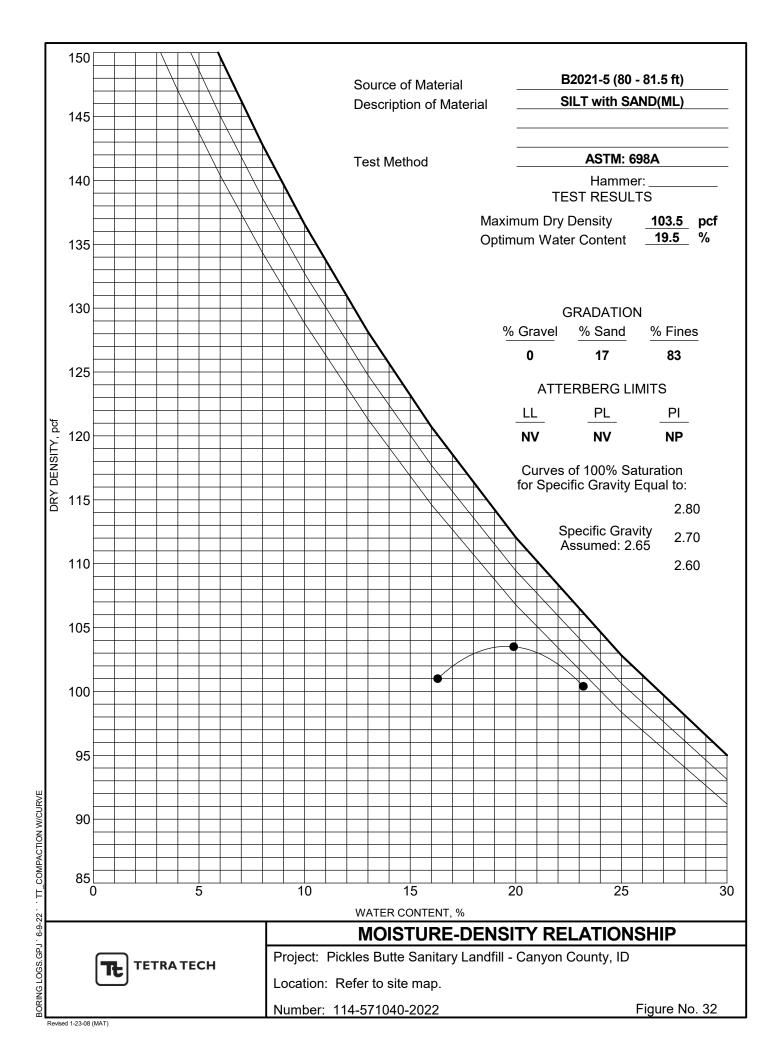
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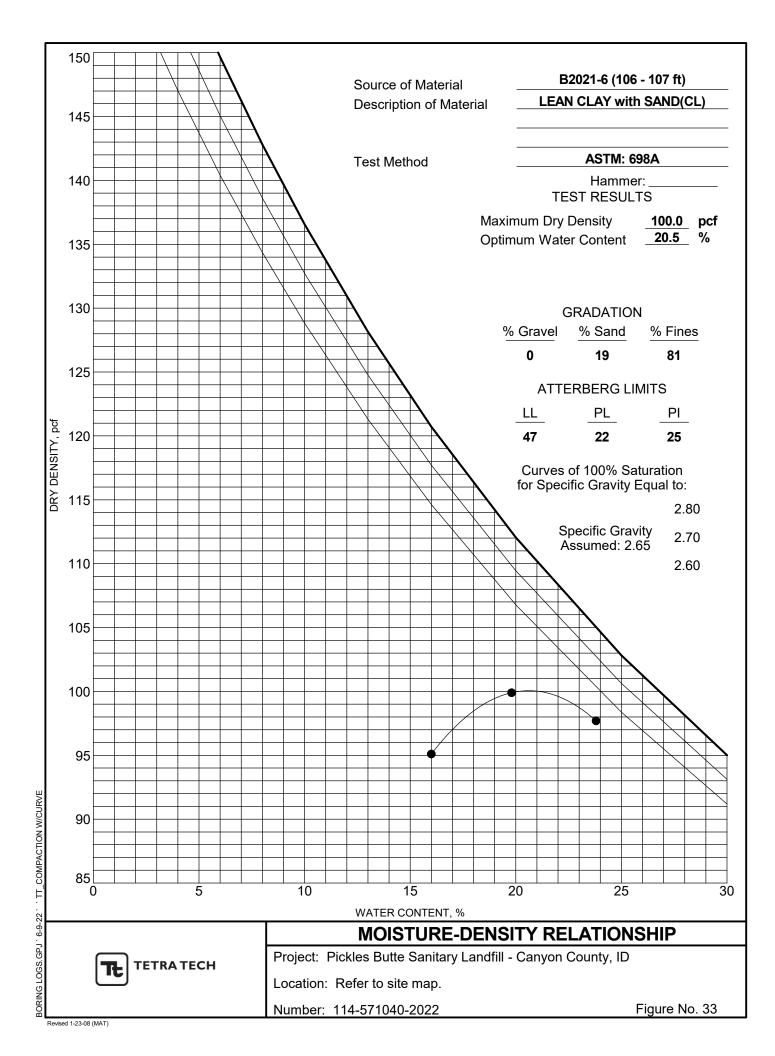


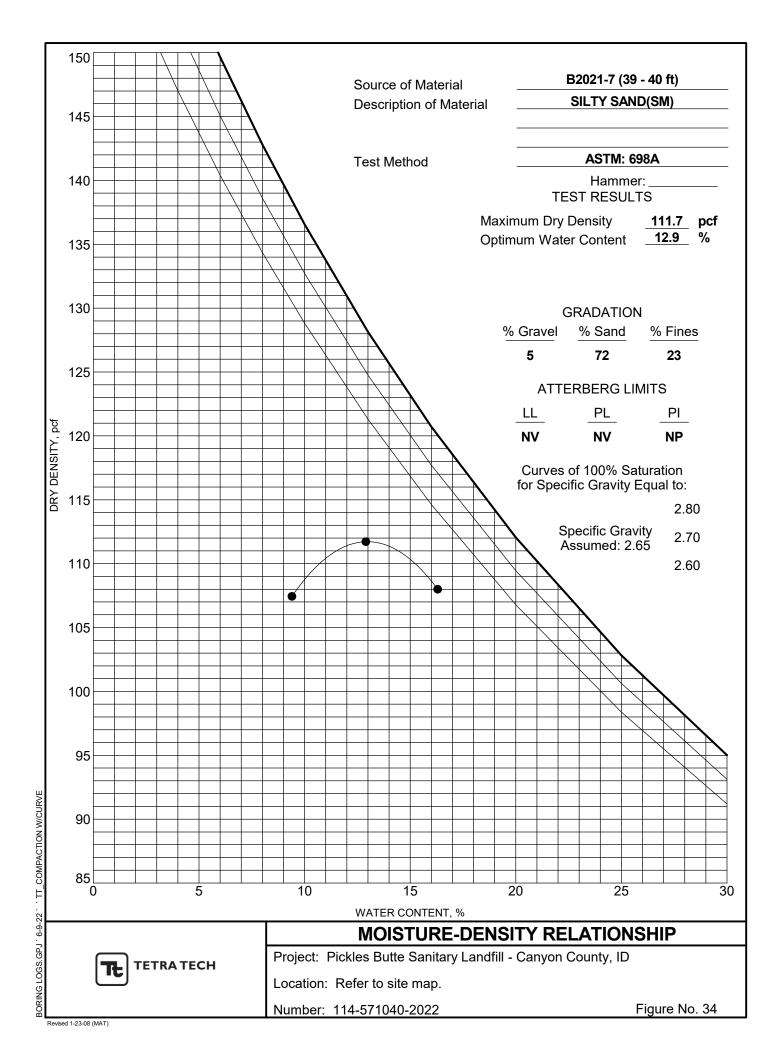
Revised 1-23-08 (MAT)

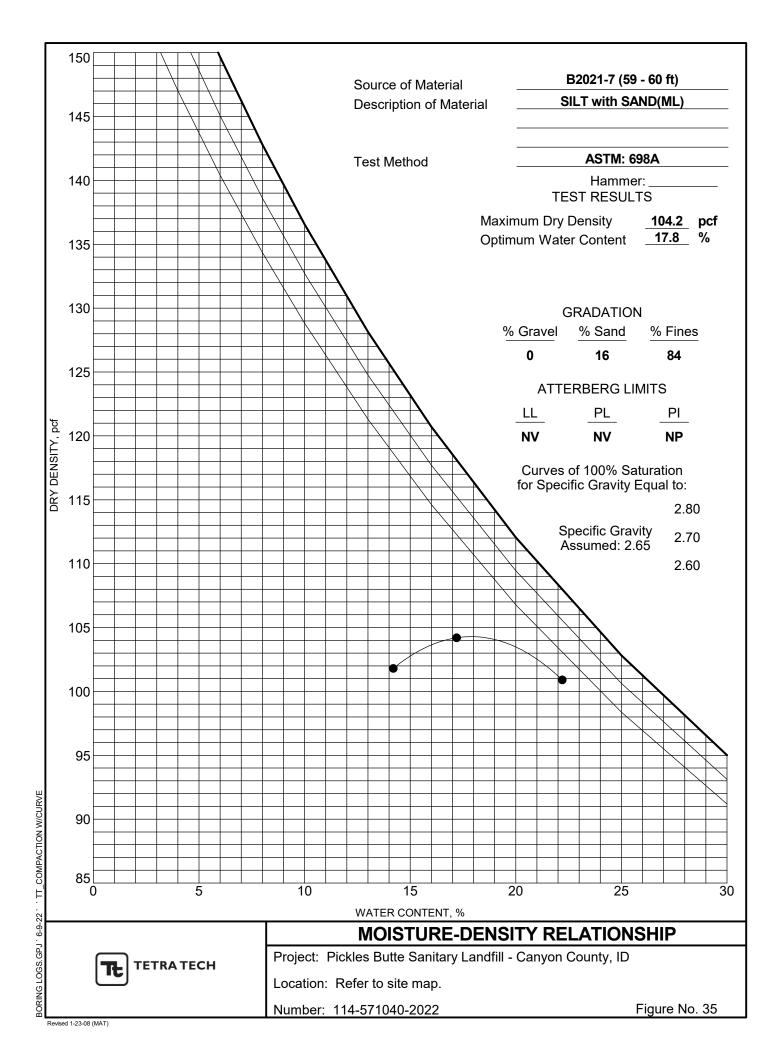


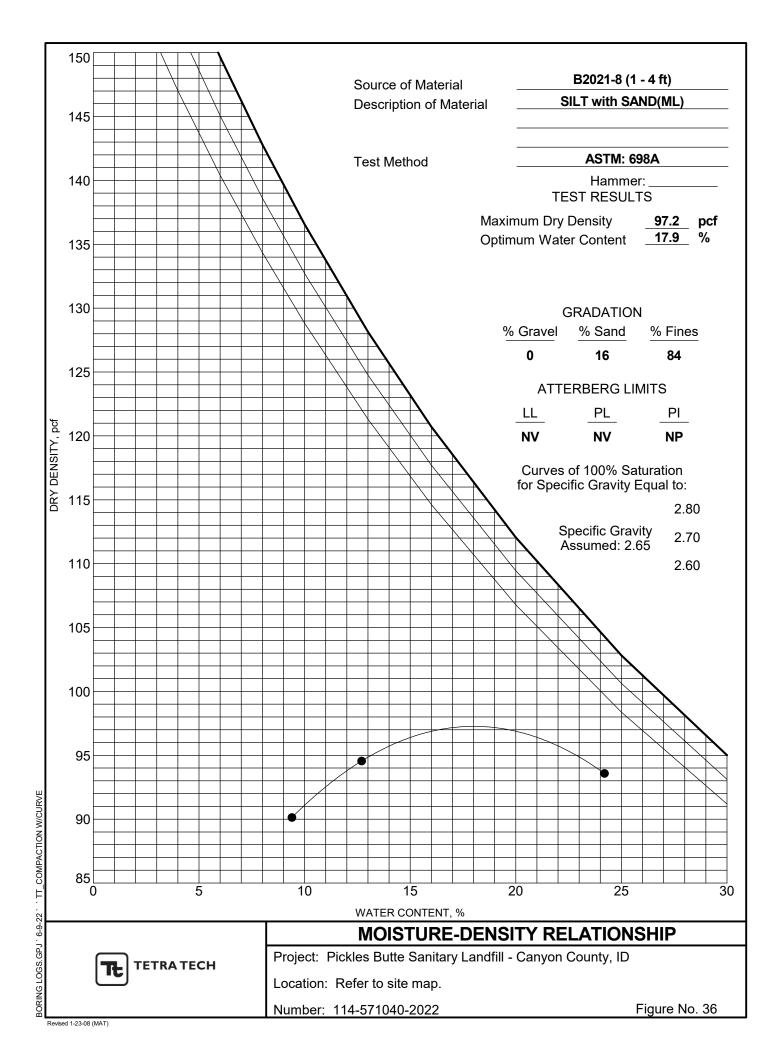


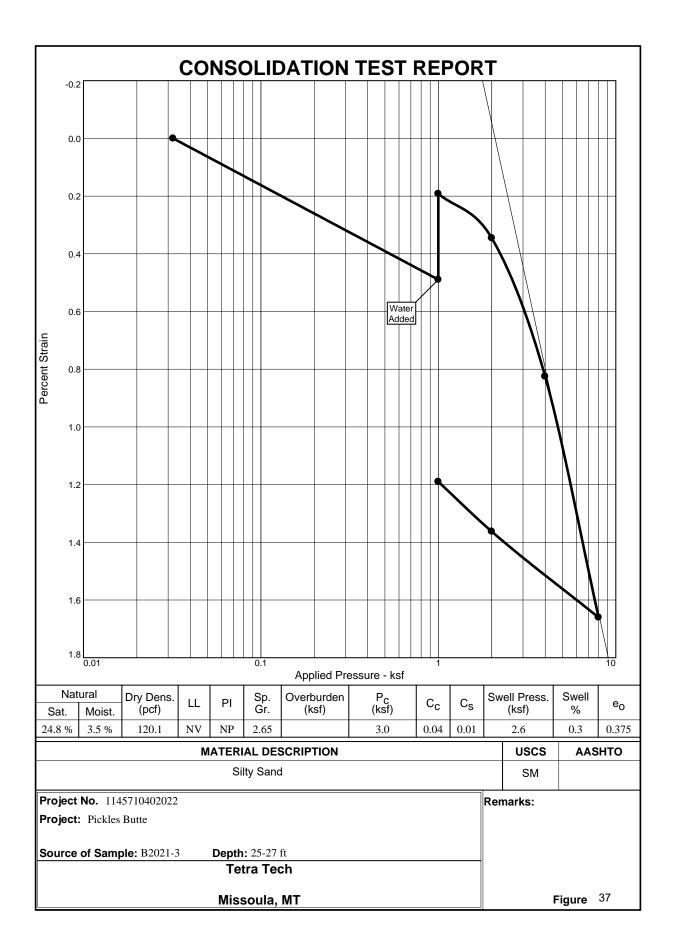


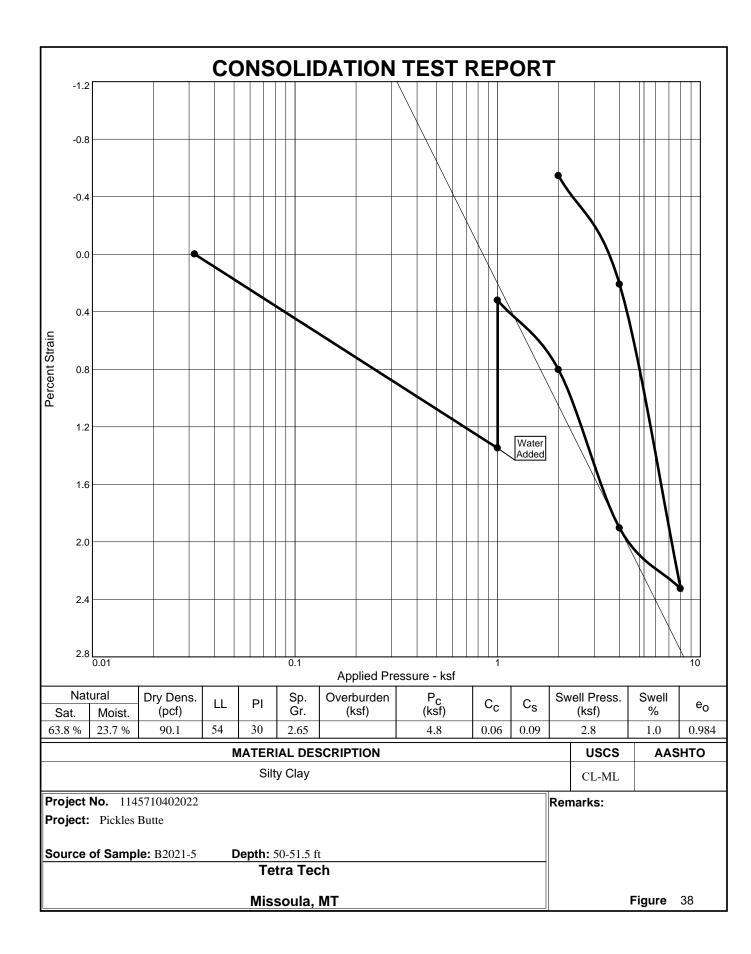


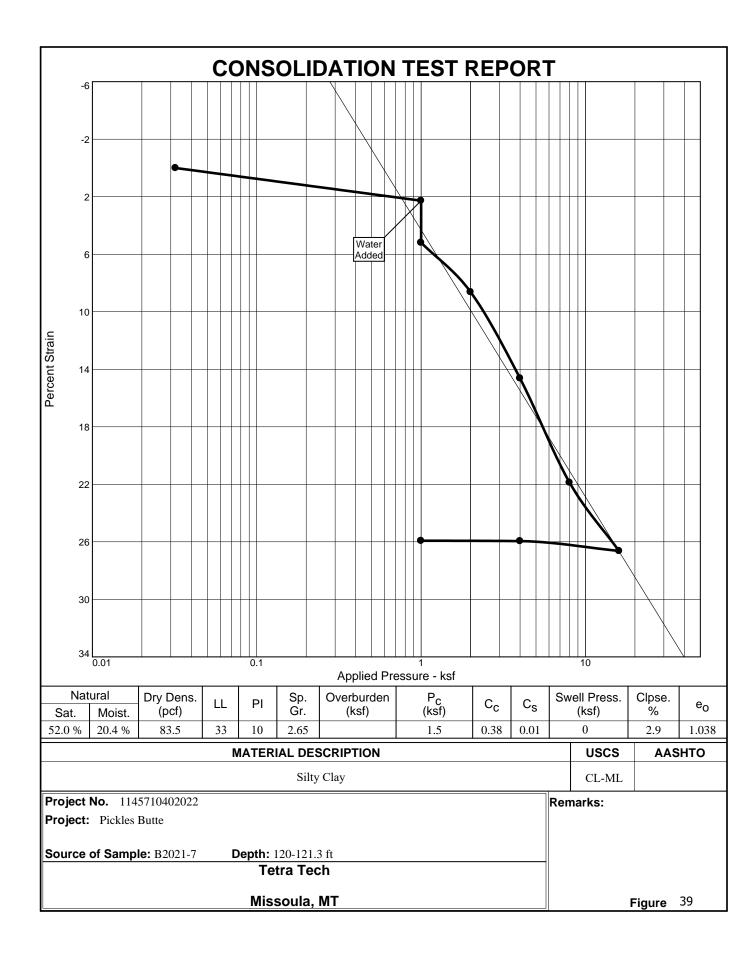


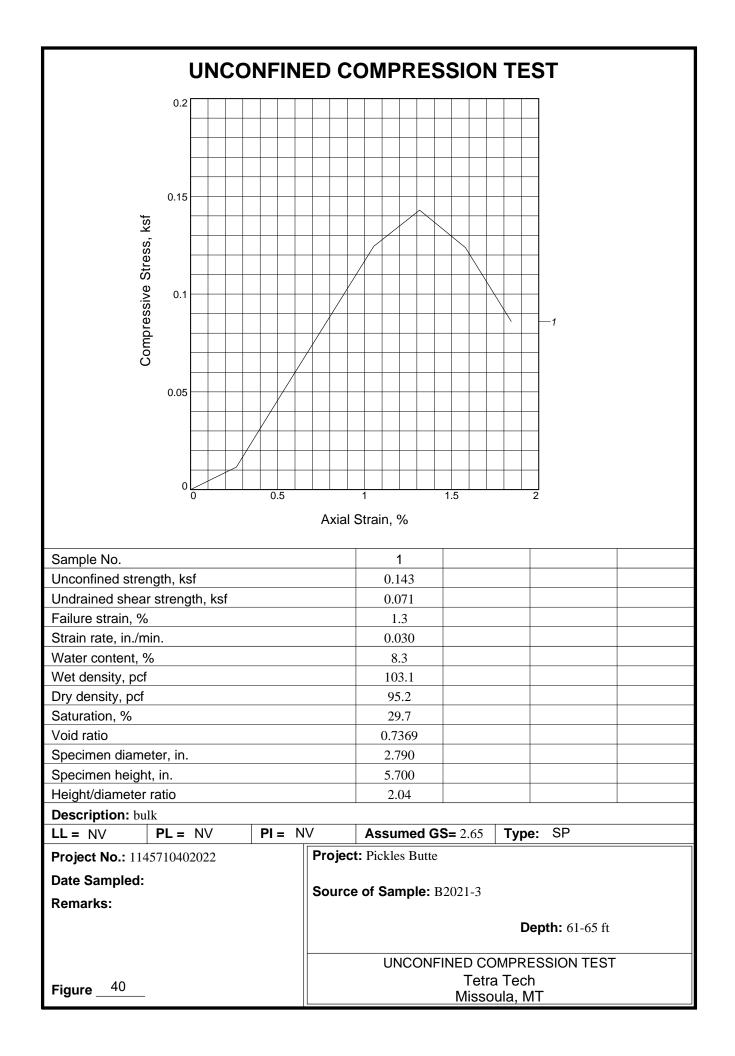


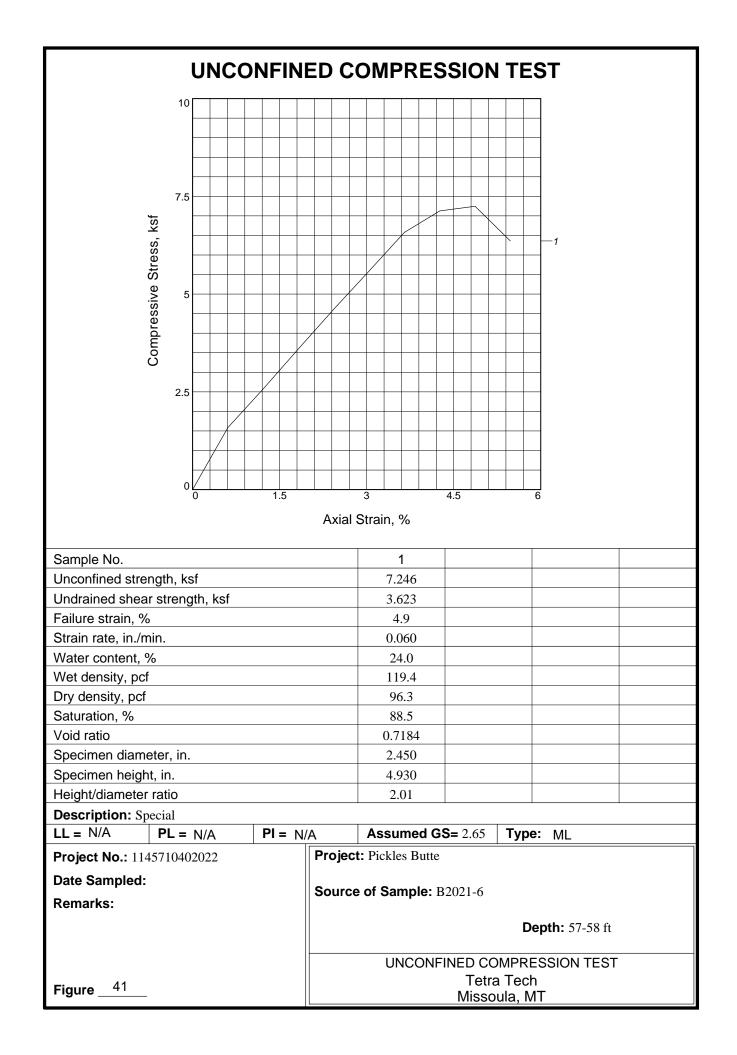


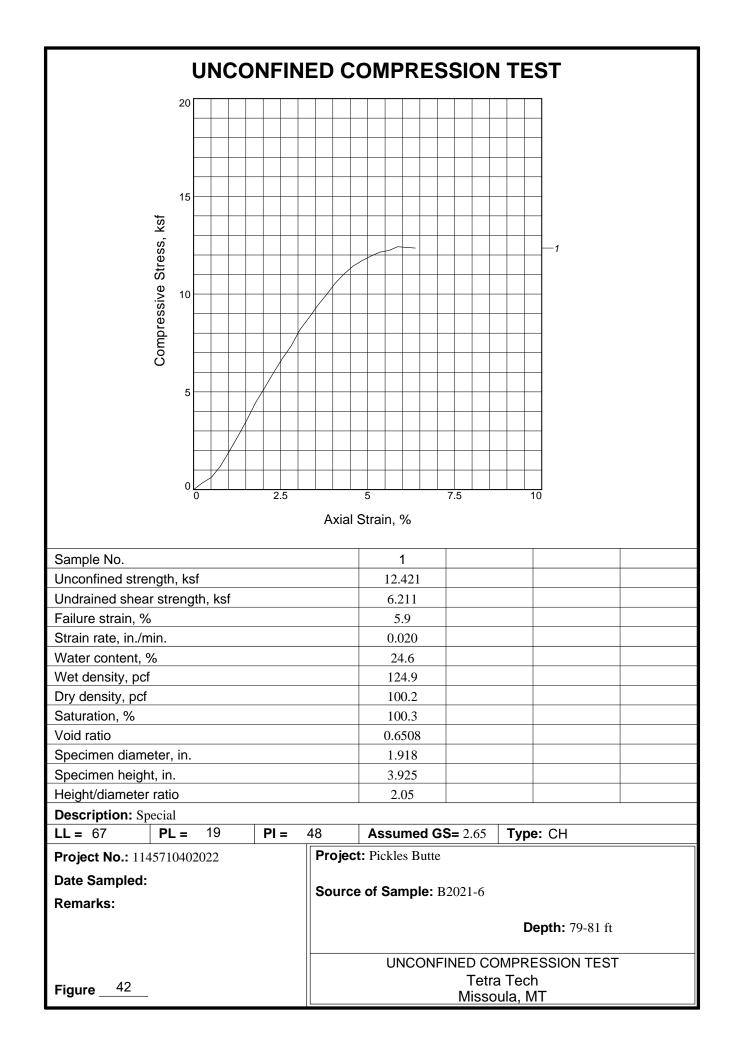


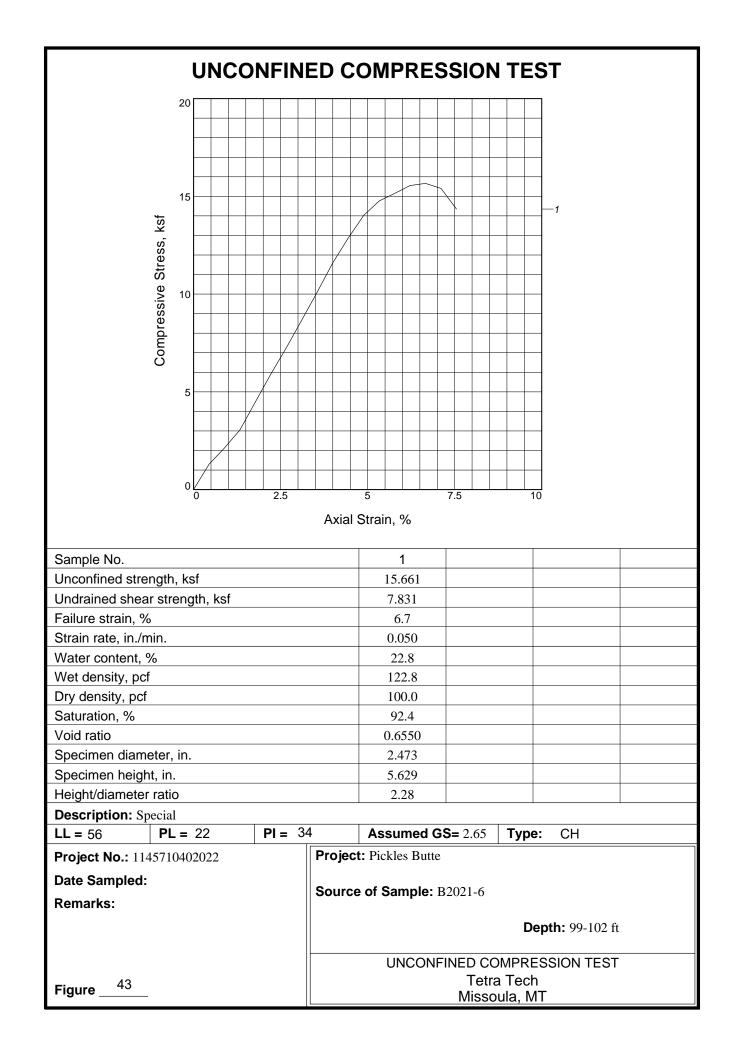


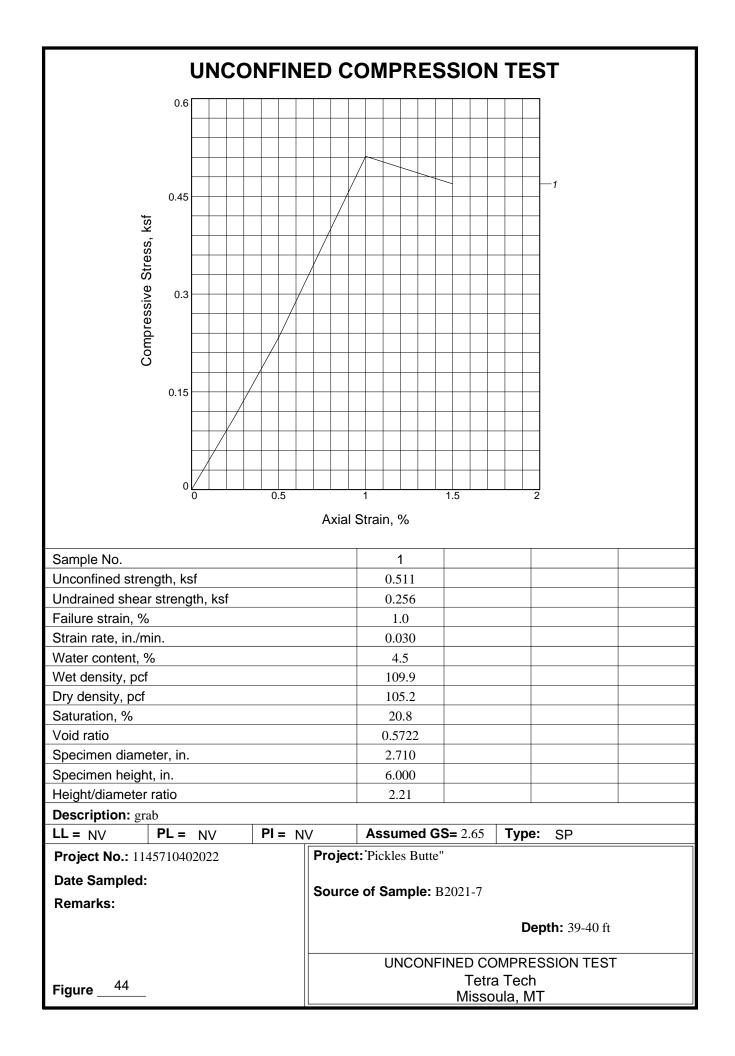


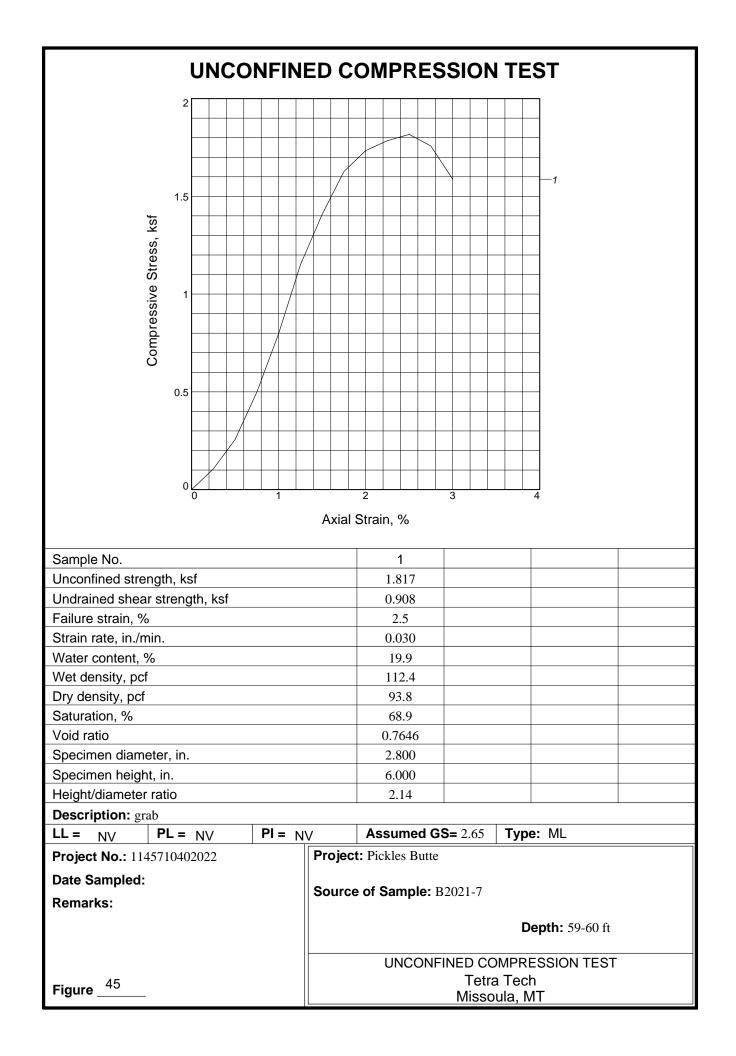


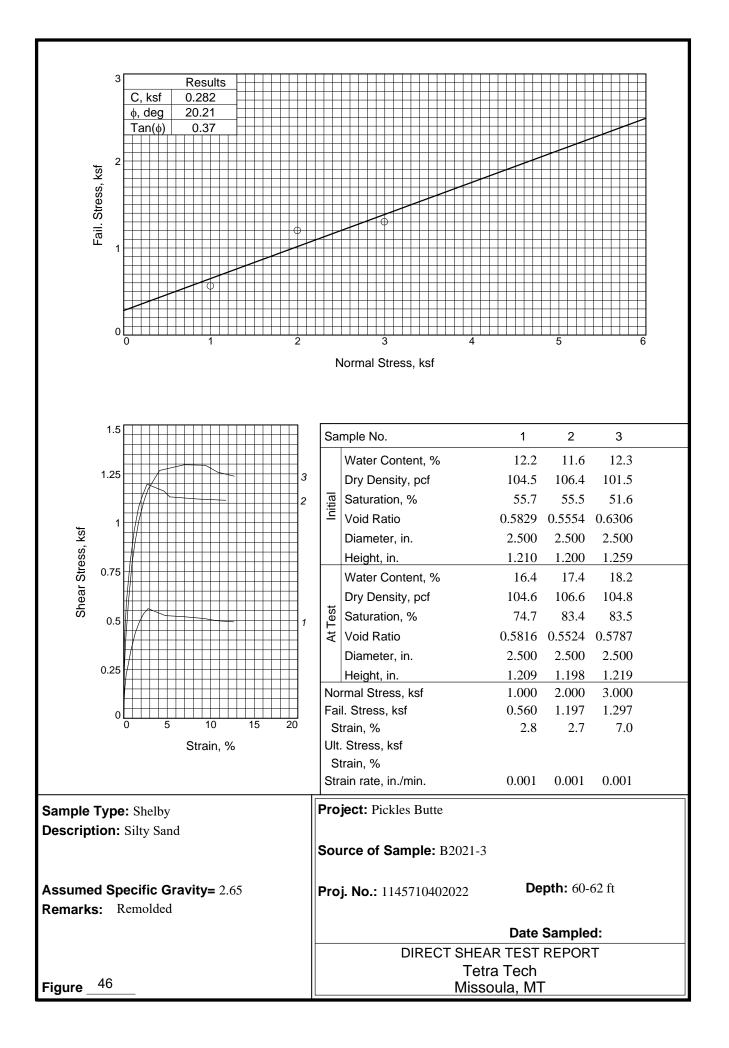


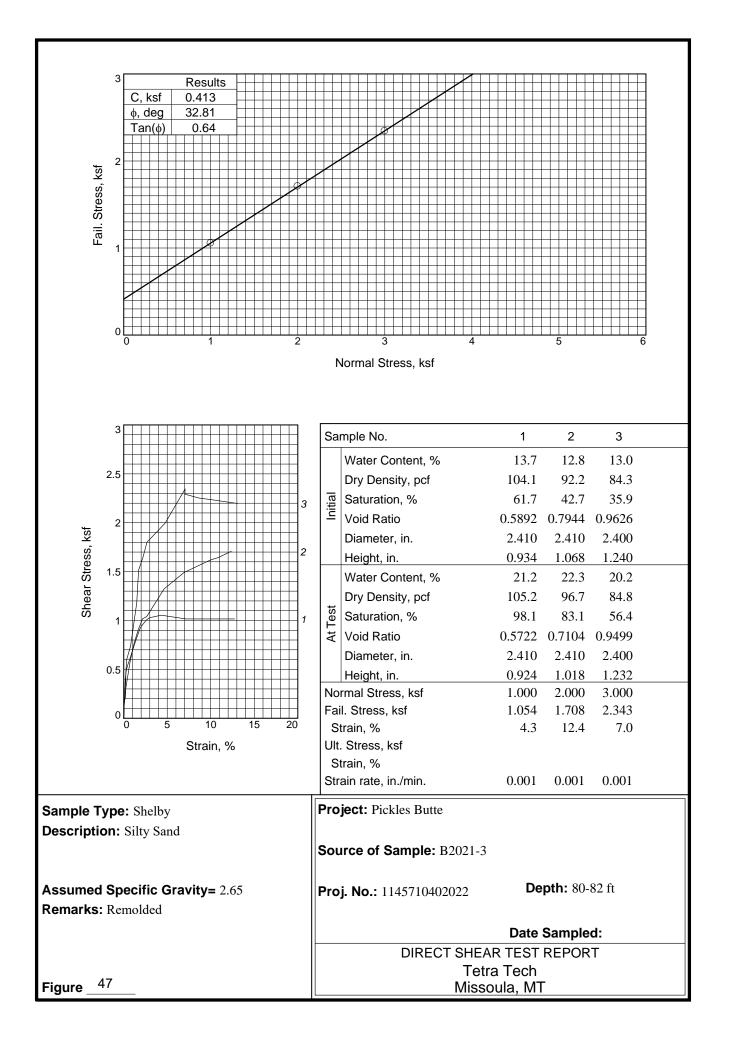


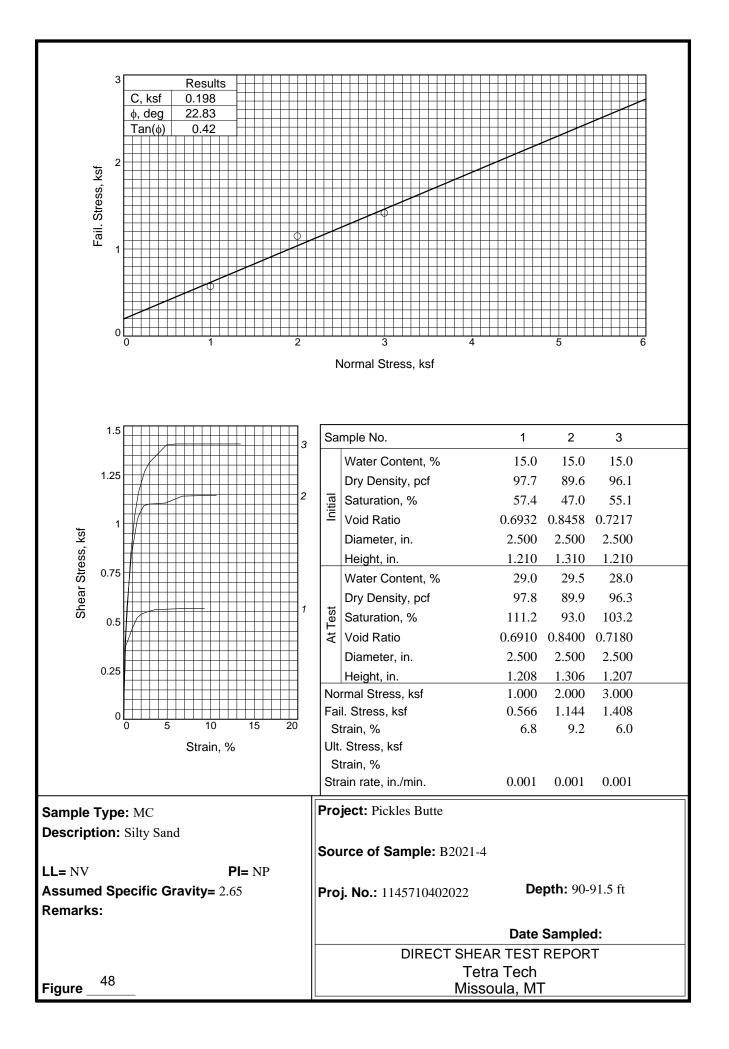


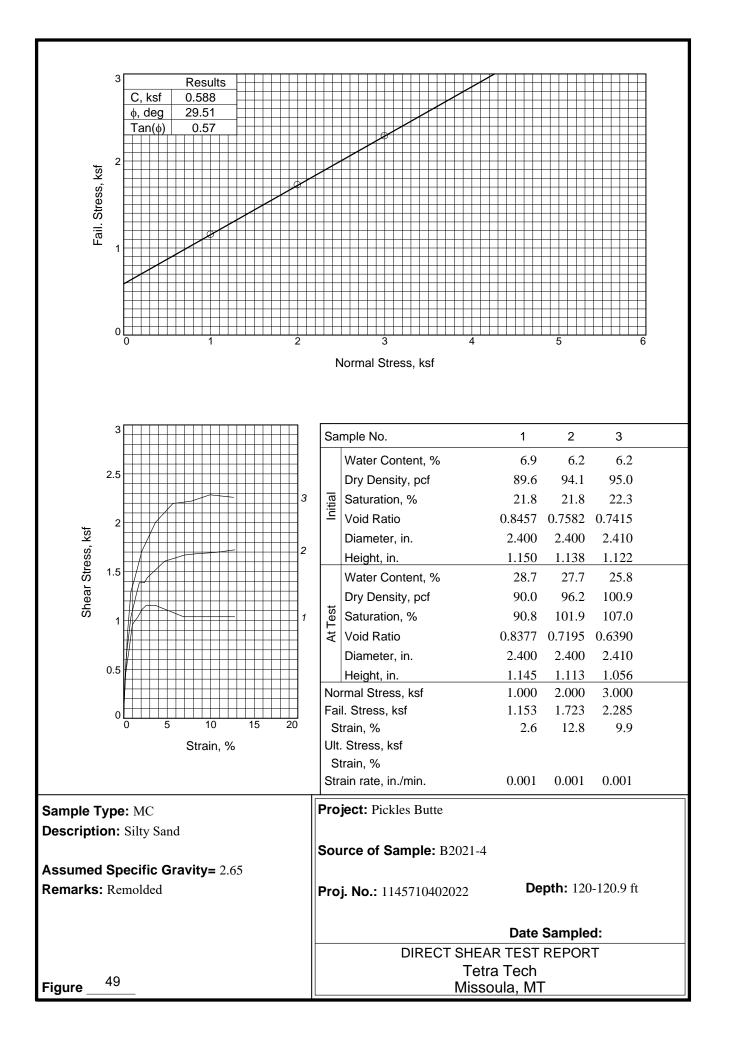


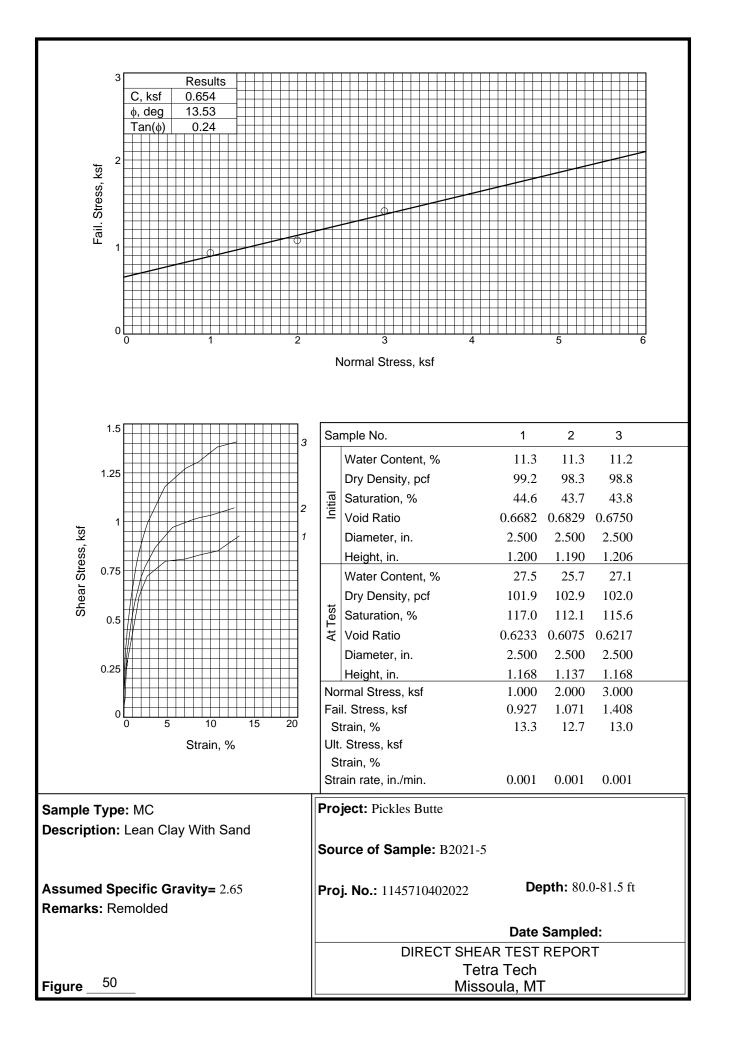


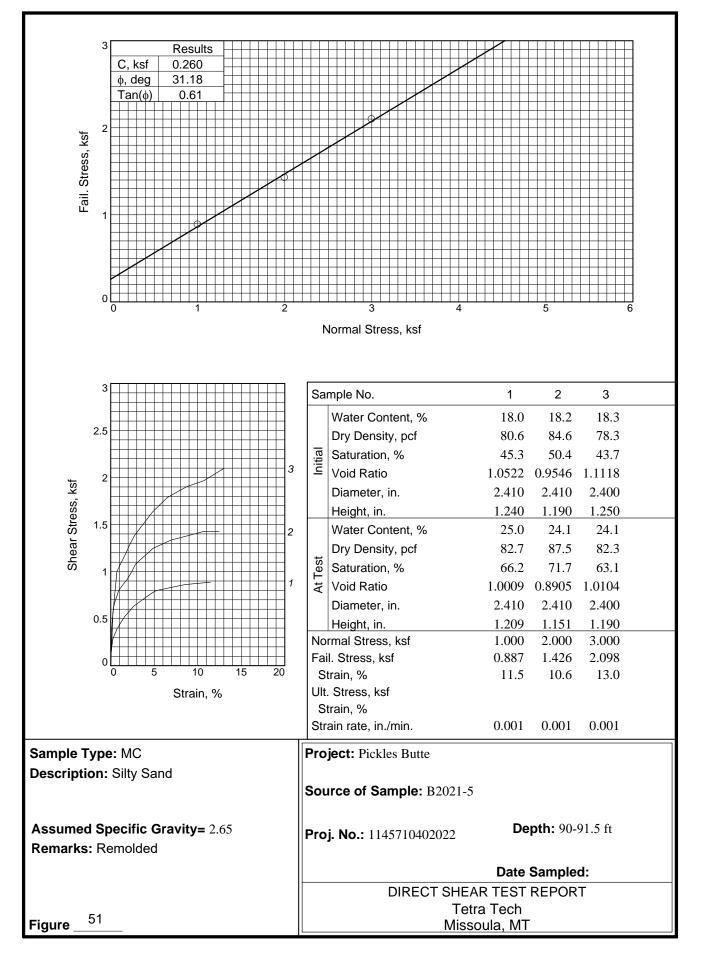


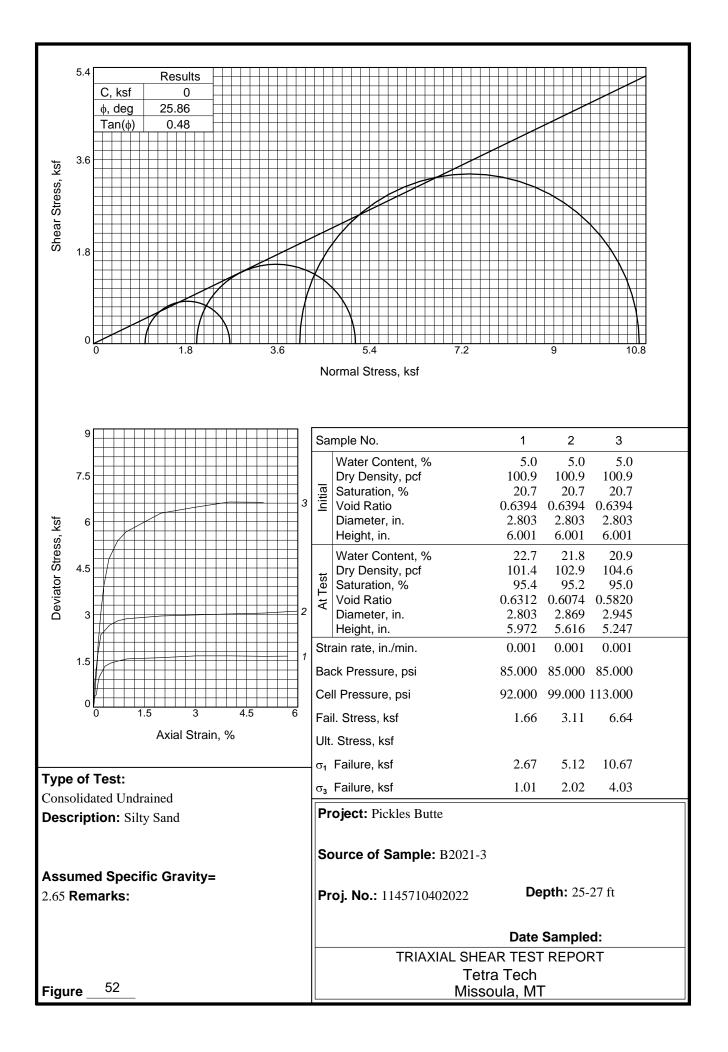


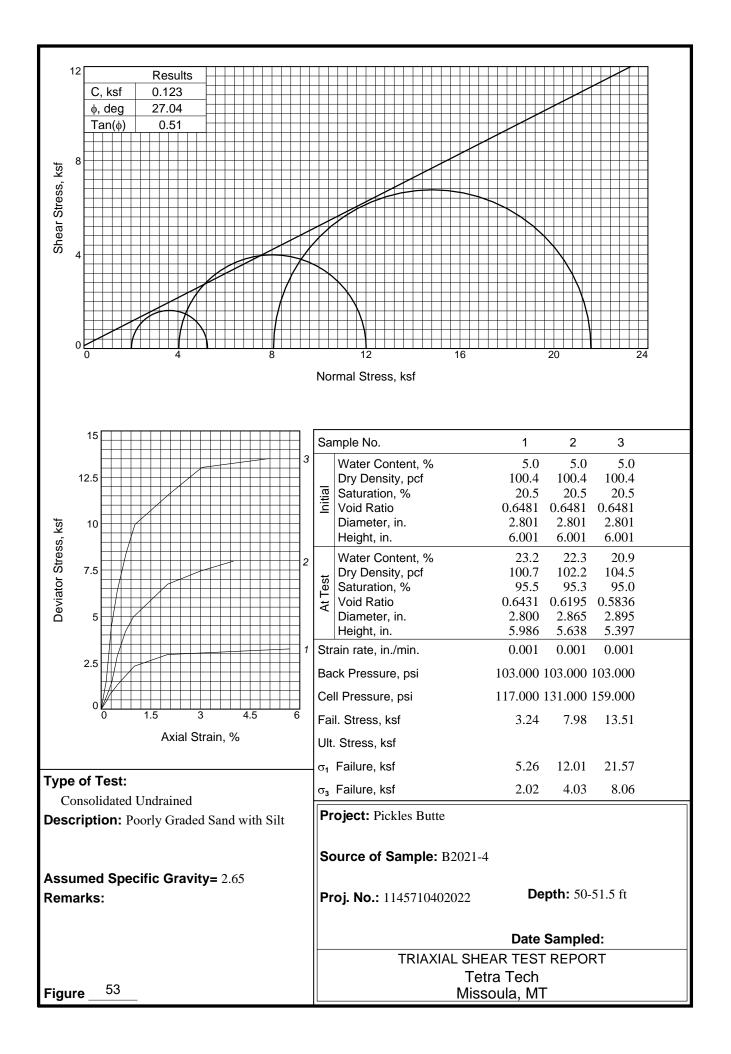


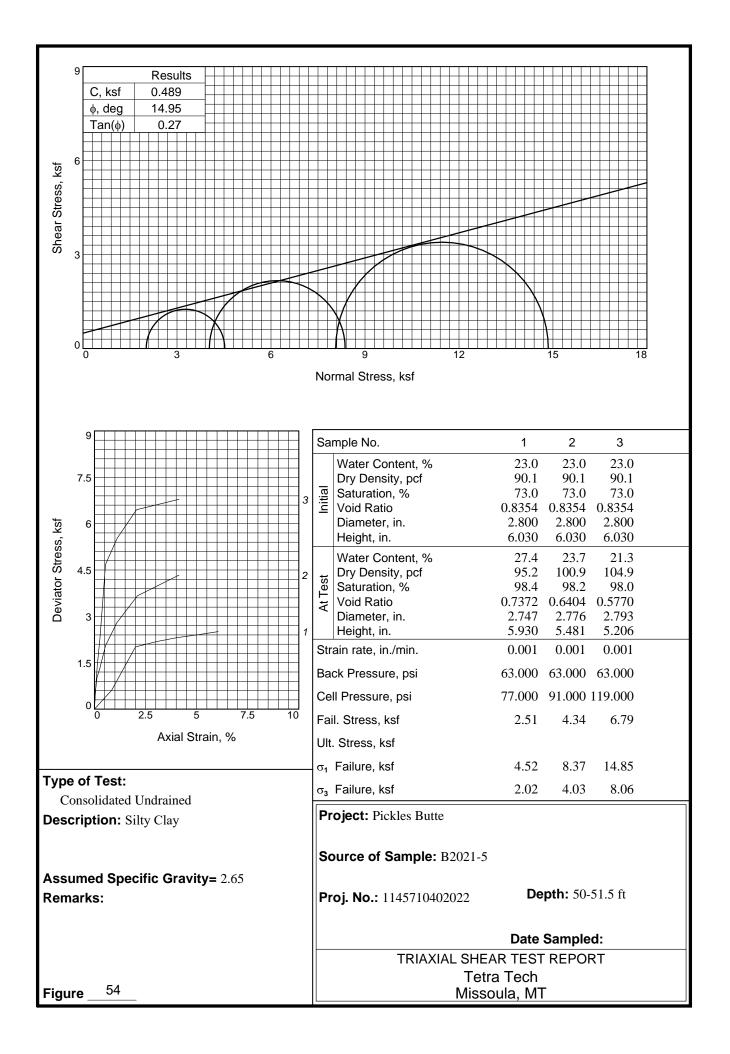


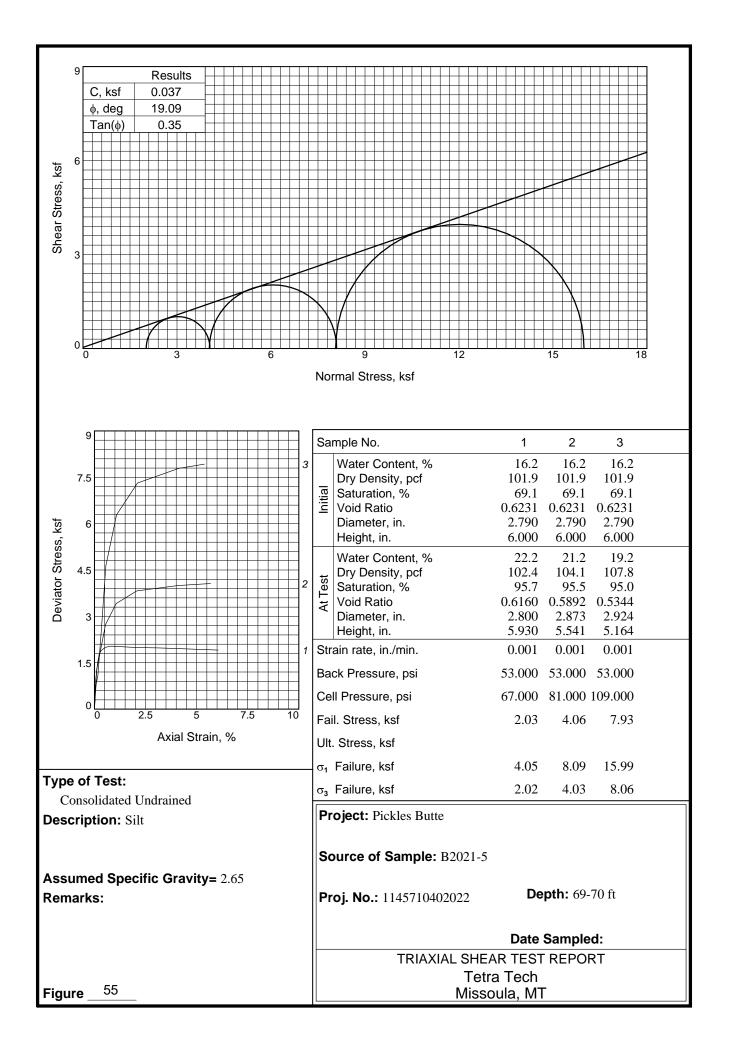


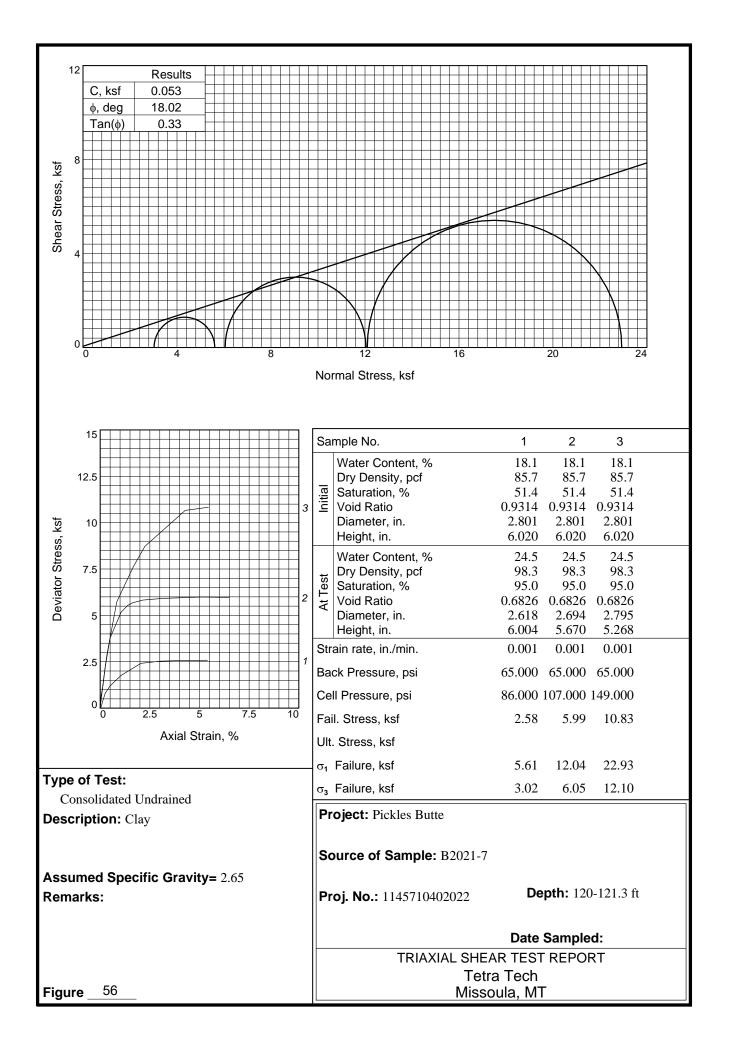














## SUMMARY OF LABORATORY RESULTS

PAGE 1 OF 8

PROJEC	PROJECT NUMBER P														PROJECT NAME _ Pickles Butte Sanitary Landfill - Canyon County, ID											
Boring Number B2021-1	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	Cc	Hd	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio	
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	0 - 1.5																					
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	2 - 3.5										9											
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	-		NV	NP		99.6	83.1	11.6	110	109.9		10.5										
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	4 - 5.5																					
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	6 - 7.5										8											
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	8 - 9.5																					
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	10 - 11.5										6											
B2021-1 B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	15 - 16.5										5											
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	20 - 21.5																					
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	25 - 27		NV	NP		99.9	94.7	6.2	113								0.03					
5 B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	27 - 28.5																					
B2021-1	11/15/2021	43.502927	-116.624204	2740.3976	30 - 31.5																					
	11/16/2021	43.501658	-116.713829	2739.0394	0 - 1.5										7											
B2021-2 B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	2 - 3.5																					
B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	4 - 5.5										3											
B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	6 - 7.5																					
B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	8 - 9.5										3											
B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	10 - 11.5																					
B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	15 - 16.5										5											
B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	20 - 21										3											
B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	25 - 26.5																					
B2021-2	11/16/2021	43.501658	-116.713829	2739.0394	30 - 31.5																					
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	5 - 6.5																					
В2021-3	11/22/2021	43.500874	-116.716768	2737.6687	10 - 11.5																					
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	15 - 16.5																					
E B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	20 - 21.5										3											
B2021-3 B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	25 - 27		NV	NP		99.8	97.7	31.3					25.86	0			0.04					
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	26 - 30																					



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PROJEC		<b>R</b> <u>114-571040</u>	-2022										Р	ROJE			Pickles	Butte	Sanitary	Landfill -	- Can	yon C	County	', ID	
Boring Number B2021-3	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	Cc	Hd	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	27 - 28.5																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	30 - 31.5										3										
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	35 - 36.5																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	40 - 41.5																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	45 - 46.5																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	50 - 51.5										3										
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	60 - 62		NV	NP		99.4	97.9	19.2					20.21	0.282							
B2021-3 B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	61 - 65		NV	NP		99.6	99.1	7.7	100	100.2		13.7			0.143						
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	70 - 71.5																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	80 - 82		NV	NP		99.8	99.1	23.6					32.81	0.413							
<u>5</u> В2021-3	11/22/2021	43.500874	-116.716768	2737.6687	82 - 83.5										2										
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	90 - 91.5																				
В2021-3	11/22/2021	43.500874	-116.716768	2737.6687	100 - 100.2																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	101 - 107																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	110 - 110.7																				
в2021-3	11/22/2021	43.500874	-116.716768	2737.6687	112 - 115																				
z B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	116 - 120		NV	NP		86.4	81.7	16.1	104	103.6		15.75									
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	121 - 121.8										4										
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	135 - 138																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	139 - 142																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	140 - 141.5																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	147 - 151																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	150 - 151.5																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	159 - 161																				
B2021-3	11/22/2021	43.500874	-116.716768	2737.6687	160 - 161.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	5 - 6.5										6										
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	9 - 10																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	10 - 11.5																				



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PROJEC		<b>R</b> <u>114-571040</u>	)-2022										P	ROJE	CT NA	ME F	Pickles	Butte	Sanitary	Landfill -	Can	yon C	county	, ID	
Boring Number	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	cc	Hd	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	15 - 16.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	20 - 21.5										5										
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	25 - 26.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	30 - 31.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	35 - 36.5										8										
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	40 - 41.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	44 - 45																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	45 - 46.5										16										
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	50 - 51.5		NV	NP		100	91.9	6.3					27.04	0.123							
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	51 - 52																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	60 - 61.5										2										
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	69 - 70																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	70 - 71.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	79 - 80																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	80 - 81.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	89 - 90																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	90 - 91.5		NV	NP		99	96	38.4					22.83	0.198							
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	98 - 99																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	99 - 100.5										22										
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	109 - 110																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	110 - 111.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	119 - 120																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	120 - 120.9		NV	NP		100	98.1	49					29.51	0.588							
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	129 - 130																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	130 - 131.5																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	139 - 140																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	140 - 141.5										2										
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	149 - 150																				



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PROJEC		<b>R</b> <u>114-571040</u>	-2022										P	ROJE		ME _F	Pickles	Butte	Sanitary	Landfill -	Can	yon C	ounty	, ID	
Boring Number B2021-4	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	cc	Н	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	150 - 150.9																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	157 - 159																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	160 - 160.9																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	169 - 170																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	170 - 170.8																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	175 - 177																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	179 - 180																				
B2021-4	12/14/2021	43.665364	-116.688388	2797.1687	189 - 190																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	5 - 6.5										4										
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	9 - 10																				
5 B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	10 - 11.5																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	15 - 16.5										3										
	12/19/2021	43.499133	-116.713491	2661.6331	19 - 20																				
B2021-5 B2021-5 B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	20 - 21.5																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	27 - 28																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	30 - 31.5																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	35 - 36.5										4										
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	39 - 40																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	40 - 41																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	45 - 46.5																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	49 - 50																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	50 - 51.5		54	30									14.95	0.489			0.06				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	59 - 60																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	60 - 60.6										4										
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	69 - 70		NV	NP		99.9	99.3	77.1	112	111.5		15.5	19.09	0.037							
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	70 - 71.5										29										
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	79 - 80																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	80 - 81.5		35	14	0.000	98.5	95.9	83.4	104	103.5	21	19.5	31.18	0.26							



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PROJEC		<b>R</b> <u>114-571040</u>	-2022										P	ROJE			Pickles	Butte	Sanitary	Landfill -	Can	yon C	County	, ID	
Boring Number B2021-5	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	Cc	Hd	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	89 - 90																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	90 - 90.8		NV	NP			98.8	33.8					13.53	0.654							
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	99 - 100										11										
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	100 - 101.3																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	109 - 110																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	110 - 110.6																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	119 - 120																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	120 - 121.5																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	126 - 127																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	130 - 131.4																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	139 - 140																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	140 - 140.9																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	149 - 150																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	150 - 151.4																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	159 - 160																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	160 - 160.6																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	169 - 170																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	170 - 171.5																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	174 - 175																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	179 - 180																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	189 - 190																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	199 - 200																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	204 - 205																				
B2021-5	12/19/2021	43.499133	-116.713491	2661.6331	209 - 210																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	5 - 6.5																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	9 - 11																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	10 - 11.5										6										
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	20 - 21.5																				1



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PROJEC		<b>R</b> <u>114-571040</u>	-2022										P	ROJE			Pickles	Butte	Sanitary	Landfill -	Can	yon C	County	<u>, ID</u>	
Boring Number	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	Cc	Hq	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	25 - 26.5										18										
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	39 - 41																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	40 - 41.5										22										
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	45 - 46.5																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	50 - 51.5																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	57 - 58														7.246						
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	59 - 61																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	60 - 61.5										25										
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	68 - 69																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	69 - 71																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	70 - 71.5																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	75 - 76																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	79 - 81		67	48			99.8	90.7													
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	80 - 81.1																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	84 - 85																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	89 - 91																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	90 - 91.5																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	99 - 102		56	34			99.8	89.7							15.661						
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	100 - 101.5																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	106 - 107		47	25		99.2	97.6	80.8	100	100		20.5									
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	110 - 111.5										21										
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	120 - 121.5										22										
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	129 - 130																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	130 - 131.3																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	140 - 141.5																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	149 - 150																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	150 - 151.4																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	159 - 160																				1



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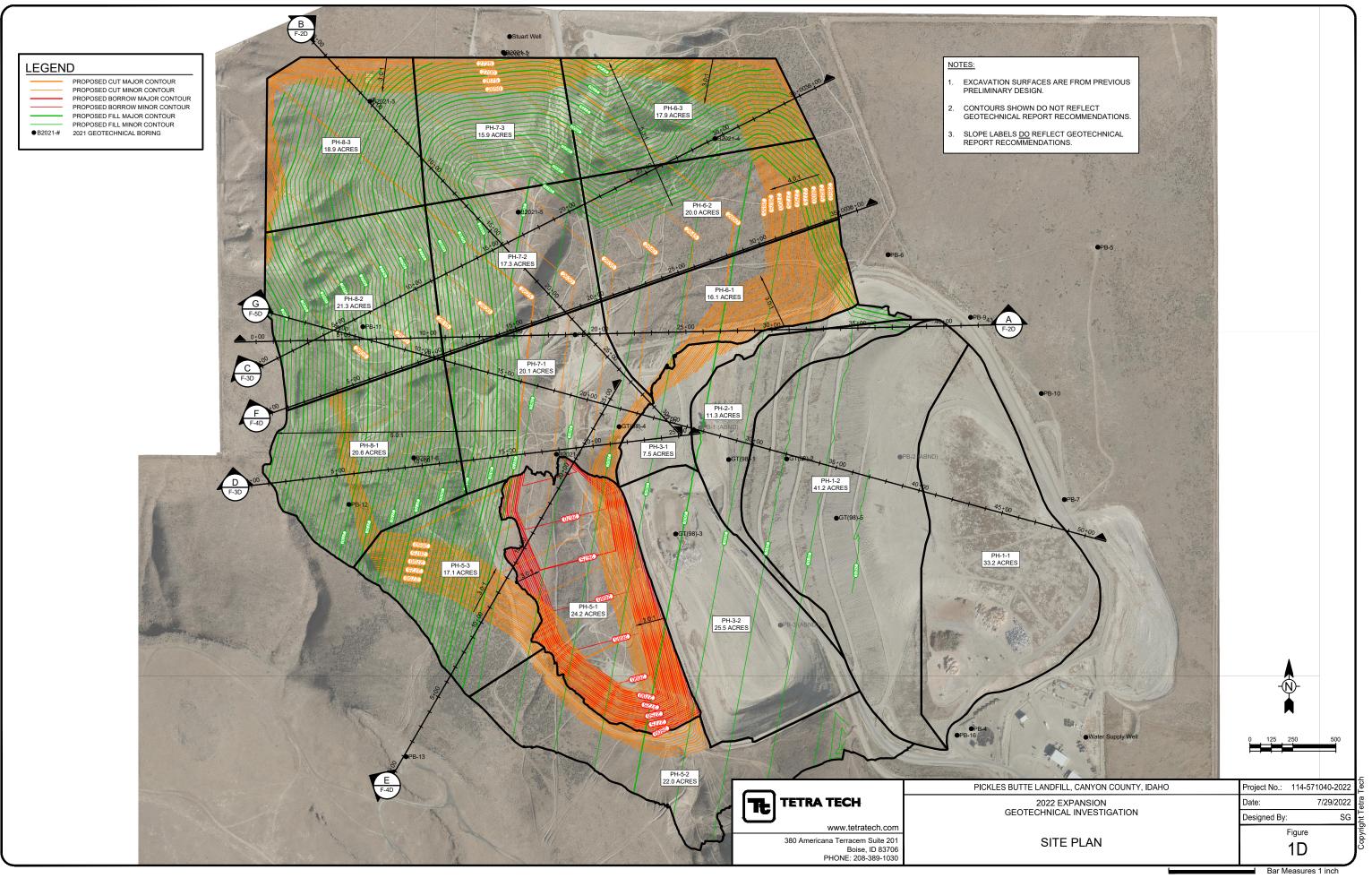
PROJEC		<b>R</b> <u>114-571040</u>	-2022										Р	ROJE			Pickles	Butte	Sanitary	Landfill -	Can	yon C	county	, ID	
Boring Number B2021-6	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	Cc	Hd	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	160 - 161.3																				
B2021-6	12/2/2021	43.495196	-116.715718	2636.7423	164 - 165																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	5 - 6.5										4										
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	10 - 11.5																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	15 - 16.5																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	19 - 20																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	25 - 26.5																				
B2021-7 B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	30 - 30.6																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	35 - 35.8																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	39 - 40		NV	NP		93.6	92	23.3	112	111.7		12.9			0.511						
5 B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	40 - 41.4										23										
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	45 - 46.5																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	49 - 50																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	50 - 51.5																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	59 - 60		NV	NP		99.9	98.9	84.3	104	104.2		17.8			1.817						
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	60 - 61.4										12										
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	69 - 70																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	70 - 71.5																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	79 - 80																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	80 - 80.7																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	89 - 90																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	90 - 90.3																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	99 - 100																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	100 - 101.5										20										
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	110 - 111.5																				
E B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	120 - 121.3		33	10									18.02	0.053			0.38				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	125 - 126																				
6 B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	129 - 130																				

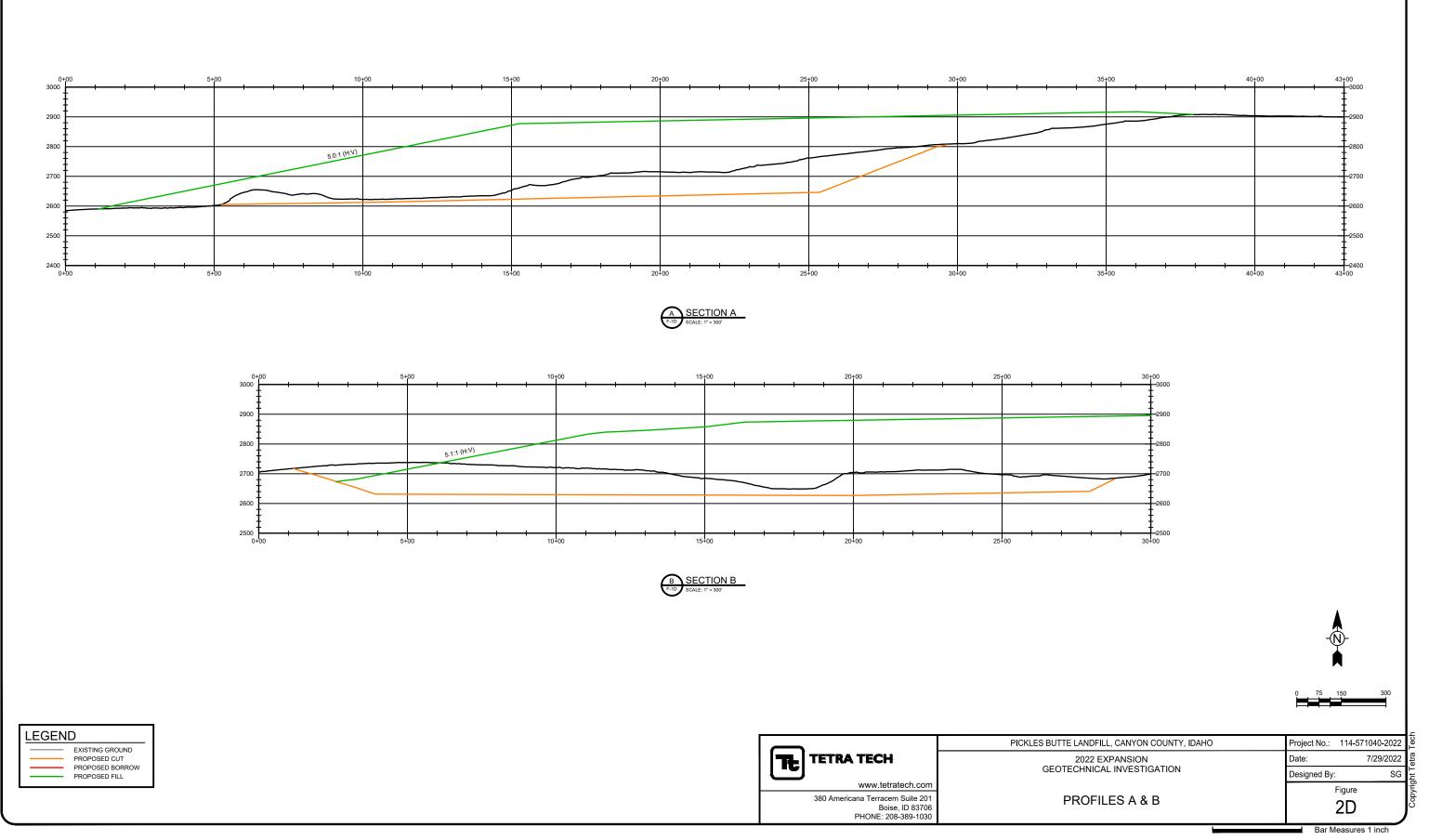
PAGE 8 OF 8

PROJEC		<b>R</b> <u>114-571040</u>	-2022											ROJEC	JT NA		vickles	Butte	Sanitary	Landfill -	Cany	/on C	ounty		_
Boring Number	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	Cc	Н	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	130 - 131.5										19										
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	139 - 140																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	140 - 141.5										24										
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	149 - 150																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	150 - 151.5																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	160 - 161.4																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	169 - 170																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	170 - 171.5																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	179 - 180																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	189 - 190																				
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	199 - 200																				
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	0 - 1.5										11										
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	1 - 4		NV	NP		98.7	95.6	83.5	97	97.2		17.9									
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	2 - 3.5																				
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	4 - 5.5										11										
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	8 - 10										12										
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	10 - 11.5										6										
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	11 - 15																				
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	15 - 16.5										5										
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	20 - 21.5										5										

# APPENDIX D: Static Slope Stability Analyses

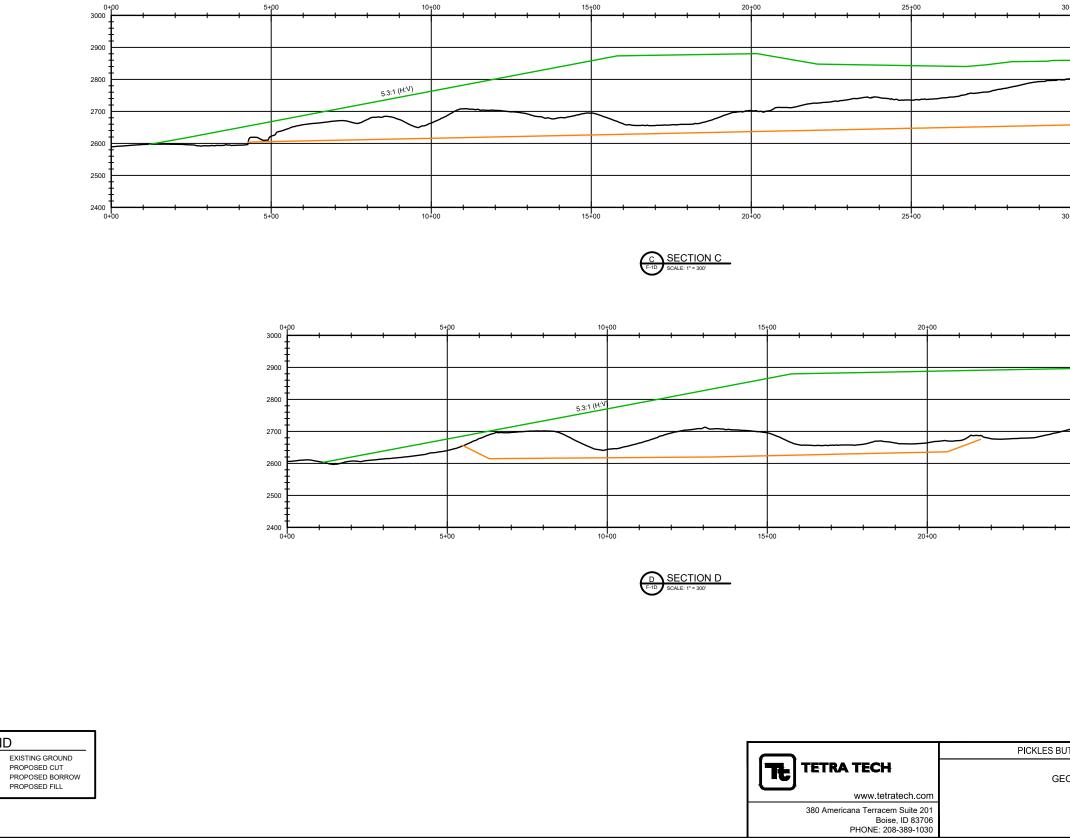
Slope Stability Cross Sections - Figures 1D thorough 5D Slope Stability Stability Analyses Printouts Figures 6D through 43D





IGURES DWG

LEGEND



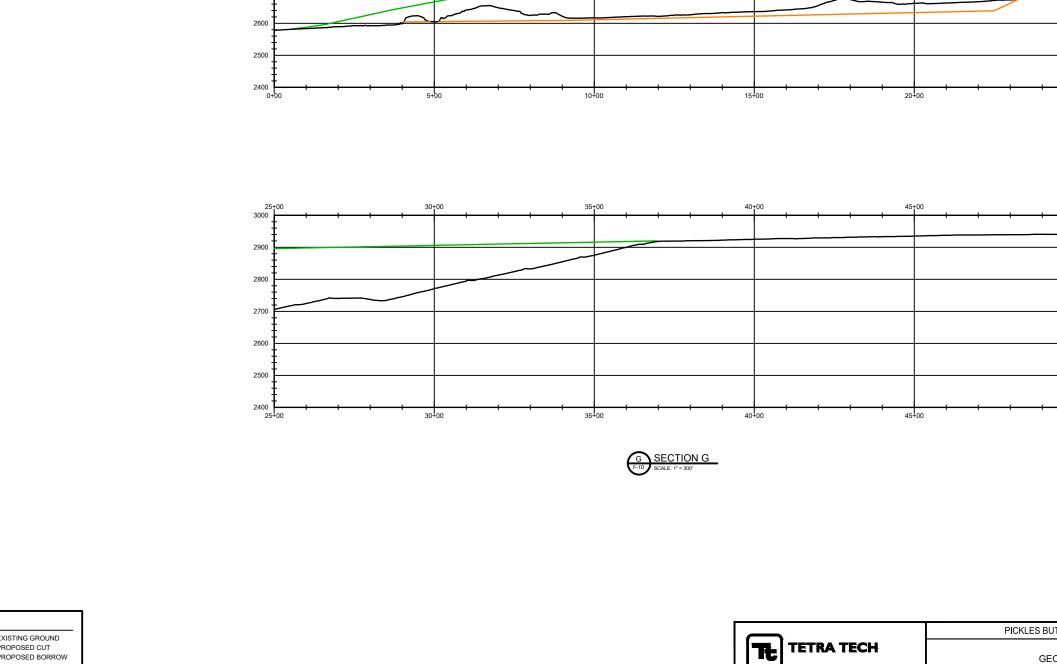
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PROFILES C & D		3D	Copy
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0+00 3200 5+00 10+00 15+00 <sup>20†00</sup> 3100 3000 2900 2800 2700 2600 2500 0+00 10+00 15+00 20+00 5+00 E SECTION E F-1D SCALE: 1" = 300' 15+00 25+00 0+00 3000 5+00 10+00 <sup>20†00</sup> 2900 2800 5.2:1 (H:V) 2700 2600 2500 2400 0+00 15+00 5+00 10+00 20+00 25+00 F-1D SCALE: 1" = 300' LEGEND PICKLES BU EXISTING GROUND PROPOSED CUT PROPOSED BORROW PROPOSED FILL TETRA TECH GEC www.tetratech.com

380 Americana Terracem Suite 201 Boise, ID 83706 PHONE: 208-389-1030

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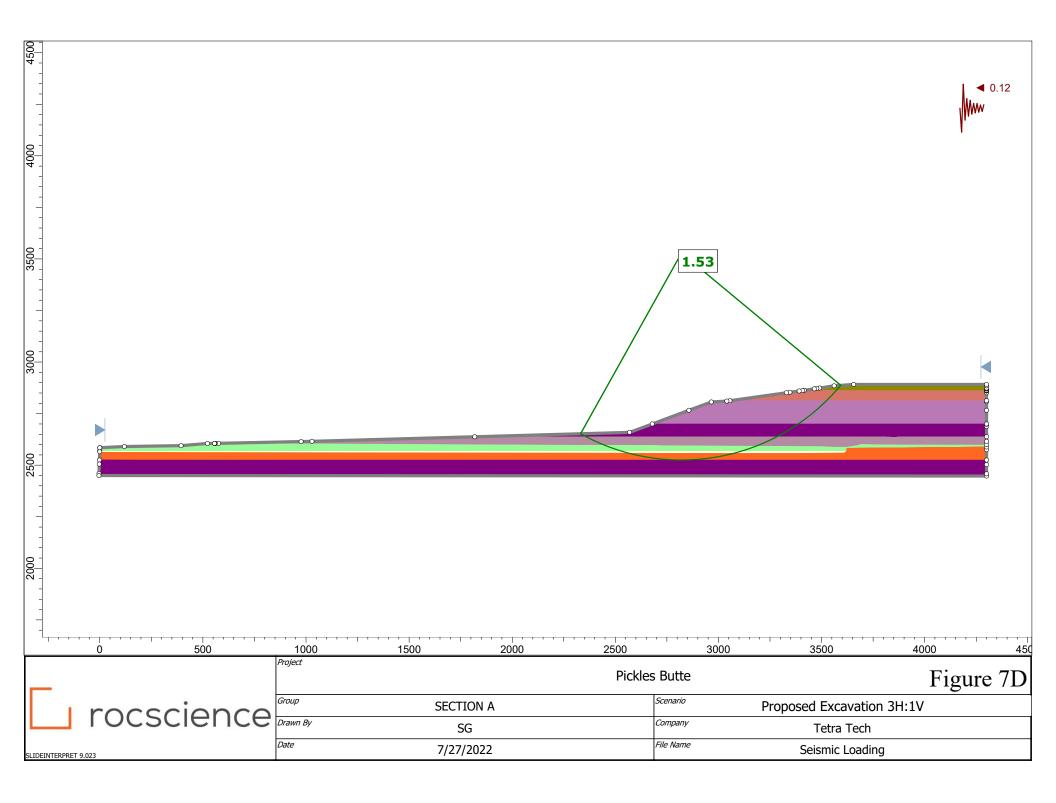
LEGEND EXISTING GROUND PROPOSED CUT PROPOSED BORROW PROPOSED FILL

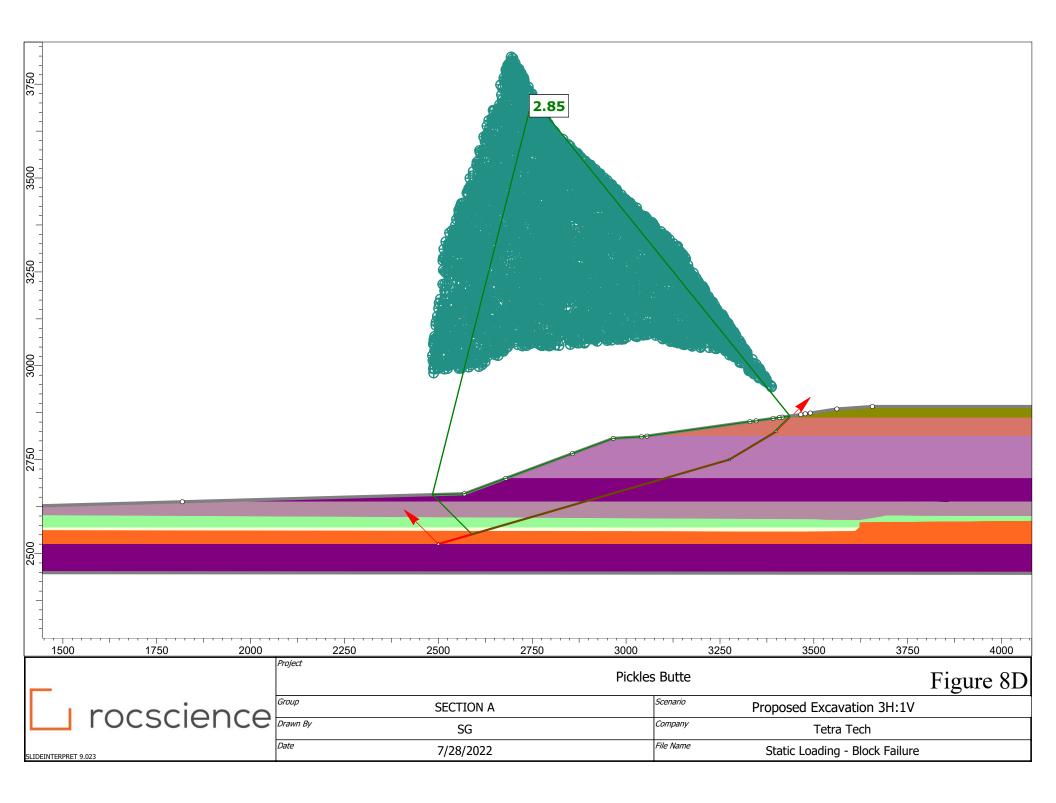
www.tetratech.com 380 Americana Terracem Suite 201 Boise, ID 83706 PHONE: 208-389-1030

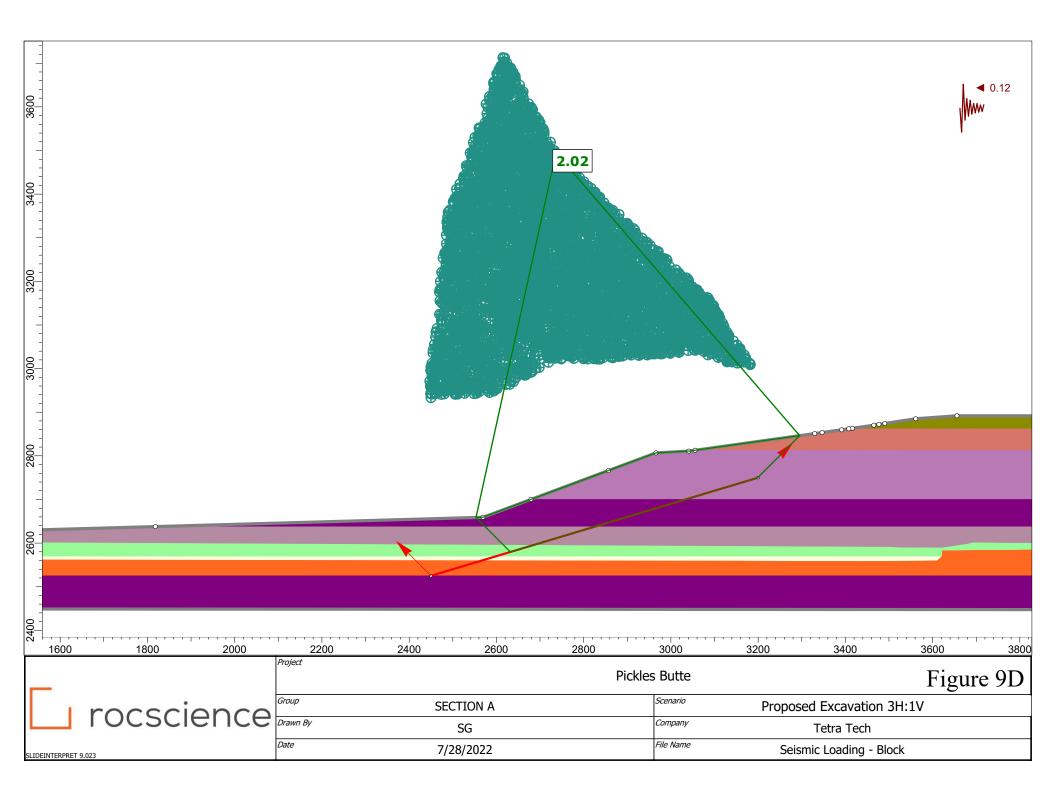
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S BUTTE LANDFILL, CANYON COUNTY, IDAHO	Project No.:         114-571040-2022         5           Date:         7/29/2022         5         1           Designed By:         SG         1         1           Figure         5         0         0         0
2022 EXPANSION GEOTECHNICAL INVESTIGATION	Date: 7/29/2022
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PROFILE G	Figure
	5D <sup>3</sup>
	Bar Measures 1 inch

4500	-											
-	-	Material Name	Color	Unit Weight (Ibs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D	D
	-	Silty Sand - B3		115	Mohr- Coulomb	400	32.8					
4000	-	Sand B3		110	Mohr- Coulomb	0	36.2					
	-	Lean Clay - Silty Clay - B5		130	Mohr- Coulomb	489	15					
	-	Clay Lean - B5		125	Mohr- Coulomb	2000	13.5					
00	_	Hard Clay - B6- 99'		125	Mohr- Coulomb	7831	10					
3500	-	Claystone		135	Generalized Hoek-Brown			700000	10	4	0	0
	_	Gravel - B PB13		135	Mohr- Coulomb	0	40					
	-	Clayey Gravel - B PB13		138	Mohr- Coulomb	1	36					
2500 3000		o∞ o∞		0 0		• • • • • • • • • • •						
	0	500		1000 Project	1500		200	0		2	500	
Г	_			-								Pickles Butte Figure 6D
	l r	rocscie	enc	Group Drawn By			TON A					Scenario Proposed Excavation 3H:1V
				Date			5G /2022					Company     Tetra Tech       File Name     Static Loading
SLID	EINTERPRET 9.023			<u> </u>		•,=,	, <b></b>					

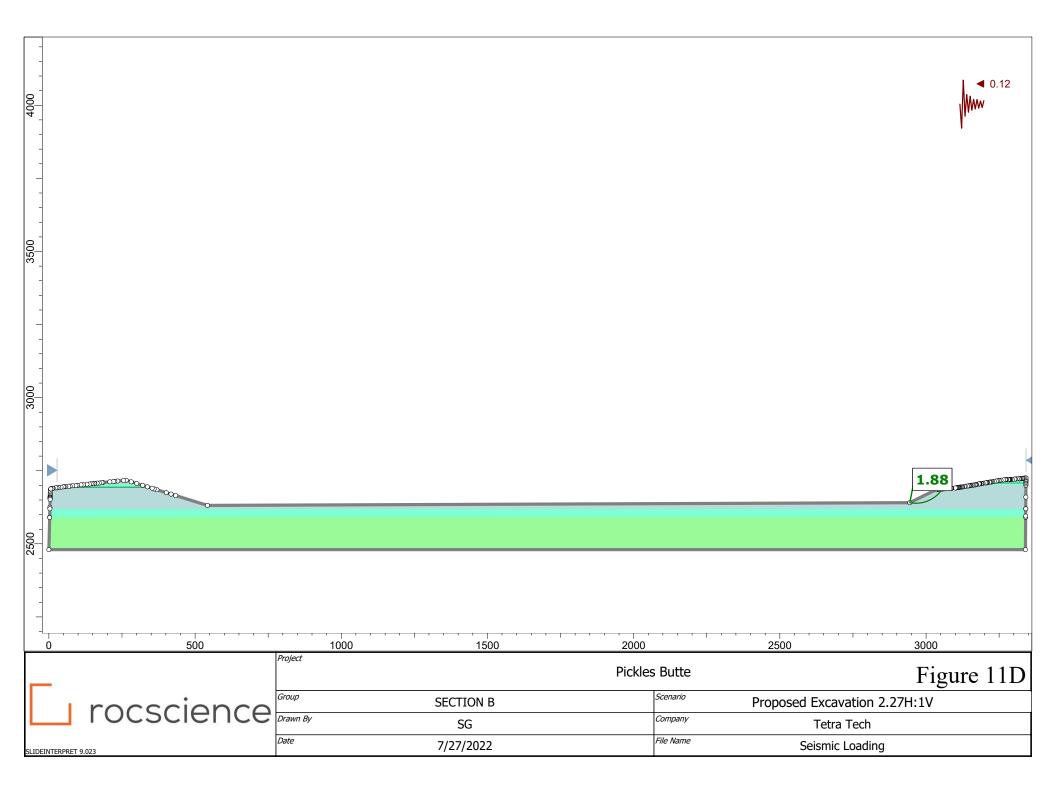


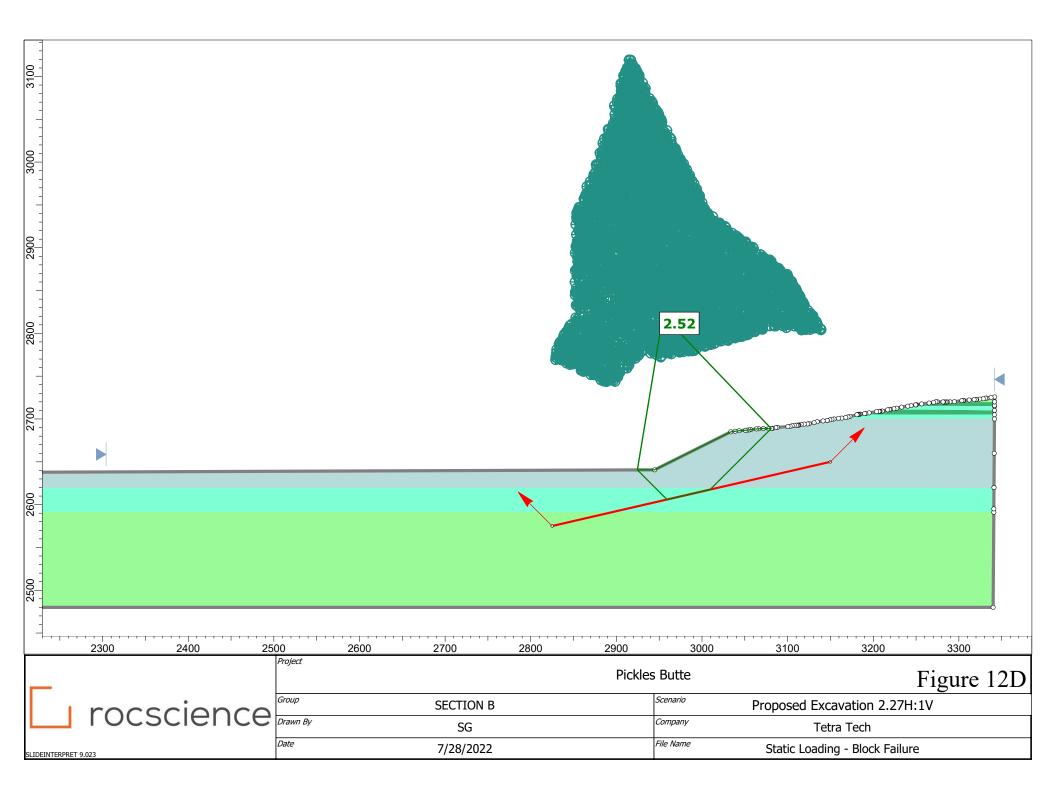


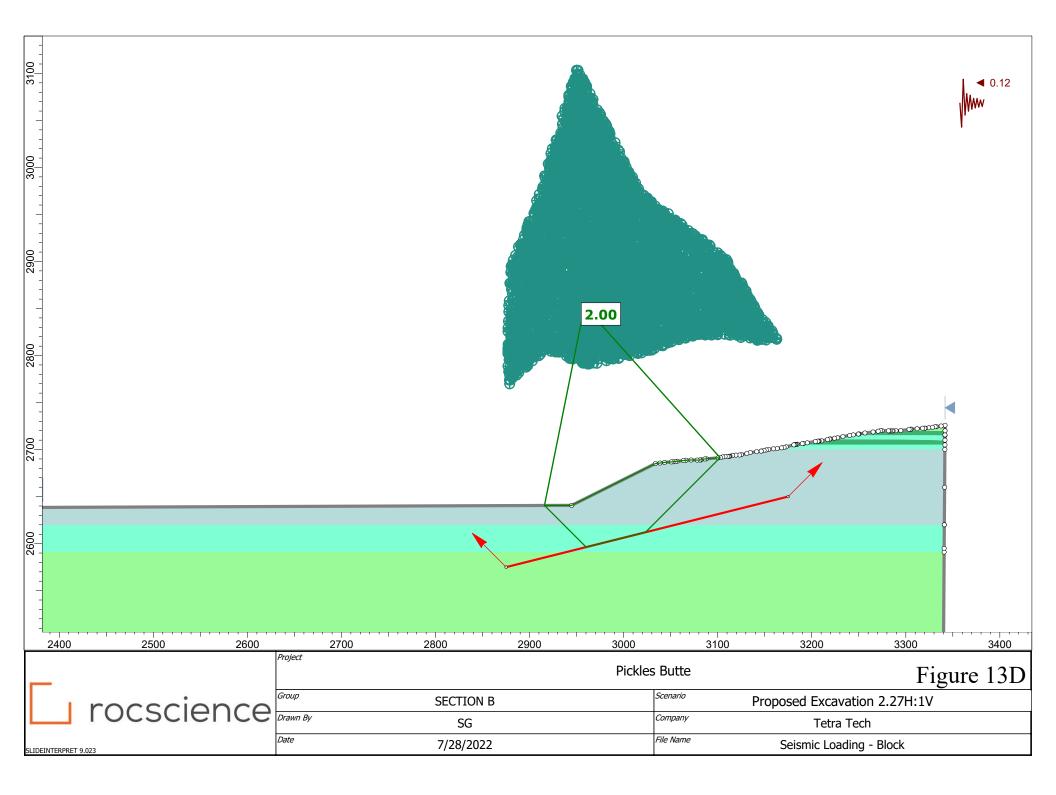


Material Name	Color	Unit Weight (lbs/ ft3)	Strength Type	Cohesion (psf)	Phi (deg)
PG Silty Sand - B3		110	Mohr- Coulomb	300	28
PG Silty Sand - B4		110	Mohr- Coulomb	123	27
Silty Sand - B3		115	Mohr- Coulomb	400	32.8
Silty Sand - B4		115	Mohr- Coulomb	580	29.5

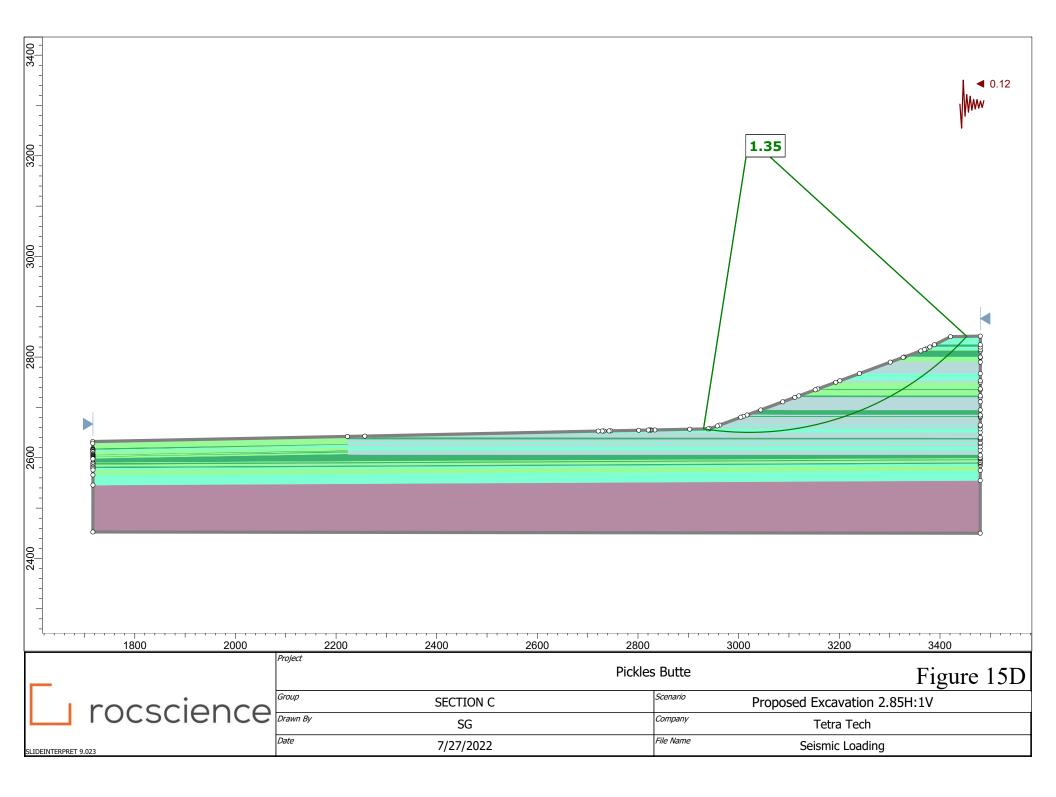
22000						2.43
_	0	1000	1500	2000	2500	3000
_	_	Project		Pickles Butte		Figure 10D
	I rocscionco	Group	SECTION B	Scenario	Proposed Excavation 2.2	27H:1V
L	<u> </u>	Drawn By	SG	Company	Tetra Tech	
SLIDE	EINTERPRET 9.023	Date	7/27/2022	File Name	Static Loading	

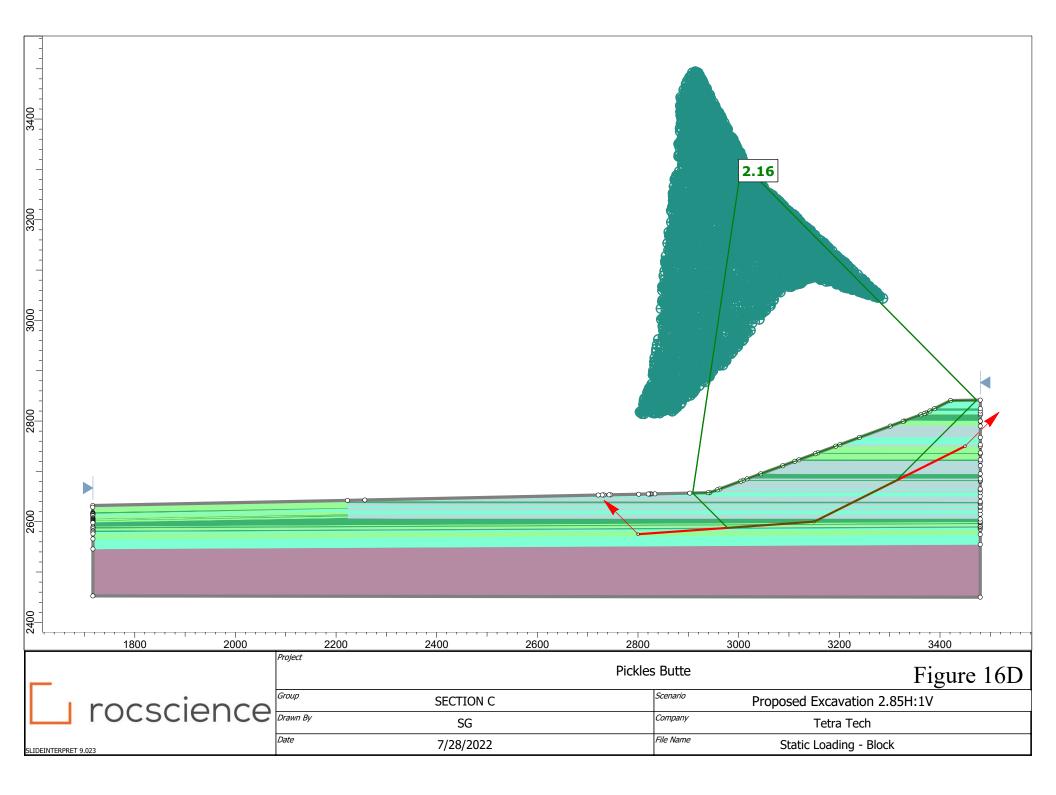


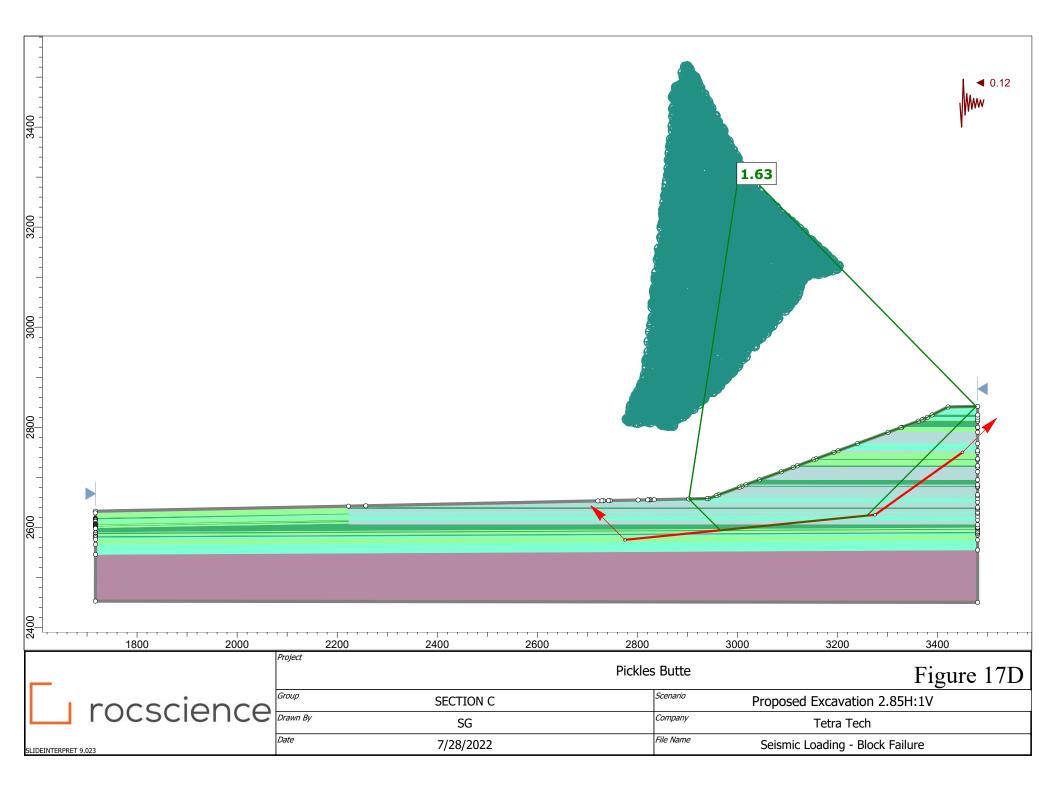




	Material Name	Color	Unit Weight (Ibs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	1.85		
	PG Silty Sand - B3		110	Mohr- Coulomb	300	28			
	PG Silty Sand - B4		110	Mohr- Coulomb	123	27			
	Silty Sand - B3		115	Mohr- Coulomb	400	32.8			
	Silty Sand - B4		115	Mohr- Coulomb	580	29.5			
	Silt - B7		110	Mohr- Coulomb	908	1			~
	Hard Clay - B6-99'		125	Mohr- Coulomb	7831	10		00 0 0	
							000000		~
		• •			0000 0	000 0			
000	2200	0	2400	2600	280	0	3000	3200	
			Project			Pickl	es Butte		Fi
T.	rocscie	ance	Group	SECTIO	NC		-	ed Excavation 2.8	5H:1V
				SG			Company	Tetra Tech	
TERPRET 9.0	23		Date	7/27/20	)22		File Name	Static Loading	



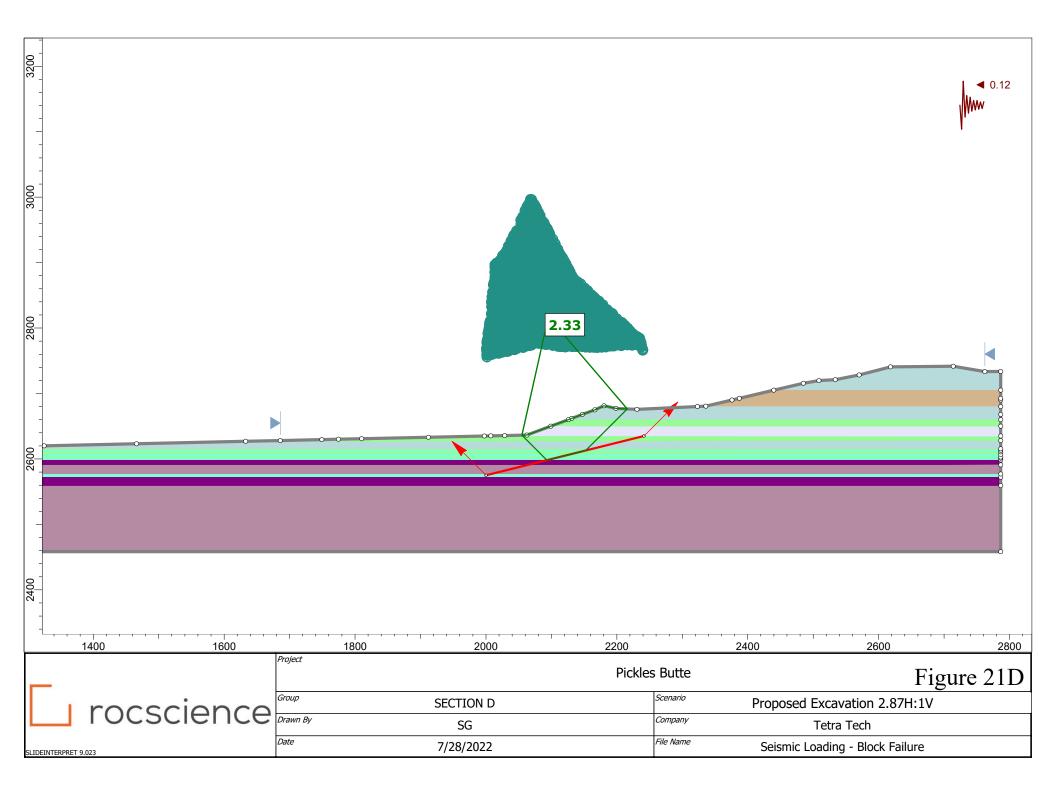




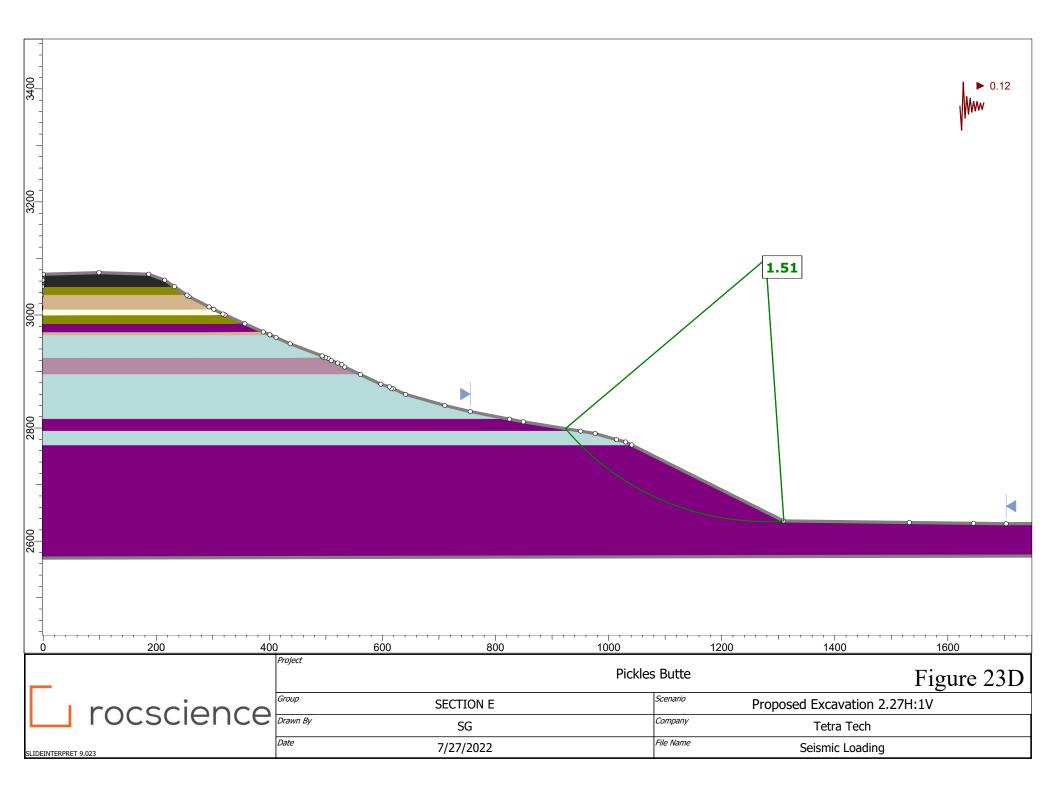
	Material Name	Color	Unit Weight (Ibs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D					
3200	PG Silty Sand - B3		110	Mohr- Coulomb	300	28									
-	PG Silty Sand - B4		110	Mohr- Coulomb	123	27									
	Silty Sand - B3		115	Mohr- Coulomb	400	32.8									
-	Silty Sand - B4		115	Mohr- Coulomb	580	29.5									
3000	Silt - B7		110	Mohr- Coulomb	908	1									
-	Hard Clay - B6-99'		125	Mohr- Coulomb	7831	10									
-	Claystone		135	Generalized Hoek-Brown			700000	10	4	0					
2800	Sand/Gravel Interbedded - B PB13		135	Mohr- Coulomb	0	37									
2600	0		0	0 0	0 0 0		0	00-0		1.93	<i>∕</i> −−−	00 00	0 0 0 0 0		
2400															
120	0	1400		1600 Project	1800		20	000			2200	2400	2600		2800
_										Pickle	es Butte		Fi	gure	18D
	l rocs	scie	ance	Group		SECTIC	DN D				Scenario	Propose	ed Excavation 2.87H:1V	!	
						SG					Company		Tetra Tech		
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Г	_		•	Group		SECTION D		Pickles	S Butte	Dronocod Ev	avation 2 97	Figure	19D
L		rocsc	ience	Drawn By		SG			Company	Proposed Exc	tra Tech	Π.1V	
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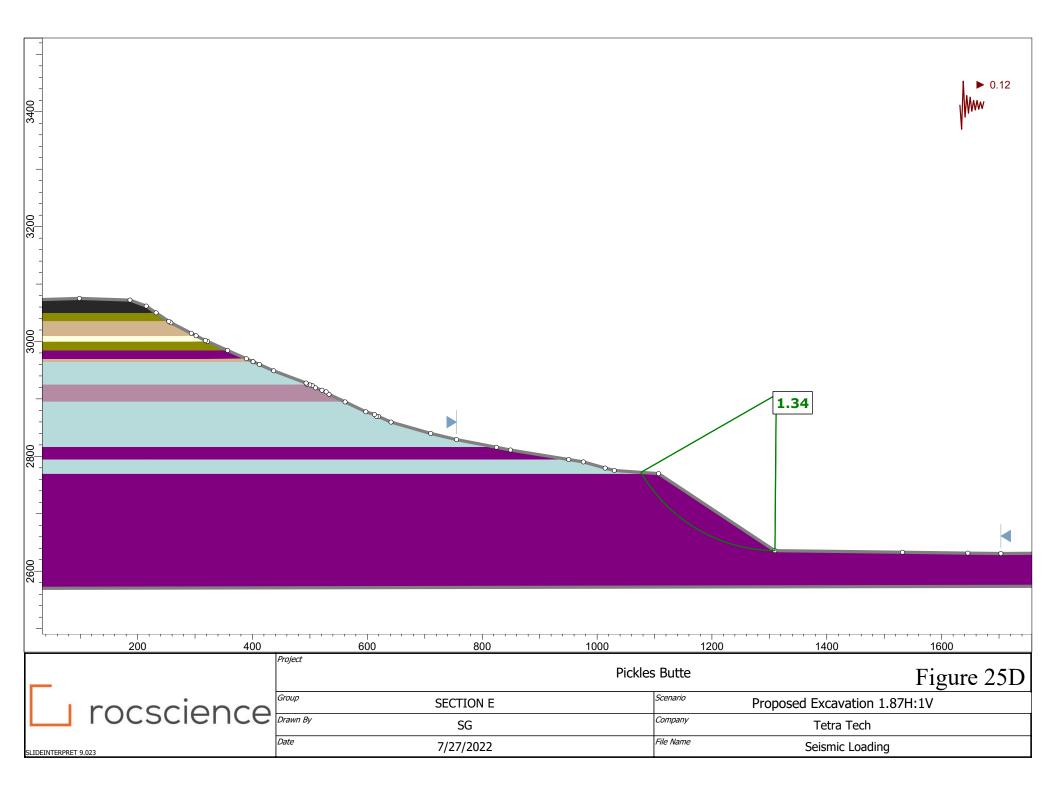
30     2600     2800     1     1       1     1     1     1     1				3.11			
2400	1600	1800	2000	2200	2400	2600	2800
_		Project			kles Butte		Figure 20D
	J rocscience	Group	SECTION D			osed Excavation 2.87	
<u> </u>		Drawn By Date	SG		Company File Name	Tetra Tech	
SLIDEINTERP	PRET 9.023		7/28/2022			Static Loading - Block	

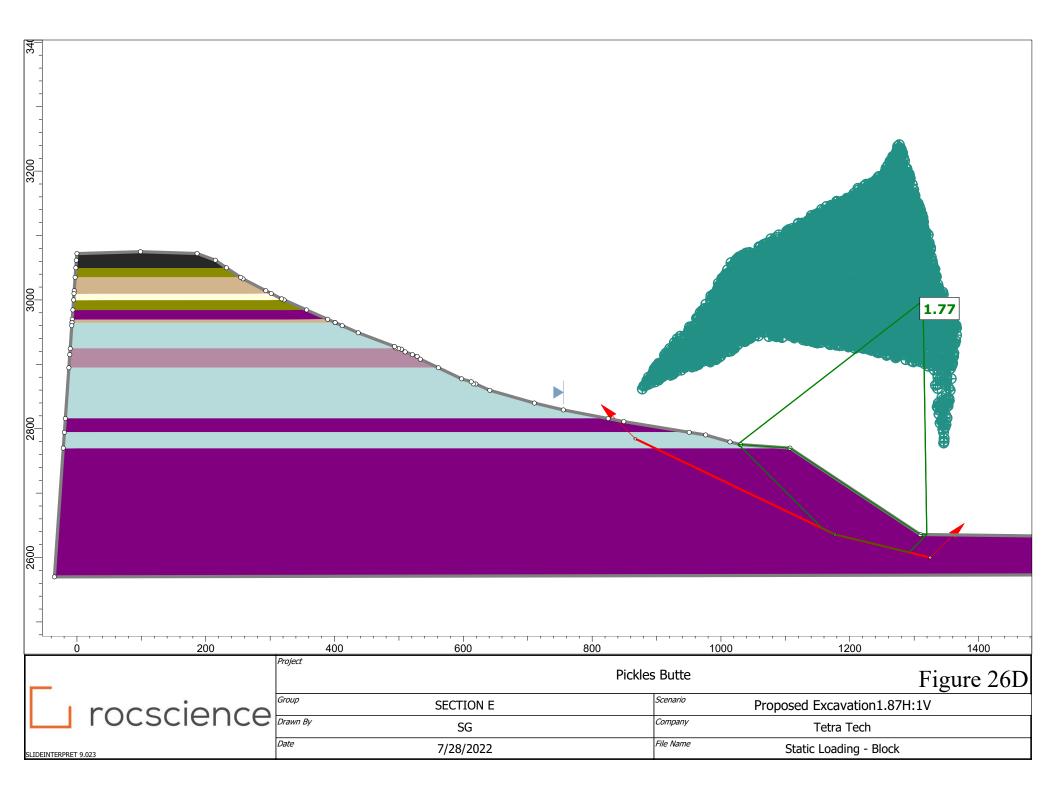


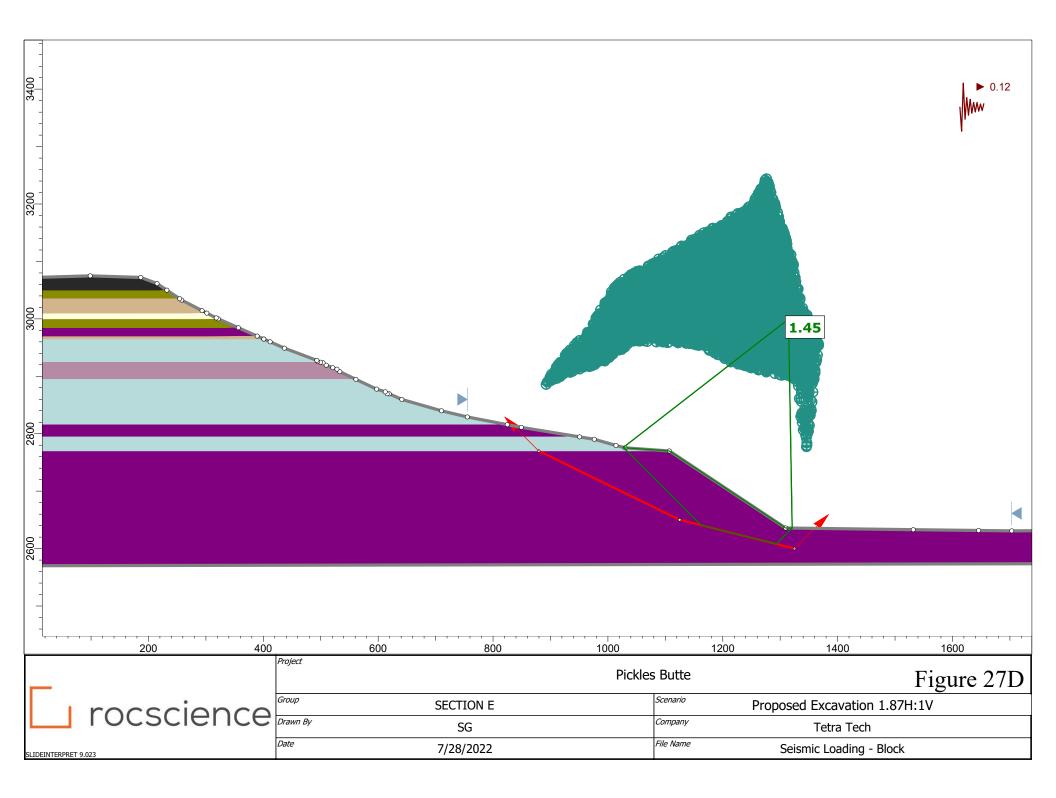
	Material Name	e Color	Unit Weight (Ibs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D
- - -	PG Silty Sand B3	-	110	Mohr- Coulomb	300	28				
- - - -	Silty Sand - B4	L	115	Mohr- Coulomb	580	29.5				
	Sand B3		110	Mohr- Coulomb	0	36.2				
- - -	Hard Clay - B6 99'	-	125	Mohr- Coulomb	7831	10				
	Claystone		135	Generalized Hoek-Brown			700000	10	4	0
	Basalt - B PB1	3	146	Generalized Hoek-Brown			3.5e+06	30	25	0.7
	Gravel - B PB1	3	135	Mohr- Coulomb	0	40				
- - - -	Sand/Gravel Interbedded - E PB13	3	135	Mohr- Coulomb	0	37				
	000000000000000000000000000000000000000				1.96					
			000	00						
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	Project				les Butte	1400		1600		
- I rocscience	Project	800 SECTIC	DN E				roposed Ex			2.27



360												
		Material Name	Color	Unit Weight (Ibs/ ft3)	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D	
3400		PG Silty Sand - B3		110	Mohr-Coulomb	300	28					
က် - -		Silty Sand - B4		115	Mohr-Coulomb	580	29.5					
_		Sand B3		110	Mohr-Coulomb	0	36.2					
-		Hard Clay - B6-99'		125	Mohr-Coulomb	7831	10					
3200		Claystone		135	Generalized Hoek-Brown			700000	10	4	0	
-		Basalt - B PB13		146	Generalized Hoek-Brown			3.5e+06	30	25	0.7	
-		Gravel - B PB13		135	Mohr-Coulomb	0	40					
3000		Sand/Gravel Interbedded - B PB13		135	Mohr-Coulomb	0	37					
2600							66		)			
	0 200 400	600			1000	1200	140			500		
_	Proj				Pickles Bu					]	Figu	ire
	_ rocscience	ир	SECTION	NE	Scen		Propose	ed Excavati		87H:	1V	
<b>_</b>			SG		Comj File I	pany Name		Tetra Te				
SLIDEIN	TERPRET 9.023		7/27/20	22	riie i			Static Loa	ding			







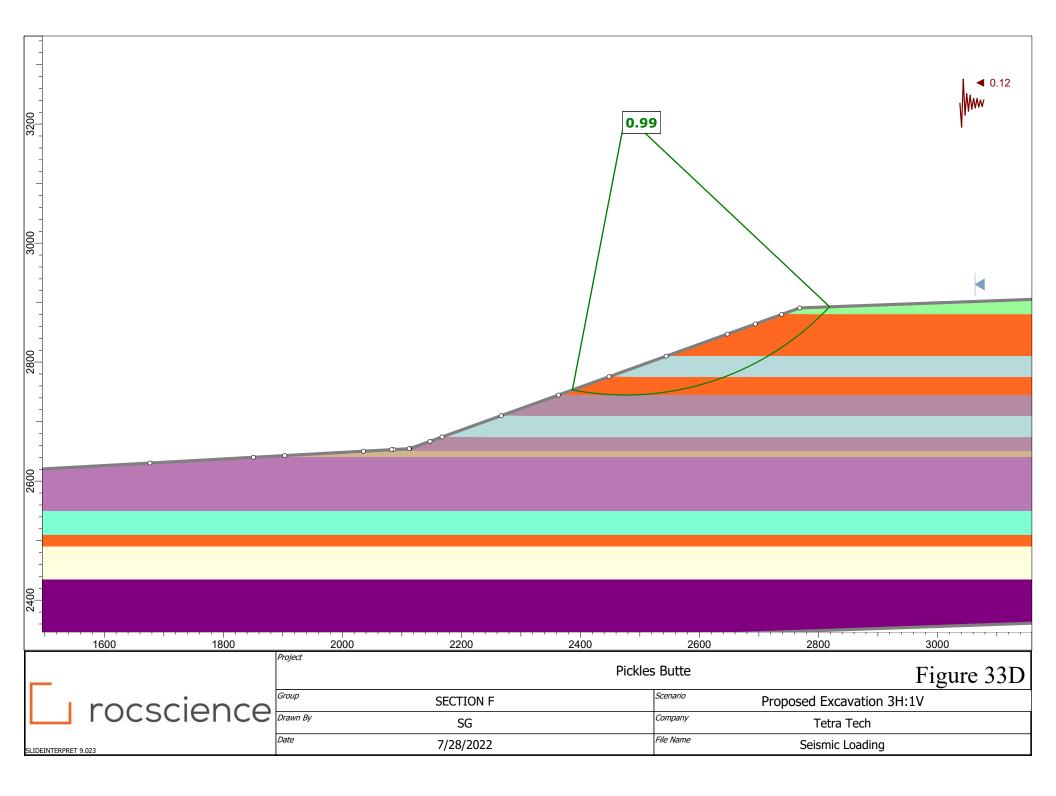
Material Name	Color	Unit Weight (Ibs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D	1.81
PG Silty Sand - B4		110	Mohr-Coulomb	123	27					
Silty Sand - B3		115	Mohr-Coulomb	400	32.8					
Silty Sand - B4		115	Mohr-Coulomb	580	29.5					
Sand B3		110	Mohr-Coulomb	0	36.2					
Lean Clay - Silty Clay - B5		130	Mohr-Coulomb	489	15					
Clay Lean - B5		125	Mohr-Coulomb	2000	13.5					
Hard Clay - B6-99'		125	Mohr-Coulomb	7831	10					
Claystone		135	Generalized Hoek-Brown			700000	10	4	0	
Sand/Gravel Interbedded - B PB13		135	Mohr-Coulomb	0	37					
0		0	0 0	0	0		0		0	
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	16	Project		2000		2200	Pic		0 24 3 Butt	
		Project		SECTION F	· · · · ·	2200	Pic			

1800       2000       2200       2400       2600       2800       3000         1800       2000       2200       2400       2600       2800       3000         Project         Pickles Butte       Figure 29D         Group       SECTION F         Drawn By       SG       Company         Date       7/(28/2002)				0			
Project       Pickles Butte       Figure 29D         Group       SECTION F       Scenario       Proposed Excavation 3H:1V Lower, 4H:1V Upper         Drawn By       SG       Company       Tetra Tech         Date       7/28 / 2022       File Name       Sciencia Logding		O0					
Pickles Butte       Figure 29D         Group       SECTION F       Scenario       Proposed Excavation 3H:1V Lower, 4H:1V Upper         Drawn By       SG       Company       Tetra Tech         Date       7/28/2022       File Name       Science January	1800	2000	2200	2400	2	600 2800	3000
Image: Second control in the second control in th		Project			Pickles Butte		Figure 29D
Date 7/30/2022 File Name Society of a state of the second		Group	SECTION F		Scenario	Proposed Excavation 3H-11/ Low	
Date 7/30/2022 File Name Society of a state of the second		Drawn By			Company		
	SLIDEINTERPRET 9.023		7/28/2022		File Name		

1000 1250 1500	1750 2000 2250 2500 2750	3000 3250 3500 3750 4000		
	Project	ckles Butte Figure 30D		
C rocscience	Group SECTION F	Scenario Proposed Excavation 3H:1V Lower, 4H:1V Upper		
		Company Tetra Tech		
SLIDEINTERPRET 9.023	Date 7/28/2022	File Name Static Loading - Block Failure		

3750			1.53			<ul> <li>■ 0.12</li> <li>● 0.12</li> </ul>
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	1050 4500	1750 2000 22		2750		2500
	1250 1500	1750 2000 22 Project	:50 2500	Pickles Butte		Figure 31D
	rocscience	Group SECTION	F		Excavation 3H:1V Lower, 4	
L				Company	Tetra Tech	
SLIDEI	NTERPRET 9.023	Date 7/28/202	22	File Name	Static Loading - Block Failur	e

Material Name         Color         Unit Weight (lbs/ ft3)         Strength Type         Cohesion (psf)         Phi (deg)         UCS (psf)         GSI mi         D           PG Silty Sand - B4         110         Mohr-Coulomb         123         27         1         1         1           Silty Sand - B3         115         Mohr-Coulomb         400         32.8         1         1         1           Silty Sand - B4         115         Mohr-Coulomb         580         29.5         1         1         1           Sand B3         110         Mohr-Coulomb         0         36.2         1         1         1           Lean Clay - Silty Clay - B5         130         Mohr-Coulomb         489         15         1         1         1           Hard Clay - B6-99'         125         Mohr-Coulomb         7831         10         1         1         1           Claystone         135         Generalized Hoek-Brown         1         700000         10         4         0           PB13         135         Mohr-Coulomb         0         37         1         1         1										
PG Silty Sand - B4       110       Mohr-Coulomb       123       27           Silty Sand - B3       115       Mohr-Coulomb       400       32.8           Silty Sand - B4       115       Mohr-Coulomb       580       29.5            Sand B3       110       Mohr-Coulomb       0       36.2            Lean Clay - Silty Clay - B5       130       Mohr-Coulomb       489       15            Clay Lean - B5       125       Mohr-Coulomb       2000       13.5            Hard Clay - B6-99'       125       Mohr-Coulomb       7831       10            Claystone       135       Generalized Hoek-Brown       700000       10       4       0         Sand/Gravel Interbedded - B       135       Mohr-Coulomb       0       37		Material Name	Color	Weight (lbs/	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi C
Silty Sand - B4       115       Mohr-Coulomb       580       29.5       Image: Constraint of the system         Sand B3       110       Mohr-Coulomb       0       36.2       Image: Constraint of the system       Image: Constraint of the system         Lean Clay - Silty Clay - B5       130       Mohr-Coulomb       489       15       Image: Constraint of the system         Clay Lean - B5       125       Mohr-Coulomb       2000       13.5       Image: Constraint of the system         Hard Clay - B6-99'       125       Mohr-Coulomb       7831       10       Image: Constraint of the system         Claystone       135       Generalized Hoek-Brown       700000       10       4       0         Sand/Gravel Interbedded - B       135       Mohr-Coulomb       0       37       Image: Constraint of the system		PG Silty Sand - B4			Mohr-Coulomb	123	27			
Sand B3       110       Mohr-Coulomb       0       36.2            Lean Clay - Silty Clay - B5       130       Mohr-Coulomb       489       15            Clay Lean - B5       125       Mohr-Coulomb       2000       13.5            Hard Clay - B6-99'       125       Mohr-Coulomb       7831       10            Claystone       135       Generalized Hoek-Brown       700000       10       4       0         Sand/Gravel Interbedded - B       135       Mohr-Coulomb       0       37		Silty Sand - B3		115	Mohr-Coulomb	400	32.8			
Lean Clay - Silty Clay - B5130Mohr-Coulomb48915IIIClay Lean - B5125Mohr-Coulomb200013.5IIIIHard Clay - B6-99'125Mohr-Coulomb783110IIIIClaystone135135Generalized Hoek-BrownI7000001040Sand/Gravel Interbedded - B135Mohr-Coulomb037IIII		Silty Sand - B4		115	Mohr-Coulomb	580	29.5			
Clay - B5       Image: State of the state o		Sand B3		110	Mohr-Coulomb	0	36.2			
Hard Clay - B6-99'       125       Mohr-Coulomb       7831       10       Image: Claystone         Claystone       135       Generalized Hoek-Brown       700000       10       4       0         Sand/Gravel Interbedded - B       135       Mohr-Coulomb       0       37       Image: Claystone       Image: Cl		Lean Clay - Silty Clay - B5		130	Mohr-Coulomb	489	15			
Claystone135Generalized Hoek-Brown7000001040Sand/Gravel Interbedded - B135Mohr-Coulomb037				125	Mohr-Coulomb	2000	13.5			
Sand/Gravel     135     Mohr-Coulomb     0     37     4     4		Hard Clay - B6-99'		125		7831	10			
Interbedded - B 135 Mohr-Coulomb 0 37				135				700000	10	4 C
		Interbedded - B		135	Mohr-Coulomb	0	37			
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	ľ									
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				Project						
1600 1800 2000 2200 Project				Group		SEC	TION F	:		
Project		rocsci	en	Ce Drawn	Ву					
1600 1800 2000 2200 Project										



Material Name	Color	Unit Weight (Ibs/ ft3)	Strength Type	Cohesion (psf)	Phi (deg)
PG Silty Sand - B3		110	Mohr- Coulomb	300	28
PG Silty Sand - B4		110	Mohr- Coulomb	123	27
Silty Sand - B3		115	Mohr- Coulomb	400	32.8
Silty Sand - B4		115	Mohr- Coulomb	580	29.5
Lean Clay - Silty Clay - B5		130	Mohr- Coulomb	489	15
Clay Lean - B5		125	Mohr- Coulomb	2000	13.5
Hard Clay - B6-99'		125	Mohr- Coulomb	7831	10
Trash		75	Mohr- Coulomb	300	28

2.22

4000

35,00

3000

2500

- 	2000	2500	3000		3500	4000
-	Project		Pickles	Butte		Figure 34D
I rocscience	Group	SECTION G		Scenario	Proposed Excavation	1 2.6H:1V
	Drawn By	SG		Company	Tetra Tech	
SLIDEINTERPRET 9.023	Date	7/28/2022		File Name	Static Loading	g

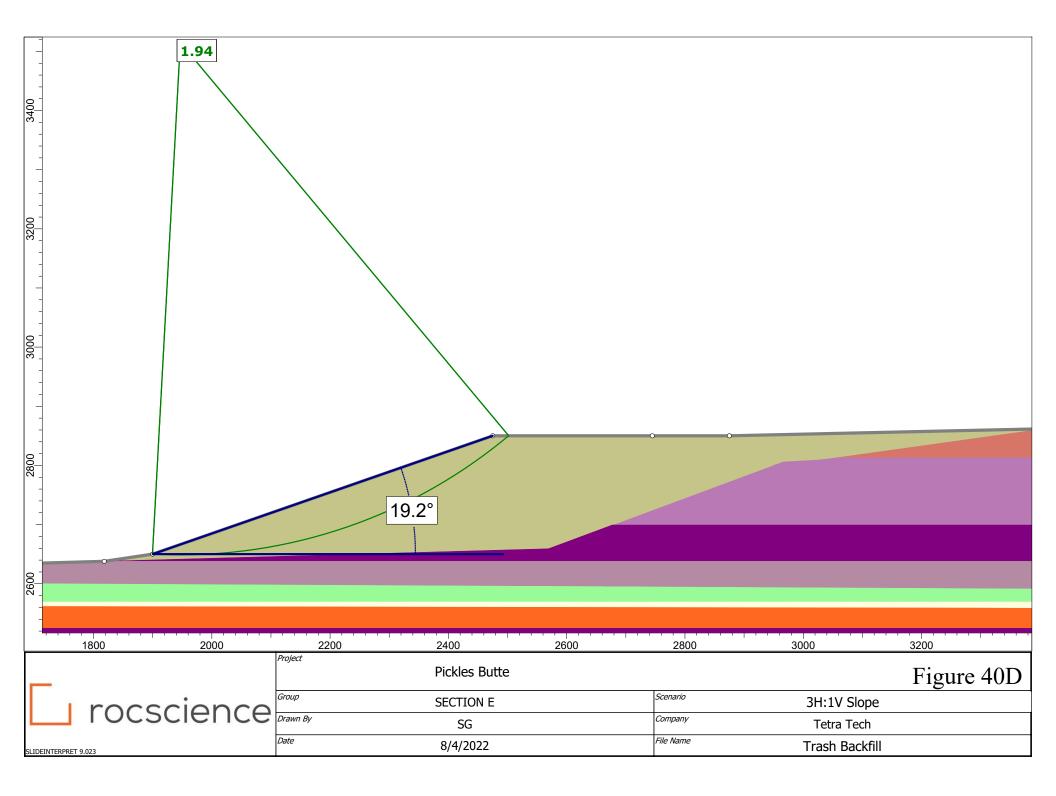
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	0		O				
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1600 1700	1800	1900 2000 Project	2100	2200 2300 Pickl	2400 es Butte	2500 2600	2700 28 Figure 35D
	science	Group	SECTION G		Scenario	Proposed Excavation 2	
	Science		SG		Company	Tetra Tech	
SLIDEINTERPRET 9.023		Date	7/28/2022		File Name	Seismic Loading	

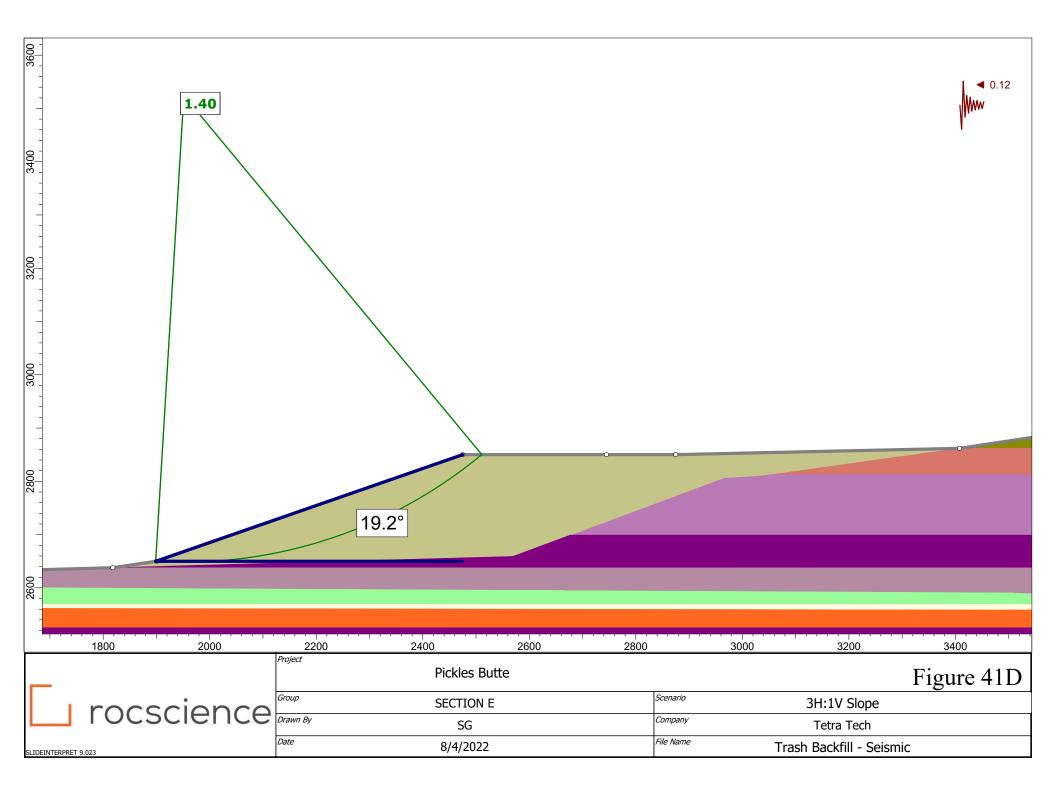
3500 4000					
3000					
25,00					
	] 	2500 3000	3500	4000 4500	
	_	Project	Pickles Butte	Figure 36	
	rocscience	Group SECTION G	Scenario	Proposed Excavation 2.6H:1V	
L			Company	Tetra Tech	
SLII	DEINTERPRET 9.023	Date 7/28/2022	File Name	Static Loading - Block	_

4500						<ul> <li>■ 0.12</li> <li>₩₩</li> </ul>
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	1000 1500	2000 Project	2500 300	0 3500 Pickles Butte	4000	4500 5000 <b>F: 27D</b>
Г	-	Group	SECTION G	Scenario	Dropocod Even	Figure 37D Ivation 2.6H:1V
L	_ rocscience	Drawn By	SG	Company		Tech
SLIDEI	NTERPRET 9.023	Date	7/28/2022	File Name		nding - Block

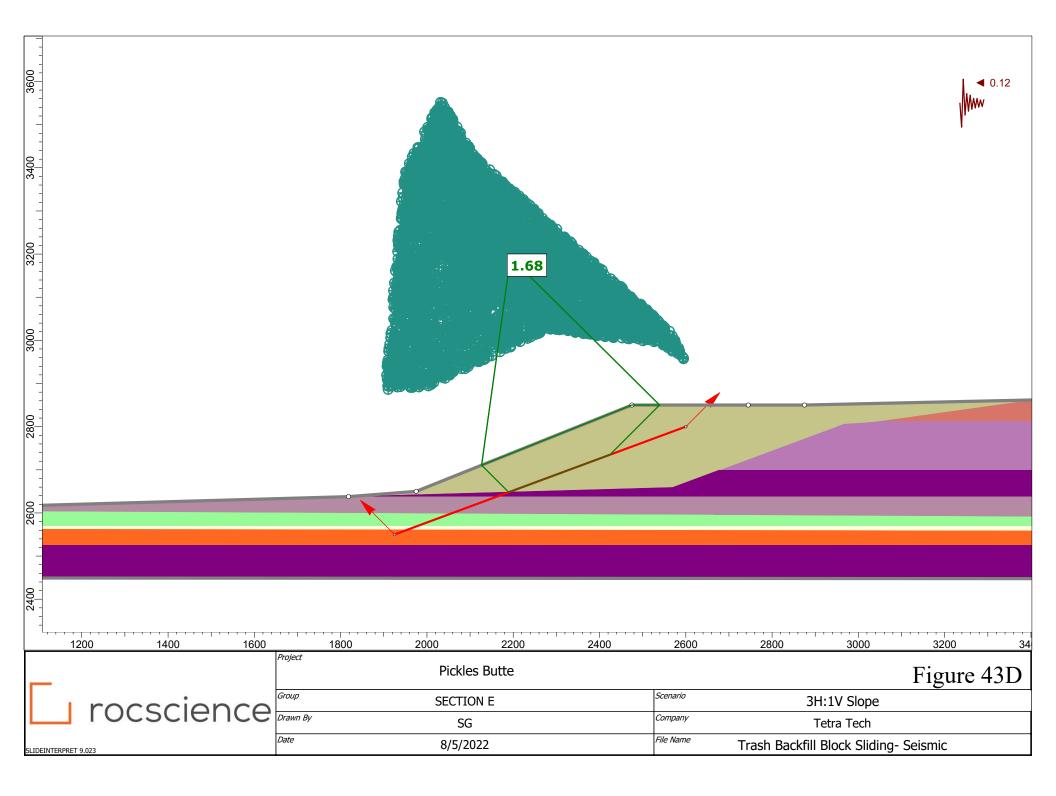
3400	1.73		
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3000			
2800		21.8°	
2600 		2200 2400 2600	2800 3000 3200 3400
	1000 2000	Project Pickles Butte	Figure 38D
Γ	<b>r</b> ocscience		Scenario 2.75H:1V Slope
			Company Tetra Tech
SLIDEINTE	RPRET 9.023	Date 8/4/2022	File Name Trash Backfill - Static

3400	1.28			<ul> <li>■ 0.12</li> <li>₩₩</li> </ul>
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	1800 2000	2200 2400 2600 Project	2800 3000 3200	3400
_		Pickles Butte	Fi	igure 39D
Γ	J rocscience	Group SECTION E	Scenario 2.75H:1V Slope	
			Company Tetra Tech File Name Trach Backfill - Soismic	
SLIDEINT	RPRET 9.023	Date 8/4/2022	File Name Trash Backfill - Seismic	





3600			
3400			
3200		2.21	
3000			
2800			
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2400	- - - 1400 1600 1800	2000 2200 2400 2600 Project	2800 3000 3200 3400 3600
	_	Pickles Butte	Figure 42D
	rocscience	Group SECTION E	Scenario 3H:1V Slope
		Drawn By         SG           Date         8/5/2022	Company     Tetra Tech       File Name     Trash Backfill Block Sliding- Static
SL	DEINTERPRET 9.023	0, 0, 2022	

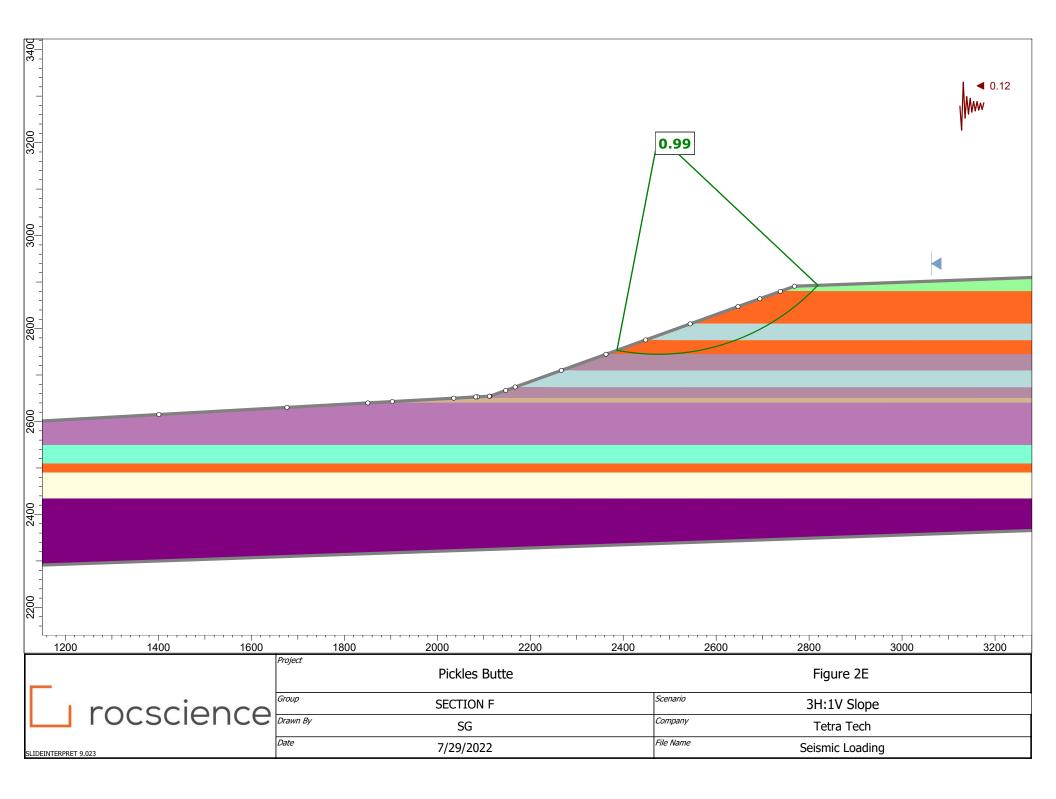


### **APPENDIX E: Deformation Analysis**

Static and Pseudo-Static Slope Stability Stability Analyses with Associated Circular and Block Failure Factor of Safety, Newmark Displacement, and Critical Acceleration for Slope 3H:1V Figures 1E through 6E

Static and Pseudo-Static Slope Stability Stability Analyses with Associated Circular and Block Failure Factor of Safety, Newmark Displacement, and Critical Acceleration for Slope 4H:1V Figures 7E through 12E

Material Name	Color	Unit Weight (Ibs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D	
PG Silty Sand - B4		110	Mohr-Coulomb	123	27					
Silty Sand - B3		115	Mohr-Coulomb	400	32.8					
Silty Sand - B4		115	Mohr-Coulomb	580	29.5					
Sand B3		110	Mohr-Coulomb	0	36.2					
Lean Clay - Silty Clay - B5		130	Mohr-Coulomb	489	15					
Clay Lean - B5		125	Mohr-Coulomb	2000	13.5					
Hard Clay - B6-99'		125	Mohr-Coulomb	7831	10					
Claystone		135	Generalized Hoek-Brown			700000	10	4	0	
Sand/Gravel Interbedded - B PB13		135	Mohr-Coulomb	0	37					1.38
			0	0	0 0	0			0	
750 100	00	1250	1500	1750		2000	.   .	2	250	2500 2750 3000 32
		Project		Pickles	Butte					Figure 1E
rocci		Group		SECTIO	NF					Scenario 3H:1V Slope
rocsci	ene	Le Drawn By		SG						Company Tetra Tech



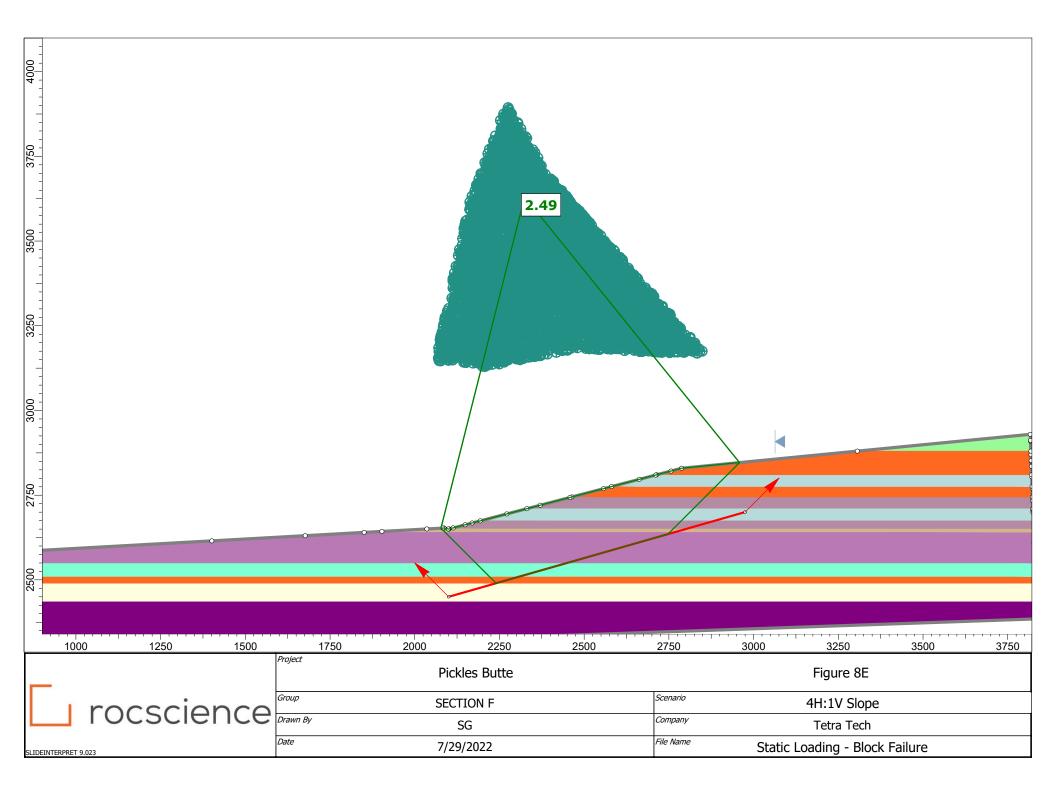
500 750 1000	1250 1500 1750 Project	2000 2250	2500 275	0 <u>3000</u>	3250	3500
	Pickles Butte			Figure 3E		
C rocscience	Group SECTION F		Scenario	3H:1V Slope		
			Company	Tetra Tech		
SLIDEINTERPRET 9.023	Date 7/29/2022		File Name	Static Loading		

3000 3500 400				1.41			<ul> <li>0.12</li> <li>0.12</li> </ul>
2500 		• • •					
-		1500 1750	2000	2250 250	)0 2750	3000	3250 3500
		Project	Pickles Butte			Figure 4E	
	rocscience	Group	SECTION F		Scenario	3H:1V Slop	
		Drawn By Date	SG		Company File Name	Tetra Tech	
SLIDEINTERPR	RET 9.023		7/29/2022		5	eismic Loading - Blo	

3200			0.12			
3000					4	•
2800		0	0			
2600 		0 0 0 0				
2400   2400				2600 2800	· · · · · · · · · · · · · · · · · · ·	
	2000	Project	Pickles Butte		Figure 5E	
			ECTION F	Scenario	3H:1V Slope	
	_ rocscience	Drawn By	SG	Company	Tetra Tech	
SLIDEI	NTERPRET 9.023	Date 7	/29/2022	File Name	Critical Acceleration	

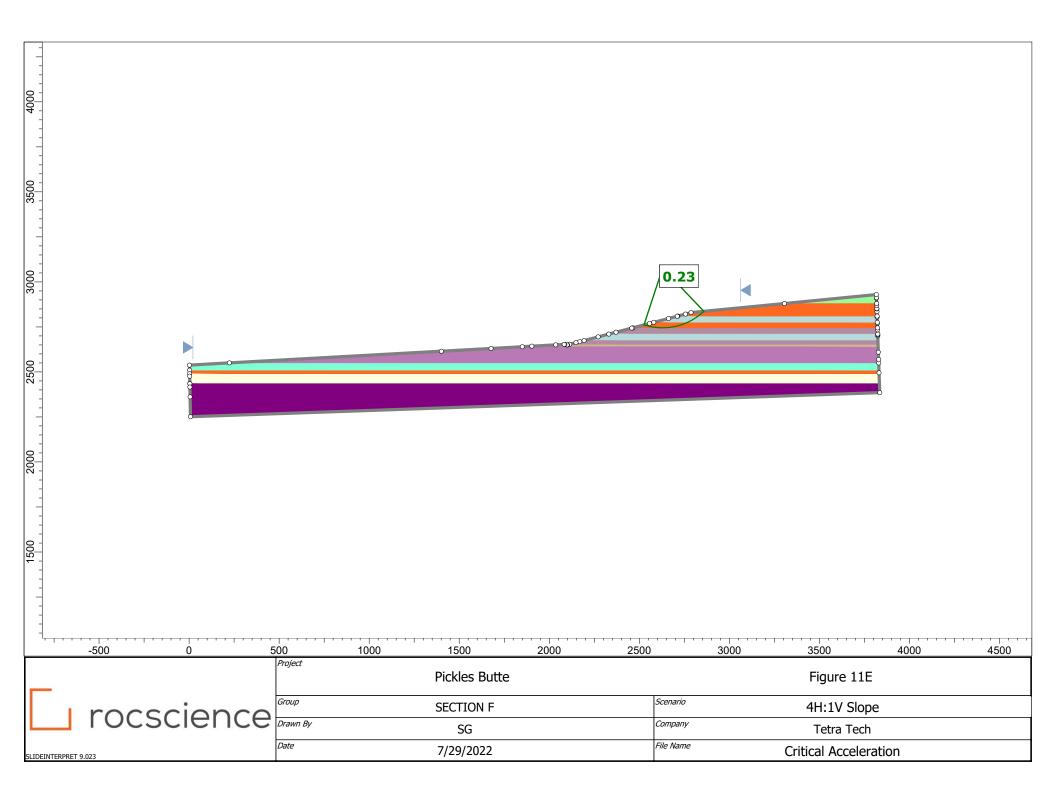
3200		
	3.19	in V V V V V V V V V V V V V V V V V V V
1000 1250 150	Project	2750         3000         3250         3500         3750           Pickles Butte         Figure 6E
	Group SECTION F Drawn By SG Date 7/28/2022	Scenario     3H:1V Slope       Company     Tetra Tech       File Name     Seismic Loading - Newmark Displacement

1400         1600         1800         2000         2200         2400         2600         2800           Project         Pro	3000 3200
Pickles Butte Figure	re 7E
	/ Slope
	a Tech Loading



3500											<ul><li>■ 0.12</li></ul>
3250											
3000					1.35				•		0
2750	• • • • • •	- <b>- - - - - - - - - -</b>	00000	0 0							
2500											
00 2250											
20	1400 1600 1800	2000	2200	2400	2600	2800	3000	3200	3400	3600	3800
	•			Pickles Bu	tte				Figure 9E		
	rocscience	Group		SECTION F			Scenario		4H:1V Slope	9	
				SG			Company		Tetra Tech		
SLIDEI	ITERPRET 9.023	Date		7/29/2022			File Name		Seismic Loadi	ng	

	1500 2000 2500	
	Project Pickles Butte	Figure 10E
C rocscience	Group SECTION F	Scenario 4H:1V Slope
		Company Tetra Tech
SLIDEINTERPRET 9.023	Date 7/29/2022	File Name Seismic Loading - Block Failure



3200 3400									
3000				0.2	25 in		•		
2800				00000	000				
2600	•	0 0 0	000 0 0 0 0 0 0						
2400									
2200									
	1400 1600 180	) 2000 Project	2200 2400	2600	2800 Pickles Butte	3000	3200 Figure 12	3400	3600
Г		Group	SECTION F		Scenario		4H:1V Sk		
L	rocscience		SG		Company		Tetra Tec		
SLIDE	NTERPRET 9.023	Date	7/28/2022		File Name	Seismic Lo	ading - Newm	ark Displacemer	it

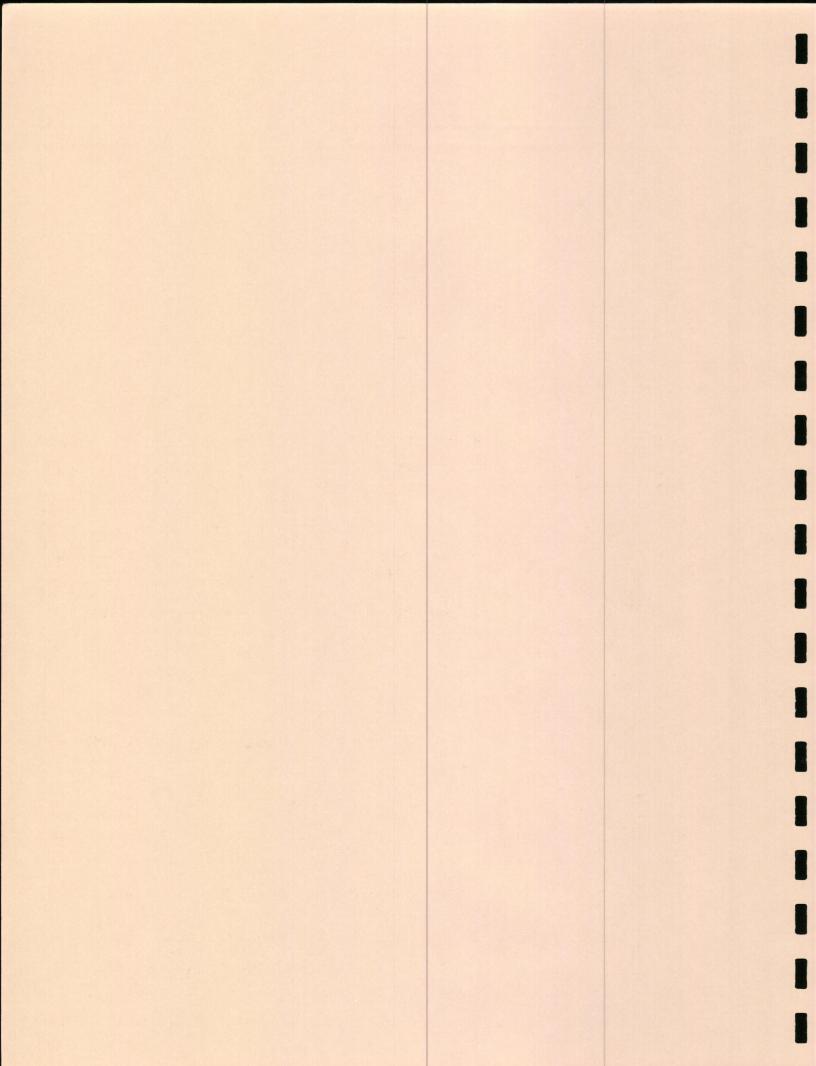
## **APPENDIX F: Previous Reporting Logs of Boring**

LOGS GT-1 THROUGH GT-8 BY HOLIDAY ENGINEERING COMPANY(HOLIDAY) LOGS PB 5 THROUGH PB12 BY HOLIDAY and DANIEL B. STEPHENS & ASSOCIATES, INC.

# **APPENDIX E: Borehole Logs**



PICKLES BUTTE SANITARY LANDFILL GEOTECHNICAL EVALUATION



		DATE	DATE COLOR			GEOPHYSICS		GRAIN	SIZE				<u>,</u> D		HYD	RAULIC	INDURA STRUC	TION &	WATER	PAGE     OF     1/1       N     R     W     Sc'       M     MODEL     The set     1/2       MODEL     The set     1/2       COMMENTS
	ORILL	lime		ROCK TYPE		LOG	ļ	SLT			ANG	wĸ	MOD	WELL	EST.	MEAS.	FXS, VOID	S.ETC.		3600 COURTS
	NOTES	11:50	Tan	fine Scorel	-													1	<b></b>	
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1-51/2				actores aniel	J	I				<b>A</b>	1							4.5%]		1" clost remained
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	10050		[	[	7							1						1		N=5 N=71
0-1172	SA MATE	,	Trin 5	Live Cand	<b>-</b>	-		1 1	Up.IUIMA		1							10-111	MOISE	10-11/12 2,3
	+ Chino <	hollmi Lyb.	~ 2001	ng lreak 6"	-									··				1	1/09	Huserkly Carsolan
5-16%	Inrico		111. 6-	Live sout					iJUUUht		i	i						15-161-	HUNGE	N= 3, 3, 2 N'= 6
				210 7000				<u>i – i</u>										1		VI. I. CAISL
					-			<u> </u>										1		
0-21/2	ļ	12:10	lib hru	In cand		-			11111:344		1				İ			20-211	· unat	N= 4,2,3,
					-						i				1					11 W. PANS.
5-26'2	1	12:26	114.10	Luce Sand	<b>-</b>							!						-	110156	
2 02-20					-							1			1					N=5
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	ORILL NOTES			ROCK TYPE			CLY		SAND	RAV .	ANG	wк	MOD	WELL	EST.	MEAS.		GRAPHIC	L	BLOW COUNTS N
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	Cil A. Friens																Chert. S		PLOUX 1	N= 42
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	DRILL	T		ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	wк	MOD	WELL	EST.	MEAS.		GRAPHIC		
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	NO bres	5 <u>11.44</u>	dia ser	a an have													· · · · ·		() West duy)	May > 4. 5 Tous/Et -
			gand lite		1													1		
	1120-1214	1:10	7.7			-	euuna	Liál								<u>-</u>	<u> </u>		weakly	12 30 48,
	NO RING			silty riad			COUNT												Moist	2-4 Trad 42 N = 3
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175-121-4	first	2:00		14 contact				1 <u>1</u>	KID M										Nausbr	and five selling wate
	н, О			inny him silly and to 126		•												I	VERY	add Live gellons wete 23 42 50 25"
	nddo.i NO RId				4														Stript Ity	N' = 3
	NO KIN	<u> </u>			4									-+					Nan 1	<u> </u>
					1															
	130-1314 RENGS	2:25		Clay clayey sitt uf		HBuch			12527								Moderat Consl		slightly b	30(7) 32 50@5" X 4 brass ring 1
,	A1865			Jery Fine son		2,00,000	1/05					¦					QU''3'.		demo	<u>' N P</u>
	j			silty clay	]															Very
135-1364	, <del> </del>	3:00	marticle	Class of forge			l WAR -	¥									WKC-1402. CONSL.		add water	add five gallows war
1 75-1967	NO Rinas		aven	Clay us frage	F=	ſ														11 21 37 N = 2
					4															ponotrometer 1.75 - 7.7 Very S
					4															· Very 2
40-1414	+ BANGS	3:45	greenist	clay & silty	E												moderidely		add water	19 27 38 N = 2
	1		gray_	clay introde		ا کې د ولید د مې د د کې د کې د مې د د د د د د د د	¥U, 4 (#										Consl.		moderatel	4 rings (test bo
					1														Moist (38%	Clay & silty clay
IE IN	No P	1:20		1 19 21	1	1	a han tare								]					- (
40-140	IFOS	4:50	gri-qry	top 6" alary			P.U.U.U.					<u> </u>		-+			WK-MON		MODENATE	23 23 28
				CIRN	T			· · · · ·								******			~ 35 %	N = 19

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INTERVAL (FT)		DATE	COLOR	LITHOLOGY		GEOPHYSICS		GRAIN	SIZE	 EERING COMPAN								WATER	COMMENTS
ORIL	DRILL			ROCK TYPE	CRAPHIC					 ANG	war	MOD	WELL		MEAS.	FXS,VOI	GRAPHIC		
En. 151%	NOTES	9:115	Wn-9ry	Clay ut introde		No- Fuil			5,000	7110						INK-MOD		clay most do	wa SILT~ 1.5 TILE in A
<u>بر</u> بر	Sample	9:45	· · · ·	Selt/Sin Same		No - Fill			4177							CONSOL CIT		silf almost de	CLAY - 4-4.5T156
Ť	RING				-											WK MONSE	ħ	ADD - Zagl	* ONF BRASS RING CI
						ļ											1	H, 1) 10/11	
55-15674	NO	10:30	<u>grn-gcy</u>	Clay		†	<u> </u>			 						PLASTIC	4	Pach 54	15 22 25 pure
ŀ	RINGS	<u> </u>		1:40		1				 						PUTOTIC	1	MOD. DAMA	GOOD CONE ZAMPLE
ŀ					1	1											1		N'=
					4	-	and the second												.11
0-161"2#	RINGS	11:00	<u>qrn-qry</u>	Dure Clay		3. Brans	MULTER	ļ	┝───┥	 						WK CONSOL	1	POD 5 gals	18 77 24
ŀ	-				-	2 Ni Fall										Transite	1	N 28-427	* 3 portest sources in
t																	1		N = 16
[						ł	电动物										4	100 5 1 4	54
65-166/14	-NO DINCC	11:45	Arn-ery	The elay ut			122		M	 						CONSOL	F	MOD DAMP	18 44 50 9 :"
ł	10/11/25	<u> </u>		fire sand	<b>-</b>											(ECAT SAND	t i	~ 40%	N = 33
ľ					]												]		Very 5-
						-	idi att if fed bi			 	!						<u>-</u> -	14070	17 31 331
70-171 1/2	PINCS	12:30	arn-gry	Pure clay ust						 						CION CONSL	1	Add 410 50	N = 22
ŀ	CINIS			SIF FIER	-		<b></b>										1	Sert	Very Sti
ļ																	1		
75-176%	- 1/2	1.46		alour oth			W.S	MA		 						WE PORCL		75 67. 1111	12 77
15-176/2	RINGS	1.72	U , Cry	Clayer silt				16.44		 						0	1	1 1	13 22 32 7 T/rt pourtroute
Ľ					]												]		
ļ					4					 			-						N = 18 Stiff
40 - 141 71	BRACS	2:25	000.00	SURV CLAY	+====	= 15 mm -	1.9.16	1.2		 						WK-MAD		~35 97	14 12 28 N 21
*	RINGS		0 7 7	3104 (	1993 - El 19	- BULL-				1	- i					Anc of	1	1000 Cont	* 2 BRASS RINGS Still
					]					 _								v	1.5-2.0 T/S+ "
ŀ				<u> </u>	4					 									
15-1861/2	NO	3:05	Arn-Lumu	KUTY PLAY			awy w	1		 <u></u> †						w man	t l	~ 359,	12 27 44 N=2
2 C	ZINIGS		, , , ,							<u> </u>						CANSOLD		AND EVICE	1.5 TISH ? VERY S
F	<u></u>				4					 				-+				Gels	
ŀ					-		<u> </u>		+	 									· · · · · · · · · · · · · · · · · · ·
90-1914	RINGS	3.40	ard - Gray	SILTY CLAY	Farrier	1 Bau -	N' IFAS									NK-MOD		- 15.18%	15 22 310 × 1 Bross
*	5		1			JUA FILLE													3.05/4
ŀ					-				+	 <del></del> +					<u> </u>				N = 19
. ŀ					1				+										SLIC
95-1961/2		4:20		cloyey silt			¥¥A									h)le		~ 30-35%	14 17 23
	D Rule +	HULE IN		· · ·						 									25T/A N= 13 3
111-4101.1	NUMPRIAM	TIME IN	171	1	1					 									<u> </u>

P	ROJECT	Pickles	BUHP DATE	START 11-7.	MNER <u>Co</u>	<u>туси Сои</u> ПNISHED <u>//-7-</u>	<u>~</u> + 9(_ н		LO EPTH.	сапон <u>75 1/2</u>	N: CO	. <i>14 ра</i> Е <u>—</u> 57	<u>مە مەر</u> <u>ن</u> ص_Di	RILL N	_SEC	Hoccow 5	4OF	- 1/4 AMETER	T //DRI	N RW
INTERVA	L (FT)	DATE TIME	COLOR	UTHOLO	)GY	GEOPHYSICS LOG	R	GRAIN	SIZE	т	GR/	AIN R	OUNDI	NG		DRAULIC	INDURA STRUC FXS, VOID	TURE	WATER	Сомме
	ORILL NOTES			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.		GRAPHIC		
	START	11.7-96		Samed Cover						$\square$							<u> </u>	4	studen.	l
	12:25			aarbuge														1	damp	check for met
				,						┝──┦								4		-melle
5-61/2		12:35						<u> </u>										]		15 8 7
· 2	PILAGS RING			soil + trash					<u> </u>	┝──┥								4		Dirt + trash
	121.00																	1		
		12100		Soil + trash				ļ		┼┦							<u> </u>	+	BALEY	7.7.12 SA
10-11/2	NO RINGS	14.05		yn 1/2														1	DANIP	NO METHANE SI
								ļ		┝──┦								4		
<b>I</b>																		1	DUTSIDE	
15-161/2	RINGS	1:05		dianer und						┝───┥								4	WET	17 14 10 5% LEL in Aures
				Her U Dripper														1		drops to 1000 to 1000 Two RINGS FINDE
				270.				+		┝╍╍╌┦								4		
20-214,		1:20		80% Tragh		-														8 8 14
2	RINGS			2090 501-						┼──┤								-	DAMP	
																		]		19 13 12
24-2512	BRASS	1:35		NOSTLY GRASS			<b> </b>			┼───┤								1	DAMP	100% LEL
	RINGS	EOH																		SHUT RIG DOWN HOLLON STEM M
								<u> </u>		┝───┦										BACK OUT OF A
					-	· -												<u> </u>		
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LOGG	PROJEC	Fictles Steens	C BJHE	Start 1/8/2		FINISHED [(18)	абу 176 но	DLE D	LOO	CATION	I: CO.	<u></u>	200 DI	RILL N	AETHOD	43 1/ 1/ SPT/AU				PAGE_1_OF N_RW ILL_MODEL_ <u>3K-81</u>
INTERV	AL (FT)	DATE TIME	COLOR	UTHOL	0GY	GEOPHYSICS	R	GRAIN	SIZE	r	GRA	NN RO	וסאטכ	NG		PERTIES	INDURA STRUC FXS,VOID	TURE	WATER	COMMENTS
	ORILL NOTES			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	wк	MOD	WELL	EST.	MEAS.		GRAPHIC		
											=							4		
5-64	NO RING	2:40	trum	Bilty very fine sound				9									lonse_		21146ly damp	2 3 2
10-12 =	DHELD	8:50	tan	fin saud		_			Wy( <b>W</b> )								MAA Loose		dry	200 lbs (cat 6"
																	Trose	4		5 12 19
																			dame	Minor Sill
20-21%	BROG RINKS	9:10	lite here	the small		83-BRASS - 10: - File		Į	DUUHAAN Calumna								Mart. 1005e		DCMA	13 21 23
25-267	2 NO RINKS	9.20	lite br	fic - med.				· · · · · · · · · · · · · · · · · · · ·									loose		VERY DAMP	13 19 29
36-311	P Park	9:30	lite Gric	Line-mad sand		3 BRASS No-Full			((((4))))) 9(19-11-1-2								inod loos	-	dramp	14 21 33 # 3 rings
35-36%	1)A 2:0155	/0:00	5,7. 501- bru	fire to in A. Sour !													lorne Lorent by To Da Veinst		Almont Solutions	23 37 33
40-41%	ROAK	10:10	hte gry bric Horne	file san l some med. Treimile comented		3-34055 - . Ko-Full -	ing::::ic,ru		No K <sup>i</sup> uł								Hund Loss. Fe Dr. Alar 1122 [ Masal		Vory dames	110 25 37
45-464	1- ADO RIAKS	10:20	tota 914-	Alay Lie fand minor fe Dr													WK CONISE	-	1954 cemp	22 30 35
		F		4hn																

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						- H											/401	= 1/4	T <u>*/2</u> "_DRI	PAGE_Z_OF_Z_ N RW ILL MODEL
INTERVA		DATE TIME	COLOR	Γ		GEOPHYSICS LOG		GRAIN	SIZE			AIN R			HYC	DRAULIC	INDURA STRUC FXS, VOID	TION &	WATER	COMMENTS
	ORILL		1	ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.		GRAPHIC		· · · · · · · · · · · · · · · · · · ·
30-51/2	11-8-96	19:25	gry tan	very Line		3 32A33			0 U.U.						_		WK-MOIS		moterally	19 31 37
¥	RINGS		<u> </u>	Filty sand		2 - 5411 2 - 20 Full							[ 				CONSOL	1	damp	+3 Rinks
					1	-												1		
55-56%	NO	10.110	an-ten	Herry Lin	<u> </u>				IIIIA								INK MOD	ļ	AIDA - STIL	16 29 40
	RIVES		1	ivery Li. E. Hu sm. P	<b>1</b> <del>.</del> .												DOWNOC	1	druns	
					-						<u>├</u>						· · · ·	-	/	
					1															
60-611/2	RINGS	10:50	Atr. tom	sour fine	<u>+</u>	3-BILASS. NO-FUI			1777 1774 -								CONSI	<b>↓</b>	dama	20 35 44
				2. (+	1										i		001037		(1000-7)	
65-610/2	XI O	11:00	ary - ton	to a 2" 2.11 line						· ·							SANDWE	}		
	RINGS			top 3" 2.14 fin				es j	i j piel								MAD - STT.	1	MOD DAND	110 29 34
			gra-grey	10" chy	4												Lon clan	4		
					1.												2012 (18 4			
70 - 7/%	PINGS	11:15	GAY	Tag 2" clay	2=	2-13 1.455	Males/ Stick										MOD CLY	<u> </u>	11/10/10 41 11	11. 20 37
10- 110			this fore	Inition 10"	<b>.</b>	2-13 nates = No Full		-			i					·····	NOD SAAN			2 RINGS - POTH OF SAND
				Lie Sand	-															
					1										i			1		· · ·
75-76%	ATO DIAL	11:20		althy etc.			Hent 2	4.15				1								14 21 27
	RINGS	11.30	1	dy for all				1, 2, 4									UNK- CONISON		WEDAND	correct into menute of
				(HAYNOR)	]															
80-8112	RINGS	11:45	ary.m	interhold Line		e - 164Ass No - Ext											MON-STR		dia dia	15 44 50@5"
				song-seit-		No- ENH.		ia li												7 RING CLAY / Sill, sons?
				Julty Claud	1															
6		12.1					, l					i								
2, 48. 5	RINCES	1/:00	112-404	Liene his silts	F.7-73		<u>. (</u>	<u>// 1:34</u>									1100-SAC			71 48 50 111111011 Clare 20120 + 3"bd
[					]													l t		WI So Drate
	lunr le		<del>  </del>		4			+						+				ļ	,	·
90-91/2	RINKSS	17:45	444- 44-1	two citte suid	E	C - Breas	9 (4	1	664		1	1					MO-STA-	+		11. 20 50
			`	· 2-cl . 1 130 à		Ver-Full												. F	Acrep	
					1							1			<u> </u>			ŀ		
15-96%	HO PINT	1:00	Jan and a	10 5.14 1-1	ن <u>ت بند بند</u>			त्या इन्द्र									11.00 4 1 12	. [	A. 19	22 36 40
			1346.44	10 site chan			nitate la						+				NOD PANSU	· ł	dam'	
					4						-	<u>.</u>						1		
100-1014	CARC	1:20	Hen over	The Jack	:		<u> </u>	18									MOD CONTON		hry singer	14 32 50 2110 4605

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	/AL (FT)	1	COLOR	цтно		GEOPHYSICS	T	GRAIN	_				OUNDI		HYC	RAULIC	INDURA STRUC FXS, VOID	TION &	WATER	PAGEOF
	ORILI	s I		ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	wĸ	MOD	WELL	EST.	MEAS.		GRAPHIC		
		11-11-90	4		4				<u> </u>											
5-64	- Rine	510:00	tan	fire to med.		4		1									hat inte		molecality	
				miner claves					<u> </u>								Careles Balicum	]	Arman'	2112
					1												CALLED -			
					-		<u> </u>	1				1								
16-114	L All	10:07	I-m_	clayer 5. 14			¥					<u> </u>					Inon		int. News	321
		ľ		Vera has som	2													-		+
				2.2	4			1										-		
15-164	- 544	¥ 10:15															1	1		
-17					_				1							·····		1		
		× 10' 25	+444	Church of the	┫ <u>┍</u>		K#A	1	I.M.H.		<u> </u>	<u> </u>					limo	<u></u>	mentub	5 6 8 dri
20-0				Clang The gand	<b>-</b> .			<u>}</u>	11 11			l	1					-	damp	Arada rings la
					-			1	<u> </u>			1	ļ							there enough
25-269	2 1.00	10:20	Han	sitty Free				19	1			 					MUR 1004.	1	wate	6 12 23
	Riey	<u>s</u>	+	find				144 											Aringues	
					7		-		+				1							
30-31	2 RING	5 10:40	DY- trum	MITE Line		2-CRASS			14				1				Donsed.	+	dings -	15 24 37
			4						<u> </u>			1	<u> </u>							
					<u></u>			1							İ		WK - MOD	1		
35-26	12 ND CINI	<u>10:50</u> 5	ary-sen	tive Jamb	-			-	i nationa								CONGOL	1	ding-	12 21 32
					7							I							- <u>614</u>	
110 11-	70 -1 1/	11:05		Citie Frank	<b>-</b>		-	1	Upmillipe		[		1						51115-	Sau 7.5. 8" 2
10-40	-13 - 1001	e	Piy-tem	4.16 g . "7641 /				1	ļ	<u> </u>		<u> </u>	<u> </u>					]	711	" B" sounde lat
1								+	<u> </u>	<u> </u>	<del> </del> -		<del>†</del>				1	1		Feile - 4 - 6" -1.

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LOGGE	D BY	- <u>2.000</u>	DATE	START_11	WNER 22	INISHED 11	/ <u>,,</u> ,	IOLE C	(( )EPTH	осапо 101 <sup>1/</sup> 2	N: CO	E	<u>, o</u>	RILL	_SEC	را درو اینونه	406 5400. Las 701	- 1/4	T ?''/2''ORI	N R	_w 
INTERVA	NL (FT)	DATE TIME	COLOR	ЦТНОЦ	.0GY	GEOPHYSICS LOG	F	GRAIN REL P			GR.	AIN R	CUNDI	NG	HYC PRO	PERTIES	INDURA STRUC FXS,VOID	TURE	WATER		COMMENT
	ORILL	11-11-96		ROCK TYPE			CLY			GRAV	ANG	wĸ	MOD	WELL	EST.	MEAS.		GRAPHIC			
50-51/2	BADDES RIUGE	11:25		Cley interbaces		2- BRASS Almost											MED-STR MALEN		millio Aque		- 50 Line ser . l
55.56%2	ALO RIANG	<u>  </u> !40	silt	fine cano !!" silt - 4" clay 10"			<b>A</b> Y	81	NA								WIK-MOD ADNISCL		iuk damp	11 18	31
60-6142	RINGS	11:55	ariston in prance	11 - francis Filt	• • • • • •	2-BRASS No - FRII			i l								MOD CONSU	-  	alius + dry		50 Z RIAISS
65-løb <sup>17</sup>	2 NO 20055	12:10	2-v-km	Frade from Loo in 120 the with frie sand, sith				4 <b>21)</b> 190									MON PAUSI		: 1 : 1027. Na 1414 F	19 36	Űζ
73-71%2	ZINCS	.2:25	ten- you	two same		2-BRASS = No Full		1.510		· · · ·							MON A-HSO		MODENERIC MOIST	2' 42	50
75-76%	24)45	12:46		Lis en 1 .	17.27.2												HAD STR		11112512767Y ALANGT	20 37	42_
5 80-81%2	LLINCU TATAA MA DUILS	7:13	rig Coyol	1/2:1/10 1 0 100		_	<u>判生</u> 4.97-	<u>ولې</u> ه									MOD STL		Meist	22 3	2 **)
25- ilo''z	NO RINGE	1:30	Art-see	Noyver day			1416-7-5	  /4   4									NICE 51		Highly Inver	1.3 25	_ਹਰ
90-91 1/2	BRASS	7:45	iy Volieta	vorven Sittaslag		2-BRASS - Almost	je i A Jestro										nieto Aria		;;;; <b>;</b> ;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;	1: 4D 2 ring	
95-96%	ND Kley,s	12:10 		VORUMARIAN with 15"				1	12			     					WA; -17		aniced	6 32 ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	e serve Ce

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P	ROJECT	TREIND		START 11/12/2		nished <u>u/u/a</u>		OLE DE	Loo ЕРТН	1011/2	ANGLE	<u>a</u> <u>- 91</u>		RILL M	IETHO	Hollow Ste	4OF	- 1/4		PAGEOFZ N RW 1 MODEL_ <u>BK_21</u>
INTERVA	L (FT)	DATE TIME	COLOR	LITHOLO	OGY	GEOPHYSICS	R	GRAIN	SIZE RCEN	r	GRA	NN RO	DUNDI	NG		DRAULIC PERTIES	INDURA STRUC FXS,VOID	TURE	WATER	COMMENTS
	ORILL			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	wк	MOD	WELL	EST.	MEAS.		GRAPHIC		
- 1%	11/12/90	10.05		MOVER ?	<u> </u>													1	MOIST	SMERBY TUBE THRU IN COVER RUNVISILT & T
12	SHEL BY	10. 0.3		TILASH	1											Fx LEL		4	70	COVER PLAY/SILT + TI
					]											Celveck +	un tall	4	1224	1/2 1+ @ 500 16.
					]			<b></b>								hole in h	ollew stem			Moshed and of tube
					1											i @ outsi		-	LIDIST	15 5 4
1-61/2	NO RINGS	10:15		MINER 1	4											ACKN ALLEL	100	ł	LIDISI	
	RINGS			TRASU	4											ditto pro	0.75	1	· · · · · · · · · · · · · · · · · · ·	MIST OF SAMPLE NAT RECOMMED (SHE BUC)
	i				4	]	<u> </u>	<del>  </del>								CH TO THO	aunes_	1		A COLLES STR. BOO
					4	1		<del>  </del>									· · · · · · · · · · · · · · · · · · ·	1		
0-11/2	100	10:30		TRAFU	+-	-		†				. 1				EY LEL	00%	<b>-</b> -	shality	27 10 8
0-1172	RUNIS	19.00			1	j												]	danna	PCOR RECOLERY (-3.4"
					]						Ī							1	/	
				<b>•</b> _	]						1					L		4		
					]	1												4	., , , ,	
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10	Rotury	4:24	lt ha -tun	fine sand ORV		-				<u> </u>	0.4	1	10-243			~ 10 <b>?</b> .	GRAVEL CLAST & 11 TO + 2"
									· · · · · · · · · · · · · · · · · · ·	+ +	1	•			<b>-</b> .		AND BERNAMS CARAGE
15		1.21		fine coul									10- 47-31				
		7.26	+ ha.+h	time sand minor growel							<u>1</u>			<u>wik- med</u>	-	~120	shiht damp
								1		· · ·							
<u></u> 20		U:30	the - tra							ý.	<u>auna</u>	1	10.2/13	we-med	<u>+</u> _	~ 127.	slightly dong
				muuer Gau.			1			· · ·	;	<u> </u>			<u> </u>		
20				1				:	:			;	· · · · · · · · · · · · · · · · · · ·				•
25		<u>u:37</u>	+ haca	Line send			\$				. <b>Viitiv</b> 1		10-3	wk		- 100.	Crier
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30		4:36	In	clamere gelt	<u></u>		<u> </u>		· · · ·	1			10- 41	WX-mod		~ 10 %	Ċry
				Sand			;	:	•		!	•		+	7 T		,
-					_ •		•	:			<u>!</u>	!	1		7 7		
35	Eosi	4:40	tan	Sandy clay	72775	1				<u> </u>	<u>1970</u> 1		10	mod		L 157	shyhth dama
						F		÷									
J.		7:30	tan 1	maney fire san	2		; 1115 - 5	4 14			in the second second second second second second second second second second second second second second second	3	10-5	yund.		~ 127.	
						F									- †		
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45	!	7:45	tan	cloging ine		þ	M I	j.					10-5	mod		- 1570	Very porch corted matine
				mon Granal		.							·•	<u>†                                    </u>	!		
40	·y			Marin sit + her		L K	M R						/6-5		:	- 17 00	
				COMPANY SELL - SALV	0	/						!	10 -	1 March			

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1	<u></u>	ROJECI	Pick	las Bi	;08 NUMBER. He	(WAIER (	I H anyan Co	OLLJ :	ADA	Y ENO	JINEEF	RING	C0	мРа 	NY	21		<	<b>ج</b> ح	PAGE_2	_ OF <u>/ 3</u> _
Ĺ	0665	0 SY	5770020	DATE	E START <u>9-27</u>	22 DATE	FINISHED 10-2	н	015 0		to ANG	<u>.</u>	90° (		METHO	AIR ROT	AY R.C.	IAMETER_	OR	N RN	i hrann
INT	ERVA	L (rī)	DATE TIME	COLOR	- чтно	LOGY	GEOPHYSICS LCG	R	GRAIN	SIZE ERCENT	c	RAIN F	RCUND	DING	HM PR(	DRAULIC DPERTIES		TICN & CTURE	WATER	· c	CMMENTS
		DRILL NOTES	9-30-92		ROCK TYP	GRAPHIC		CLY	SLT	SAND	RAV ANG	5  WK	M00	WELL	EST.	MEAS.		GRAPHIC			
	-	Aig Romey 5/4"				-						1	1	1		1					
	55		1:15	tan	silly clay										10-5		mod.	-	~ 257.	chy is part	cally "ball
	60			ten	- 16 - 1									   							
			4.10		silty clay up		_					#/   	<u>1</u> 1	<u>, 1</u>	10-5		mod.		~ 267.	Same Lat"d	mp fee
	65		8:45	gy-tan	fine samely sit							<u> </u>   	1 1 1/44		/o-4 :		wk-med.	]	~ 159.	almost"dry	
												1		   						true grav	<u>+ 2034y</u>
	<u>70 [</u>		9:00	gy-tan	fin candy sil		-				_	1		1	6-51		at most		~15%	minor que	url
												i									
	75		9:02	gy	ritty fine some										10-4		wk - mod		~157.	"flowing Sa	I" almost
	40 H		1:05	tan	fris sandy sitt				   				V/////		10-51						
										1 !			1 1		1		wt-mod		~ 157.		
	<b>8</b> 5		9:00	tra	cluyes free som		l P		4					E	/0.5		WK-mod		- 1576		
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6	<u>10 -</u>		9:10	gy-tan	the sandy you	م میں بر میں اور اور اور اور اور اور اور اور اور اور			·						/0-4		K-mod		- 129.		
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		F	ROJECT	Pickia	- But	e number I te	WINER	- H(			ENGINI	N: CO	Ca	<u></u>		SEC	<u>21</u> 1,'	ィ <u>チン</u> OF	1/4_50	<u> </u>	N <u>R 3</u>	3_0F_/3_ W
1		INTERVA		DATE	DATE			GEOPHYSICS		GRAIN		1			Ī	HYC	PERTIES		TURE	WATER		COMMENTS
		[	ORILL			ROCK TYPE	GRAPHIC		CLY	SLT	SAND GRAV	ANG	WK	MOD W	EL	EST.	MEAS.		GRAPHIC			
	i	AA	D.C.	9-30-92			<u> </u>						i			i 						
		A.m.y	<u>Поталя</u> 15%	0.14	<u>шь.</u> Д.,	sitty fire same							!			10-51		wk-moo		~ 12-152		
			¥	7.12																		
		110		<i>4:20</i>	lf ba-ham	silte frie sand				H	111	i i			/	10-J		wk		~ 107.	DRY , al	most us the fraction
;											   											· ·
		/15		9:25	lt bn • tan	silty him good	† ]:7:5:3#\$			().						10-4		wk-moo		~129.	Some el	uy syan
		120		4.30	lt gytan	silty fite soul		-		W.		1			=†	<u>10 - 3  </u> 		wk		~12 %	less cla	-7
												1					····					
		125		9:32	Hgy tur	clannic It up milet gravel									-/	10.51		WE MOD		~127.		
		/30	USING	9:35	lt gy tam	character in mine gravel		· · ·						<u>+ 1000</u>		10"5 1	·	WK MORS		~12%	Almst dev	<u></u>
			COMPERSI				1 				1	1		1		1 10-4					<u> </u>	
		/35	Up.	9:40	H gy tan	sitty fine and												wk		~ 102	174.	
,		140		9:45	It av-los	silte fire and							:		=	10-4		wk		~ 1292		
	:					minic grovel		-							$\overline{+}$	· · ·						
		145		9:51	ltgy tan	Silty fin sand										10-3/L	•4	WK		~ 15%	almost dam	A / cleanar some
	1		[					÷				•				1						
		150	ł 	9:58	<u> </u>	alt. In contra	() 			f.			· · · ·			10-41		1.1 k - mint	ł	~ 17.90		

		BER_	70-4 D LI	J(	DB NUMBERI He	212049	H H	ULL	ADAI	r Er			NG C	201	47A 	N Y SEC	21.	، <del>ج</del> س ،	e 1 4 5	<b>E</b> - 2	PAGE_4_OF
1.06																					IL MODEL Schra
INTER			DATE TIME	COLOR	r		GEOPHYSICS		GRAIN	SIZE		r -	AIN R			нч	DRAULIC DPERTIES	INDURA STRUC FXS.VOI	TION &	WATER	СЭММ
	OR	TES			ROCK TYPE	GRAPHIC		CLY	SLT	SANC	GRAV	ANG	wĸ	MOD	WELL	EST.	MEAS.		GRAPHIC	-	
	AIR					1			<u> </u>		1		) 						1		
	R. 54	<u>C.</u>				]				1	1				1		1		1		
15	5		/0:00	H be-lan	sandy citt up						1					10-5	!	wk-mod		12-1570	
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14	₀⊟		10:10	tan-ben	silly five same		_		1					pm.	<u> </u>	10-4		Ink . MOD	<u> </u>	~12-157.	
	H				ur gravel	1			1	<u> </u>	1 							<u> </u>			
		_								1	 				1		l				
16	5 —		10:20	ten-hen	ailty fine sand						i I					10-3		we	1	~ /2 7.	Almost Day
						1				<u> </u>	!				 				1		
17	) 10m		10:30	lf . bon tan	silte fine same	<u> </u>	 		w		1			11.5	4	10-3		wk	<u>i</u> .	~1270	still flowing &
	tor ve	-1			·	ł				 	1										
	dri sta				1-				1					1	! !				İ		,
17	5		10:40	bra-tan	sandy CAAUEL				1							/0-3		WE-meo		-12.15%	LASTS MALE BEEN
						İ			!	1											
18		_	10:43	to -tan	fin sandy				u	18					<b>T</b>	10-3		WK-MOD	<u> </u>	129.	
		_			( groud)	4			1												·····
18		_	/0. < .	<u> </u>	file sand	•			1					17/1-1		10-3		wk		127.	fairly well sorted
	Έ	=#							·	ł 	i i	1	1	1							possible few gra
		_		<u> </u>							_			_							
190		_	/0:55	Fa-ben	fine sand		-			UCH5 1						10-3 1		WK		~1270	Alean send
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i					fore sand				_	UCI						10-3		NK		~107.	DRY

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LOGGET		Steened	OATE	START. <u>7-27-</u>	TLOATE	FINISHED 10-2	<u>/</u> н		)EPTH-	640	ANGL	<u> </u>	70 0	RILL, I	LSEC.	······	4. <u>2</u>	AMETER_	ORI	N R <u>3</u>	chrown
TERVAL	」(〒丁)	DATE TIME	COLOR	СТНО	.0GY	GEOPHYSICS LOG			SIZE		GR/	AIN R	CUNDI	ING		RAULIC	INCURA STRUC FXS.VOID	TURE	WATER	c	COMMENTS
	ORILL			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.		GRAPHIC			
	R.C.	9-30-92			1			l	1	<u> </u>	1	_	1					4			
	ROTHRY		<u> </u>	ļ	-			<u> </u>	+									1			
	K 1/12				<u> </u>	]			Ī	1	1			1	1			1			
205	_	11:15	tonbre	silty fine card	4		ļ	<u> </u>		<u> </u>			<u> </u>	·	10-41		WKIMUT	-	~ 126	AMOST DRY	HAVE OF AL
ŀ				·	-	]		I	1	1	1			i							
Ì					1				Ţ	ļ	!		ļ					]			
210		11 : 4 5		finto coarga					199	1		<b></b>	11		10-3		wk	4	~127	LESS SILT	
		11.63	LIDER- BALK	Sand		-			i l	1	1	· · · ·			1						
ļ					]			}	<u> </u>	<u> </u>					1			1			
ł					-			, 										i			
215		11:30	Have bru	silty sound	<b>1</b>	1		U	it juit i	1			UM		10-41		wk		~123	MORE SILT	AS DEFORE
ļ				· · · · · · · · · · · · · · · · · · ·	4			 		 				i				1			
ŀ									<u>i</u>	i .				i				1		·	
								1					11). 11).		10-5		WK-mo	ł	~127.	MORE CLAY	
220	<	11:40	How-bra	silty fire some	<u></u>	- 1				1				7	10 - 1		WE - MAD	÷ -	~! <u>~</u> /•	MORE CERY	
l	<u> </u>				1			i	1		I				1			1			
Į	ط- السنو		<b>_</b>		4			1	<u></u>	<u> </u>	i										
225	< 1000 mg	11:55	1+600	fine - coarse									ШĽ,		70.31		WK . MOD		~10-12%	NO CLAY	
[	down			gand my	<u> </u>			!	1		!				!			!			
-				some Gammer	-			1			1							i			
ł					4			i	1	i	1				, j			!	4100		
		17:19	br-tan	silty good up	2	· -		<u> </u>		g			ША		10.41		MOD		Typed Delynn	+ Cause on	
ŀ	vp			gravel	-			···· `·	1								<u> </u>		~127.	+ 200149	
Į				L	]			1	1	1					!						
		1-2-4.		sit fire same					N/L	1	<u>.</u>				10-4 :		WK-MOD		- 17.20	l	
235		12.30	MA DA	Sing the source					1	1											
ſ					4				1	<u>.                                    </u>											
l					┥.				1												
240		12:50	tan-bon	sitty fine sind		-			III ii				li da		10-4 .		WK-MOD		~ 12 ?		
. 1				<u> </u>	÷		'	• •	+	<u></u>					•	·····					
į				<u> </u>					1								[				
									і И.),			-	-		10-4/10				~ 12.90	GETTING FINE	<u> </u>
245!		100	therebon	time same sense		T .	· · · · ·					8			10//		WK-MOD		···/	DEILING CING	<u> </u>

						Herry Co.									21 1/	4500 01	- 1/4 <u>5</u> 6	<u> </u>	PAGE 6 OF 13
LOGGE	о ву <u> </u>	front	DATE	START 9-29-	ZLOATE P	TNISHED 10-2	L н	0120	EPTH 640	- ANGL	<u>e - 9</u>		RILL	METHO	)	DI	AMETER	DR	ILL MODEL Schramm
NTERVA	L (FT)	DATE TIME	COLOR	UTHOL	OGY	GEOPHYSICS		GRAIN	SIZE	GR,	AIN R	CUND	ING		DRAULIC DPERTIES	INDURA STRUC FXS.VCIC	TURE	WATER	COMMENTS
	ORILL	1		ROCK TYPE	GRAPHIC		CLY	SLT	SANDGRAV	ANG	wк	мор	WELL	EST.	MEAS.		GRAPHIC		
	R.C.	9-30-92			1							1	i		1		4		
	ROPARY	_			i i						_	!			1		4		
255	5'/4"	1:45		gilts fin and										10-4		MOD	4	~12.15%.	TRACE CLAY
	¥											 				CONSOCIUM	9		
	rean to																		
20	12 4	2.00	hen - her	fre sandy filt				WALK .						10-5		NOD	4	~12?	WRITUALLY DAY + DUSTY
	Set.				+			[	<u>   </u>	. !			i						
	Casing																i		
7.5	0 to 270	2:03	han ben	fine soundly's. It						<u> </u>	(	illa li	1	10-5		wk-MOD	1	~127.	
دملا				miner gravel					1 1				[						
2-10 7-10		7:10	4 hon	elaystone			il in the	//	<u> </u>	<u>  </u>		 		10-6/10		NOD-STR		ATTECT	INSTA MOISTURE WAS
	Pulmer																	POLYMER	"DAY " SAMNE WENTED
272	ANTECTAL	r		<u> </u>	ł					<u> </u>									TPACE SAND, MINDLSILT
276	CALINE		11.6	CLAY STONE			111/06		1 <u> </u>					10-7		NOD-STR.		~~~	WETTER JAMALE BUT
	UP ON	615	VE DEN	CLAYSTONC					·!		-			10 1				···· •	CLAY DUST BEFOR INJECTU
	VODT			l <u></u>	4														
280			7	ILAY STONE			il Taf.		 					10-7	· · · · · · · · · · · · · · · · · · ·	MOD-STR .		6209.	DUST P DISCHARGE (PAY)
609		2:20	Tun	CLAY STONE	====	-		n						10		- au zik		60. Gev 7.	MUCH OF SILT FRACTION BEA
					ł													·····	AS DUST CLAY BLOWING AWAY
		4					10.05							10-7:		un De CO			
Z85		2:25	tan	CLAN STONE									/	( <u>0- / i</u>		NOD-5TR	ł	~ 25%.	WETTER BY INFECTION SLIGHTLY
					İ.												ŀ		
-					!		171151		1					1			ļ	1	
290	:	2:30	1-tan	CLAMSTONS		-	!Г .: Ц							16-7		MOD-STA	+	< 70%	
					1									1			F		
					i												L L		
295	<u>-</u> -	2:35	tan	CLAYSTONG				I		!				<u>10-7 +</u>		MOD-STR		- 20 %	R.C. AR; WILL FRAM 1244
					]				1	· · ·		1					Ē		MUD RUTA RY 0-300 PT. END OF SHIFT & 5:00
			<u> </u>	<b></b>	-					<u> </u>				····· ;			-		HEND FE DENT (P 3:00

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	PAIECT	Pille	es Bi	B NUMBERI	WNER_C	anyon Co			ENC	ATION	N: CO.	Ca	ngo	۰	_SEC	<u>211</u>	/ <u>4 جند _o</u> f	1/4 <u>5</u>	5 7 2	PAGE 7 OF 13 N R 3 W
LOGGE	) в <u>ү.5</u>	newo	OATE	START 9-29-	22. DATE	FINISHED 10-2	Цн	OLE D	EPTH_4	40	ANGL	<u> </u>	200	RILL M	AETHO	AIRRO	<u>912.7</u> 01	AMETER_	<u>8"</u> ORI	LL MODEL Schramn
INTERVA	_ (FT)	DATE TIME	COLOR	итноц	OGY	GEOPHYSICS LOG		GRAIN	SIZE ERCENT		GR/	AIN RI	CUND	ING		DRAULIC IPERTIES	INDURA STRUC FXS,VCI	TURE	WATER	COMMENTS
	DRILL			ROCK TYPE	GRAPHIC		ar	SLT	SANDG	RAV	ANG	wĸ	MOD	WELL	EST.	MEAS.		GRAPHIC		
	S AIR	10-13-92			1													4	NO HOO	REAMED 0-279' CHECK FOR WATER - JOND MORPHERETURN WATER
305		7:40	ليم	SILTY CLAY											10-6		wk-mon cousello	ł	wetted to	REAL MOLE WAIT 2 HALS - NO H. 
	AIR		LTT-TAW	SILTYCLAY			I DUL E								10-6 -6		WE-MOD	Leare	~ 357,	HEQUIDES ELOWING
310	CORE			и П				<del>‼</del> —	┝──┼						- 6			CLAT _		POOL SAMPLE CORE
310	Y	2:30	14	u	1=====	-	1440		<u> </u>						-6		<i>"</i>	No CAR	> 35%	304 - 311: L 1 ft RECOVERED
	AIR	[	LTTAN	SHITY CLAY					$\left  - \right $						-6		м	vnas f	>35%	COLE ATTEMPT AGAM
	CORE AGAIN	5.	<u>u</u>	16			ŴЛ.								-6			王	>35%	COST RECOVERY (311 - 315 BAMPLE VERY DAMP - DELEASE
315	V	5:30	- 10	14		-	<u> </u>						· · · · ·		- 6	) 		i	2.35°4	FILM OF MOISTURE ON CONLET
	an	10-14-92	<u> </u>	ļ	-			<u> </u>	+				l	<u> </u>		I		1		32-313 Pulled for 1ab hest
	Anner 4"	<del> </del>	<u> </u>		1			1										]		
					]	.1	â.				ļ		<u> </u>		10-5/10	1	WE MOD	-	>15%	SLIGHTLY DELEA FROM HOT
320		7:15	IT TAN	SULTI CLAY		न -			<del>†</del>				<u> </u>	<del>;</del>	10 710		The mer	<u> </u>		Compressor HIR ROTHLY
	$\neg$				1									1				]		
					]				<u>↓</u>					<u>+</u>			<u> </u>	{	<u> </u>	
		12.22		SHTY CLAY		4	<b>T</b> ille (1	1/1	┼╍╍┼					+	10-6		wk-mon	1	>357.	
325		1.23	VT TAN	SITT COAY		1		1	<u>i i</u>			i				ļ		]		
					]			<u> </u>	╄			} 	<u>                                      </u>	┝───	<b> </b>			4		
	<u> </u>				4		-	<u> </u>	++					+				1		
330	<u> </u>	7.50	IT TAN	CLATEN SILT	<u>1=-=-=</u>	F .	li -	14	1			1		1	10.5		<u>uk</u>	<u>]</u>	~ 5<2	
			1		<u> </u>			ļ	<b>┼</b> ──┼				<u> </u>	<u> </u>	<b>[</b>	l	+	1		
		<u> </u>	<u> </u>		-			<u> </u>	┼╍╼┼						<u> </u>			1		
				1	1			1										]		
305		4 05	LT TAN	CLAYFY SILF		-	μ.		┼──┼		<u> </u>				10-5	<u> </u>	WK	4	~ 32 %	
	<u> </u>			·	4		$\vdash$		+ +									1		
															ļ	ļ		]		
340							-		$\frac{1}{1}$		<u> </u>	<u> </u>			10-5		WK	-	~ 3575	
	<u> </u>	8:15	IT TAN	CLAMES SILT				1	1 1				1	i		1				
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					_			<u>+</u>	<u>+                                    </u>		<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u>}</u>	+	1	<u> </u>	
345		8.30	LTTAN	CLAYPY SILT		<u>.</u>	1	<b>p</b> %	<u>i i</u>			İ		1	10-5		₩K	1	> 3571	QUITE DANP
			1		1	-1		1							ļ		+	4		<u></u>
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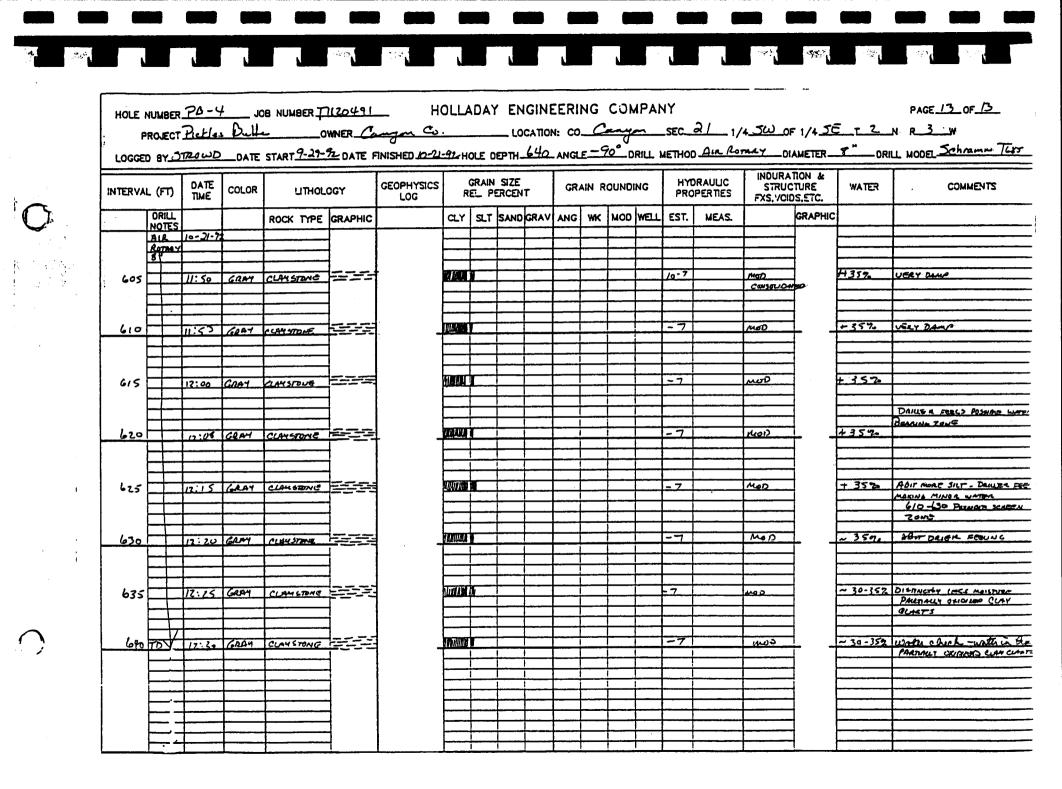
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LOGGE	0 BY	strowd	OATE	START 9-29-	22-DATE	FINISHED 10-24	<u> </u>	OLE O	EPTH 640	ANG		<u>'0° (</u>	RILLI	NETHO	0	01	AMETER_	OR	LL MODE Schrenn
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505	AIR COLE NO NECOLE AIR LOTANY	10-20-7 7 10-21-9 10:35	Z Max gay	<u>CLAM</u>			    						2 2 2 3	10-7		12k-200		As were	Clean field to Trip in them water of sector 9:00 - 1020 none (10-21-91) 10-20-7 - AIR Cont H49 No Ascorery DUP TO COSE FORMATION - 40 BUDING MATERIAL FORMATION - 40 BUDING CATERIA.
510		10:40	Tenk 687	SILTY CLAY		_		<b>é</b>					1	-7		wk-mai)		+ 35%	Soo-SOS VERY BAAD
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515		10:45		SILTY CLAY										-6		مدموم - بحن		~ 35 %	ALA LOUGER IN HALLS @ DISCOME
<u> </u>		10:47	MEDGRY	CLAYEY SILT			KO1							-57-	6	WK		~?5%	
525		10:50	GRAY	Эктчесач										-6]	-7	wκ.		~ 357.	Trace sand
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535		10:55	60.07	SILTY CLAY										- 7		UNC 601016		+ 35 <i>9</i> 1	
<u> </u>		10:59	GRAY	<u> &lt;11.79</u> (LAY		-		 						- 7		WK=M07		<u> ナ マぐ り。</u>	DUITE DAME
<i>క</i> #5		11:01	GRAY	SILTY CLAY						· · · · · · · · · · · · · · · · · · ·	1					wk hamap		+ 35 %	
イボル	y	11:05	(-An	SILTY CUM				: :				1				2)+ Jamos		1 75%	

HOLE		BER_	<u>PB-4</u>	JC	DB NUMBERI	2120491				Y ENGI						21	ر <del>ر</del> لیا <del>ک</del> ر		<del>2</del> - Z	PAGE 12 OF 13
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58			/1:28	GRAY	CLAY STONG		-1 -			<u> </u>		<u> </u>	<u>ii</u>							
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58	۶H		11:30	BRAY	CLAY STONE			101 - L				+	1		-7		MOP		+ 55 %	ABIT HARDER MATTA
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Form 238-7 4/92 State law requires that this report be filed with within 30 days after the completion	NATEI	R RES S R Directo		ORT artment of Water Resources		
1. WELL OWNER         Name       PICKLES BUTTE SANITARY LANDFILL         Address      15_Albany, Caldwell, ID 83605         Drilling Permit No.          Water Right Permit No.	S F A C	tatic wa lowing? rtesian ontrolle	closec closec ed by:	rel <u>514</u> feet below land surface. Yes INO G.P.M. flow d-in pressure p.s.i. IValve ICap IPlug 77 °F. Quality <u>Poor</u> Describe artesian or temperature zones below.		
<ul> <li>2. NATURE OF WORK</li> <li>X New well Deepened Replacement</li> <li>Well diameter increase Modification</li> <li>Abandoned (describe abandonment or modification procedures such as liners, screen, materials, plug depths, etc. in lithologic log, section 9.)</li> </ul>		] Pum	EST D p G.P.M.	🗇 Bailer 🗇 Air 🗆 Other	<b>_</b>	
3. PROPOSED USE Domestic Irrigation X Monitor Industrial Stock Vaste Disposal or Injection	Bore	De	OGIC	LOG 70568 Material		ater
Other (specify type)  4. METHOD DRILLED	124		4.0	tan fine sandy silt	Yes	No
Air □ Auger ★ Reverse rotary     Cable □ Mud □ Other     (backhoe, hydraulic, etc.)	11 11 17 17 17	40 48 140 185 225	140 185 225	brown sandy gravel tan silty clay gray silty fine sand gray fine to med sand light gray clayey silt		
5. WELL CONSTRUCTION Casing schedule: X Steel Concrete Other Thickness Diameter	11 11 11 11 11	240 250 275 320	250 275 320 400	light gray silty fine sand tan clay fine to med sand mixed gray fine sand and tan clayey silts gray fine sand		
Was casing drive shoe used?       Yes       No         Was a packer or seal used?       Yes       No         Perforated?       Yes       No         How perforated?       Factory       Knife       Torch         Size of perforation?       inches by       inches         Number       From       To	10" 10"	435 455 485 560	455 485 560 620	no sample tan gray silty claystone gray brown silty fine sand clayey silt and fine sand blue gray claystone	X X	
Top Packer or Headpipe Bottom of Tailpipe				RECEIVED		
Diameter <u>4</u> Slot size <u>.020</u> Set from <u>512.5</u> feet to <u>522.5</u> feet Diameter <u>Slot size</u> Set from feet to <u>feet</u> Gravel packed? Types No Size of gravel <u>10/20</u> Placed from <u>496</u> feet to <u>535</u> feet				NOV 3 0 1993 WATER RESOURCE		
400-496 Surface seal depth <u>Material used in seal</u> : Cement grout Bentonite Puddling clay <u>Sealing procedure used</u> : Slurry pit	, · ·			RECEIVED NOV 2 6 1093		
<ul> <li>□ Temp. surface casing</li> <li>□ Overbore to seal depth</li> <li>Method of joining casing:</li> <li>□ Solvent Weld</li> <li>□ Cemented between strata</li> </ul>	10.	0 <b>9</b>	1004	Dopt control of or any Treasure		
Describe access port Top of casing with locking cap and protective cover	··	Work	started	<u> </u>	3- <u>9</u>	<u>'</u>
6. LOCATION OF WELL Sketch map location must agree with written location. N Subdivision Name <u>Pickles Butte</u> Landfill Lot No Block No County <u>Canyon</u> Address of Well Site <u>Perch Road</u> , Pickles Butte	11.	I/We of compl Firm N Addres	certify ied with Name <u>B</u> ss <u>Box</u>	CERTIFICATION that all minimum well construction stand h at the time the rig was removed. <u>oyles Brothers</u> Firm No. <u>503</u> 25608 Salt Lake, Date <u>1-23</u> rilling Supervisor		
Address of Well Site <u>Perch Road</u> , <u>PICKIes Burte</u> (give at least name of road) $\underline{SW} \ \underline{W} \ \underline{NE} \ \underline{V4} \ \underline{Sec.} \ \underline{21} \ , R. \ \underline{3} \ \underline{SV} \ \underline{C} \ or \ \underline{V} \ \underline{V}$				and perator)	perviso	<i>or)</i>

USE ADDITIONAL SHEETS IF N 30" 2" " FO Y "FD THE WE TE CO PY TO THE DEPARTMENT

. Form 298-7 4/92

## STATE OF IDAHO DEPARTMENT OF WATER RESOURCES

**WELL DRILLER'S REPORT** State law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

1.	WELL OWNER		ATER				
	Name PICKLES BUTTE SANITARY LANDFILL	s	tatic wa	ater lev	el <u>491</u> feet below land surface.		
		F	lowing?	• 🗆 •	Yes 🖾 No G.P.M. flow		
	Address 6284 Perch Road, Caldwell	A	rtesian	closed	d-in pressure p.s.i.		
	Drilling Permit No. <u>63-93-W-0554-001</u>		ontrolle	ed by:	□ Valve □ Cap □ Plug		
	Water Right Permit No		empera	.ure	75 °F. Quality <u>Poor</u> Describe artesian or temperature zones below.		<u> </u>
2.	NATURE OF WORK	8. W	/ELL T	EST D	ATA		
<b>.</b>	X New well Deepened Deplacement	1 г	] Pum	o	🗆 Bailer 🗆 Air 🗆 Other		
	Well diameter increase			-			
	<ul> <li>Abandoned (describe abandonment or modification procedures</li> </ul>	D	Ischarge	G.P.M.	Pumping Level Hours Pu	Imped	
	such as liners, screen, materials, plug depths, etc. in lithologic						
	log, section 9.)						
3.	PROPOSED USE						
	Domestic     Irrigation     R     Monitor	9. L	ITHOL	UGIC	Log 70567		
	□ Industrial □ Stock □ Waste Disposal or Injection	Bore	Dep		Material	_ Wa	
	Other (specify type)	Diam.		То		Yes	No
	METHOD DRILLED	12 <b>3/4</b>			silty sand		ļ
4.		11	<u>17</u> 18		sandy gravel		
	Image: A contract of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	1	60		tan silty clay med sand		
	Cable Mud Other	11	95		tan calyey silt		
	<pre></pre>	14	125	160.	tan_clav		
5.	WELL CONSTRUCTION	12 74	160	195	fine sand		
<b>.</b>	Casing schedule: 2	<u>7 18</u>	195	. 220	silty_clay		
	Thickness Diameter From To	11	220		fine and med sand		
	25 inches <u>4</u> inches + <u>2.5</u> feet <u>487.5</u> feet	11	360	380	tan clayey silt fine sand		
	inches feet feet	11 11	380 435		<u>tine sand</u> 435-490 tan, 490-510 gray si	lit v	ļ
	inches feet feet	11	435 510		gray silty clay		
	Was casing drive shoe used?  Yes Xo Was a packer or seal used? Yes Xo Yes	11	620	600	gray clay stone		
	Perforated?	7 78	690	-700	gray silty clay		<u> </u>
	How perforated?  Factory  Knife  Torch  Gun	<b> </b>	<b> </b>				┣──
	Size of perforation? inches by inches						
	Number From To						-
	perforations feet feet feet		<u> </u>				
	perforations feet feet						
	Well screen installed?  Yes  No						<u> </u>
	Manufacturer <u>Houston</u> Type <u>Stainless Stee</u> 1						
	Top Packer or Headpipe		+		RECEIVED		
	Bottom of Tailpipe		1		NOV 3 0 1993		<del> </del>
	Diameter Slot size 020. Set from $487.5$ eet to $497.5$ eet	<b> </b>	1				<u> </u>
	Diameter Slot size Set from feet to feet				WATER RESOURCES		
					WESTERN REGION		
	Gravel packed? $\Box$ Yes $\Box$ No $\Box$ Size of gravel Placed from478 feet to515 feet	<u> </u>		[			–
					RECEIVED		
	Surface seal depth $\frac{478}{100}$ Material used in seal: Example 2 Comment grout		+	<b> </b>	NOV 2 C JOSE		
	Bentonite      Puddling clay     Sealing procedure used:     Slurry pit	<b> </b>	1		<u> </u>		<b>†</b>
	∑ Temp. surface casing □ Overbore to seal depth		<b></b>		Disguidefinite of the doubt the second	<u>.</u> 1	
	Method of joining casing: 🔀 Threaded 🗆 Welded	L	1				<u> </u>
	□ Solvent Weld □ Cemented between strata	10.					
	Top of casing with locking				9 71 07	07	
	Describe access port Top of casing with locking cap and protective cover.		Work s	started	<u>7-31-93</u> finished <u>11-20-</u>	<u>93</u>	
	^ <b>^</b>						
6.		11.					
	Sketch map location must agree with written location		J/We c	ertify 1	that all minimum well construction standa	ards v	vere
	Subdivision Name Pickles Butte	1.腳	<b>Con</b> pli	ea witl	h at the time the rig was removed.		
			Firm N	lame _	Boyles Brothers Firm No. 503		
	WE Lot No Block No09	1994	Addres		<b>f</b>	9-	د _
	County Canyon	7			Date 11-23-		_ر
	Address of Well Site <u>6284 Perch Road</u>	1	Signec	by Di	illing Supervison Sary K. Hull	<b>.</b>	
	(give at least name of road)			•	and 17 422		
	·- · ·			: (O)	perator)		
	<u>SE</u> ¼ <u>NW</u> ¼ Sec. <u>21</u> , R. <u>3</u> E □ or W 🖄				/If different than the Drilling Supe	erviso	r)
				• • • • • •	· L		•
	USE ADDITIONAL SHEETS IF NECESSARY - F	ORWA	BU Th	in an an	TELC DAY TO T T PEDA T T'T		

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Form 23 4/92	<sup>38-7</sup>	•
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## STATE OF IDAHO DEPARTMENT OF WATER RESOURCES

**WELL DRILLER'S REPORT** State law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

1.	WELL OWNER		ATER					
	Name PICKLES BUTTE SANITARY LANDFILL				rel <u>539'</u> feet below la			
	Address _6284 Perch Road, Caldwell		lowing?			P.M. flow		
	Drilling Permit No63-93-w-0554-001 003				I-in pressure p.s. □ Valve □ Cap □			
	-							
	Water Right Permit No.		51112010		<u>77</u> °F. Quality <u>Poor</u> Describe artesian or temperature zon	nes below.		
			/ELL T		ATA			
2.	NATURE OF WORK		/ELL T					
	Image: Well diameter increase     Image: Modification	"	] Pum	р	🗆 Bailer 🗀 Air 🛛	Other		
	<ul> <li>Well diameter increase</li> <li>Modification</li> <li>Abandoned (describe abandonment or modification procedures</li> </ul>	D	ischarge	G.P.M.	Pumping Level	Hours P	umped	
	such as liners, screen, materials, plug depths, etc. in lithologic							
	log, section 9.)		··· ··-					
	· · · · · · · · · · · · · · · · · · ·							
3.			ITHOL	00101	06	70565		
	Domestic      Irrigation      Monitor     Industrial      Stock      Waste Disposal or Injection		· · · · · · · ·					
	Other (specify type)	Bore Diam.	Dep	oth To	Material		Wa Yes	ter No
ļ		12 <b>1</b> 4			tan clayey sand		169	NU
4.	METHOD DRILLED	"	25	35	sandy gravel			
	🗶 Rotary 🛛 X Air 🗂 Auger 🗴 Reverse rotary		35		fine sand			
l	Cable Mud Other		55		tan clayey silt			<u> </u>
	(backhoe, hydraulic, etc.)	- H - H	65 130		fine and med sand tan clay			
-	WELL CONSTRUCTION		185		clayey fine sand			
5.		11	210	_250	silty clay			
	Casing schedule: Steel Concrete Other	и и	250	260	fine sand			
	Thickness Diameter From To <u>25</u> inches <u>4</u> inches <u>+</u> <u>2.2</u> feet <u>535</u> feet	 	260		<u>clayey silt</u>		••	
	inches feet feet		280 370		fine sand clayey silt			
	inches inches feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet feet  feet feet feet feet feet feet feet feet feet	1234	390	455	fine sand		·	
	Was a packer or seal used?	10"	455	515	silt			
	Perforated?	<u> </u>	515	525	tan clayey silt		X.	
	How perforated?  Factory  Knife  Torch  Gun		545	540 570	gray clayey silt gray clay		X	
	Size of perforation? inches by inches	54"	570					
	perforations feet feet	54"		630	blue gray clay			
	perforations feet feet							
	perforations feet feet	<u> </u>						
	Well screen installed? 🛛 Yes 🗆 No Manufacturer <u>Houston</u> Type <u>Wire Wrap</u>				<u>~~~~~</u>			
	Top Packer or Headpipe				RECEIVED			
	Bottom of Tailpipe	}	<u> </u>		NOV 3 0 1993			
	Diameter4"_ Slot size02 'Set from 535 feet to 555 feet			<u> </u>			<u>.</u> .	
	Diameter Slot size Set from feet to feet				WATER RESOUL WESTERN REGION		-	
	Gravel packed? ⊠X Yes □ No □ Size of gravel 10/20							
	Placed from525_ feet to566_ feet							
	Surface seal depth520 Material used in seal: 🛛 Cement grout				RECE	EIVED		
	Bentonite     Puddling clay				Nov 3	6 1993		
	Sealing procedure used:  Sturry pit Tomp, surface casing Overham, to seal depth							
	□ Temp. surface casing □ Overbore to seal depth Method of joining casing: □ Threaded □ Welded		<u> </u> .		<u>ceparinent er</u>	water Recource		
	Solvent Weld     Cemented between strata	10.						
	Describe second and Tan of section with most state		\A/!	ا اس جد	10 01 00		,	
	Describe access port <u>Top of casing with protective</u> cover and lock	۲ ۱	work s	arted	<u>10-01-93</u> finishe	a <u>11-20-9</u> 3	<u> </u>	
6.	LOCATION OF WELL		DRILLI	ER'S C	ERTIFICATION			
	Sketch map location must agree with written location.				hat all minimum well const	ruction stands	ards v	vere
	Subdivision Name <u>Pickles Battee</u>			-	at the time the rig was rem			
	Landfill		-		Boyles Brothers Firm			
	w E E Lot No Block No		1 ( <b>1</b> )				a.	` ,
	County Canyon FED		Addres	s	Date	<u> </u>	-7	<u>j</u>
	· · · · · · · · · · · · · · · · · · ·	9 190	Signed	by Dr	illing Supervisor	KHill.		
	Address of Well Site <u>6284 Perch Road</u> (give at least_name of road)	'~.74	7	1	and	····	7	
	<u>. NW 14 SE 14 Sec. 21</u> , R. <u>3</u> E □ or W K				perator)	- +7		
	<u> </u>			\ <b>~</b>	Ut different than th	e prilking Sup	erviso	r)
<b></b>	USE DDITIONAL SHEETS IF MFOR SO 'TY - F	ÖRWA	RD TH			-		
	° − 1−−41 × − − − − − − − − − − − − − − − − − −		erer y Ki	N 1	- see a second of the second of the	<b>.</b>		

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Form 23	B-7 <sup></sup>
4/92	

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## STATE OF IDAHO DEPARTMENT OF WATER RESOURCES

State law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

4	WELL OWNER	7. W	ATER	LEVEL	_			
1.	CANVON COUNTY (DICKLES DUTTE LANDETLI)	7. WATER LEVEL         Static water levelfeet below land surface.         Flowing?       Yes         X No       G.P.M. flow         Artesian closed-in pressure p.s.i.						
	Name <u>CANYON COUNTY (PICKLES BUTTE LANDFILL</u> )							
	Address 115 Albany, Caldwell, ID 83605							
					-			
	Drilling Permit No. <u>63-93-W-0554-<del>001</del> <b>の</b>のみ</u>			-	□ Valve □ Cap □ Plug			
	Water Right Permit No		empera	ture	<u>74</u> °F. Quality <u>Poor</u> Describe artesian or temperature zones below.			
			/= <b>T</b>					
2.	NATURE OF WORK	8. WELL TEST DATA						
	🖄 New well 🛛 Deepened 🔅 Replacement				🗆 Bailer 🗆 Air 🗆 Other			
	Well diameter increase     Modification							
	□ Abandoned (describe abandonment or modification procedures			G.P.M.	Pumping Level Hours P	umped		
	such as liners, screen, materials, plug depths, etc. in lithologic							
	log, section 9.)							
	· · · · · · · · · · · · · · · · · · ·							
2	PROPOSED USE							
5.		70566						
	Domestic     Irrigation     Monitor	9. L	9. LITHOLOGIC LOG					
	Industrial   Stock  Waste Disposal or Injection		Dep	oth	Meterial	Wa	ter	
	Other (specify type)	Diam.	From	Τo	Material	Yęs	No	
		1234	0	10	tan silty sand		x	
4.	METHOD DRILLED	11	10		tan clayey silt		x	
	🕅 Rotary 🖾 Air 🗂 Auger 🖾 Reverse rotary	11	25		fine sand		x	
	□ Cable □ Mud □ Other	11	35		tan clayey silt		x	
	(backhoe, hydraulic, etc.)	17	50		tan clay		x	
		11	70		silty fine sand		x	
_		<u>ψ</u>	100		clay		X	
5.	WELL CONSTRUCTION	!!	105		fine sand		X	
	Casing schedule:  Steel  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  Concrete  C	9.1 11	11 5	120	tan clay		·x	
	I hickness Diameter From IO	11	120		fine sand		x	
	<u>25</u> inches4 inches _+2,5 feet377 feet	11	120 125		tan silty clay		x	
	inches inches feet feet	11	145		sand with cobbles		x	
	inches inches feet feet	17	150		tan silty clay		x	
	Was casing drive shoe used?   Yes  No	1.	240		gray clay		X	
	Was a packer or seal used? 🛛 Yes 🖾 No	1234			gray clay	x		
	Perforated?   Ves X No	<u> </u>	305	424	gray Clay	.^		
	How perforated? 😰 Factory 🛛 Knife 🗆 Torch 🗔 Gun						<u> </u>	
	Size of perforation?020 inches by inches		<u> </u>					
	Number From To							
	perforations feet feet							
	perforations feet feet						<u> </u>	
	perforations feet feet							
	Well screen installed?	ļ						
	Manufacturer Houston Type Stainless Steel					<b>.</b>		
	Top Packer or Headpipe							
	Top Packer or Headpipe							
					NOV 3 0 1993			
	Diameter <u>4<sup>tt</sup></u> Slot size <u><math>020</math></u> Set from <u><math>377</math></u> feet to <u>407</u> feet	<u> </u>						
	Diameter Slot size Set from feet to feet		<u> </u>		WATER RESOURCES WESTERN FLIGION			
	Gravel packed?  Yes No Size of gravel	<u> </u>					<u> </u>	
	Placed from299 feet to424feet	┣──	<u> </u>				<b> </b>	
	004	<u> </u>	ļ		RECEIVED			
	Surface seal depth $294$ Material used in seal: 🕱 Cement grout	<b> </b>		· · · · ·				
l	🗶 Bentonite 🛛 Puddling clay 🛛	<u> </u>			NOV 2 6 1593			
1	Sealing procedure used:   Slurry pit	J	<u> </u>	L				
Í	🙀 Temp. surface casing 🛛 🗆 Overbore to seal depth	┣	<b>_</b>		ວິຊີຍະຫລັກປະຊິດ ເປັນເປັນສາ (ມີຍິວເປັນໄດ	~	<u> </u>	
	Method of joining casing: 🙀 Threaded 🖾 Welded	<b>—</b>			l			
	Solvent Weld Cemented between strata	10.						
		-			A 00 FF	z		
ĺ	Describe access port <u>Top of casing with protective</u>	/e	Work s	tarted	<u> 10-26-93</u> finished <u>11-20-9</u>	<u>р</u>		
I	cover and locking cap.							
6.	LOCATION OF WELL	11.	DRILLI	ER'S C	CERTIFICATION			
ĺ								
ĺ	Sketch map location must agree with written location	(		-		alus V	w¢1¢	
		Subdivision Name <u>Pickles</u> <u>Buttle</u> Sanitary Landfill Lot No Block NoFEB_0 9 1994 dress Date Date						
ĺ								
ĺ	W Lot No Block No FFR A							
ĺ								
	s County <u>Canyon</u>							
	Address of Well Site Perch Road Pickle Butte	1	Signed	by Dr	illing Supervisor Lawyk Hill	<u></u>		
ĺ	Address of Well Site <u>Perch Road, Pickle Bufte</u> (give at least name of road)				and			
	T.     2     N     3     0# S       SW     ¼     NW     ¼     Sec.     21     , R.     3     E     or W     ⊠	1		in	perator)			
	<u>_SW</u> ¼ <u>_NW</u> ¼ Sec. <u>21</u> , R. <u>_3</u> E □ or W 🖄	T**		1	/ If different than the Drilling Supe	erviso	r)	
							·/	
	USE ADDITIONAL SHEETS IF NECESSARY F	ORWA	RD TH	37 - 40	TO THE DEPART - T			

	F WATER RESOURCES Use Typewriter or BRIS REPORT NOV 2 1 1995 Ball Point Pen
	<b>FRIS REPORT NOV 2 1 1995</b> Ball Point Pen
	ENSNEFONI NUV 2 0 1955 Bailt Onit / en
	63855 WATER RESOURCES OF 2
1. DRILLING PERMIT NO. 63-95-6-6564-001	11. WELL IESIS:
Other IDWR No.	Pump     Bailer     Air     Flowing Artesian
2. OWNER: County of Campon Name HOLLADAY ENGINEERING	Yield gal./min. Drawdown Pumping Level Time
Address 1431 BUS ALT HWY 95	
City PAYETTE State II) Zip 83661	NOV 2 7 1995
	Water TempBottom hole temp Water Quality test or comments:
3. LOCATION OF WELL by legal description:	Water Quality test or comments:
Sketch map location must agree with written location.	12. LITHOLOGIC LOG: (Describe repairs or abandonment) Water
	Bore
Twp. 2 North or South	Dia. From To Remarks: Lithology, Water Quality & Temperature Y N
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$\begin{array}{c c} & & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ &$	17 28 CARGER GRAVEL + HARD PAN
	/ 28 30 CLAY & SMALL GRAVEL
Address of Well Site PICKLE BUTTE DumP	2 30 32 MORE GRAVEL LODGER
(Give at least name of road + Distance to Road or Landmark)	7 32 40 CLAY-TIGHT IN SMALL GRAVEL
· ·	10 40 90 CLAY-TIGHT IN SMALL GEAVEL 2 90 95 COARSE SAND IN CLAY
Lt BlkSub. Name	7 95 112 SANDY CLAY
4. PROPOSED USE:	7 112 120 CLAY
Domestic Municipal	> 120 135 CLAY W/COARSE SAND
🗌 Thermal 🔄 Injection 🔄 Other	(135 180 HARD CLAY
5. TYPE OF WORK	(180 182 JUPER HARD CLAY 182 205 CLAY
• New Well Decide Modify or Repair Replacement Decide Abandonment	205 210 COARSE SAND ! CLAY
Mud Rotary Air Rotary Cable Other	7 210 743 VARY HARD CLAY THRU REG
	S 263 265 VERY HARD CLAY
7. SEALING PROCEDURES	( 245 305 SOFT ELAY/ JANDY CLAY
SEAL/FILTER PACK AMOUNT METHOD Material From To Sacks or	7 305 315 SAND ( 315 375 CLAY
BCDTODITE OF 381 1900 # POUR	7 375 400 VERY HARD GLAY (CLAY ROLD)
	SHOD 405 JOFT SANDY CLAY/CLAY
	5 405 430 REG CLAY
Was drive shoe used? 👾 Y 🔲 N Shoe Depth(s)	7 430 435 SOFT CLAY OK SANDY CLAY 7 435 445 CLAY REG TYPE
8. CASING/LINER:	5 445 455 HARD CLAY "DARK PEAGRAVEL/COARSE SAN
Diameter From To Gauge Material Casing Liner Welded Threaded	1455 465 SAME 1 1 1 1
41 + 3 508 Smulless # 🗆 🗆	7465 470 JOFT CLAY LIKE SANDY CLAY
	5 470 475 CAAY 4 475 480 CLAYSTONE + SANDSTONE LIKE POS
Length of Headpipe Length of Tailpipe	9 475 480 CLAYSTONE SANDSTONE LIKE PCS 8 480 487 11 " & K 4 6 "
9. PERFORATIONS/SCREENS	2 HOT 510 GRAY BLUE CLAY
Perforations Method	CONTINUES
X Screens Screen Type 3 Husion	Completed Depth <u>544</u> MAR 0.7 199(Measurable)
From To Slot Size Number Diameter Material Casing Liner	Date: Started Completed
From To Slot Size Number Diameter Material Casing Liner	13. DRILLER'S CERTIFICATION
	I/We certify that all minimum well construction standards were complied with at
	the time the rig was removed.
	Firm Name HDAMSON FUMPS DULLING Firm No. 0457
10. STATIC WATER LEVEL OR ARTESIAN PRESSURE:	A Si
<u>513.11</u> ft. below ground Artesian pressurelb. Depth flow encounteredft. Describe access port or	Firm Official Laure Ungenuson Date 11-17-95
control devices:	and Supervisor or Operator Dave, Adams m. Date 11-17-95
	(Sign once If Firm Official & Operator)

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FORWARD WHITE COPY TO WATER RESOURCES

						itor	
Form 238-7 7/94				R RE	SOURCES Use Typewr or Ball Point P		
	WELL DRILL				63656		
1. DRILLING PERMIT NO.	<u>13-95-W-0564-001</u>	11.	WELL D Pu		TS: PG 2092 Bailer Air Flowing Artesian		
2. OWNER:			Yield gal./			me	
	<u> </u>					••	
	StateZip					•	
3. LOCATION OF WELL by	legal description:				Bottom hole temp or comments:		_
Sketch map location must agree wit	h written location.	12			IC LOG: (Describe repairs or abandonment)		
	,	Bore	T	<b>r</b>	Remarks: Lithology, Water Quality & Temperature	Wat y	
		Dia. 8	From	To 511	FRAC GRAY & BLUE CLAY	Ť	N
	East □ or West ↓ 		511	513	REG. " "		
Gov't Lot	County C. AD acres 160 acres	$\mathbf{D}$		528	FRAC CLAY		
					VERY HARDCLAY BLUE/GRAY		
Address of We	Il Site	Ĥ	523.6	530	REG. FRAC/HARD DRILLINGCLAYF	20	
(Give at least name of road + Distance to Road or L	Landmark)	1	531	544	REG CLAY BLUE/GRAY	>	
Lt BikS	ub. Name						
							-
4. PROPOSED USE:	Monitor Irrigation						
🗆 Thermal 🛛 🗆 Injection	□ Other						
5. TYPE OF WORK	air 🗆 Replacement 🛛 Abandonmen	,t			RECEIVED		
6. DRILL METHOD		· _					
Mud Rotary Air Rotary			<u>+</u>		NOV 2 0 1953		
7. SEALING PROCEDURES SEAL/FILTER PACK	AMQUNT METHOD	ı			WATER RESOURCES WESTERN REGION		
Material From To	Sacks or Pounds						
		┨┠──	-				
Was drive shoe used?	N Shoe Depth(s)	1					
Was drive shoe seal tested? Y $\square$ N		.			RECEIVED		
8. CASING/LINER:	Motorial Copies Lines Wolded Threads						
Diameter From To Gauge	Material Casing Liner Welded Threaded		<del>.</del> .		NOV 2 7 1995		
					Department of Water Resources		
Length of Headpipe	 Length of Tailpipe		An e	7 19	96		
9. PERFORATIONS/SCREE	NS		1				
Perforations Method     Screens Screen Type	j		<u>I</u> molete	l		surabl	e)
		Da	ite: Sta	rted	8-25-951 Completed 9-29-		- '
From To Slot Size Number	+ + · · · · · · · · · · · · · · · · ·	**************************************			CERTIFICATION		
					S CERTIFICATION minimum well construction standards were compl	ied wit	th at
		the t	ime the	rig was	s removed.		
		Firm	Name	AA	AMSON Pune DRILLING Firm No The algeringon Date 11-1 rato Dave Alamson Date 11-1	04	57
· • · - · · · · • · · · · - · · · · ·	OR ARTESIAN PRESSURE:		G	5×	510		
	sian pressurelb.	Firm	Officia	Шã	Ut Clauson Date 11-1	7-4	5
Depth flow encountered control devices:	ft. Describe access port or	and	onvioor	or 0	Pain Adamson mult-	74	25
	· · ·	_ oup	ervisof (	u opei	Sign once if Firm Official & Operator)	- /	$\mathbf{\nabla}$

(Sign once if Firm Official & Operator)

Normalized       Well DRILLER'S PEPORT NOV 201955       Ball Point Pen PL 04 201956         DRILLING PERMIT NO. 623-95-W-0565-001       11. Well TESTS: WATER RESOURCE November 2019       Pl 04 201957         Drine TDWR No.       Pump       Different Permit Participation Pump       Pump       Different Permit Participation Pump       Pl 04 201957         DWNER:       Country 91 Caruyen Country 91 Caru		
DRILLING PERMIT NO. 02.2.72.40.2020.       DUT         IN MELL TESTS: MAIL MAY Section         Nowners:       County 4         IN MELL TESTS: MAIL MAY Section         Name Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABA		MEVHIC
DRILLING PERMIT NO. 02.2.72.40.2020.       DUT         IN MELL TESTS: MAIL MAY Section         Nowners:       County 4         IN MELL TESTS: MAIL MAY Section         Name Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABAY EXERCISE         Mare Hold LABA	$\bigcirc$	Dagar NON S I BAD D 10 F 2
Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ         Differ <thdiffer< th=""> <thdiffer< th=""> <thdiffer< t<="" td=""><td>. DRILLING PERMIT NO. 63 - 95 - W-0565 - 001</td><td>11. WELL TESTS:WATER RESOURCES</td></thdiffer<></thdiffer<></thdiffer<>	. DRILLING PERMIT NO. 63 - 95 - W-0565 - 001	11. WELL TESTS:WATER RESOURCES
MOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         North # or South C	Dther IDWR No	Pump 🗇 Bailer 🗆 Air 🗆 Flowing Artesian
MOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         NOV 2.7 1555         North # or South C	OWNER: County of Caryon	Yield gal./min. Drawdown Pumping Level lime
Inty       Aviet Time       Isteint D, 2p, S.366/1       NULL Z / SS3         a. LOCATION OF WELL by legal description:       Water Tomp       Baltom hole turny.         b. LOCATION OF WELL by legal description:       Water Tomp       Department of Water Resources         intermal       Twp       Anoth iff or west #       Water Tomp       Department of Water Resources         intermal       Twp       Anoth iff or West #       112       Standard P, Standard M, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Oueldy, Water Ouel	lame HOLLADAY CUGINEERING CO	
No. LOCATION OF WELL by legal description:       Water Temp		
I. DCATION OF WELL by legal description:       Water Quark fest or comments:       Department of Water Resources         N       Image: Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21. Sec. 21.		
North # for South	LOCATION OF WELL by legal description:	
n       Twp2       North for a South for a South for a south for a sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control of the sendard control control the sendard control control of the senda	• •	Water Glashy lest of comments.
Twp         North #         or         South #         or         South #         or         South #         or         North #         or         North #         or         North #         or         North #         or         North #		12. LITHOLOGIC LOG: (Describe repairs or abandonment) water
Two         Z         North %         or         South %           Rgo         East         or         West %         1         5         TOP % OIL         1         5           Sec         21         30         14         ALC 14         14         1         5         TOP % OIL         12         5         10         ALAY %         14         15         TOP % OIL         12         3         14         5         10         20         GeAviel 1         5         12         12         3         14         20         GeAviel 1         5         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         14         15         15         17         10         14         15         15         15         15         15         15         15         15         15         15         15         15         16         14         16         16         16         16         16		Roro
Sec.         21         30         14         14           GortLat         Counter         Counter         12         5         10         CLAY W/SmALL GRAVEL           Soc         Address of Weil Site (55 D0         M/15S OURL,         10         20         GraveL 4         SADD           Soc         Address of Weil Site (55 D0         M/15S OURL,         Soc         14         47         CLAY W/SmRL GRAVEL           Soc         Marketin         Soc         14         47         CLAY W/SmRL GRAVEL         SADD           Soc         Marketin         Soc         14         47         CLAY W/SmRL GRAVEL         SADD           Soc         Marketin         Soc         14         47         CLAY W/SmRL GRAVEL         SADD           Soc         Marketin         Soc         14         47         CLAY W/SmRL GRAVEL         SADD           PROPOSED USE:         Soc         Soc         Marketin         Fingeliacament         Abandonmart         Soc		Dia. From To Remarks: Lithology, Water Quality & Temperature Y N
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S. TYPE OF WORK         I 125       130       SALD       Work       CLAY         I Nodify or Repair       Replacement       Abandonment       130       135       SALD       Work       CLAY         I Nuck Curry       Cable       Other       130       135       SALD       Work       CLAY         I Nuck Curry       Cable       Other       130       135       SALD       Work       CLAY         I Nuck Curry       Cable       Other       130       135       SALD       Modele Curry         I Statemain       From       To       Seaustrip       Werk       Hardon       Modele Curry       Werk       Hardon         I Statemain       From       To       Seaustrip       Metria       Metria       Seaustrip       Metria       Metria       Metria       Metria       Metria       Seaustrip       Metria       Seaustrip       Metria       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip       Metria       Seaustrip	🗆 Domestic 🛛 Municipal 🛶 Monitor 🗂 Irrigation	
We Well       Modify or Repair       Replacement       Abandonment         Mult RetHop       Mult Rotary #Rain Rotary       Cable       Other       135 135       Saudo 4 Multic Clay         SEALING PROCEDURES       SEALING PROCEDURES       205 210       Saudo 4 Multic Clay       136 135 134       Very 4 March Clay         SEALING PROCEDURES       Material       From 10       Seate of 100 POLLC       205 210       Saudo 4 Multic Clay       126 205 210       Saudo 4 Multic Clay         Seate of 10 Police       Material       From 10       Seate of 100 Police       205 210       Saudo 4 Multic Clay       215 220       Saudo 4 Multic Clay       206 215       Saudo 4 Multic Clay       216 220       205 20       Saudo 4 Multic Clay       216 220       Saudo 4 Multic Clay       206 275       Saudo 4 Multic Clay       216 220       Saudo 4 Multic Clay       206 337       Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic Clay       Multic	Thermal Injection Other	
S. DRILL METHOD       Mud Rotary * Air Rotary       Cable       Other       135       136       Yere + HARD CLAY         Mud Rotary * Air Rotary       Cable       Other       136       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205       205<	5. TYPE OF WORK	
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8       225       2/0       SANDY       CLAY         SEALFILTER PACK       AMOUNT       METHOD       2/5       SANDY       CLAY       2/10       2/15       SANDY       CLAY       2/10       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       CLAY       2/15       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY       SANDY	5. DRILL METHOP	
SEALING PROCEDURES         SEAL/FILTER PACK       AMOUNT         Material       From         To       Sacks or Pounds         BELITEN DITE       Do         Material       From         Seal/FILTER PACK       AMOUNT         Material       From         BELITEN DITE       Do         Material       From         Seal result       Seal result         Was drive shoe used?       Material         Casing Liner       Casing Liner         Was drive shoe seal tested?       Material         Casing Liner       Casing Liner         Was drive shoe seal tested?       STEEL         Benetice       From         To       Gauge         Material       Casing Liner         Was drive shoe seal tested?       To         Benetice       Casing Liner         Was drive shoe seal tested?       To         Secaling Liner       Casing Liner         Benetice       Casing Liner         Benetice       Casing Liner         Benetice       Statuless         Benetice       Casing Liner         Statice       Material         Sod       Statice <t< td=""><td>🗆 Mud Rotary 🚽 Air Rotary 🗆 Cable 🛛 Other</td><td></td></t<>	🗆 Mud Rotary 🚽 Air Rotary 🗆 Cable 🛛 Other	
SEALFILTER PACK       AMOUNT       METHOD         Material       From       To       Sacks or Pounds         BENTD NITE       DP ROOD       POUR       325       SANDY CLAY       SEALFILTER PACK         BENTD NITE       DP ROOD       POUR       320       Soch Short CLAY       Sack of CLAY       Sack of CLAY         Was drive shoe used?       PY       N Shoe Depth(s)       330       305       SANDY CLAY       SANDY CLAY       SANDY CLAY         Vas drive shoe used?       PY       N Shoe Depth(s)       333       341       UERY HARD CLAY       300       305       SAND         Vas drive shoe used?       PY       N Shoe Depth(s)       339       341       UERY HARD CLAY       330       305       SAND       247       341       300       305       SAND       247       247       341       300       305       SAND       247       341       300       305       SAND       247       341       300       305       300       305       SAND       247       341       341       341       341       341       341       341       341       341       341       341       341       341       347       341       347       346       347 <td></td> <td></td>		
Material       From       To       Sacks or Pounds         BENTONITE       20       12.000       POUR         Was drive shoe used?       Y       N       Shoe Depth(s)         Was drive shoe used?       N       How?       33.91       U.L.A.Y         Beauter       From       To       Gauge       Material       Casing       Liner         10       0       1/4       72.5       STEEL       How?       32.9       341       430       LLA.Y         8       H2       SOULTS       STEEL       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?       How?		
Pounds       Pounds         BEUTD NITE       Pounds       Pounds         BEUTD NITE       Pounds       Pounds         BEUTD NITE       Pounds       Pounds         BEUTD NITE       Pounds       Pounds         BEUTD NITE       Pounds       Pounds         Beuton Nite shoe used? Material       N Shoe Depth(s)       Pounds         Vas drive shoe used? Material       Casing Liner Welded Threaded       Point Not State Not CLAY       Point Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not State Not Not State Not Not State Not Not Not Not Not Not Not Not Not Not	Material From To Sacks or	
300       305       SAND         Was drive shoe used?       Y   N Shoe Depth(s)       331       334       CLAY         Was drive shoe seal tested?       Y   N Boold       How?       331       334       CLAY         B. CASING/LINER:       Diameter / from to Gauge Material       Casing Liner Welded Threaded       455       455       457       YSuper VIRV HARD CLAY       Dejutice You         8. +2       500       25       STEEL       -       -       446       470       CLAY       Dejutice You         8. +2       500       25       STEEL       -       -       -       446       470       CLAY       -       -       -       446       470       CLAY       -       -       -       446       470       CLAY       -       -       -       446       470       CLAY       -       -       -       -       -       -       -       446       470       CLAY       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       - <td>Pounds</td> <td></td>	Pounds	
Was drive shoe used? Y N N Shoe Depth(s)         Was drive shoe used? Y N N Shoe Depth(s)         Was drive shoe seal tested? Y N N How?         Was drive shoe seal tested? Y N N How?         S. CASING/LINER:         Diameter From To         0 O       140         10 O       140         12 Stop 125       STEEL         14 + 2       500         15 O Headpipe       Length of Tailpipe         16 O       140         17 Hos       Rec. CLAY         18 + 2       500         19 O Headpipe       Length of Tailpipe         19 Perforations       Method         10 O       Streens         10 O       140         110 O       1400         110 O       1400         110 O       1400         110 O	BENTONITE POUR	
Was drive shoe used?       Image: Material casing liner weided Threaded       339       341       VERY HARD CLAY         Biameter       From To Gauge Material Casing liner weided Threaded       455       457       150       162       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455       455	·	
Was drive shoe seal tested? Y I N How?       Image: State of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the stat		
B. CASING/LINER:         Diameter       From       To       Gauge       Material       Casing       Liner       Welded       Threaded         10       0       140       125       STEEL       Image: Completed       H455       467       Stupper ("VERY HARD)       CLAY       Image: Completed       H457       H455       H457       H455       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457       H457	Vas drive shoe used? # Y N Shoe Depth(s)	
Diameter       From       To       Gauge       Material       Casing       Liner       Welded Threaded         10       0       1-0       125       STEEL       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel       Image: Steel<		HAD 455 VERY HORN CLAN FROM
10       0       140       125       STEEL       #       0       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       Reg. CLay       457       455       855       555       CLay       457       455       555       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556       556		H55 467 NEW DEC W/LOV LLOPN CUNN
8       +2       500       125       STEEL       14       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       - <td< td=""><td></td><td></td></td<>		
4       1+2       504       STANLESS       Image: Stand Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standing Standi	أثالته ومستحد ومستحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتحد والمتح	
ength of Headpipe       Length of Tailpipe         D. PERFORATIONS/SCREENS         Derforations       Method         Method       Mage 0, 7, 199         Screens       Screen Type         From       To         Stot Size       Number         Diameter       Material         Casing       Liner         504       534         Jo 20       41         StrainNess       Casing         Liner       Image: Casing         StrainNess       Certify that all minimum well construction standards were complied with all the time the rig was removed.         Liner       Firm Name         HDAM SDA       Firm No. D4457         Firm Official       Cath Completed Date         Liner       Firm Official         To below ground		
Perforations Method Perforations Method Screens Screen Type Houston Casing Liner So4 534 .0 20 44 StratNes Casing Liner To Slot Size Number Diameter Material Casing Liner So4 534 .0 20 44 StratNes Casing Liner To Slot Size Number Diameter Material Casing Liner So4 534 .0 20 44 StratNes Casing Liner To Slot Size Number Diameter Material Casing Liner So4 534 .0 20 44 StratNes Casing Liner So4 534 .0 20 44 StratNes Casing Liner So4 534 .0 20 44 StratNes Casing Liner So4 534 .0 20 44 StratNes Casing Liner So4 534 .0 20 44 StratNes Casing Liner So4 534 .0 20 44 StratNes Casing Liner So4 534 .0 20 50 Stratic Water Level OR ARTESIAN PRESSURE: The below ground Artesian pressure Lib.	· · · · · · · · · · · · · · · · · · ·	
Perforations       Method       Mill 0 7 19       S25 540 SAND COARSE W/CUAY         Screens       Screen Type Houston       Casing Liner       Completed Depth       Completed Depth       Completed 9 29 9 5         From       To       Slot Size       Number Diameter       Material       Casing Liner       Iner       Completed Depth       Completed 9 29 9 5         504       534       o 20       41       Stranvers       Casing Liner       INer       <		
Screen       Screen Type       Hou Ston       Completed Depth       CONTINUED       (Measurable)         From       To       Slot Size       Number       Diameter       Material       Casing       Liner         504       534       0 20       4'       Statives       Image: Casing       Liner         13. DRILLER'S CERTIFICATION       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casing       Image: Casi	フロークション Perforations Method Market Market Market Market Market Market Market Market Market Market Market Part 1	
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From       To       Stot Size       Number       Diameter       Material       Casing       Liner         504       534       020       41       StAtN/25       0       0       13. DRILLER'S CERTIFICATION         504       534       020       41       StAtN/25       0       0       13. DRILLER'S CERTIFICATION         10. STATIC WATER LEVEL OR ARTESIAN PRESSURE:       0       0       10.       10.       10.         11. below ground       Artesian pressure       1b.       10.       10.       10.       10.		
Artesian pressureIb.     Idve certify that all minimum well construction standards were complied with at     the time the rig was removed.     Firm Name ADAM SON RUNP \$) RILUXEFirm No. 04/157     Firm Official Data addressed by the firm No. 04/157     Firm Official Data addressed by the firm No. 04/157	From To Slot Size Number Diameter Material Casing Liner	
Artesian pressureIb.     Idve certify that all minimum well construction standards were complied with at     the time the rig was removed.     Firm Name ADAM SON RUNP \$) RILUXEFirm No. 04/157     Firm Official Data addressed by the firm No. 04/157     Firm Official Data addressed by the firm No. 04/157		13. DRILLER'S CERTIFICATION
Image: the below ground       Artesian pressureIb.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the time the rig was removed.       Image: the time the rig was removed.       Image: the time the rig was removed.         Image: the timage: the time the rig was removed.       <		
10. STATIC WATER LEVEL OR ARTESIAN PRESSURE:        ft. below ground       Artesian pressureIb.         Depth flow encounteredft.       Describe access port or ontrol devices:		
IO. STATIC WATER LEVEL OR ARTESIAN PRESSURE:        ft. below ground       Artesian pressurelb.         Depth flow encounteredft.       Describe access port or ontrol devices:		Anonenittura : Daving num
ft. below ground       Artesian pressurelb.       Firm Official Data (form for		Firm Name IUITINON IUNP \$/ KILUNE Firm No. 0495
π. below ground Artesian pressureID. Firm Official Java UGametro Date <u>11-11-75</u> Depth flow encounteredft. Describe access port or and control devices: Date <u>11-11-95</u>		CALL THE IS OF
ontrol devices: Date 11-11-95		Firm Official Java Ugam Jon Date 11-17-75
Supervisor or Operator 12 dula 1-11 275	•	and Dave Adams
(Sign once if Firm Official & Operator)		

7/94	OF WATER RESOURCES Use Typewriter or Ball Point Pen
1. DRILLING PERMIT NO. <u>63-95-W-0565-001</u>	63658 PEZOF 2
Other IDWR No	🗆 Pump 🗆 Bailer 🔤 Air 🗔 Flowing Artesian
2. OWNER: JULY DAY ENGINEERING CO	Yield gal./min. Drawdown Pumping Level Time
Address CityP_B_10StateZip	
3. LOCATION OF WELL by legal description:	Water Temp Bottom hole temp Water Quality test or comments:
Sketch map location <u>must</u> agree with written location.	12. LITHOLOGIC LOG: (Describe repairs or abandonment) Water
	Bore From To Remarks: Lithology, Water Quality & Temperature Y N
Twp North 🕅 or South 🗆	
V East U U West Q Esec. $\lambda$ 1/4 $\int U$ 1/4 $\int U$ 1/4	COARSE SAND
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	
s /	
Address of Well Site	CAVED IN TO 544
(Give at least name of road + Distance to Road or Landmark)	
LtBlkSub. Name	
4. PROPOSED USE:	
Domestic Injection Information     Thermal Injection Other	
5. TYPE OF WORK	
New Well     Modify or Repair     Replacement     Abandonment	RECEIVED
6. DRILL METHOD	NOV 2 7 1995
7. SEALING PROCEDURES	Department of Water Resources
SEAL/FILTER PACK AMOUNT METHOD Material From To Sacks or Material From To Sacks or	
Pounds	
Was drive shoe used?  Y N Shoe Depth(s)	
Was drive shoe seal tested? Y I N How?	RECEIVED
Diameter From To Gauge Material Casing Liner Welded Threaded	
	M04 5 0-000
	WATER RESOURCES
	WESTERN REGION
Length of Headpipe Length of Tailpipe	
□ Perforations Method <u>MAR 0 7 1996</u>	
Screen Screen Type	Completed Depth_544 (Measurable)
	Date: Started 8-25-95 Completed 9-29-95
From To Slot Size Number Diameter Material Casing Liner	13. DRILLER'S CERTIFICATION
	I/We certify that all minimum well construction standards were complied with at
	the time the rig was removed.
	Firm NameFirm No
10. STATIC WATER LEVEL OR ARTESIAN PRESSURE:	OX A.
ft. below ground Artesian pressurelb.	Firm Official Have (Colam Son Date/1-17-95
Depth flow encounteredft. Describe access port or control devices:	Firm Official Auto Actam son Date 11-17-95 and Supervisor or Operator David Acta Mison Date 11-17-95
	(Sign once if Firm Official & Operator)

FORWARD	WHITE COPY TO	WATER RESOURCES

#### S:\Projects\ES09.0154\_Pickles\VR\_Drawings\ES09\_0154\_07B\_borelogs.dwg PB-11 (1of5)

Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome         Outcome <t< th=""><th>1</th><th></th><th>_Fickles (VR_browings (E303</th><th>1</th><th>UOI E(U</th><th></th><th></th><th></th><th></th></t<>	1		_Fickles (VR_browings (E303	1	UOI E(U				
0       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -		[		Graphic		Designation		Symbol	Comments and Lithology
100.0'       100.0'       100.0'       255/252       1015       CL-SC       Sandy day/days send, light brownich gray (2.5Y 6/2).         200.0'       10 <sup>+</sup> Steel cesing (1mmoorry)'       -0.0'-0.0'       255/252       1015       CL-SC       Sandy day/days send, light brownich gray (2.5Y 6/2).         300       -15 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesing (1mmoorry)       -10 <sup>+</sup> Steel cesing (1mmoorry)'       -10 <sup>+</sup> Steel cesi					1 7		0-5	CL	Silty clay, light brownish gray (2.5Y 6/2).
10-1       10-2       252/255       10-15       Cl-50       Sandy cloy/cloyey send, light brownish gray (2.5Y 6/2).         20-1       10-3       252/255       10-15       Cl-50       Sandy cloy/cloyey send, light brownish gray (2.5Y 6/2).         20-1       10-3       252/255       10-15       Cl-50       Sandy cloy/cloyey send, light brownish gray (2.5Y 6/2).         20-3       305/205       20-24       MH       Cloyey sill, gray/nb brown (251 % 5/2), for platicity, hard.         30-3       50       305/205       22-23       305       305       Sand, dipt brownish gray (2.5Y 6/2).       Him is to medium-grained, moderately sorted, moderately sorted, moderately sorted, moderately sorted, moderately sorted, moderately sorted, moderately sorted, moderately sorted, moderately indurated.         30-3-340.01       757/755       35-50       SP       Sand, dipt is provide well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately to well sorted, moderately indurated.         90-12       707/705       50-55       SV       Sand, dipt if we sond, gray (2.5Y 6/1), modsine, grading, medium-grained, down or (2.5Y 6/2), fine-grained, weaki inducted.         90-12						70%/90%	5-10	SP	Sand, light gray (10YR 7/2), medium gravel, well sorted.
and and any state of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the se	10-			777777	10	25%/25%	10-15	CL-SC	Sandy clay/clayey sand, light brownish gray (2.5Y 6/2).
29       4.5" O.D. Stainless steller (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank stell (S.S.) blank			(temporary)			40%/50%	15-20	SM	Silty sand, light yellowish brown (7.5Y 7/3), fine-grained, well sorted.
30       4.5° 0.0. Stanless steel (S.5) blanc 0.0° - 04.0°       3907,907 397,907       22-36 27-36       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 04.0°       Sm steel (S.5) blanc 0.0° - 00.0°       Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm steel (S.5) Sm	20-				20-	90%/90%	20-24	мн	Clayey silt, grayish brown (2.5YR 5/2), low plasticity, hard.
30       0.0       - casing 0.0       0.0       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solution       - solut	, , , , , , , , , , , , , , , , , , ,		6666	is SP		90%/90% 70%/90% 70%/90%	24-25 25-27 27-30	SP SP SV	Same as above.
0.0-340.0°       60°       75%/75%       35-40       MH-SM       Cloyey all and ally fine sand, light gray (5Y 7/1), lowind ted, some arrange banding, moderately inducted.         9       40       75%/75%       35-40       MH-SM       Cloyey all and ally fine sand, light gray (5Y 7/1), lowindted, some arrange banding, moderately inducted.         90       50       30%/30%       50-55       SP       Sand, dry (2.5YR 7/1) to light brownish gray (2.5YR 6/2), prominent orange banding, medium-grained, moderately inducted.         100       12° Borehole       50.0°-200.0°       50-30       Sitty and, light gray (2.5YR 7/1) to light brownish gray (2.5YR 6/2), prominent orange banding, medium-grained, moderately inducted.         10       12° Borehole       13%/4°       80       40%/40%       60-65       ML-SP       Sitty and, light gray (2.5YR 7/1) to light brownish gray (2.5YR 6/2), prominent orange banding, medium-grained, weakly inducted.         10       12° Borehole       13%/4°       80       40%/40%       60-65       ML-SP       Sitty and, light gray (2.5Y 6/1), mossive, grading downward to sand, alive yellow (2.5Y 6/6), medium-grained, well sorted, ford.         10       100°       100°       100°       100°       100°       100°       100°       100°       100°         10       100°       10°       100°       100°       100°       100°       100°       100° </td <td></td> <td>× 1</td> <td></td> <td>SM:</td> <td>- <sub>-</sub> -</td> <td></td> <td></td> <td></td> <td></td>		× 1		SM:	- <sub>-</sub> -				
a       40       3/4" Bentonite onlog       3/4" Bentonite onlog       3/4" Bentonite onlog       10/7/3/2       3/3-80       40-45       SP       Some as above.         3       50       50       50       50       50       Some as above.       Some as above.         3       50       50       50       50       50       50       Some as above.         50       50       50       50       50       50       Some as above.         50       50       50       50       50       Some as above.         50       12" Borehole 50.0"-200.0"       55-60       SM       Sitty send, light gray (25 YR 7/1) to light brownish gray (25 YR 6/2), prominent orange banding, medum- grained, moderately sorted, sort.         70       10       60       60-65       ML-5P       Sitty send, light aray (25 Y 6/1), massive, grading downward to sand, slightly moist.         70       10       60       60-65       ML-5P       Sitty send, light brownish gray (25 Y 6/2), fine-grained, slightly moist.         70       10       600,7/600       70-75       SM       Sitty send, light brownish gray (25 Y 6/2), fine-grained, slightly moist.         80       657,7657       80-85       SP       Sond, light brownish gray (2.5Y 6/2), fine-grained, slightly moist.         9	30-1								moderately cemented.
B								MH-SM	
B       10/7/5%       60-50       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G       G <td< td=""><td>8 40- </td><td></td><td>Chips</td><td><u> <u> 111111111111</u></u></td><td>40</td><td>70%/70%</td><td>40-45</td><td>SP</td><td>Sand, dry color light gray (10YR 7/2), medium—grained, moderately to well sorted, moderately to well indurated.</td></td<>	8 40- 		Chips	<u> <u> 111111111111</u></u>	40	70%/70%	40-45	SP	Sand, dry color light gray (10YR 7/2), medium—grained, moderately to well sorted, moderately to well indurated.
grained, moderately sorted, sort.         grained, moderately sorted, sort.         grained, moderately sorted, sort.         grained, moderately sorted, sort.         grained, moderately sorted, sort.         grained, moderately sorted, sort.         grained, moderately sorted, sort.         sitty sort, light of the brown (2.5Y 5/4) to grayish brown (2.5Y 6/1), massive, grading downward to sand, olive yellow (2.5Y 6/6), medium-grained, weakly inducated.         multiple         multipl	ין יי S pun		0.0'-60.0'	SP		75%/75%	4550	SP	Same as above.
a       12" Borehole       12" Borehole       50.0° 200.0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°       50° 0°				SW	50	30%/30%	50-55	SW	Sand, light gray (2.5YR 7/1) to light brownish gray (2.5YR 6/2), prominent orange banding, medium— grained, moderately sorted, soft.
1       0       0000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       10000       100000       100000       100000	t Belo		12" Borehole			20%/20%	55-60	SM	Silty sand, light olive brown (2.5Y 5/4) to grayish brown (2.5YR 5/2), fine—grained, weakly indurated.
70       70       70       59/ML       70       50/60%       70-75       SM       Silty sand, light brownish gray (2.5Y 6/2), fine-grained, slightly moist.         80       90       65%/65%       80-85       SP       Sand, ight brownish gray (2.5Y 6/2), fine-grained, slightly moist.         90       55%/55%       80-85       SP       Sand, light brownish gray (2.5Y 6/2), fine-grained, well sorted, moderately indurated, slightly moist.         90       55%/55%       80-85       SP       Sand, light brownish gray (2.5Y 6/2), fine-grained, well sorted, moderately indurated, slightly moist.         90       55%/55%       85-90       SP       Same as above, dry.         90       55%/55%       85-90       SP       Same as above, dry.         90       55%/55%       85-90       SP       Same as above, dry.         90       50%       50%/20%       90-95       SP       Sand, light brownish gray (7.5YR 6/2), fine- to medium-grained, moderately sorted.         100       55%/85%       95-100       SM       Sand, light gray (2.5Y 6/1), silty fine-grained, softer than above, slightly moist.         100       90       95%/85%       95-100       SM       Sand, light gray (2.5Y 6/1), silty fine-grained, softer than above, slightly moist.         100       90       95%/85%       95-100       SM	<u>ยั</u> 60 -				60-	40%/40%	60-65	ML-SP	Silty very fine sand, gray (2.5Y 6/1), massive, grading downward to sand, olive yellow (2.5Y 6/6), medium- grained, well sorted, hard.
Neat cement grout       SM						45%/45%	65-70	SP-ML	Sand, as above, grading downward to silt and silty fine sand, slightly moist.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	70-				1 1	60%/60%	70–75	SM	Silty sand, light brownish gray (2.5Y 6/2), fine-grained, slightly moist.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			Neat cement grou 60.0'-308.0'	ıt (	- III	20%/20%	75-80	SM	Similar to above, finer—grained, dry.
90       90       SP       90       20%/20%       90-95       SP       Sand, light brownish gray (7.5YR 6/2), fine- to medium-grained, moderately sorted.         100       100       SS / 85%       95-100       SM       Sand, light gray (2.5Y 6/1), silty fine-grained, softer than above, slightly moist.         Geologist: J. Raucci       Drilling method: Core, air rotary       Northing: 668731.199         Driller: HAZ-Tech       Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420')       Northing: 263735.206         Elevation: 2654.1 (TDC)	80-				80	65%/65%	80-85	SP	Sand, light brownish gray (2.5Y 6/2), fine—grained, well sorted, moderately indurated, slightly moist.
Geologist: J. Raucci       Drilling method: Core, air rotary         Driller: HAZ-Tech       Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420')         Easting: 243735.206         Elevation: 2654.1 (TDC)				SP		55%/55%	85-90	SP	Same as above, dry.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	90				90-	20%/20%	90-95	SP	Sand, light brownish gray (7.5YR 6/2), fine— to medium—grained, moderately sorted.
Geologist: J. Raucci       Drilling method: Core, air rotary       Northing: 668731.199         Driller: HAZ-Tech       Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420')       Easting: 243735.206         Date completed: 6=30=11       Sempleted: 10" (0'-50"), 12" (50'-200'), 9 7/8" (200'-420')       Elevation: 2654.1 (TOC)						85%/85%	95-100	SM	Sand, light gray (2.5Y 6/1), silty fine-grained, softer than above, slightly moist.
Driller: HAZ-Tech Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420') Easting: 243735.206	100				100				
Date completed: 6-30-11 Semiling during 10 corp. in other contract (200) (200) Flevation: 2654.1 (TOC)			-				•	•	
$\mu$ but to indicate $\nu$									
Steel suface casing: 16" steel (0'-50')		npieteu:		g aevice: face casin	нQ ( na: 16	ore, air i " steel ((	rotary cu )'—50')	tungs (	PICKLES BUTTE
Note: TOC = top of casing Well Log: PB-11					-	-	-		
Daniel B. Stephens & Associates, Inc. 6-05-2012 JN ES09.0154		6-0	5-2012	<i>a Ass</i>					

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100-7				Graphic Log		Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
					<sup>100</sup> ]	20%/20%	100-105	ML	Sandy silt, pale yeliow (2.5Y 8/2), moderately indurated, dry.
				ML/SP		20%/20%	105-110	ML-SP	Same as above, interbedded with dark gray (2Y 3/1), medium—grained sandstone, very hard, CaCO3 cement.
110-					110	20%/20%	110-115	ML	Sandy silt and silt, light alive gray (5Y 6/2), weakly indurated, slightly moist.
			12" Borehole	ML ML/SP		20%/20%	115-120	ML-SP	Same as above, interbedded with dark gray medium—grained sandstone.
120-			50.0'-200.0'		120-	50%/50%	120-125	SM-SP	Sandy silt, light olive gray, similar to above, slightly moist, with white fine—grained, well sorted sandstone, cross bedded, some yellow with orange banding, dry, hard.
				SM/SP		20%/20%	125-130	SM-SP	Same as above, interbedded with sandstone, dark gray (2Y 3/1), medium—grained.
130-					130-	60%/60%	130–135	SM-SP	Sandy silt, pale yellow (2.5Y $7/3$ ), with white fine—grained sand with yellow color banding, dry.
1				SM II		30%/30%	135–140	SM	Silty sand, light gray (5Y 7/2), fine—grained, moist, reddish yellow color banding.
140 Surface עולייייו			— Stainless steel centralizer		140	0%/30%	140–145	ML	Sandy silt, light gray (2.5Y 7/2), fine—grained, slightly moist with small (less than 1 inch) reddish yellow clay lenses.
S cound Si Ground Si 150				ML		55%/55%		ML	Siltstone, light gray (2.5Y 7/2), hard, dry.
				SM/CL	150	100%/100%		SM-CL	Interbedded, silty sand/sandy silt, light brownish gray (7.5Y 6/2) with clay, dark greenish gray (5GY 4/1), thin bands of reddish clay, fine—grained.
Feet Below 101			4.5" O.D. S.S. blank casing 0.0'-340.0'		1	20%/20%		SM	Silty sand, light yellowish brown (2.5Y 6/4), laminated and color banded, cross bedded, fine-grained, weakly cemented, slightly moist.
u 160-			0.0 - 340.0	SM ·	160-	50%/50%		SM	Silty sand, light brownish gray (2.5YR 6/2), otherwise as above, very fine—grained, borderline sandy silt.
				SP	1	100%/100%		SP	Similar to above, but dominantly fine sand.
170-				3P 	170	100%/100% 50%/50%		SP SM	Sandstone, light olive brown (2.5Y 5/4), color banded, cross bedded, fine, soft, slightly moist. Silty sandstone, grayish brown (7.5Y 5/2), massive to laminated, color banding (yellow), trough cross bedded, fine—grained, organic material (?).
			Neat cement grout 60.0'-308.0'	SM		30%/50%		SM	Silty sandstone, light olive brown (7.5Y 5/3), fine—grained, similar to above, slightly moist.
180-				SM/ML	180	100%/100%		SMML	Sandy silt and silty sand, gray (5Y 5/1) to grayish brown (2.5Y5/2), moderately indurated, slightly moist.
				ML	1	85%/85%		ML	Sütstone, gray (5Y 5/1), moderately to strongly cemented, massive, slightly moist to dry.
190-				CL	190- -	0%/0%	190–195	CL	Little recovery, clay, appears to be dark gray (5Y 4/1).
200					200	65%/75%	195–200	ML	Siltstone, sandy silt and clayey silt intervals, gray (5Y 5/1), reddish brown color banding, moderately indurated, very slightly moist.
	jist: J. Rau	cci	Drilling m			ir rotary			
Driller:	HAZ-Tech		Bit diame	ters: 19"	' (0'-	50'), 12"	(50'–20	0'), 9	7/8" (200'-420')
Date a	completed:	6–30	—11 Sampling Steel sufa	device: ice casin	HQ c a: 16	ore, air i " steel (C	rotary cu )'—50')	ttings (	400'-420') PICKLES BUTTE
	- 46				•				Well Log: PB-11
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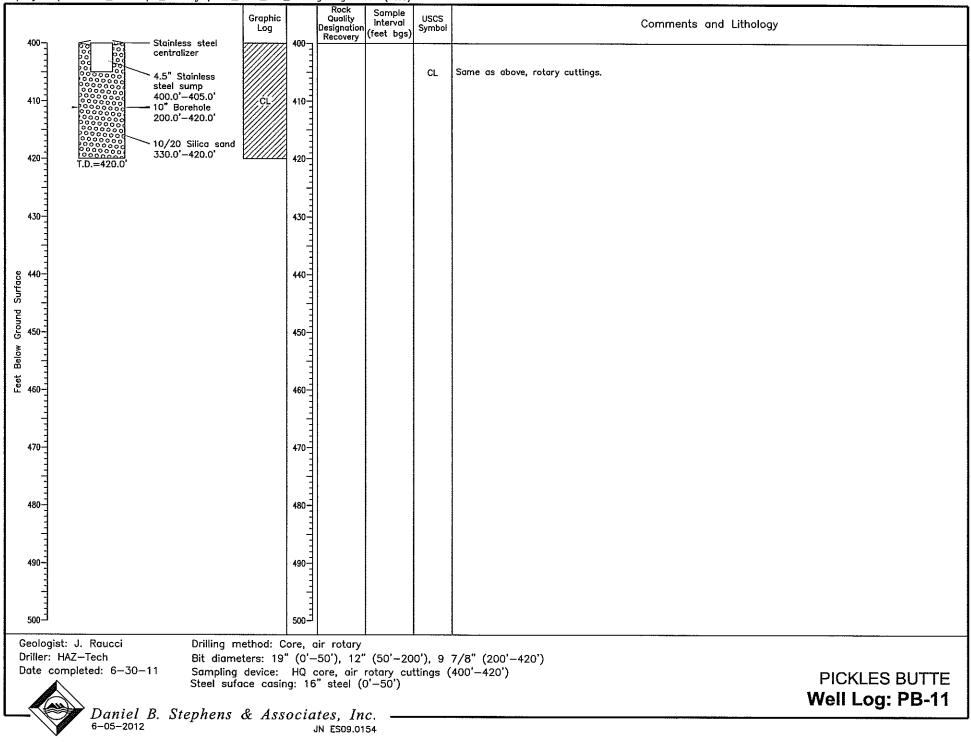
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300-					iphic .og	100	Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
200						200	60%/85%	200–205	ML	Siltstone, gray (5Y 5/1), same as above.
							90%/100%	205–210	ML	Same as above.
210						210-	100%/100%	210-215	ML	Same as above.
							85%/100%	215-220	ML	Same as above.
220-	-		10" Borehole			220	100%/100%	220-225	ML	Siltstone, dark gray (5Y 4/1), finely laminated, moderately indurated, slightly moist.
			200.0'-420.0'				100%/100%	225–230	ML	Same as above.
230-						230	75%/85%	230–235	ML	Same as above.
				5 1				235–240	ML	Same as above, lighter color (5Y 5/1).
90 240 1 - 1 - 1 1 - 1 - 1 1 - 1 - 1	X					240	25%/75%	240-245	ML	Same as above, highly fractured.
is punor 250 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -							90%/90%	245–250	ML	Same as above.
						250-1	40%/100%	250-255	ML	Same as above, many fractures.
et Below			4.5" O.D. S.S.			ددياي	60%/100%	255–260	ML	Same as above.
10 260 T			blank casing 0.0'—340.0'			260-	70%/100%	260-265	ML	Same as above.
							80%/100%	265–270	ML	Same as above.
270						270				Similar to above, finer—grained (claystone, some silt).
			Neat cement grout 60.0'-308.0'			280-	100%/100%			Similar to above, silty, locally cross bedded.
280-				HII	ML	-				Siltstone, same as above.
						***	50%/100%			Silty claystone, similar to above.
290-		NIII.		ME ME		290-				Siltstone and claystone, same as above, fractured.
300						300-T	60%/100%	233-300		Predominantly silty claystone, two prominent, steeply inclined fractures.
	jist: J. R	aucci	Drilling me	tho	d: C					
Driller	HAZ-Te	ch	Bit diamet	ers	: 19'	' (0'-	-50'), 12"	(50'–20	0'), 9	7/8" (200'-420')
Date		u. 0-30	Steel sufac	ce	ice: casin	но і g: 16	core, air i 5" steel (C	rotary cu )'—50')	tungs (	400'-420') PICKLES BUTTE
	, <i>4</i>	Dania	I R Stanhans -	e.	100	ocic	itas In	c		Well Log: PB-11
	G E	-05-20	l B. Stephens &	x.	A35	ocia	<i>IES, IN</i> JN ES09.01	54		

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F		Fickles (MC_Drdwings (E309_0						
300			Graphic Log	300-j	Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
		Neat cement grout 60.0'-308.0'			100%/100%	300-305	CL/ML	Clay, silty claystone and siltstone, color as above (5YR 4/1—5/1), siltstones are laminated, locally cross bedded, claystone is massive to finely laminated, slightly moist, moderately indurated, brittle to slightly plastic.
					100%/100%	305-310	CL-ML	Same as above.
310-	X	4.5" O.D. S.S. blank casing		310	40%/75%	310-315	CL-ML	Same as above.
		0.0'-340.0'			80%/100%	315-325	CL-ML	Same as above.
320-	×	X 3/4" Bentonite	CL/ML	320-				
	X	chips			100%/100%	325-330	CL-ML	Same as above.
330-				330-	100%/100%	330-335	CL-ML	Same as above.
	000000	0.0'-60.0'			100%/100%	335–340	CL-ML	Becoming more dominantly claystone and silty claystone.
8 340-	11	Stainless steel		340-	100%/100%	340-345	CL	Same as above.
es 340 Integer	200000 200000 1 1 1 1				90%/90%	345-350	CL	Same as above.
1 1 2 350 1	0000 0000 1111	od od od od od od od od od od od od od o		350	75%/90%	350-355	CL	Claystone, siity claystone and siitstone, gray (5Y 5/1), interbedded, predominantly claystone and siity claystone, slightly moist, slight to moderate plasticity.
t Below	00000 00000 00000 00000 00000 00000 0000	200.0'-420.0'			100%/100%	355-360	CL	Same as above.
te 3601		ord ord ord ord ord ord ord ord ord ord		360-	90%/90%	360-365	CL	Same as above.
		330.0'-420.0'			85%/85%	365–370	CL	Same as above.
370-			GL	370-	95%/95%	370–375	CL	Same as above.
	200000 200000 200000 11111	4.5" O.D. Stainless steel slot 20		1 1	75%/90%	375–380	CL	Same as above.
380-		50' screen 20 340.0'-400.0' 20 340.0'-400.0'		380-	100%/100%	380-385	CL	Same as above.
					80%/80%	385–390	CL	Same as above.
390-	20000			390-	55%/100%	390–395	CL	Same as above.
	00000			-	90%/90%	395-420	CL	Same as above.
400-1	1 <u>2</u> []	ě	V///////	400-				
	st: J. Rauc	-						
	HAZ—Tech Impleted: 6							7/8" (200'-420') 400'-420') DICKLES DUTTE
	N	Steel sufa	ice casin	ig: 16	steel (C	)'-50')	tungo (	FICKLES BUTTE
		nial R Stanhaus	& Ann	oni-	ton I.	0		Well Log: PB-11
	6-05	niel B. Stephens 6 5–2012	<b>x</b> A55	0010	IES, IN JN ES09.01	54		
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# S:\Projects\ES09.0154\_Pickles\VR\_Drawings\ES09\_0154\_07B\_borelogs.dwg PB-12 (1of6)

Locking steel vai	It Graphic Log	Rock Quality Designation	Sample Interval	USCS	Comments and Lithology
0 - Cround surfac		A Recovery	(feet bgs)	Symbol	
- 16" Borehole 0.0'-50.0'		0%/0%	0–15		No recovery.
	SP	0%/20%	15-20	SP	Sand, olive brown (2.5Y 4/3), coarse—grained, no plasticity.
20 20 20 20 20 20 20 20 20 20 20 20 20 2	s ITFILITI A	20-135%/60%	20-25	SM	Silty sand, olive brown (2.5Y 4/4), fine-grained, no plasticity.
casing 0.0'-480.0'		35%/60%	25–30	SM	Same as above.
30-1	3	0 25%/55%	3035	SM	Same as above.
		25%/55%	35-40	SM	Same as above.
40 - 3/4" Bentonite chips 0.0'-97.0'	4	0-100%/100%	40-45	SM	Silty sand, olive brown (2.5Y 4/3), fine-grained.
	SM 1	100%/100%	45-50	SM	Clayey silty sand, light olive brown (2.5Y 5/4), very low plasticity.
	5	25%/90%	50-60	SM	Silty sand grading into sand, light yellowish brown (2.5Y 6/3), fine— to medium—grained, no plasticity, hard, clayey silty sand, light alive brown (2.5Y 5/3), fine—grained, hard no plasticity.
60	6	100%/100%	60-70	SM	Clayey silty sand, light olive brown (2.5Y 5/3), hard no plasticity.
60       -       10" Borehole         70-       50.0'-555.0'         80-       -       Stainless steel         centralizer       -	13 PT 14 14 14 14 14 14 14 17 14 14 17 14	95%/95%	70-80	ML	Sandy silt, light yellowish brown (2.5Y 6/3), no plasticity.
80	80 ML	100%/100%	80~90	ML	Clayey sandy silt, grayish brown (2.5YR 5/2).
		100%/100%	90-100	ML :	Same as above.
100 Neat cement grout 97.0'-450.0'	100				
Driller: HAZ—Tech Bit diame Date completed: 7—15—11 Sampling	ethod: Core, ters: 16" (0 device: HQ ce casing:	'-50'), 9 7/ core (0'-3	/8" (50'-: 50'), air i	555') rotary (	Northing: 667697.966 Easting: 243653.665 :uttings (350'-555') Elevation: 2657.2 (TOC)
Daniel B. Stephens	2				Note: TOC = top of casing Well Log: PB-12

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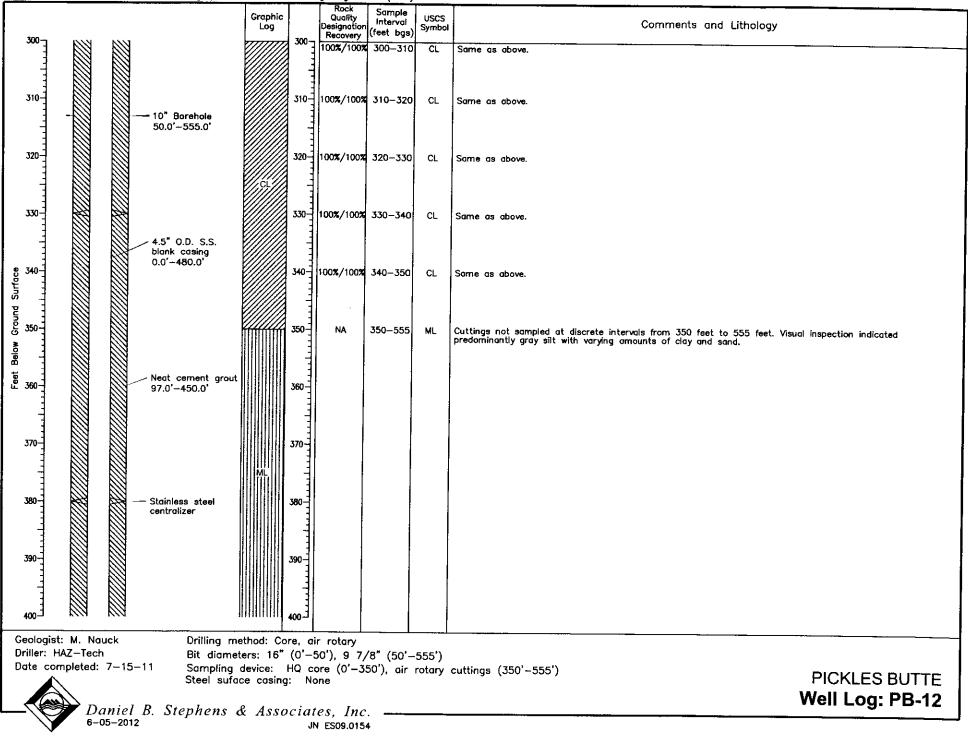
#### Rock Sample Graphic Quality USCS Interval Comments and Lithology Designation Log Symbol (feet bgs) Recovery 100-100 m 35%/48% 100-110 Clayey silt with abrupt transition to clay, light olive brown (2.5Y 5/4), clay has iron and manganese stain. ML 110-110-100%/100% 110-120 ML Same as above with interbedded silty sand. 10" Borehole 50.0'-555.0' 120-1 100%/100% 120-130 ML-CL Silty claystone, gray (5Y 5/4), no plosticity, hard. 120-130-130-100%/100% 130-140 ML-CL Same as above. 4.5" O.D. S.S. blank casing 140 140-40%/65% 140-150 Ground Surface 0.0'-480.0' CL Similar to above; claystone, gray (5Y 5/1), no plasticity, hard to brittle. 150-150 100%/100% 150-160 CL Same as above. Below Feet Neat cement grout 160-160-100%/39% 160-170 CL 97.0'-450.0' Same as above. 170-170-1100%/100% 170-180 CL Same as above. 180-Stainless steel 180-5%/18% 180-190 CL Same as above with multiple fractures. centralizer 190-190-190%/100% 190-200 ÇL Same as above. 200-200 -Geologist: M. Nauck Drilling method: Core, air rotary Driller: HAZ-Tech Bit diameters: 16" (0'-50'), 9 7/8" (50'-555') Date completed: 7-15-11 Sampling device: HQ core (0'-350'), air rotary cuttings (350'-555') PICKLES BUTTE Steel surface casing: None Well Log: PB-12 Daniel B. Stephens & Associates, Inc. 6-05-2012 JN ES09.0154

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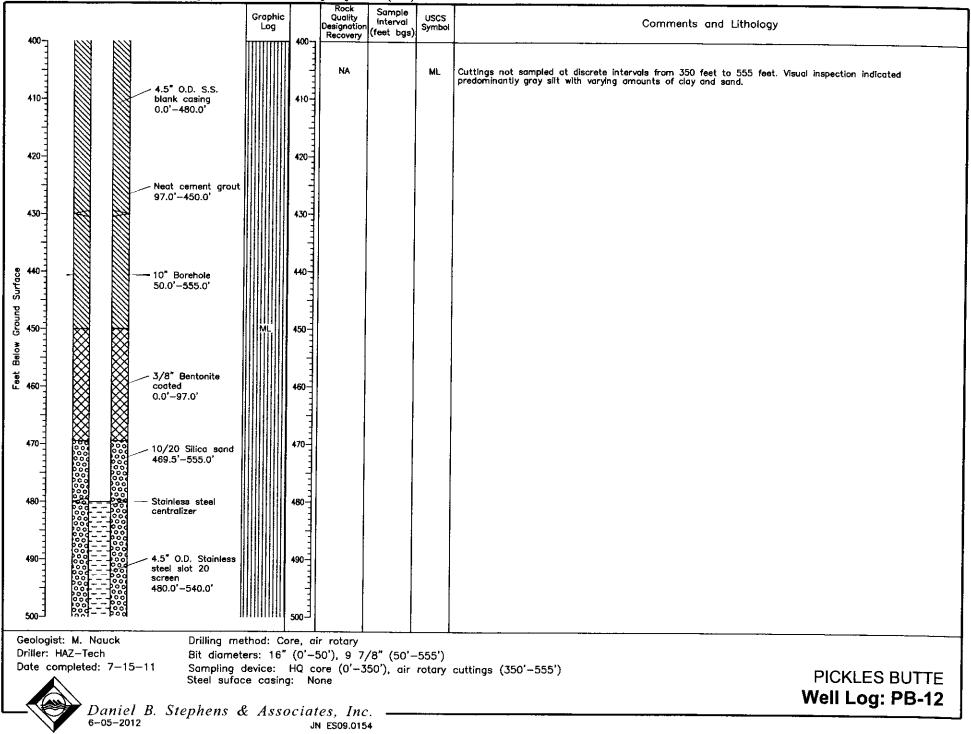
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200	Graphic Log		Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology	
		200-1	100%/100%	200-210	CL	Same as above.	
210- 		210	85%/89%	210–220	CL	Same as above.	
220-		220	100%/100%	220–230	CL	Same as above.	
230- 4.5" O.D. S.S. blank casing 0.0'-480.0'		230-	85%/95%	230~240	CL	Same as above, massive, non-fractured.	
240- 250- 250-		240	75%/75%	240-250	CL	Claystone, gray (5Y 5/1), no plasticity, hard, brittle, slightly moist.	
		250	90%/90%	250–260	CL	Same as above.	
260- 97.0'-450.0'			100%/100%	260–270	CL	Same as above.	
270-		270 - 1	100%/100%	270–280	CL	Same as above.	
280- Centralizer			00%/35%		CL	Same as above.	
290- 		90 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00%/100%	290-300	CL	Same as above.	
eologist: M. Nauck Drilling me	thod: Core	e, air	r rotary				
briller: HAZ-Tech Bit diameter bate completed: 7-15-11 Steel sufac Daniel B. Stephens &	levice: H e casing:	Q co Noi	ore (0'-3) ne	50'), air	555') rotary (	cuttings (350'-555')	PICKLES BUTTE Well Log: PB-12

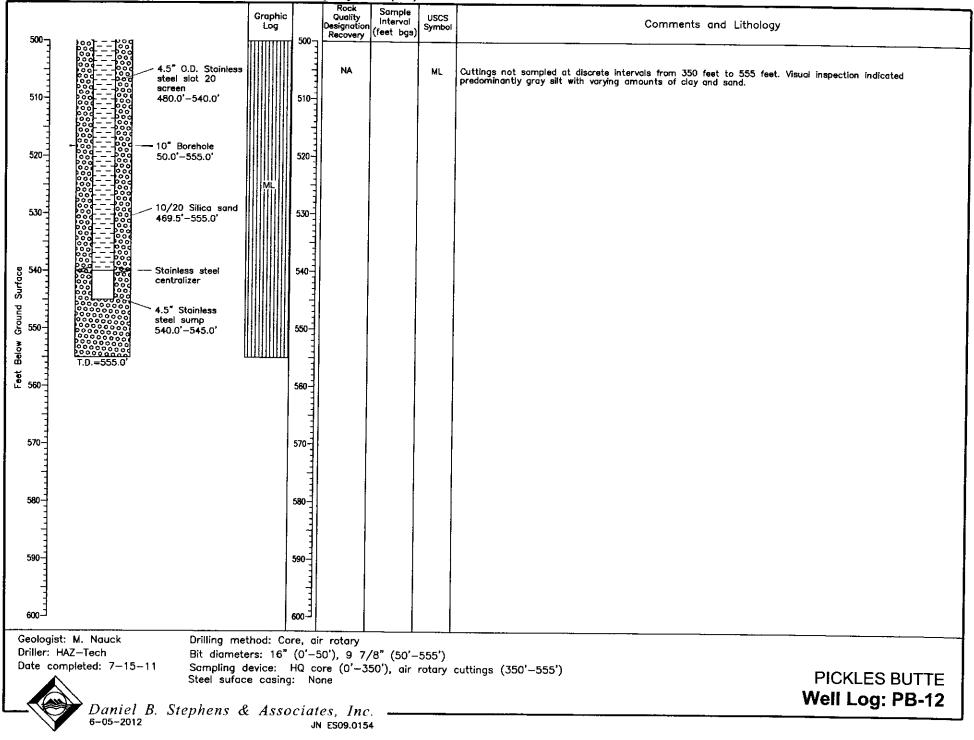
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Rock Locking steel voult Sample Graphic Quality USCS Interval Comments and Lithology Log Designation Symbol (feet bgs Recovery Ground surface 07 90%/95% 0-5 Vesicular basalt, gray (2.5Y 5/1), several fractures near top of core, slightly glassy texture. 100%/100% 5-10 Same as above. Neat cement grout 0.0'-770.0' 80%/95% l Basalt 10-10-15 Same as above with vertical and horizontal fractures. 25%/70% 15 - 20Vesicular basalt, gray (2.5Y 5/1), highly fractured. 20-0%/2% 20 - 25GP Gravel, unconsolidated, well rounded, loose, 1 to 2.5 inches diameter. 4.5" O.D. Stainless 071 steel (S.S.) blank casing 0%/10% 25-35 Same as above, 0.25 to 3.0 inches diameter. GP 0.0'-840.0' 30-00 0%/0% SP/GW No core recovery. Rotary cuttings indicate predominantly medium- to coarse-grained sand and interbedded 35-45 aravel. 15-1/4" Borehole 40-40-0.0'-440.0' Ground Surface 08 0%/0% 45-55 SP/GW No core recovery, some as above. SP/GW2 50 50-Below 10" Steel casing 8%/15% Gravel, 0.5 to 3.0 inches diameter with abrupt change to clayey silty fine sand, light olive brown (2.5Y 5/3). 55-65 GP 0.0'-440.0' very fine-grained, well graded, well rounded, moderate plasticity, soft. Feet SC 60 60~ 0%/23% 65-75 SM 65 to 69 feet silty fine sand, light olive brown (2.5Y 5/3). 69 to 75 feet coarse sandy gravel, polychromic. well rounded, 0.25 to 2.0 inches diameter, loose. 70 70-Steel casing 0.0'-600.0' o' 0%/10% 75-85 Greater than 2 inches diameter, loose. CP 80 80-85%/95% 85-95 Claystone to silty claystone, pale olive (5Y 6/3), none to medium plasticity, hard to stiff, dry, transition to CL very well consolidated to well consolidated. Stainless steel centralizer 90-90-55%/55% 95-105 CL/GP Silty claystone, light yellowish brown (2.5Y), medium plasticity, medium density, slightly moist, some ferric like staining. Gravel lenses noted at 95 to 100 feet in rotary cuttings. 100 -100-Geologist: M. Nauck/J. Raucci Drilling method: Core, mud rotary, air rotary Northing: 666231.696 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923') Driller: HAZ-Tech Easting: 243986.781 Date completed: 12-15-11 Sampling device: HQ core, air rotary cuttings Elevation: 3073.9 (TOC) PICKLES BUTTE Steel surface casing: 8" (0'-600'), 10" (0'-440') Notes: HAZ-Tech core drilling 0'-666'; Adamson Pump and Drill air rotary drilling 666'-920' Well Log: PB-13 TOC = top of casing Daniel B. Stephens & Associates, Inc. 6-05-2012 JN ES09.0154

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S: (Frojects (ESU9.0154_Pickles (VK_Drowings (ESU9_0	Graphic Log	Rock Quality Designation	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
100 	CL/GP} CL/GP} 4 0 2 0 2 5 0 2 5 0 2 5 0 2 110-	Recovery 0%/12%		SW	Sand, grayish brown (2.5Y 5/2), medium— to fine-grained, subrounded, poorly sorted, na plasticity, soft, wet (drilling fluid).
		0%/0%	115-125	SP	No core recovery. Rotary cuttings predominantly loose, medium-grained sand with few fines.
120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120- 120-	SP 130-	0%/0%	125–135	SP	No core recovery, same as above.
		0%/0%	135–145	SP	No core recovery, same as above.
8 140-7 1/4" Borehole 9	140-1	12%/25%	145155	CL-ML	Silty claystone to claystone, light brownish gray (2.5Y 6/2), stiff/brittle, dry.
8 8 10 10" Steel casing 10" - 10" Steel casing 10" - 440.0'		15%/22%	155–165	CL	Claystone, light brownish gray (2.5Y 6/2), stiff, dry.
170- 170- 8" Steel cosing	160- CL 170-	15%/20%	165–175	CL	Same as above.
		0%/0% 1	175-180		No recovery.
180- 	180-1 	0%/18% 1	85–195	SP	Fine to medium sand, olive gray (5Y 5/2), poorly graded, loose, wet.
	200-	0%/0% 1	95–205		No recovery.
Driller: HAZ-Tech Bit diame Date completed: 12-15-11 Sampling Steel suf	nethod: Core, eters: 15 1/4 device: HQ face casing: 8	-" (0'-440 core, air 3" (0'-600	)'), 9 7/1 rotary cu )'), 10" (	8" (44) uttings	666'-920'
Daniel B. Stephens & 6-05-2012		es, Inc. ES09.0154			

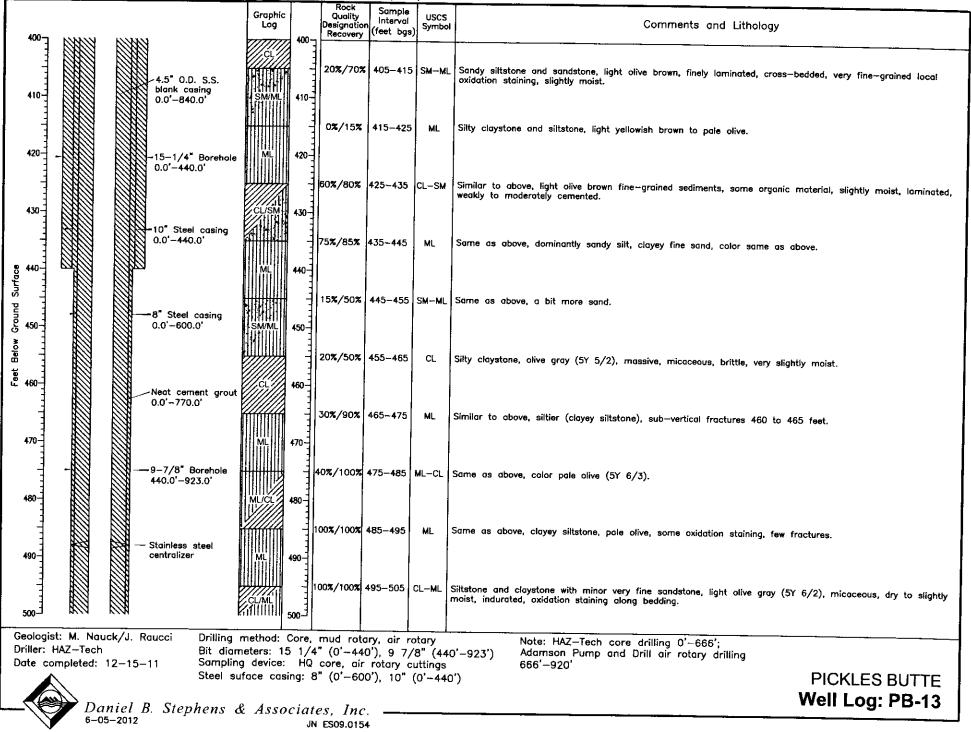
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200-7			Graphic Log	200-	Quality	Interval	USCS Symbol	Comments and Lithology
210-		Neat cement grout	SP	210	0%/20%	205215	SP	Sand, olive brown (2YR 4/3), medium-grained, well sorted, loose, wet.
•		4.5" O.D. Stainless			0%/0%	215225		No recovery.
220-		steel (S.S.) blank casing 0.0'-840.0'		220				
230-				230	0%/15%	225–235	SP	Same as above.
		-15-1/4" Borehole 0.0'-440.0'			0%/15%	235-245	SP	Same as above.
9240 920 920 920 920 920 920 920 920			SP	240	0%/35%	245–255	SP	Sand, same as above, color (2.5Y 4/2), then 3 inches of claystone, light yellowish brown (2.5Y 6/2), slight plasticity, slightly moist.
250 * B B B C C C C C C C C C C C C C C C C		10" Steel casing		250	35%/90%	255–265	CL-SP	Interbedded brown sand, same as above, with light yellowish brown claystone, some oxidation color banding.
270-		0.0'-440.0'	CLISP	270-	30%/80%	265–275	CL-SP	Same as above, predominantly sand with sandy claystone interbeds.
280		8" Steel casing 0.0'-500.0'		280	50%/100%	275–285	SP	Sand, light yellowish brown (2.5Y 6/3), fine—grained, well sorted, micaceous, claystone interbeds, moderately compact, slightly moist.
290		-Stainless steel centralizer	SP	290	45%/95%	285–295	SP	Sand, grayish brown (7.5Y 5/3) medium~grained, well sorted with uncommon silty and clayey interbeds, 1 to 2 centimeters thick, loose to weakly cemented, moist, prominent oxidation color banding.
300 <sup>-1</sup>			SP/ML	300-1	40%/90%	295305	SP-ML	Similar to above, grayish brown sand interbedded with lighter colored silty fine sand and sandy clay, loose to weakly cemented.
Driller: H	: M. Nauck/ AZ-Tech npleted: 12-	-1511 Bit dian Samplin	neters: 1 g device:	5 1/4 HQ	mud roto 4" (0'-44 core, air	0'), 9 7/ rotary c	/8" (44 cuttings	666'-920'
					3" (0'-60			o') PICKLES BUTTE
		el B. Stephens d	& Asso					Well Log: PB-13
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5. (Projects (ESU9.0154_Pickies (VR_Drawings (ESU9_0	Graphic Log	Rock Quality	Sample Interval (feet bgs)	USCS	Comments and Lithology
300 	300 SP/ML SM/ML SM/ML 310	50%/85%			Sandy silt and silty sand, light yellowish brown (2.5Y 6/3—6/4), fine—grained, weakly cemented, brittle, moist, interbedded with olive brown sand, similar to above.
320- 320- 320-		70%/100%	315325	SM	Similar to above, but also several thin layers (5 to 10 centimeters) very hard fine sandstone, pale yellow (5Y 8/2), prominent oxidation color sanding, hard rock is dry.
330-	SM 320-	50%/100%	325-335	ML-SP	Sandy siltstone, pale yellow (2.5Y 7/4), hard, dry, interbedded with light olive brown loose sand, similar to above.
340- 340- 3 5 340- 3 5 340- 3 5 340- 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	4 C	0%/90%	335–345	SM	Silty sandstone and sandy siltstone, light yellow brown (2.5Y 6/4), generally weakly cemented with loose and very hard layers, oxidation staining especially in very hard layers.
Puno 25 350-	SM	60%/90%	345–355	SM	Same as above, color mottled with olive yellow (2.5Y 6/6), massive to finely laminated, dry to slightly moist.
8 0 0 1 1 1 10" Steel casing 0.0'-440.0' 1 1 1 1 1 1 10" Steel casing 1 10" Steel casing	ML/SM 360-	40%/90%	355-365		Siltstone, sandy siltstone and very fine sandstone, pale yellow (2.5Y 7/4) to light olive brown (2.5Y 6/3), weakly to moderately cemented, laminated, local oxidation staining, dry to slightly moist.
370	370-	50%/90%		·	Interbedded silty fine sandstone, and siltstone, same as above, with olive brown, fine— to medium—grained sandstone, weakly cemented, slightly moist.
380	380-	40%/75%			Sandstone, light olive brown, fine-grained, similar to above, finely laminated, cross-bedded, claystone 384 to 385 feet, slightly moist.
390- Jack Stainless steel centralizer	ML 390-	25%/75% 3 0%/15% 3			Similar to above, sandy siltstone and very fine-grained silty sandstone, local oxidation staining, highly fractured, slightly moist. Sandy claystone and siltstone, color same as above.
	400- hethod: Core,	mud rota	ry, air ra	otary	Note: HAZ-Tech core drilling 0'-666';
Date completed: 12-15-11 Sampling	eters: 15 1/4 device: HQ	core, air	rotary c	uttings	0'—923') Adamson Pump and Drill air rotary drilling 666'—920'
Steel suf	ace casing: 8	° (0'–600	D <sup>r</sup> ), 10" (	(0'-440	PICKLES BUTTE Well Log: PB-13
Daniel B. Stephens & 6-05-2012		es, Inc. ES09.0154		<u></u>	

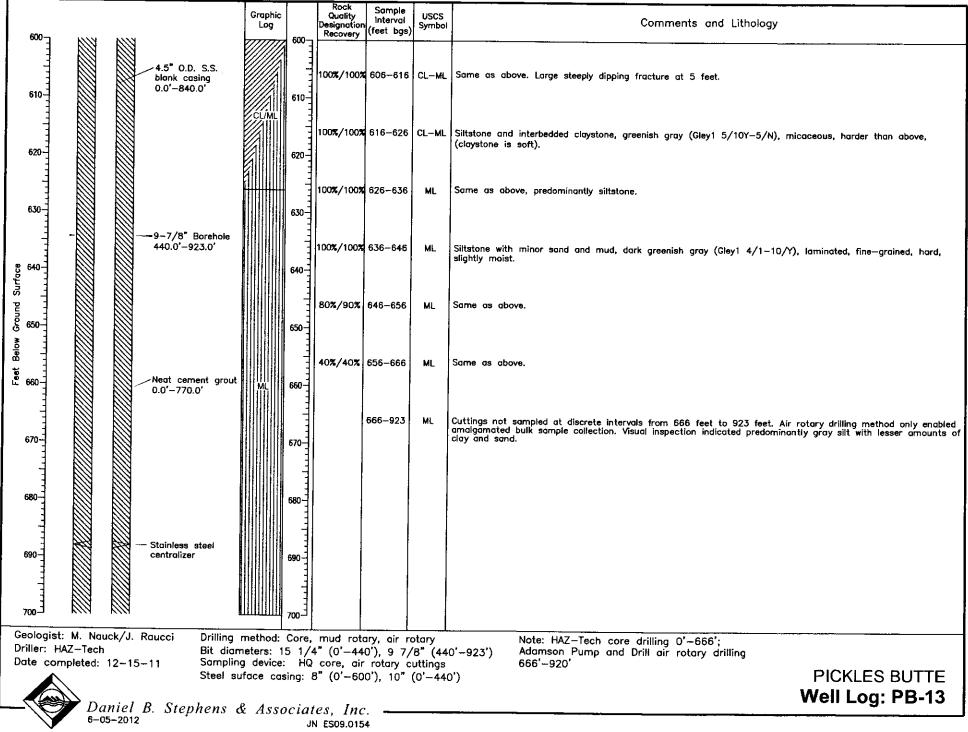
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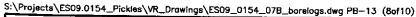


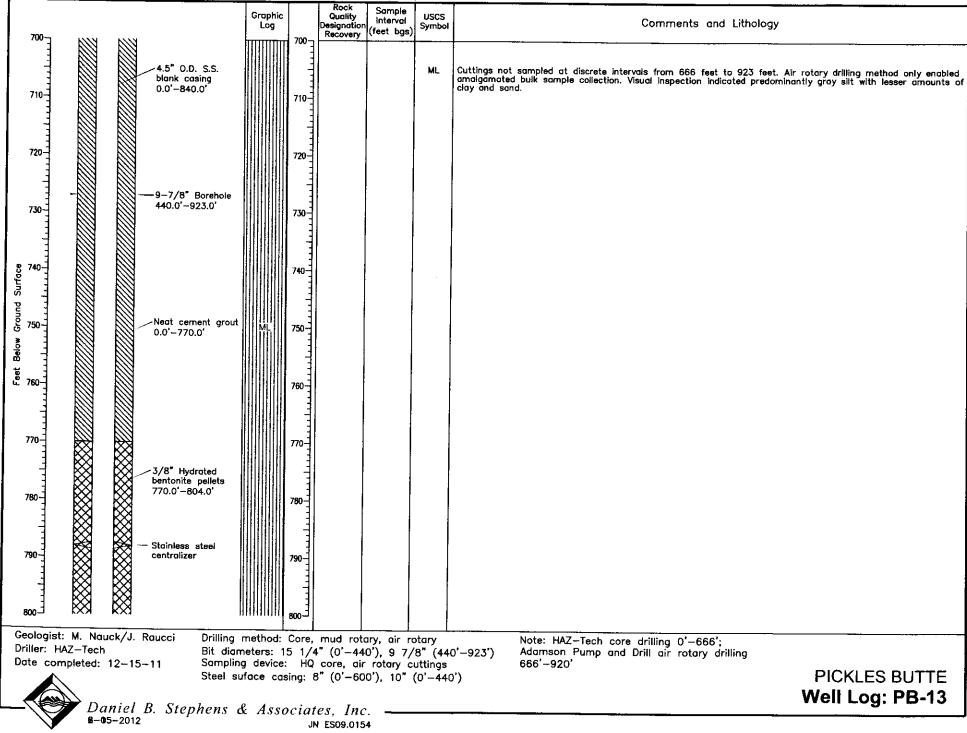
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5. (10)608 (2303.0104_Pickles (VA_Drawings (2303_0	Graphic Log	Rock Quality Designation	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
500 	500	80%/100%	505-515	CL-ML	Same as above, silty clay and clayey silt, abundant organic material and oxidation staining.
520-	CL/ML 520-	0%/100%	515–525	CL-ML	Same as above.
	530-	80%/100%	525–535	ML	Similar to above, less muddy, siltstone and silty very fine sandstone with claystone, olive (5Y 5/3), sandy layers are laminated, cross—bedded.
8 540- PL S	т МЦ 540-Т т	0%/100%		ML	Predominantly fine-grained silt, sandstone and clayey siltstone.
0.0'-770.0'	550-	100%/100%			Silty claystone, pale olive to olive gray, weakly cemented to 553 feet, then clayey siltstone, gray (5Y 5/1), dense, finely laminated, slightly moist. Contact with "blue clay" unit at 552.5 feet.
570	560	not recorded 40%/100%	555-565 565-576		Silty claystone with minor sand, gray (5Y 5/1), massive to laminated, fine-grained, weakly to moderately cemented, dense, very slightly moist. Silty claystone, dark greenish gray (Gley1 4/1), hard, brittle, numerous fractures.
580		70%/100%	576-586	CL	Same as above.
590- 590-	590-	85%/100% :			Silty claystone, dark greenish gray (Gley1 4/1), slight plasticity, brittle, slightly moist, micaceous.
	CL/ML 11111111600-	80%/100% :	596-606 (	SL-ML :	Same as above, a bit siltier, greenish gray (Gley1 5/1), interbedded with hard micaceous siltstone.
Driller: HAZ-Tech Bit diame Date completed: 12-15-11 Sampling	nethod: Core, eters: 15 1/4 device: HQ ace casing: 8	4" (0'—44( core, air	0'), 9 7/6 rotary cu	8" (44( uttings	PICKLES BUTTE
Daniel B. Stephens & 6-05-2012		tes, Inc N ES09.0154			Well Log: PB-13

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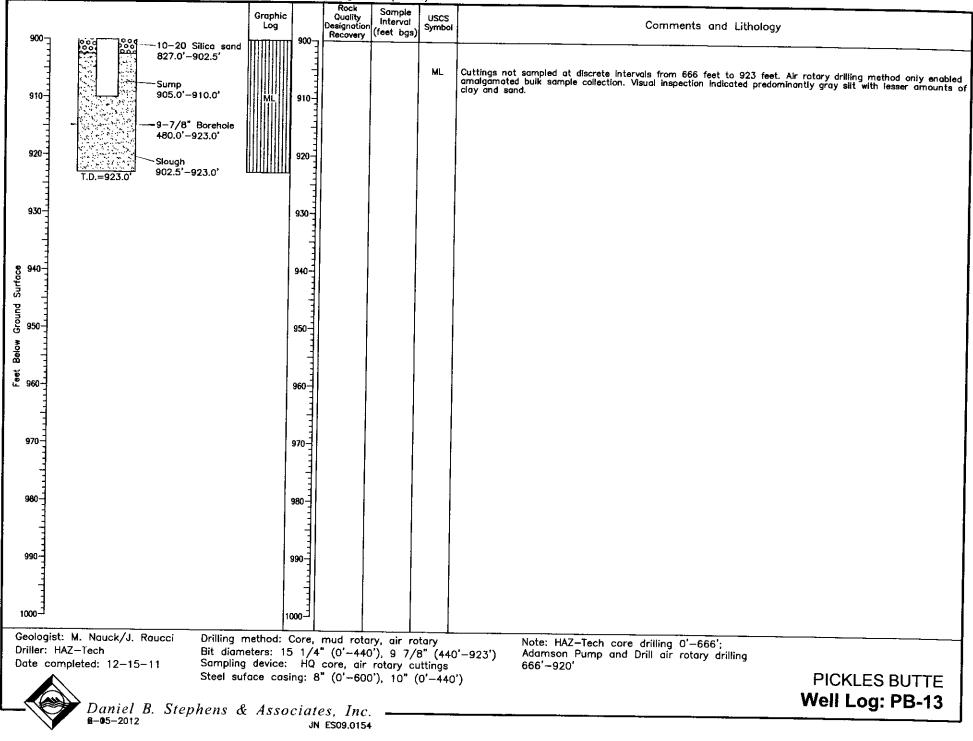




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	Graphic Log	Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology	
800 3/8" Hydrated bentonite pellets 770.0'-804.0'				ML	Cuttings not sampled at discrete intervals from 666 feet to 923 feet. amalgamated bulk sample collection. Visual inspection indicated predomiclay and sand.	Nir rotary drilling method only enabled nantly gray silt with lesser amounts o
810- Sand and slough 804.0'-827.0'		810				
820 820 830 830 830 830 830 830 830 83		820-				
		830-				
• 840- • 840- • 0°0		850				
3         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -		860-				
870- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000- 000-		870-				
880		880				
890 - 000 - 000 centrolizer - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000	9	890				
Geologist: M. Nauck/J. Raucci Drilling Driller: HAZ-Tech Bit diam Date completed: 12-15-11 Sampling	imethod: C neters: 15 g device: face casi	Core, mud roto 5 1/4" (0'~440 HQ core, air ng: 8" (0'-600	0'), 9 7/ rotary c 0'), 10"	8" (44) uttings	666'-920'	PICKLES BUTTE Well Log: PB-13

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#### S:\Projects\ES09.0154\_Pickles\VR\_Drawings\ES09\_0154\_078\_borelogs.dwg PB-14 (1of10)

		7	Locking steel vault	Graphic Log		Rock Quality Designation Recovery	Sample interval (feet bgs)	USCS Symbol	Comments and Lithology
0- <u>1</u> -			<u>Ground surface</u>	000000000000000000000000000000000000000		0%/0%	0-10	GP	No core recovery. O to 30 feet description based on rotary cuttings unconsolidated gravel, meterolithic clasts up to 3 inches, rounded, coarse—grained, poorly sorted, sand matrix.
10 10			-Cement grout 0.0'50.0'	00000000000000000000000000000000000000	10- 10- 10-		10~20	GP	Same as above.
20			<ul> <li>4.5" O.D. Stainless</li> <li>steei (S.S.) blank</li> <li>casing</li> <li>0.0'-845.0'</li> </ul>	SP	20		20-30	SP	Sand, medium— to coarse—grained, moderately well sorted, loose.
30-			-15-1/4" Borehole		30-	80%/80%	30-35	ML	Silstone, light brownish gray (2.5Y 6/2), weakly cemented.
			0.0'-480.0'			85%/85%	35-40	ML	Siltstone—sandy siltstone, light brownish gray (2.5Y 6/2), weakly cemented.
Surface Linite					40-	85%/85%	40~45	ML	Siltstone—cloyey siltstone, pale yellow (2.5Y 7/3), weakly cemented.
			– Stainless steel centralizer			45%/75%	45-50	ML	Sandy silstone, light yellowish brown (2.5Y 6/3), very weakly cemented, highly fractured, oxidation staining.
50 TIT				ML	50-	60%/75%	50-55	ML	Same as above.
Below						25%/40%	55-60	ML	Same as above, fine-grained.
-00 Feet	-	-	-10" Steel casing 0.0'-480.0'		60	50%/95%	60-65	ML	Same as above, fine-grained, highly fractured.
			0.0 - 480.0			35%/35%	65-75	SM	Silty sandstone, light yellowish brown (2.5Y 5/4), laminated, fine— to medium—grained, weakly cemented.
70			Neat cement grout 0.0'-807.0'		70- 	25%/30%	75–85	SM	Same as above, light olive brown (2.5Y 5/4).
					-	19%/19%	85–91	SM	Same as above with coarse-grained sand in drilling fluid matrix.
90-				4 (GP, 00	90		91-95	GP	Rotary cuttings indicate gravel layer at 91 to 95 feet.
Ì				SW	1	60%/99%	95–100	SW	Sand, pale yellow (2.5Y 8/3), coarse—grained, subrounded, loose, wet.
100-J	1 1000	1///	 		100-	60%/99%		SM	Silty sandstone, pale yellow (2.5Y 8/3), fine—grained, weakly cemented.
Driller:	HAZ-Te Drill complete	ch; Adam d: 10—11	nson Pump and -11 B. Stephens	Bit diame Sampling Steel suf Note: TO	eters: devid ace d C =	casing: 10 top of ca	and 9—7 :ore, NQ " sing	7/8"	rotary Northing: 665549.182 Easting: 244947.947 otary cuttings Elevation: 3080.9 (TOC) Note: HAZ-Tech core drilling 0'-385', 520'-750' (NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923'

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Log			Interval	I Symbol	Comments and Lithology
	100-	Designation Recovery	(feet bgs)	Symbol	
<u>Hhītu</u>	110	0%/0%	105–115	SP	No core recovery 105 feet to 175 feet, rotary cuttings indicate dominantly medium sand, moderately well sorted, unconsolidated.
5" 0.D. S.S. ank casing 0'-845.0'	120	0%/0%	115-125	SP	Same as above.
1/4" Develop	130-	0%/0%	125-175	SP	Same as above to 175 feet (rotary cuttings).
0'-480.0'					
ainless steel ntralizer					
" Steel casing )'-480.0'	160				
at cement grout	170-1 170-1	0%/50%	175–180	sw	Sand, dark yellowish brown (10YR 4/4), coarse-grained, non~plastic, loose, wet.
SM 1	11				Silty sand, light yellowish brown (2.5Y 6/4), fine-grained, iow plasticity, loose, wet. Sandstone, dark grayish brown (2.5Y 5/2), coarse-grained, subrounded, weakly cemented, vertical fractures.
		35%/35%	195–205	SP-SM	Sandstone grading to silty sandstone, olive brown (2.5Y 4/3), coarse— to fine—grained, weakly cemented.
Pump and Drill Bit o Sam	liamete pling d	ers: 15–1, evice: He c	/4" and Q core, N uttings	9-7/8	(NQ core 600'-750'); Adamson Pump and Drill
	5" 0.D. S.S. ank casing 0'-845.0' -1/4" Borehole 0'-480.0' steel casing 1'-480.0' Steel casing 1'-	5" O.D. S.S. ank casing O'-845.0' -1/4" Borehole O'-480.0' -1/4" Borehole O'-480.0' SP 140 -1/4" Borehole O'-480.0' SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SP 140 -1/4" SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' SV -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' -807.0' - - - - - - - - - - - - -	5" 0.D. S.S. ank casing 0'-845.0' -1/4" Borehole 0"-480.0' -1/4" Borehole 0"-480.0' SP 140- 130- 130- 130- 130- 130- 130- 150- 150- 150- 160- 170- 160- 170- 170- 0%/0% 180- 0%/50% 30%/40% 190- 35%/35% SP/SM 200- 35%/35% SP/SM 200- 35%/35% SP/SM 200- 35%/35% SP/SM 200- 35%/35% SP/SM 200- Steel suface casing: */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-807.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */-707.0' */- */- */- */- */- */- */- */-	5" 0.D. S.S. Drik casing 0'-845.0' -1/4" Borehole 0'-480.0' -1/4" Borehole 0'-480.0' SP 140- -1/4" Borehole 0'-480.0' -1/4" Borehole 0''-480.0' -1/4" Borehole 0''-480.0' -1/4" Borehole 0''-480.0' -1/4" Borehole 0'''-480.0' -1/4" Borehole 0''''''''''''''''''''''''''''''''''''	5" 0.D. S.S. 20% 20% 115-125 SP 20% 20% 115-125 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 125-175 SP 20% 20% 20% 125-175 SP 20% 20% 20% 20% 20% 20% 20% 20% 20% 20%

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200 200 200 200 200 200 200 200 200 200		(2000.0.11	<u>(_)</u> , (01400	\VR_Drawings\ES09_(	Graphic Log	Rock Quality Designation Recovery	Somple	USCS Symbol	Comments and Lithology
201       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10 <t< td=""><td></td><td></td><td></td><td></td><td></td><td>0%/48%</td><td>205–215</td><td>sw</td><td>Sand, dark yellowish brown (10YR 4/4), coarse—grained, non—plastic, loose, wet.</td></t<>						0%/48%	205–215	sw	Sand, dark yellowish brown (10YR 4/4), coarse—grained, non—plastic, loose, wet.
20       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -	210			blank casing		]	215–225	sw	Same as above.
g 240       07/487       235-245       SM       Sity sandstone, light yellowish brown (2.5Y 6/3), fine- to medium-grained, weakly cemented, fractured.         g 240       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       - <td>220</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>225-235</td> <td>SP-SM</td> <td>Loose sand graiding to silty sandstone, light yellowish brown (2.5Y 6/3), fine-grained, weakly cemented.</td>	220						225-235	SP-SM	Loose sand graiding to silty sandstone, light yellowish brown (2.5Y 6/3), fine-grained, weakly cemented.
group       group       Stointees steel       0%/48%       245-255       SM       Same as above with iron staining.         group       group       10°       Steel cosing       0%/48%       245-255       SM       Same as above with iron staining.         group       10°       Steel cosing       0%/48%       245-255       SM       Same as above with iron staining.         group       10°       Steel cosing       0%/48%       245-255       SM       Sandstone, light olive brown (2.5Y 5/3), lominated, coarse-groined, very weakly cemented, iron staining.         group       10°       Steel cosing       0%/48%       255-285       SM       Sandstone, light vellowish brown (2.5Y 6/3), iron stained banding, fine-groined, weakly cemented.         group       Next cement grout       10°       SM       280       0%/48%       275-285       SM       Silty sandstone, light yellowish brown (2.5Y 6/3), iron stained banding, fine-groined, weakly cemented.         group       0°       0%/48%       285-295       ML       Sandy siltstone, light yellowish brown (2.5Y 6/3), fine-groined, weakly cemented, fractured.         group       0%/48%       295-305       ML       Sandy siltstone, light yellowish brown (2.5Y 6/3), fine-groined, weakly cemented, fractured.         group       0%/48%       295-305       ML       Sandy siltstone, light y	230			-15-1/4" Borehole 0.0'-480.0'	SP/SM 230	]	235–245	SM	Silty sandstone, light yellowish brown (2.5Y 6/3), fine— to medium—grained, weakly cemented, fractured.
B	Surfac				1111111111111		245-255	SM	Same as above with iron staining.
0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°       0.0°-480.0°	Below						255-265	SW	Sandstone, light olive brown (2.5Y 5/3), laminated, coarse—grained, very weakly cemented, iron staining.
Anat cement grout       Naat cement grout       0%/48%       275-285       SM       Silty sandstone, light yellowish brown (2.5Y 6/3), iron stained banding, fine-grained, weakly cemented.         280- 290- 300-       0%/48%       285-295       ML       Sandy siltstone, light yellowish brown (2.5Y 6/3), fine-grained, weakly cemented, fractured.         280- 300-       0%/48%       285-295       ML       Sandy siltstone, light yellowish brown (2.5Y 6/3), fine-grained, weakly cemented, fractured.         280- 300-       0%/48%       295-305       ML       Same as above, light olive brown (2.5Y 6/3).       Fine-grained, weakly cemented, fractured.         Geologist:       J. Fisher/M. Nauck/J. Raucci Driller: HAZ-Tech; Adamson Pump and Drill Date completed: 10-11-11       Drilling method: Core, mud rotary, air rotary Cuttings       Note: HAZ-Tech core drilling 0'-385', 520'-750' (NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923'       PICKLES BUTTE	260- 				260	0%/48%	265–275	ML	Sandy clayey silt, light yellowish brown (2.5Y 6/3), low plasticity, soft, damp.
300       0%/48%       285-295       ML       Sandy siltstone, light yellowish brown (2.5Y 6/3), fine-grained, weakly cemented, fractured.         290       0%/48%       285-295       ML       Sandy siltstone, light yellowish brown (2.5Y 6/3), fine-grained, weakly cemented, fractured.         300       0%/48%       295-305       ML       Same as above, light olive brown (2.5Y 5/3).         Geologist: J. Fisher/M. Nauck/J. Raucci Driller: HAZ-Tech; Adamson Pump and Drill       Drilling method: Core, mud rotary, air rotary Bit diameters: 15-1/4" and 9-7/8" Sampling device: HQ core, NQ core, rotary cuttings       Note: HAZ-Tech core drilling 0'-385', 520'-750' (NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923'         PICKLES BUTTE	270				ML 270	1	275–285	SM	Silty sandstone, light yellowish brown (2.5Y 6/3), iron stained banding, fine—grained, weakly cemented.
Geologist: J. Fisher/M. Nauck/J. Raucci Driller: HAZ-Tech; Adamson Pump and Drill Date completed: 10-11-11 Date completed	280				280 . SM 1 2280	]	285–295	ML	Sandy siltstone, light yellowish brown (2.5Y 6/3), fine-grained, weakly cemented, fractured.
Geologist: J. Fisher/M. Nauck/J. Raucci Driller: HAZ-Tech; Adamson Pump and Drill Date completed: 10-11-11 Date completed	290				ML .		295305	ML	Same as above, light olive brown (2.5Y 5/3).
Driller: HAZ-Tech; Adamson Pump and Drill Date completed: 10-11-11 Bit diameters: 15-1/4" and 9-7/8" (NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923' PICKLES BUTTE									
	Driller:	HAZ-Te	ch; Ádan	nson Pump and Dr	ill Bit diam	eters: 15– device:	1/4" and HQ core,	9-7/8	3" (NQ core 600'-750'); Adamson Pump and Drill re, rotary mud rotary drilling 385'-520', air rotary drilling
Steel suface casing: 10" Well Log: PB-14 Daniel B. Stephens & Associates, Inc.		A				face casin <u>c</u>	ı: 10" <sup>°</sup>		Well Log: PB-14

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300	Graphic Log	De:	Rock Quality	14 (4of10 Sample Interval (feet bgs)	USCS	Comments and Lithology
300 		300		305-315	ML	Same as above.
320-		- 100	0%/100%	315325	ML	Same as above, light alive brawn (2.5Y 6/2).
			0%/100%	325-335	SM	Silty sandstone, light olive brown (2.5Y 5/3), fine-grained, moderatedly cemented.
Neat cement grout 0.0'-807.0'	SM.		0%/100%	335-345	SM	Silty sandstone, pale yellow (2.5Y 7/3), fine—grained, weakly cemented dry.
So 340 Line			%/95%	345–355	SM-ML	Same as above grading into siltstone, light yellowish brown (2.5Y 6/3), weakly cemented.
Below	SP/SM 3	45 60-1	7/887	355-365	SP-SM	Same as above, with loose medium—grained sand.
370	SP/SM 3	70-1	%/0%	365–375		No recovery.
	ML			375-381 381-385	i	Siltstone, plae yellow (2.5Y 7/3), weakly cemented, dry. No recovery.
390-	39	31		385-395	SM	Clayey slity sand, light yellowish brown (2.5Y 6/3), fine— to medium—grained, moderately sorted, moderate plasticity, soft (cuttings from mud rotary).
400-1	SM	0 1 1 1 1	NA 3	395-405	SM	As above, more sand than fines (cuttings from mud rotary).
Geologist: J. Fisher/M. Nauck/J. Raucci Driller: HAZ—Tech; Adamson Pump and Drill Date completed: 10-11-11	Bit diar Samplir	meters: ng devid	/15—1 ce: HC در	/4" and ⊋ core, № µttings	9-7/8'	ir rotary Note: HAZ-Tech core drilling 0'-385', 520'-750' (NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923' PICKLES BUTTE
Daniel B. Stephens &	Steel s Assoc	iates,	-			Well Log: PB-14

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400 - NNINA KIINAN	Log		Quality Designation Recovery	Interval (feet bgs)	USCS Symbol	Comments and Lithology
410- 410-			NA	405-415		Same as above, clayey silt with sand, more fines than sand (cuttings from mud rotary).
420-1		420	NA	415-425	ML	Same as above (cuttings from mud rotary).
430-1		430	NA	425–435	ML	Same as above (cuttings from mud rotary).
8 440-		440	NA	435–445	ML	Same as above, few cutting returns (cuttings from mud rotary).
e 440- tur - pen - Stainless steel centralizer		450	NA	445-455	ML.	Same as above (cuttings from mud rotary).
* * * * * * * * * * * * * *		460	NA	455-465	ML	Same as above (outtings from mud rotary).
470- 470- 470-		470 1	NA	465-475	ML	Same as above (cuttings from mud rotary).
480		480 1111	NA	475–485	ML	Same as above (cuttings from mud rotary).
490		490 1 1	NA	485–520		No cuttings return.
500		500 J		-		
Geologist: J. Fisher/M. Nauck/J. Raucci Driller: HAZ-Tech; Adamson Pump and Dr Date completed: 10-11-11	ill Bit d Sam	diamet pling o	ethod: Cor ers: 15—1 device: H ce casing	I/4" and HQ core, cuttings	9-7/8	" (NQ core 600'—750'); Adamson Pump and Drill

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<b>500</b>		Graphic Log	500	Rock Quality Designation Recovery	Sample Intervai (feet bgs)	USCS Symbol	Comments and Lithology
500	4.5" 0.0. S.S.		500	NA			No cuttings return.
520-	blank casing 0.0'-845.0'			70%/77%	520-525	CL	Siity clayatone, olive gray (5Y 3/2), weakly cemented.
					525-530		Same as above.
530			530-11	90%/90%	530-540	CL	Silty sandy claystone, dark olive gray (5Y 3/2), fine—grained, weakly cemented, moist.
85540			540	90%/95%	540-550	CL	Same as above, with dark gray mottling, moderately cemented, few fractures.
			550	95%/95%	550-560	CL	Some as above.
560-	Neat cement grout	5.	560	95%/95%	560–570	CL	Same as above.
570-	0.0'-807.0'		570-1	70%/95%	570–580	CL	Sandy silty claystone, light yellowish brown (7.5Y 6/3), very fine—grained, weakly cemented, slight to mod plastice when wet.
580			580	82%/82%	580-590	CL	Same as above, some fractures.
590-			590-	70%/90%		CL	Sandy silty claystone, dark greenish brown (2.5Y 4/2), very fine—grained, weakly cemented, dry to damp.
600			500	0%/37%	595-605	CL	Sandy silty claystone, greenish gray (Gley1 5/1), very fine~grained, slight plasticity, moderately cemented, brittle, dry.
	er/M. Nauck/J. Raucci Adamson Pump and Dril 10—11—11	l Bit die	amete	thod: Core ers: 15-1 levice: H	/4" and	9-7/8	" (NQ core 600'-750'): Adamson Pump and Drill
	niel B. Stephens &			e casing:	10"		Well Log: PB-14

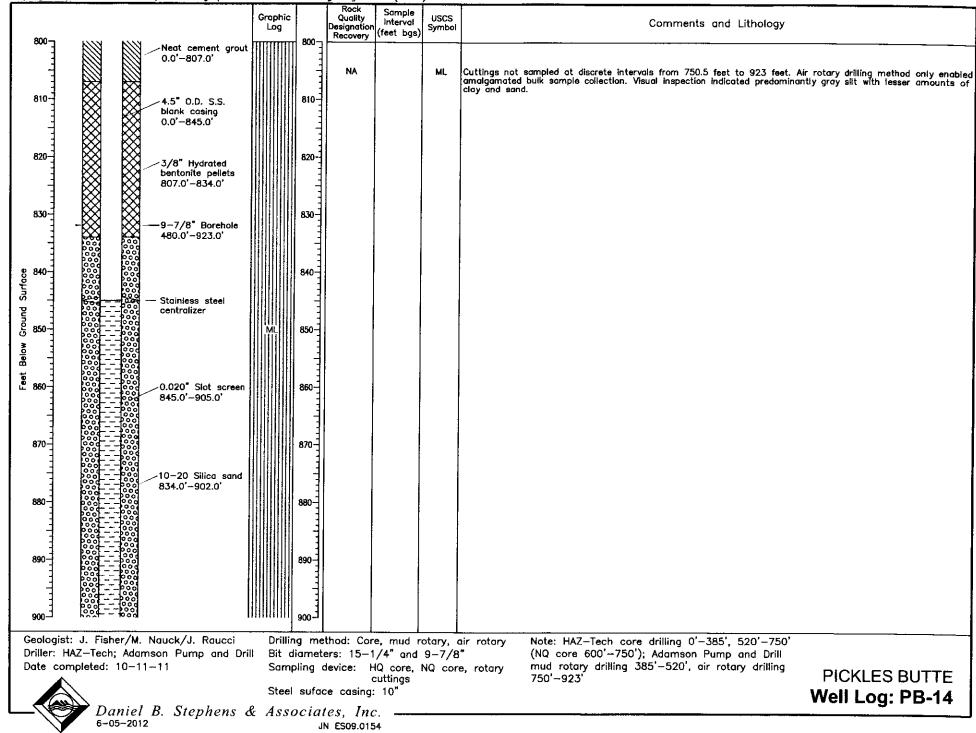
# S:\Projects\ES09.0154\_Pickles\VR\_Drawings\ES09\_0154\_07B\_borelogs.dwg PB-14 (7of10)

				Graphic Log		Rock Quality Designation Recovery	Sample Interval	uscs	Comments and Lithology
600			4.5" 0.D. S.S. blank casing 0.0'-845.0'		600 1 1 510		605-615	<u>-</u>	Sandy silty claystone, dark greenish gray (Gley1 4/1), fine—grained, slight to moderate plasticity when wet, dry (608—615 feet no recovery).
620-					620-	65%/84%	615-625	CL	Same as above.
630-			9-7/8" Borehole 480.0'923.0'		630	40%/64%	625-635	CL	Claystone, dark greenish gray (Gley1 4/1), plastic when wet, hard, brittle, dry-damp, massive.
				SL I		0%/84%	635-640	CL	Same as above.
epopuration for the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second sec					640 · · · · · · · · · · · · · · · · · · ·	0%/20%	640–650	CL	Same as above.
Below Ground					650	30%/44%	650-660	CL	Same as above.
1000 E			-Neat cement grout		660-1 1 1	10%/34%	660–670	CL	Same as above.
670- - - - -			0.0'-807.0'		670	0%/38%	670~690	SP :	Sandstone, dark greenish gray (Gleyl 4/1), fine—grained, well sorted, round to subround, non—plastic, hard, dry—damp.
680 690					680-1 	0%/0%	690-700	n	la recovery.
700_1					E.				
Driller: I	it: J. Fishe HAZ—Tech; mpleted: 1	Adam	Nauck/J. Raucci son Pump and Drill -11	Bit dia Sampli	imetei ing de	rs: 15-1/ evice: H(	, mud roi (4" and 9 core, N uttings 10"	97/8"	(NQ core 600'-750'); Adamson Pump and Drill rotary mud rotary drilling 385'-520', air rotary drilling 750'-923' PICKLES BUTTE
-7	Dar 6-05	n <i>iel</i> 2012	B. Stephens &	Assoc		es, Inc. ES09.0154			Well Log: PB-14

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				Graphic Log		Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
700					700		700-710	CL	Claystone, dark greenish gray (Gley1 4/1), plastic when wet, hard, brittle, damp.
710-			4.5" O.D. S.S. blank casing 0.0'~845.0'		710	07/637	710-720	CL	Same as above, most likely borehole slough.
720-			9-7/8" Borehole 480.0'923.0'	CL	720-	20%/55%	720–730	CL	Claystone, dark greenish gray (Gley1 4/1), plastic when wet, hard, brittle, dry—damp, massive, with few fractures.
730-					730-1-1	90%/96%	730–740	CL	Same as above, without fractures.
Protoce					740 1	70%/100%	740750.5	CL	Same as above.
Feet Below Feet Below Feet Below Feet Below					750 - - - - - - - - - - - - - - - - - - -	NA	750.5-923		Cuttings not sampled at discrete intervals from 750.5 feet to 923 feet. Air rotary drilling method only enabled amalgamated bulk sample collection. Visual inspection indicated predominantly gray silt with lesser amounts of clay and sand.
770-			Neat cement grout 0.0'-807.0'		770-				
780-					780-1				
790- 					790-1				
Driller: I		Adan	Nauck/J. Raucci nson Pump and Drill I—11	l Bit di Samp	iamete Iling d	thod: Core ers: 15-1, levice: Hi c e casing:	/4" and 1 Q core, N uttings	97/8'	(NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923' PICKLES BUTTE
	Dan 6-05	1iel -2012	B. Stephens &	k Asso		es, Inc ES09.0154			Well Log: PB-14

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	0.020 <sup>■</sup> Slot screen 845.0'-905.0'	Graphic Log	Oneternet	Sample Interval feet bgs)	USCS Symbol	Comments and Lithology
900 n 1 910 n 910 n	900	900 - 	NA		ML	Cuttings not sampled at discrete intervals from 750.5 feet to 923 feet. Air rotary drilling method only enabled amalgamated bulk sample collection. Visual inspection indicated predominantly gray silt with lesser amounts of clay and sand.
920- 	480.0'-923.0' Slough 902.0'-923.0' T.D.=923.0'	920-				
930-		930				
esond Surface		940-				
Feet Below ( 096		9601				
970- 		970				
980-1 980-1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		980				
990-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-		990				
Driller:	ist: J. Fisher/M. Nauck/J. Raucci HAZ—Tech; Adamson Pump and Drill ompleted: 10—11—11	Bit diamet Sampling	ithod: Core, ers: 15-1/ device: HQ cu ce casing:	(4" and ) core, N Ittings	97/8	' (NQ core 600'-750'); Adamson Pump and Drill
	Daniel B. Stephens & 6-05-2012		<i>tes, Inc.</i> n esog.0154			

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		Graphic Log	D	Rock Quality Designation Recovery	Sample Intervai (feet bgs)	USCS Symbol	Comments and Lithology
	Ground surface	0800		NA	0-10	GP-SP	Gravelly sand, olive gray (5Y 5/2), fine— to medium—grained, subrounded, well sorted, non—plastic, loose, moist
	eat cement grout g 0'-757.0'	SW	10	NA	10–20	SW	Sand, light gray (5Y 7/2), fine- to coarse-grained, well sorted, subrounded, non-plastic, loose, dry.
20-			20	NA	20-30	SP	Same as above.
30-] 30-] 30-] 30-]	5" O.D. Stainless eel (S.S.) blank psing 0'-790.0'	SP.	30	NA	30-40	SP	Same as above.
Ground Surface			40	NA	40-50	SC-SM	Clayey silty sand, pale yellow (5Y 7/3), fine-grained, subrounded, low plastic, soft, slightly moist.
Feet Below Ground	i−1/4" Borehole 0'-400.0'		50	NA	50-60	SC-SM	Same as above
		SC/SM	60	NA	60-70	SC-SM	Same as above.
	ainless steel ntralizer		70	NA	70~80	SC-SM	Clayey silty sand, light olive brown (2.5Y 5/3), fine— to coarse—grained, rounded to subrounded, low plastic, soft, moist
80			80 1 1 1	NA	80~90	SP	Sand, pale yellow (2.5Y 7/4), fine-grained, non-plastic, loose, moist
90 <sup>-11</sup>	" Steel casing 0'-400.0'	SP	90 1 1 1	NA	90-100	SP	Same as above.
100-J NNNN NNNN Geologist: M. Nauck/J. Rau					e, mud ro		Nothing 665617.169
Driller: HAZ-Tech; Adamson Date completed: 10-26-11	Pump and Drill	Bit die Sampl Steel Note:	ameter: ling der suface TOC =	s: 15—1, vice: H casing: top of	/4", 12" Q core, r 10" casing	and 9	

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3: (Projects (E309.0134_Pickles (VR_Drdwings (E509_C		Rock	1		
	Graphic Log	Quality Designation Recovery	Somple Interval (feet bgs)	USCS Symbol	Comments and Lithology
		NA	100-110	SP	Sand, light yellowish brown (2.5Y 6/3), fine-grained, poorly sorted, subrounded, non-plastic, loose, moist
110- 110-	1	110-1 NA	110-120	SP	Sand, light olive brown (2.5Y 5/3), fine— to medium—grained, subrounded, poorly sorted, non—plastic, loose, moist
120-	1	120-1 NA	120-130	SP	Same as above.
130- 130- 130- 130- 130- 130- 130- 130-	1	30-1 NA	130-140	SP	Same as above.
e 140-	1	40 NA	140150	SP	Same as above
es 140- 	SP 1	50 NA	150-160	SP	Same as above.
Feet Below	1	60NA	160–170	SP	Same as above.
170- - - - - - - - - - - - - - - - - - -	1	70 NA	170–180	SP	Same as above.
	11	80-1 NA	180-190	SP	Same as above with iron staining.
190- 190- 10" Steel cosing 0.0'-400.0'	15	30	190–200	SP	Sand, pale yellow (2.5Y 8/4), fine to coarse-grained, poorly sorted, subangular to subrounded, non~plastic, loose, dry.
Geologist: M. Nauck/J. Raucci Driller: HAZ—Tech; Adamson Pump and Dril Date completed: 10—26—11	l Bit dia Samplir	method: Cor meters: 15—1 ng device: H uface casing:	/4", 12" Q core, r	and 9	Note: Adamson Pump and Drill mud rotary -7/8" drilling 0'-425'; HAZ-Tech core drilling suttings 425'-625'; air rotary drilling 625'-870' PICKLES BUTTE
Danial P. Stanker					Well Log: PB-15
Daniel B. Stephens &	L ASSUC	JN ES09.015			

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S. (Projects (2003.010+_Pickles (VR_DR		107_0/0_	DOI BIC				
200		Graphic Log	200	Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
			200	NA	200-210	SP	Same as above, medium-coarse grained
210- 	cement grout 757.0'		210-1 	NA	210-220	SP	Same as above.
220-			220-1	NA	220–230	SP	Same as above.
230- 	D.D. Stainless (S.S.) blank 1 790.0'	SP	230	NA	230–240	SP	Same as above with iron staining.
e 240- punoug punoug 250-1			240	NA	240–250	SP	Same as above.
punoug 250-1	/4* Borehole 100.0'		250	NA	250–260	SP	Sand, pale yellow (2.5Y 8/3), fine-grained, well sorted, subrounded, non-plastic, loose, dry.
And And And And And And And And And And			260	NA	260~270	SM-SC	Silty clayey sand, pale yellow (5Y 7/3), fine-grained, subrounded, low plastic, soft, moist
270- central		SM/SC	270	NA	270-280	SM-SC	Same as above.
280-		SM I	280	NA	280–290	SM	Silty sand, pale olive (5Y 6/3), fine-grained, subrounded, non-plastic, loose, slightly moist
290- 	eel casing 00.0'	SM/SC	290	NA	290~300	SM-SC	Clayey silty sand, clive (5Y 5/3), fine-grained, subrounded, very low plastic, soft, slightly moist
VX///A V//X/A L_006			300-				
Geologist: M. Nauck/J. Raucci Driller: HAZ-Tech; Adamson Pu Date completed: 10-26-11	mp and Drill	Bit dia Sampl	amete ling d	thod: Core ers: 15–1 levice: H :e casing:	/4", 12" Q core, i	and 9-	Note: Adamson Pump and Drill mud rotary -7/8" drilling 0'-425'; HAZ-Tech core drilling cuttings 425'-625'; air rotary drilling 625'-870' PICKLES BUTTE
							Well Log: PB-15
— Daniel B. St. 6-05-2012	epnens &	ASSO		<i>es, Inc</i> NES09.015		· .	
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3: (FI0]ects (E309:0134_Fickles (VR_Drdwings (E309_0			Rock	r		
300-7 (1)1/11 (1)1/11	Graphic Log	300	Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
		300-	NA	300-310	SM	Silty sand, pale yellow (5Y 8/2), fine-grained, subrounded, non-plastic, loose, dry.
310- 310-	M SM	310- 310-	NA	310320	CL	Sandy silty clay, light yellowish brown (2.5Y 6/4), fine-grained, subrounded, medium plastic, soft, moist
320		320	NA	320-330	CL	Same as above.
4.5" O.D. Stainless steel (S.S.) blank casing 0.0'~790.0'		330-1	NA	330-340	CL	Same as above.
Surface L		340	NA	340-350	CL	Same as above.
e 340- pun yun 350- - - - - - - - - - - - - -	GL	350	NA	350-360	C∟	Silty clay, pale olive (5Y 6/3), very fine-grained, highly plastic, soft, wet
		360		360-370		
370- centralizer		370	NA	370380	CL	Same as above.
		380	NA	380-390	CL	Same as abova
390- 0.0'-400.0'		390	NA	390-400	CL	Same as above
		100				
Geologist: M. Nauck/J. Raucci Driller: HAZ-Tech; Adamson Pump and Dri Date completed: 10-26-11 Daniel B. Stephens d	l Bit di Samp Steel	iamete ling d sufac	thod: Con ers: 15–1 levice: H e cosing:	/4", 12" IQ core, r 10"	and 9	
6-05-2012			N ES09.015			

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	Graphic Log	Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
400 - 12" Borehole 400.0'-405.0' 410-	400 CL 410		400-410 410-425	CL	Same as above. No recovery.
420- 9-7/8" Borehole 405.0'-870.0'	420-		425-435	ML	Siltstone, pale yellow (5Y 7/3) to light yellowish brown (2.5Y 6/3), moderately soft, significant clay fraction
430- 4.5" 0.D. S.S. blank casing 0.0'-790.0'	SP 	75%/100%	435–445	SP ML	Sand, light yellowish brown (2.5Y 6/4), medium—grained, well sorted, loose (from 435 to 437 feet) then siltstone as above to 445 feet.
e 440- e 440- b 1 c 1 c 1 c 1 c 1 c 1 c 1 c 1 c	450-		445-455 455-465	SM SM-ML	Silty clayey sand, pale olive (5Y 6/3), fine-grained, appreciable clay with alternately clayey soft and hard layers, with organic material and orange oxidation. No recovery from 452.5 to 455 feet. Silty sand and sandy silt, pale olive (5Y 6/3), laminated, fine-grained, alternating soft and hard layers,
470- 470- 470- 470- 470- 470- 470- 470-	SM/ML 460-	100%/100%	465–475	SM-SP	brittle to plastic, slightly moist, with abundant organic material. Same as above interbedded with sand, olive gray (5Y 5/2), fine— to medium—grained, moderately well sorted, loose, soft
480-	1. 	85%/100%		ML SMMI	Sandy siltstone, pale olive (5Y 6/3), laminated, weakly to moderately cemented, micaceous with some clay. Similar to above silty sand and sandy silt, color mottled pale olive (5Y 6/3) to light olive gray (5Y 6/2),
490-1 1	50	60%/75%			massive to laminated, weakly cemented, interbedded clay and clayey layers.
500-J NN NN Geologist: M. Nauck/J. Raucci Driller: HAZ-Tech; Adamson Pump and Dri Date completed: 10-26-11 Date Daniel B. Stephens c	Drilling m Drilling m Bit diame Sampling Steel sufe	iethod: Cor eters: 15-1 device: F ace casing:	/4", 12"  Q core, : 10"	and 9	

#### Rock Sample Graphic Quality USCS Interval Comments and Lithology Designation Symbol Log (feet bgs) Recovery 500-500-SM/MÍ 90%/100% 505-515 ML Same as above, predominantly silt. 510-510-9-7/8" Borehole 405.0'-870.0' 80%/90% 515-525 ML Same as above. 520-520-85%/100% 525-535 ML. Same as above, predominantly silt with minor sand and clay, massive to laminated, locally crossbedded, slightly moist 530 ML 530-4.5" 0.D. S.S. blank casing 0.0'-790.0' 50%/65% 535-545 ML Same as above. 540-540-Surface 100%/100% 545--555 ML Similar to above, clayey siltstone, light yellowish brown (2.5Y 6/2-6/3). Ground Neat cement grout 550-550-0.0'-757.0' Below 100%/100% 555-565 ML-CL Same as above at 555 feet silty clay, brownish gray (2.5Y 5/2), at 565 feet weakly to moderately cemented. Feet 560-ML/CL 560-100%/100% 565-575 ML Clayey silt, olive (5Y 4/3), soft, slightly plastic to 568.5 feet, silstone, dark greenish gray (Gley1 10Y 4/1), siltstone with sand and clay, sandy at top, well cemented, contact w/ "blue clay" unit at 568.5 feet 570-570-Stainless steel ME centralizer 20%/30% 575-585 CL Sandy clay, dark gray (Gley1 4/N), well cemented, slightly plastic when wet, micaceous, dry. 580 580-100%/100% 585-595 ML Silstone with clay and minor sand, mottled dark gray (Gley1 4/N), well cemented, micaceous. 590-590-90%/95% 595-605 ML Sandy silstone with clay, dark gray (Gley1 4/N), massive to laminated, micaceous. 600 <sup>\_</sup> 600-Geologist: M. Nauck/J. Raucci Drilling method: Core, mud rotary Note: Adamson Pump and Drill mud rotary Driller: HAZ-Tech; Adamson Pump and Drill Bit diameters: 15-1/4", 12" and 9-7/8" drilling 0'-425': HAZ-Tech core drilling 425'-625'; air rotary drilling 625'-870' Date completed: 10-26-11 Sampling device: HQ core, rotary cuttings PICKLES BUTTE Steel suface casing: 10" Well Log: PB-15 Daniel B. Stephens & Associates, Inc. 6-05-2012 JN ES09.0154

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#### Rock Sample Graphic Quality USCS Interval Comments and Lithology Designation Log Symbol (feet bgs) Recovery 600-600-80%/90% 605-625 SM-SP Sand and silty sand, mottled gray and light gray, laminated, fine- to medium-grained, moderately sorted, loose to well cemented, slightly moist to moist; interbedded w/ thin (1 to 2 cm) clay lenses. 610 610-9-7/8" Borehole 405.0'-870.0' SM/SP 620-620 Cuttings not sampled at discrete intervals from 625 feet to 870 feet. Air rotary drilling method only enabled amalgamated bulk sample collection. Visual inspection indicated predominantly gray silt with lesser amounts of clay and sand. 625-870 ML 630-630 4.5" O.D. S.S. blank casing 0.0'-790.0' 640 64A Ground Surface Neat cement grout 650-650-0.0'-757.0' Below Feet 660-660 670 Stainless steel 670centralizer 680 680-690 690 700-700-Geologist: M. Nauck/J. Raucci Drilling method: Core, mud rotary Note: Adamson Pump and Drill mud rotary Driller: HAZ-Tech; Adamson Pump and Drill Bit diameters: 15-1/4", 12" and 9-7/8" drilling 0'-425'; HAZ-Tech core drilling 425'-625'; air rotary drilling 625'-870' Date completed: 10-26-11 Sampling device: HQ core, rotary cuttings PICKLES BUTTE Steel suface casing: 10" Well Log: PB-15 Daniel B. Stephens & Associates, Inc. 6-05-2012 JN ES09.0154

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