

## APPENDIX F: GEOTECHNICAL INVESTIGATION REPORT

# Report of Geotechnical Investigation and Analysis

## Slope Stability Evaluation Pickles Butte Sanitary Landfill Expansion Canyon County, Idaho

Tetra Tech Project No. 114-571040-2022

August 16, 2022

### PRESENTED TO

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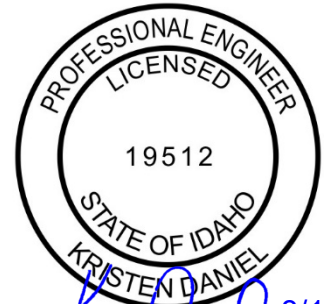
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## ACRONYMS/ABBREVIATIONS

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Acronyms/ Abbreviations	Definition
AASHTO	American Association of State Highway and Transportation Officials
ASTM	ASTM International (formerly known as American Society for Testing and Materials)
bgs	Below ground surface
CFR	Code of Federal Regulations
IDEQ	Idaho Department of Environmental Quality
EPA	U.S. Environmental Protection Agency
FS	factors of safety
ksf	kips per square foot
MCE	Maximum Credible Earthquake
mm	millimeter
MSWLF	Municipal Solid Waste Landfills
PBSL	Pickles Butte Sanitary Landfill
PGA	Peak Ground Acceleration
PSHA	Peak spectral horizontal acceleration
SPT	Standard Penetration Testing
USGS	United States Geological Survey

## EXECUTIVE SUMMARY

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The Pickles Butte Sanitary Landfill is developing a plan for the expansion of the landfill to include an additional four phases, (Phase 5 through Phase 8). The proposed expansion consists of approximately 231 acres of unlined cells pending the approval of an arid exemption. Proposed permanent excavation slopes are planned to be on the order of 3H:1V to 4H:1V, with maximum cut depths on the order of 150 to 165 feet.

Tetra Tech previously completed a slope stability evaluation that included static and seismic stability evaluations for Phases 2 through 4 of the Canyon County Landfill (October 7, 2015). Tetra Tech also reviewed the previous evaluations conducted by Holladay Engineering Company for the Pickles Butte Sanitary Landfill, dated 1998, and conducted a seismic survey that was dated February 21, 2022 titled, 'Pickles Butte Sanitary Landfill 3D Seismic Survey Report'. The survey was designed to image and delineate a suspected fault in support of the proposed expansion program at the PBSL.

For this stability evaluation, Tetra Tech incorporated the following information: 1) the soils strength data available from previous analysis, 2) materials strength properties assigned based on the laboratory testing of the geotechnical samples collected in 2021 and also correlated from the Standard Penetration Testing (SPT) N-value (blow count) data collected during the geotechnical drilling and previous well installation reports.

Based on findings from former and 2021 site investigations, the subsurface conditions beneath the areas of proposed landfill expansion are assumed to generally consist of silty and clayey sand, clay, and gravel overlying the Glenns Ferry Formation (300 to 950 feet thick), which includes younger lacustrine and fluvial sediments. The surrounding local geology includes an igneous basalt group of the Hat Butte-McElroy Butte type<sup>1</sup> that was not encountered in area of the proposed expansion.

Slope stability and pseudo-static analyses were performed using the computer program Slide2 (2020), developed by Rocscience, Inc., to determine the factors of safety (FS) of critical slip surfaces using both circular (rotational) and block failure analyses and vertical slice limit equilibrium methods. Circular failures can be viewed as a soil 'slump' with a remnant head 'scarp' or drop in elevation where the slide started, and a resultant 'hump' or bulge at the slide terminus. A block failure represents a large mass or 'chunk' of soil failing outwardly as a larger intact mass. Where the pseudo-static analysis indicated a factor of safety of equal to or less than 1.3 (industry standard for pseudo-static factor of safety for landfills), the internal slope of the landfill cell prior to waste emplacement was evaluated using the Newmark displacement analysis method to determine a range of potential seismic-induced deformations of the refuse mass.

Results of the slope stability evaluations indicate that the preliminary design for the expansion phases will meet the requirements of the Idaho Administrative Rules IDAPA 58.01.06 for the Idaho DEQ's administration of municipal solid waste landfills (MSWLF). The analyses indicate static FS values on the order of 1.38 to 2.43, and 1.83 to 3.11 for circular and block failure respectively, while the pseudo-static FS values were on the order of 0.99 to 1.88, and 1.45 to 2.16 for circular and block failure, respectively. Subsequent seismic deformation analyses indicate maximum probable displacements on the order of 0.25 to 3.19 inches (0.5 to 8 cm) for the anticipated peak ground acceleration of 0.12g generated during the design seismic event at the project site. In general, the seismic displacement analyses indicate permanent seismic-induced displacements within the tolerances 6 to 12 inches (15 to 30 cm) that are typically considered acceptable for design of landfill systems with no liner.

Multiple slope angles were considered for Tetra Tech's slope analyses, ranging from 2.5:1 to 4:1 depending on the soil and bedrock types at each location. Based on Tetra Tech's analysis and the required FS's, the following two slope angles are recommended for the preliminary landfill site grading plans:

3H:1V: for the majority of the site slopes

4H:1V: where silt is encountered (Section F discussed below)

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<sup>1</sup>Mancos - Macrostrat.org

The 4:1 slope was analyzed and recommended for Section F because silt was interbedded between poorly-graded sand and fine sand and created a weakened soil profile. In areas where a high concentration of silt is predominant during construction, a slope of 4H:1V is recommended for cut areas. The soil profile within Section F was identified as having a high concentration of silt in the upper 135 feet of the proposed slope cut, thus decreasing the factor of safety. There are other areas where the silt was present; however, based on the analysis the proposed cut slope of 3H:1V was allowable for the silts as they were interbedded into stronger soil deposits. As the stratification is exposed during excavation of future cells, it is recommended that the soil conditions be reviewed to verify they match the design criteria.

The slope with compacted refuse were modeled to confirm the slope angles that were allowable during the backfilling process. Slopes of 3H:1V are recommended as a maximum angle for the backfill process. A steeper slope of 2.75H:1V was modeled as an iteration to confirm the recommendations, and in this situation the pseudo static conditions produced a factor of safety below 1.3 and is not recommended.

Portions of the soil profile were defined as claystone, and have unconfined compression strengths higher than the site soils; however, the claystone had interbedded layers of softer soils, and for this reason Tetra tech has treated these areas as a soil rather than a rock and also recommends a slope cut of 3H:1V for the claystone zones.

This executive summary has been prepared solely to provide a general overview and should not be relied upon for any purpose except for that for which it was prepared. The full geotechnical report must be referenced for information about findings, recommendations, and other concerns.

## 1. INTRODUCTION AND BACKGROUND

The following report is the geotechnical evaluation of the slope stability that provides recommendations for the planned lateral expansion of the landfill. The Pickles Butte Sanitary Landfill (PBSL) is located at 15500 Missouri Ave. in Nampa, Idaho. The landfill is located approximately 6-miles south of Nampa, north of Missouri Avenue, south of Deer Flat Road, and ¼- mile west of Farner Road. Canyon County (County) owns approximately 1,180 acres of land in the area, which includes the active area of the PBSL. The County has operated the landfill since it began accepting waste in April 1983. PBSL currently services the residents of Canyon and Owyhee Counties.

The Idaho Department of Environmental Quality (DEQ) approved the original design and operating plan for the PBSL in June 1973, and reconfirmed approval in May 1975 (Holladay, 1994). The Southwest District Health Department approved the landfill in December 1979. Then when Subtitle D was implemented, the County obtained a site certification for the landfill from the DEQ in August 1993 for 116.7 acre. The County applied to modify the site certification boundary in 2020 and received approval from DEQ in February 2021 for approximately 600 acres. The current waste disposal area occupies the original footprint of approximately 116.7 acres, which has a natural soil liner. The Site Certification for the planned lateral expansion was approved on February 26, 2021.

The DEQ Site Certification approval included a request that engineering design considerations be evaluated for resisting peak ground accelerations, prior to the design and construction of containment structures. This report addresses that request and discusses the seismic considerations and slope stability. After the approval was received, a data gaps analysis was conducted in 2021 to identify missing or additional data required for the design focusing on geotechnical and seismic considerations. The evaluation identified locations where additional data would be beneficial and proposed a geotechnical drilling program that was initiated in November 2021 to collect additional data for the analysis.

This report is organized as follows: **Section 1** presents the introduction and background; **Section 2** presents the purpose and the scope; **Section 3** provides information on the proposed expansion; **Section 4** provides highlights of the field exploration; **Section 5** provides information on the geotechnical laboratory testing; **Section 7** discusses the engineering analysis and recommendations; **Section 8** **Section 9** provides limitations of the study; and **Section 10** provides references. **Appendix A** provides miscellaneous figures and details, **Appendix B** provides exploratory boring logs, **Appendix C** provides the laboratory testing, **Appendix D** provides slope analysis, **Appendix E** provides deformation analysis, and **Appendix F** provides previous boring logs.

## 2. PURPOSE AND SCOPE OF STUDY

Tetra Tech performed stability analyses and seismic evaluations of the proposed expansion cell geometries to verify adequate stability or to indicate if flatter slopes are required to achieve stability. The analyses were performed in accordance with Tetra Tech's proposal and contract with Canyon County Solid Waste.

The regulatory requirements for the stability analysis are discussed in the administrative rules for the Idaho Solid Waste Facilities Act (Idaho Statutes, Title 39 – Health and Safety, Chapter 74, Section 39-7407) for the Idaho Department of Environmental Quality's (IDEQ) administration of municipal solid waste landfills (MSWLF) and are discussed further in **Section 7.1**.

The purpose of this study is to demonstrate that slope stability requirements are met for the conceptual design of the following containment structures:

- Phase 5-1, 5-2, 5-3 Temporary Cut Slope, Maximum Section (Section E)
- Phase 6-1, 6-2, 6-3 Temporary Cut Slope, Maximum Sections (Sections C and F)
- Phase 7-1, 7-2, 7-3 Temporary Cut Slope, Maximum Section (Sections B, C, D, F, G)
- Phase 8-1, 8-2, 8-3 Temporary Cut Slope, Maximum Section (Sections B, C, D, F, G)

- Final Slope with Waste Backfilled (Section A was used to represent final slope criteria).

This report details and summarizes the analyses, the material properties selected for the analyses, the seismic design criteria, and presents conclusions based on the existing subsurface conditions and proposed landfill design and construction.

### 3. PROPOSED EXPANSION

The proposed area for the expansion has been sectioned into smaller units and labeled as the phases listed in Figure 1040-1, Data Gap Areas & Proposed Boring Plan (**Appendix A**). The proposed conceptual expansion of Phases 5 through Phase 8 will consist of approximately 231.4 acres of unlined cells. Proposed fill slopes are planned to be on the order of 5.3H:1V (horizontal to vertical) to 4H:1V, with maximum waste fill depths on the order of 254 feet. Proposed excavation slopes are planned to be on the order of 3H:1V to 4H:1V, with maximum cut depths on the order of 150 to 165 feet. The finished fill slopes will consist of a sequence of slopes with 20-foot-wide storm water/erosion-control benches for every 40 to 60 feet of elevation gain. The purpose for selecting flatter slopes includes more effective erosion and stormwater control on the final slopes.

If the design, locations, or conditions are significantly different from those described above, Tetra Tech should be notified to reevaluate the recommendations contained in this report.

### 4. FIELD EXPLORATION

Tetra Tech conducted a field investigation for Phases 5 through 8 between the dates of November 15 and December 19, 2021. The field investigation consisted of drilling eight boreholes to explore subsurface conditions at the locations shown on Figure 1040-1 (Data Gap Areas & Proposed boring Plan, **Appendix A**). Figure 1040-1 includes the conceptual expansion cells for the landfill, the locations of the exploration borings, and the location of borings drilled in previous phases. Prior to mobilization, Tetra Tech contacted Idaho One Call to request the location and clearance of public underground utilities before performing drilling. Well logs from the previous well installations are included in **Appendix F**, and they include extracted pages from the Geotechnical Evaluation by Holiday Engineering Company (Holiday), Borehole Logs GT-1 through GT-5, and the combination of Well Driller's Reports and Well Logs PB logs 5 through 15 by Holiday and Daniel B. Stephens & Associates, Inc. The logs provide general descriptions and depths of the site soils at each location.

Canyon County's drilling subcontracted with Holt Drilling to advance the borings through overburden soils with a track-mounted TS150 Crawler drilling rig equipped with auger, 6-inch diameter outer casing and core barrel. The TS150 Crawler provides very accurate and detailed soil profiles when compared to other drilling methods like auger. Tetra Tech's field engineer provided technical oversight during the field investigation, logged the borings, and obtained samples. The borings were backfilled with grout.

Sampling of the borings included determination of the N values, collection of split spoon samples, and bulk samples. Split-spoon samplers were driven into the various strata using a 140-pound hammer falling 30 inches. Sampling was done every 2 feet in the first 10 feet to obtain accurate soil strengths in the depths most critical to the evaluation of the dust control system and landfill gas flare pad. After 10 feet sampling was done every 5 feet to the final depth. For the expansion design sampling was done every 5 feet done to a depth of 50 feet and every 10 feet to 170 feet to collect information about the relative densities of the soil stratum.

The number of blows required to advance the sampler each of three successive 6-inch increments was recorded. When using the split-spoon sampler, the total number of blows required to advance the sampler the second and third 6-inch increments is the penetration resistance (N value), as described by ASTM International (ASTM) Method D1586. Penetration resistance values generally indicate the relative density or consistency of the subsurface soils.



Samples of the subsurface materials were obtained with both 2-inch and 2.5-inch outside- diameter split-spoon samplers. Bulk, Shelby tube and modified California samples were collected at various layers by the field engineer under the direction of a senior geotechnical engineer. More specific drilling and subsurface information regarding individual borings is listed below. Bulk samples of soil were obtained from cuttings based on visual observations in the field.

**B2021-1/B2021-2**

- Geotechnical borings for dust control system drilled to 30 ft
- Deep layer of poorly graded sand

**B2021-3**

- Geotechnical boring for landfill expansion
- Winch line snapped imbedding sampling rod deep into a clay layer at 170 feet.

**B2021-4**

- Geotechnical boring for landfill expansion
- Thick layers of loose sand extended to 90 feet, which created an issue with keeping the hole open. The hole collapse was especially problematic between 50 - 90 feet.
- The deep clay layers were not encountered as in all other deep borings.

**B2021-5**

- This boring was sited after geophysical seismic testing
- Samples were collected for analysis in the zone geophysics indicated the fault splay was located
- No visual evidence was found during drilling to confirm the existence of a fault plane

**B2021-6**

- Geotechnical boring for landfill expansion
- Altering layers silt and sand were encountered till 75 feet
- Dense clay to 200 feet with occasional silt seams between 100 - 110 feet

**B2021-7**

- Geotechnical boring for landfill expansion
- Altering layers of dense sand and silt were encountered till approximately 65 feet followed by dense clay with varying amounts of silt to 145 feet.
- Dense blue-gray clay continued to 200 feet.

**B2021-8**

- Geotechnical boring for Landfill Gas Flare Station
- Type II cement should be used for concrete in contact with silt soils

Boring logs were prepared noting the borehole location, equipment and drill methods used, subsurface profile and descriptions per ASTM D2487. Groundwater was not encountered in any of the borings. Boring depths are referenced to the existing ground surface elevation. Depths at which the samples were obtained along with the penetration resistance values are shown on the logs of exploratory borings, presented in **Appendix B** (Figures 1-B through 8-B).

## 5. LABORATORY TESTING

Samples obtained during the field exploration were taken to Tetra Tech's accredited laboratory, where they were observed and visually classified in accordance with ASTM Method D2488, which is based on the Unified Soil Classification System.

Following the field exploration, a senior Tetra Tech geotechnical engineer reviewed all the boring logs and samples obtained and created an inventory of samples available for testing. The senior engineer reviewed the potential depths of cut, and locations of fill, and selected samples along the depths of each boring for testing. The tests assigned in each boring were intended primarily to identify the precise type of soil at each depth, as well as the associated strength properties of each soil type, with the ultimate goal of incorporating all of the strength testing directly into the slope stability models in each cross section analyzed. The laboratory testing data was directly utilized in the slope stability models to determine the resultant factor of safety at each cross-section location.

The laboratory testing was performed in general accordance with the Idaho Materials Manual of Test Procedures, American Association of State Highway and Transportation Officials (AASHTO), ASTM, or other approved procedures. Tetra Tech's laboratory is an AASHTO Materials Reference Laboratory (AMRL) and Concrete and Cement Reference Laboratory (CCRL) accredited facility conforming to ASTM E 329 - Standard Specification for Agencies Engaged in Construction Inspection, Testing, or Special Inspection.

**Table 1** describes laboratory testing performed for this investigation, and their purpose:

**Table 1. Laboratory Testing Completed by Tetra Tech**

Test Conducted:	To Determine:	Test Procedure:
Natural Moisture Content	Moisture content representative of field conditions at the time samples were taken.	ATM D2216
Grain-size Distribution	Size and distribution of soil particles (i.e., clay, silt, sand, and gravel).	ASTM D6913
Natural Moisture Content	Moisture content representative of field conditions at the time samples were collected.	ATM D2216
Atterberg Limits	The effect of varying water content on the consistency of fine-grained soils.	ASTM D4318
Moisture-Density Relationship	The optimum moisture content for compacting soil and the maximum dry unit weight (density) for a given compactive effort.	MT 210-16 MT 230-16
Unconfined Compression	Unconfined compressive strength of soil and rock.	ASTM D2166 ASTM D7012
Direct Shear	Standard Test Method for Direct Shear Test of Soils Under Consolidated Drained Conditions	ASTM D3080
Triaxial Shear	Consolidated-Undrained soil strength properties.	ASTM D4767
Resistivity and pH	The combination of these characteristics determines the potential of soil to corrode metal.	ASTM G187/D4972 MT 232-16
Consolidation	The amount a soil sample compresses with loading and the influence of wetting on its behavior. For use in settlement analysis, determining expansive potential and foundation design.	ASTM D2435

Field and laboratory test results are presented graphically and summarized in **Appendix C**. This data, along with the field information, were used to prepare the exploration boring logs in **Appendix B**.

## 6. SUBSURFACE CONDITIONS

Subsurface soil conditions are variable throughout the boring depths; elevations ranged between 2956.6 to 2436.6 feet. The borings contained interbedded layers of poorly graded sand, poorly graded sand with silt, silty sand, silty with sand, silt, lean clay with sand, and silty clay. One layer of fat clay was observed in boring B2021-6 as described below. Given the variability of the site soils, other variations in the soil classifications are entirely possible. The top elevation of the individual borings varied, so the boring descriptions were broken into sections based on elevation for a more defined classification throughout the proposed cells.

Subsurface soils were classified in accordance with standards set by AASHTO. Descriptive terms were obtained using the ASTM Soil Classification System. Both the AASHTO and ASTM classifications are noted on the logs and laboratory data presented in **Appendix C** for each soil sample. **Appendix C** includes a summary of all the soil types and properties obtained in the borings drilled along the project length. Each soil type encountered is briefly described below.

### 6.1 Sand

Sand was encountered in all borings, B2021-1 through B2021-7, at depths ranging in elevations on the order of 2799 to 2470 feet. The sand gradations included poorly-graded sand, poorly-graded sand with silt, and silty sand. The poorly-graded sand generally consisted of a fine to medium-grained matrix, while the silty sand was fine-grained. In Boring B2021-8, the sand included 10 feet of fine-grained, silty sand, and 2.5 feet of a poorly-graded fine to medium grained sand.

Penetration resistance values in the sand ranged from 2 to greater than 50 blows per foot which indicates a potentially very loose to very dense soil stratum. The looser densities were encountered near the surface, with an increase in density at depths of approximately 10 feet and deeper. The natural moisture contents in the sand ranged from 2 to 22 percent at the time of drilling.

Laboratory testing performed on bulk and split spoon samples of the sands indicated a range of maximum dry density between 100.2 and 111.7 pcf, and an optimum moisture content between 11 and 16 percent. (**Appendix C**). Results of the Unconfined Compression Test for boring B2021-3 between 61 and 65 feet indicates an unconfined compression strength on the order of 0.143 kips per square foot (ksf). Direct shear testing of the sand in Boring B2021-3 between 60 to 62 feet indicates a cohesion of 0.282 ksf and a friction angle of 20.2 degrees, and between 80 and 82 feet a cohesion of 0.413 ksf, and a friction angle of 32.81 degrees. Consolidation testing indicated an under-consolidated soil in with preconsolidation pressure 3.0 ksf and a swell pressure of 2.6 percent. (**Appendix C**).

In Boring B2021-4 between 90 and 91 feet, the direct shear testing indicated a cohesion of 0.198 ksf, and a friction angle of 22.83 degrees, and between 120 and 120.9 feet, the cohesion was on the order of 0.588 ksf, with a friction angle on the order of 29.51 degrees. Direct shear testing in Boring B2021-5 between 90 and 91.5 feet indicated a cohesion of 0.260 ksf, and a friction angle of 31.18 degrees.

In Boring B2021-3 between 25 and 27 feet, the triaxial shear testing indicated a cohesion of 0 ksf, and a friction angle of 25.86 degrees. Triaxial shear testing of the soil in Boring B2021-5 between 50 and 51.5 feet indicated a cohesion of 0.123 ksf, and a friction angle of 27.04 degrees.

### 6.2 Silt

Silt was encountered in Borings B2021-3 through B2021-7 at depths ranging in elevations from 2,784 to 2,490 feet. The silt classifications varied between silt and silt with sand. The silt and silt with sand layers varied in thickness between 1 and 28 feet.

Generally the silt was tan to gray and had low plasticity. Penetration resistance values in the silt ranged from 10 to greater than 50 blows per foot which indicates a potentially stiff to hard matrix soil stratum.

Laboratory testing performed on bulk and split spoon samples of the silt soils indicated natural moisture content of samples ranged from 4 to 29 percent at the time of drilling. Boring B2021-5 was sited to attempt to intersect the suspected fault in the area. In Boring B2021-5 at 70 feet, the liquid limits were on the order of 27 with a plastic index of 21 and a dry density of 112 pounds per cubic feet (pcf). The soils and soil matrix in this boring did not differ substantially from the other borings, and therefore there was not conclusive evidence to indicate the presence of a fault. In Boring 2021-8 at 100 feet the liquid limits were non plastic, and the dry density was 97 pcf.

In Boring the B2021-5 between 69 and 70 feet, the triaxial shear testing indicated a cohesion of 0.037 ksf, and a friction angle of 19.09 degrees (**Appendix C**).

### 6.3 Lean Clay

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Lean Clay and lean clay with sand was encountered in Borings B2021-5 through B2021-7, at depths ranging in elevations on the order of 2,615 to 2,456 feet. The clay layers varied between 1 foot and 54 feet thick. Penetration resistance values in the lean clay ranged from 45 to greater than 50 blows per foot which indicates a potentially hard to very hard soil stratum. The clay color was gray to tan to blue and had high plasticity.

Laboratory testing performed on bulk and split spoon samples of the clay soils indicated natural moisture content of samples ranged from 20 to 21 percent at the time of drilling. In Boring B2021-5 between 80 and 81.5 feet, the liquid limits were on the order of 35 with a plastic index of 14. In Boring 2021-6 at 106 feet the liquid limit was 47 with a plastic Index of 25, with a maximum dry density of 100.0 pcf and an optimum water content of 20.5 percent.

In Boring the B2021-7 between 120 and 121.3 feet, the triaxial shear testing indicated a cohesion of 0.053 ksf, and a friction angle of 18.02 degrees (**Appendix C**).

### 6.4 Silty Clay

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Silty clay was encountered in Borings B2021-4 through B2021-7, at elevations on the order of 2,774 to 2,510 feet. The layers of silty clay were not as prevalent as the other soil types and averaged in thicknesses between 2 and 15 feet.

Generally, the silt clay was tan to gray and has higher plasticity. Penetration resistance values in the silt ranged from 26 to greater than 50 blows per foot which indicates a potentially hard to very hard soil stratum.

Laboratory testing performed on Shelby, bulk and split spoon samples of the silt soils indicated natural moisture content of samples ranged from 16 to 24 percent at the time of drilling. In Boring B2021-5 at 50 feet, and in Boring B2021-7 at 120 feet, the consolidation testing indicated an under-consolidated soil in with pre-consolidation pressures of 4.8 and 1.5 ksf. Boring B2021-5 had a swell pressure of 2.8 percent.

In Boring B2021-5 between 50 and 51.5 feet the triaxial shear testing indicated a cohesion of 0.489 ksf, and a friction angle of 14.95 degrees (**Appendix C**).

Boring B2021-5 was sited to attempt to intersect the suspected fault in the area. The soils and soil matrix in this boring did not differ substantially from the other borings, and therefore there was not conclusive evidence to indicate the presence of a fault.

### 6.5 Fat Clay

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Silty clay was encountered in Boring B2021-6 from elevations 2,555 to 2,531 feet. The fat clay was very dark gray, had a high plasticity, and consolidated similar to claystone. It was identified in this single boring; however, may exist in surrounding areas. Penetration resistance values were greater than 50 blows per foot which indicates a potentially very hard soil stratum.

Laboratory testing performed on split spoon samples of the fat clay indicated liquid limits were on the order of 56 to 67 with a plastic index of 19 to 22. (**Appendix C**).

## 6.6 Groundwater

Groundwater was not encountered in any of the previous or more current borings drilled at this site. Based on the well data presented in previous reports, the natural groundwater elevation is assumed to be below the proposed excavation depths of up to 200 to 250 feet for the proposed landfill expansion. Numerous factors contribute to groundwater fluctuations, and evaluation of such factors is beyond the scope of this report.

# 7. ENGINEERING ANALYSIS AND RECOMMENDATIONS

## 7.1 Seismic Impact Zone Characterization

The seismic evaluation of the landfill was completed to comply with the Idaho Department of Environmental Quality's administration of municipal solid waste landfills. The Canyon County Landfill is located within a "seismic impact zone" as defined by the Administrative Rules for the for the Idaho Solid Waste Facilities Act (Idaho Statutes, Title 39 – Health and Safety, Chapter 74, Section 39-7407) that states:

*"A MSWLF unit shall not be located: ... (ii) within seismic impact zones except as provided in 40 CFR §258.14;"*

The United States Environmental Protection Agency (EPA) 40 CFR §258.14 defines a seismic impact zone as;

*"...an area with a ten percent or greater probability that the maximum horizontal acceleration... will exceed 0.10g in 250 years."*

The EPA requires that MSWLF units located within a seismic impact zone shall demonstrate that all landfill containment structures are designed to resist the maximum horizontal acceleration in lithified earth material for the site. Based on the United States Geological Survey (USGS) National Seismic Hazard Mapping application, the peak horizontal ground acceleration at the project site having a 10 percent probability of exceedance in any 250-year period is 0.12g, which exceeds the criteria above and therefore classifies or designates the site by rule definition to be within a seismic impact zone.

The results for the USGS National Seismic Hazard Mapping application were based on a risk category II, with the landfill as a moderate risk to human life determined based on the normal-day operations with human operators processing and covering the trash. The soil conditions were considered Site Class D for stiff soils with Standard penetration Resistance, N values, between 15 and 50.

Tetra Tech reviewed the most recent published USGS probabilistic earthquake hazard information for seismic events with a 10 percent probability of exceedance in a 250-year period (USGS 2008 NSHMP PSHA Interactive Deaggregation Web Application), as current state of practice warrants, to select a peak spectral horizontal acceleration (PSHA). Based on our review of the USGS probabilistic earthquake hazard information, including site specific deaggregation characteristics of the Maximum Credible Earthquake (MCE), including magnitude, distance, and probability, a PSHA of 0.23g was selected to represent the extreme seismic case.

Based on recommendations in the EPA's Seismic Design Guidance for Municipal Solid Waste Landfill Facilities (1995), the maximum horizontal acceleration was reduced by 50 percent to represent the average horizontal acceleration for the given slope. In this case, 50 percent of the maximum horizontal acceleration (0.23g) yields an average horizontal acceleration of 0.115g. An adjusted horizontal acceleration of 0.12g was applied for pseudo-static analysis of the modeled slope configurations. The above acceleration values were applied for pseudo-static analysis of the modeled slope configurations.

To model the proposed slope cuts an initial angle between 2.25H:1V to 2.75:H:1V was removed to the proposed base elevation and the factor of safety for slope stability was calculated. The slope angle was adjusted using iterations of the same process until a resulting factor of safety was established that was above the criteria of 1.5 for static, and 1.3 for pseudo-static. The proposed fill was then added into the cut section and iterations were used with varied slopes between 2.75H:1V and 3H:1V to achieve a long-term factor of safety as described.

## 7.2 Material Strength Properties

Tetra Tech previously completed a slope stability evaluation that included static and seismic stability evaluations for Phases 2 through 4 of the Canyon County Landfill (October 7, 2015). Additionally, Tetra Tech reviewed the previous evaluations from Holladay Engineering Company for the Pickles Butte Sanitary Landfill, dated 1998.

For this stability evaluation, Tetra Tech incorporated the following information: 1) the soils strength data available from the previous analysis, 2) materials strength properties assigned based on the laboratory testing of the geotechnical samples collected in 2021 and correlated data from the SPT N-value (blow count) data collected during the geotechnical drilling and well installation.

As discussed in the laboratory testing section, Tetra Tech's senior geotechnical engineer specifically selected samples for testing in each boring to directly incorporate into the slope stability models at each cross-section location. An attempt was also made to provide duplicate or crossover testing to identify variations in strength parameters for similar soil types. Several different tests were also performed to obtain a range of soil strength properties for each soil type. **Tables 2 and 3** presents a detailed breakdown of some of the data utilized to analyze the cross sections.

Conservative (lower bound) shear strength values were used to evaluate slope stability for static and seismic conditions. The following **Tables 2 and 3** present the material values that were assumed for this analysis.

**Table 2. Material Strength Properties - Soil**

Material	ASTM Classification	Unit Weight (pcf)	Friction Angle (deg)	Cohesion (psf)
Waste Fill		75	28	300
Poorly-Graded Silty Sand	SP-SM	110	20	280
Poorly-Graded Silty Sand	SP-SM	110	27	123
Silt (B,C)	ML	110	19	37
Silt (D,E)	ML	110	0	908
Lean Clay	CL	130	14	2000
Lean Clay-Silty Clay	CL-ML	109	15	489
Clay (Hard)	CL	125	0	6211
Clay (Hard)	CL	125	10	7831
Silty Sand - B3	SP-SM	115	32	400
Silty Sand - _B4	SP-SM	115	30	580
Sand B3	SP	110	36.2	0
Sand/Gravel Interbedded	GW	135	37	0
Clayey Gravel	GW	138	36	1

**Table 3. Material Strength Properties - Rock**

Generalized Hoek-Brown Material	UCS (ksf)	GSI	mi	Unit Weight (pcf)
Basalt	3,500	30	25	146
Claystone	7,000	10	4	135

### 7.3 Slope Stability Analyses

Slope stability and pseudo-static analyses were performed using the computer program Slide2 v.9.023, developed by Rocscience, Inc., to determine the factors of safety of critical slip surfaces using both circular and block failure searches and vertical slice limit equilibrium methods. Because the proposed expansion of the landfill would be unlined, the potential of a critical interface between the waste fill and the natural subgrade soil is low. Therefore, circular failure analyses were performed at the critical sections. A screening analysis for block failure was performed to verify the potential for failure along the waste-soil interface is low compared to circular failure through the waste fill.

The EPA recommends a minimum FS of 1.5 for static slope stability analysis and a FS of 1.3 for pseudo-static slope stability analysis, based on Table 2-4 of the EPA's Solid Waste Disposal Facility Criteria Technical Manual (1998). For temporary cut slopes, a minimum FS of 1.2 is typically considered acceptable. Tetra Tech did not analyze temporary slopes given that it is anticipated that most all of the cut slopes will be open for a minimum of 6 months to 1 year, which per geotechnical standard of practice, are considered permanent slopes for purposes of slope analyses. Higher values for the FS indicate that the design is less likely to fail.

The cross-sections were created in the areas with the highest proposed cut and fill slopes where the critical soil slope conditions were identified, and in the areas incorporating the existing landfill with the proposed additional cells. There are seven section profile views, A through G, shown on Figures 2D to 5D, and included in **Appendix D**. A summary of the slope stability analysis results are presented in **Table 4** below and the corresponding output plots are Figures 6D through 37D in **Appendix D**.

**Table 4. Factors of Safety for Slope Stability Analyses**

Section	Analyzed Slope Long term	Factor of Safety			
		Static Analysis, Circular Failure	Pseudo-Static Analysis, Circular Failure	Static Analysis, Block Failure	Pseudo-Static Analysis, Block Failure
A	3H:1V	2.3	1.53	2.85	2.02
A – Final Slope Configuration	2.75H:1V	1.73	1.28	-	-
	3H:1V	1.94	1.40	2.21	1.68
B	2.27H:1V	2.43	1.88	2.52	2.00
C	2.85H:1V	1.85	1.35	2.16	1.63
D	2.87H:1V	1.93	1.37	3.11	2.33
E	2.27H:1V	1.96	1.51	-	-
E	1.87H:1V	1.66	1.34	1.77	1.45
F	3H:1V	1.38	0.99	-	-
F- 2 Tier	3H:1V on lower, and 4H:1V on upper	1.81	1.19	2.14	1.53
F	4H:1V	2.06	1.35	1.83	1.69
G	2.6H:1V	2.22	1.68	2.65	2.16

The analysis as represented above indicates FS values for the static determinate loading on the order of 1.38 to 2.43, and 1.83 to 3.11 for circular and block failure, respectively. The seismic FS values were on the order of 0.99 to 1.88, and 1.45 to 2.16 for circular and block failure, respectively. The silty soils within the proposed cut in Section F produced a FS below 1 for the seismic loading condition. The slope was modeled with 4H:1V slope cut and a FS of 1.35 was obtained which met the minimum requirements of 1.3. Various degrees of slope cuts were modeled in an iterative manner to define the most effective slope cut for the soil conditions. The final slope

configuration was modeled on Section A and was representative of the backfill method and slope for the remaining project area. An iterative process was used to define which slope complied with the required factor of safety criteria of 1.5 for static stability and 1.3 for pseudo-static stability.

## 7.4 Pseudo-static

When the pseudo-static analysis indicates a factor of safety of equal to or less than 1.3, the containment structure is required to be evaluated utilizing at least two independent methods to estimate permanent seismic induced displacement of the refuse mass. The displacement analysis methods are typically used as a screening method to evaluate if the structure or slope under analysis is within the range of critical displacement. For design of municipal solid waste landfill facilities, a maximum displacement less than 0.5 to 1.2 inches (1 to 3 cm) is typically acceptable for design. Where the pseudo-static analysis indicated a factor of safety of equal to or less than 1.3, the containment structure was evaluated using the Newmark displacement analysis method to determine a range of seismic-induced deformation. There was one cross-section, Section F, where the pseudo-static analyses indicated a factor of safety below 1.3. Yield accelerations were performed using Slide2 and are provided in the **Table 5** below.

The Slide2 program calculates the Newmark displacement based on the program SLAMMER (2013), developed by the USGS. The Slide2 program allows the user to enter a seismic record directly (time and acceleration data) or choose from a database of available historical seismic records. For the seismic analysis, a historical earthquake record was selected based on comparison to the design seismic event stated above. The earthquake record selected was the Mammoth Lakes – 1 1980, CVK-090 record, with a magnitude of 6.1 and Peak Ground Acceleration (PGA) of 0.416g, and represents an average high magnitude earthquake in similar soil conditions.

The performance of landfills subjected to strong earthquake ground motions is an extremely complicated process for which all of the variables affecting the behavior are not yet fully understood or capable of being analyzed. The historical performance of landfills subjected to seismic events similar to the design earthquake generally indicates satisfactory performance for the landfills studied.

For Section F, a conceptual slope was evaluated based on the methods above. Two different slope angles were analyzed, 3H:1V (20.8- degrees) and 4H:1V (14-degrees) with the 0.12g peak ground acceleration and the section F geometry. A summary of the analyses results is presented in **Table 5** and the corresponding output plots (Figures 1E through 12E) are included in **Appendix E**.

**Table 5. Section F Stability Analysis Results for Displacement**

Slope 3H:1V	Static Analysis		Pseudo-static Analysis	
	Circular Failure	Block Failure	Circular Failure	Block Failure
Factor of Safety	1.38	1.90	0.99	1.41
Yield Acceleration (%g)	-	-	-	0.12
Estimated Displacement (in)	-	-	-	3.19
Slope 4H:1V				
Factor of Safety	2.06	2.49	1.35	1.69
Yield Acceleration (%g)	-	-	-	0.23
Estimated Displacement (in)	-	-	-	0.25

## 7.5 Comprehensive Seismic Survey for Fault identification

Tetra Tech prepared a 3D Seismic Survey report dated February 21, 2022. The project site is located within the Western Snake River Plain (WSRP) fault system and a portion of an undifferentiated Quaternary aged northeast-dipping WSRP normal fault is mapped within the project boundaries, extending northwest through the proposed expansion area. The mapped fault is labeled as a normal fault with an approximate slip rate of less than 0.2



mm/year. Proposed excavations within the fault areas are expected to extend up to 150 feet below ground surface, potentially intercepting this fault.

The report prepared by Tetra Tech presented the results from an active-source 3D seismic survey. The seismic survey was designed to image and delineate the suspected fault. Seismic imaging over the suspected fault area was attained by using 3D seismic velocity tomography and reflection processing. Seismic reflection is a reliable method for imaging faults when present and can help to orient the faults and subsurface structure. The 3D seismic tomography provides the information needed to accurately convert seismic reflection data in time to depth and elevation. The information gained from this survey was used to site the location of Boring B5 to aid in the evaluation of the fault.

The summary of the seismic investigation and report were as follows:

- 1) The USGS NW-striking NE-dipping WSRP normal fault that is mapped as extending into the project site from the northwest does not appear to displace ~100ka age sedimentary units.
- 2) From a probabilistic perspective there seems to be little possibility of significant shallow (< 200 feet) faulting within the project site southeast of the west edges of the mapped tip splay faults.
- 3) To best characterize the potential movement and absolute location of faulting would require geologic mapping during excavation of the future landfill cell. This area of the proposed landfill expansion would be constructed in >50 years in the future. When the area is excavated for cover material in the future before waste is placed in this area it is recommended that geologic mapping of the fault is conducted, with particular attention to identifying narrow fault zones with evidence of recent activity and areas of potential materials suitable to date the most recent age of fault activity to determine if any detected fault activity is recent (unlikely) or > 100 ka in age (most likely).

Tetra Tech's slope evaluation recommendations presented in **Section 7.3** are not affected or altered by the results of the results of the February Seismic Survey Report. We suggest that a geotechnical engineer observe the slope cuts in the future to determine the potential presence of a faulted area. Should a faulted area be identified, the geotechnical engineer should determine at that time whether further investigation or analysis is required for the specific cells in the suspect fault area.

## 7.6 Conclusions and Recommendations

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The material strength properties incorporated in the geotechnical analyses were based on lower bound shear strength values and are considered conservative estimates. The stability analyses performed are considered to be the worst-case slope configurations with conservative material strengths and resulted in the factors of safety and displacements indicated above.

Results of the geotechnical investigation and analyses indicate that the proposed excavation and design as shown on Figure 1D in **Appendix D** will meet the Factor of Safety requirements of the Idaho Administrative Rules for the Idaho Solid Waste Facilities Act for the Idaho DEQ's administration of MSWLF.

Multiple slope angles were considered for Tetra Tech's slope analyses, ranging from 2.5:1 to 4:1 depending on the soil and bedrock types at each location. Based on Tetra Tech's analysis and the required FS's, the following two slope angles are recommended for the preliminary landfill site grading plans:

3H:1V: for the majority of the site slopes

4H:1V: where silt is encountered (Section F)

The 4:1 slope was analyzed and recommended for Section F because silt was interbedded between poorly-graded sand and fine sand and created a weakened soil profile. In areas where a high concentration of silt is predominant during construction, a slope of 4H:1V is recommended for cut areas. For now, Section F is the only area identified as having a high concentration of silt.

If it can be confirmed that bedrock exists for the entire depth of cut during construction, a 2:1 slope may be utilized. However, if there are any soft silt or clay seams interbedded withing the bedrock layer at any location along the

cut, a 3:1 slope must be used. If slope angles are proposed to be steepened to a 2:1 slope during construction, a licensed geotechnical engineer from Tetra Tech must observe and evaluate the slope prior to make the determination if the slopes can be steepened, otherwise the slope must remain at 3:1.

In general, the seismic displacement analyses indicate permanent seismic-induced displacements are within the tolerances of 6 to 12 inches (15 to 30 cm) that are typically considered acceptable for landfill design. The preliminary seismic evaluation presented above was performed in accordance with generally accepted standards of the geotechnical engineering profession.

Because it is anticipated that most all of the cut slopes will be exposed for a minimum of 6 months to 1 year, Tetra Tech analyzed all slopes as permanent, and did not consider reducing the factor of safety for temporary slopes.

Some states specify the maximum allowable steepness of landfill cut or fill slopes, sometimes also based on the height of the slopes. In Pennsylvania for example, the maximum allowable slope steepness is 3:1. Other states have varying specifications or slope steepness limits for short term or longer-term slope exposures. The requirements are based both on historical slope failure data and slope analysis data, along with added factors of safety. Therefore, states have somewhat calibrated requirements based on the soil types and rainfall. The 3:1 maximum slope steepness for Pennsylvania landfills matches that determined for this investigation.

## 8. CONTINUING SERVICES

Two additional elements of geotechnical engineering service are important to the successful completion of this project.

- 1) **Design Phase.** During the design phase, it is essential to ensure that the intent of the recommendations is incorporated in design decisions related to the project and that changes in the design concept consider geotechnical aspects. If issues arise, Tetra Tech's geotechnical engineers should be consulted for clarification and additional analysis on an as needed basis.
- 2) **Observation and monitoring during construction.** PBSL Operations should be trained to observe the types of materials encountered during the earthwork phases of the project, including the site grading and landfill cell excavations, to determine that the subsurface conditions are compatible with those used in the analysis and design. If conditions change, a geotechnical engineer should be consulted to evaluate the stability or potential impact on the design. During site grading, placement of fill should be observed and tested to confirm that the proper compaction has been achieved. PBSL should continue the annual aerial evaluation of the site and performance analysis to verify that the compaction remains consistent.

## 9. LIMITATIONS

The subsurface conditions and recommendations presented in this document are based on conditions encountered at the boring locations and based on the laboratory analysis. Due to the complexity and variability of natural earth and rock formations and materials, significant variations may occur between and around these locations or with time. Because these data represent a very small statistical sampling of subsurface conditions, it is possible that conditions may be encountered that are substantially different from those indicated. In these instances, modification and adjustment to the recommendations presented may be warranted.

This study has been conducted in accordance with generally accepted geotechnical engineering practices in the region where the work was conducted. The conclusions and recommendations submitted in this report are based upon project information collected and provided to Tetra Tech. The nature and extent of subsurface variations across the site may not become evident until construction. Tetra Tech should be on site during construction, to verify that actual subsurface conditions are consistent with those described herein.

This report has been prepared exclusively for the client. This report and the data included herein shall not be used by any third party without the express written consent of both the client and Tetra Tech. Tetra Tech is not responsible for technical interpretations by others. As the project evolves, Tetra Tech or another qualified geotechnical engineer should provide continued consultation and field services during construction to review and monitor the implementation of the recommendations and verify that the recommendations have been appropriately interpreted. Significant design changes may require additional analysis or modifications of the recommendations presented herein. On-site observation of excavations and foundation bearing strata and testing of fill should be performed by a representative of the geotechnical engineer.

## 10. REFERENCES

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## **APPENDIX A: MISCELLANEOUS FIGURES AND DETAILS**

**Important Information About Your Geotechnical Engineering Report (Published by ASFE)**

**Tetra Tech Boring Log Descriptive Terminology Key to Soil and Rock Symbols and Descriptive Terms**

**Classification of Soils for Engineering Purposes**

**Tetra Tech Exploratory Boring Locations – Figure 1040-1**

## **APPENDIX B: LOGS OF EXPLORATORY BORINGS**

**Figures 1-B through 16-B**

## **APPENDIX C: LABORATORY TESTING**

**Summary of Laboratory Results - Table 1-C**

**Sieve Analysis Results**

**Moisture Density Relationship Results**

**Consolidation Tests**

**Unconfined Compressive Strength Results**

**Triaxial Tests**

## **APPENDIX D: SLOPE ANALYSIS**

**Figures 1D through 43D**



## APPENDIX E: DEFORMATION ANALYSIS

Figures 1E through 12E

**Static and Pseudo-Static Slope Stability Analyses with Associated Circular and Block Failure Factor of Safety, Newmark Displacement, and Critical Acceleration for Slope 3H:1V  
Figures 1E through 6E**

**Static and Pseudo-Static Slope Stability Analyses with Associated Circular and Block Failure Factor of Safety, Newmark Displacement, and Critical Acceleration for Slope 4H:1V  
Figures 7E through 12E**

## **APPENDIX F: PREVIOUS BORING LOGS**

**Logs GT-1 through GT-8**

**Logs PB-5 through PB-15**

## **APPENDIX A: Miscellaneous Figures and Details**

Important Information about Your Geotechnical Engineering Report (Published by ASFE/GBA)

Tetra Tech Boring Log Descriptive Terminology Key to Soil and Rock Symbols and Terms

Classification of Soils for Engineering Purposes

Figure No. 2001-1 – Location of Exploratory Borings

# IMPORTANT INFORMATION

## ABOUT YOUR

### GEOTECHNICAL ENGINEERING REPORT

More construction problems are caused by site subsurface conditions than any other factor. As troublesome as subsurface problems can be, their frequency and extent have been lessened considerably in recent years, due in large measure to programs and publications of ASFE/The Association of Engineering Firms Practicing in the Geosciences.

The following suggestions and observations are offered to help you reduce the Geotechnical-related delays, cost-overruns and other costly headaches that can occur during a construction project.

#### **A GEOTECHNICAL ENGINEERING REPORT IS BASED ON A UNIQUE SET OF PROJECT-SPECIFIC FACTORS**

A Geotechnical engineering report is based on a subsurface exploration plan designed to incorporate a unique set of project-specific factors. These typically include: the general nature of the structure involved, its size and configuration; the location of the structure on the site and its orientation; physical concomitants such as access roads, parking lots, and underground utilities, and the level of additional risk which the client assumed by virtue of limitations imposed upon the exploratory program. To help avoid costly problems, consult the geotechnical engineer to determine how any factors which change subsequent to the date of the report may affect its recommendations.

Unless your consulting Geotechnical engineer indicates otherwise, *your Geotechnical engineer report should not be used:*

- When the nature of the proposed structure is changed, for example, if an office building will be erected instead of a parking garage, or if a refrigerated warehouse will be built instead of an unrefrigerated one;
- when the size or configuration of the proposed structure is altered;
- when the location or orientation of the proposed structure is modified;
- when there is a change of ownership, or
- for application to an adjacent site.

*Geotechnical engineers cannot accept responsibility for problems which may develop if they are not consulted after factors considered in their reports' development have changed.*

#### **MOST GEOTECHNICAL "FINDINGS" ARE PROFESSIONAL ESTIMATES**

Site exploration identifies actual subsurface conditions only at those points where samples are taken, when they are taken.

Data derived through sampling and subsequent laboratory testing are extrapolated by Geotechnical engineers who then render an opinion about overall subsurface conditions, their likely reaction to proposed conditions, their likely reaction to proposed construction activity, and appropriate foundation design. Even under optimal circumstances actual conditions may differ from those inferred to exist, because no Geotechnical engineer, no matter how qualified, and not subsurface exploration program, no matter how comprehensive, can reveal what is hidden by earth, rock and time. The actual interface between materials may be far more gradual or abrupt than a report indicates. Actual conditions in areas not sampled may differ from predictions. *Nothing can be done to prevent the unanticipated, but steps can be taken to help minimize their impact.* For this reason, *most experienced owners retain their Geotechnical consultants through the construction stage, to identify variances, conduct additional tests which may be needed, and to recommend solutions to problems encountered on site.*

#### **SUBSURFACE CONDITIONS CAN CHANGE**

Subsurface conditions may be modified by constantly-changing natural forces. Because a Geotechnical engineering report is based on conditions which existed at the time of subsurface exploration, *construction decisions should not be based on a Geotechnical engineering report whose adequacy may have been affected by time.* Speak with the Geotechnical consultant to learn if additional tests are advisable before construction starts.

Construction operations at or adjacent to the site and natural events such as flood, earthquakes or groundwater fluctuations may also affect subsurface conditions and, thus, the continuing adequacy of a geotechnical report. The geotechnical engineer should be kept apprised of any such events, and should be consulted to determine if additional tests are necessary.

#### **GEOTECHNICAL SERVICES ARE PERFORMED FOR SPECIFIC PURPOSES AND PERSONS**

Geotechnical engineers' reports are prepared to meet the specific needs of specific individuals. A report prepared for a consulting civil engineer may not be adequate for a construction contractor, or even some other consulting civil engineer. Unless indicated otherwise, this report was prepared expressly for the client involved and expressly for purposes indicated by the client. Use by any other persons for any purpose, or by the client for a different purpose, may result in problems. *No individual other than the client should apply this report for its intended purpose without first conferring with the*

*geotechnical engineer. No person should apply this report for any purpose other than that originally contemplated without first conferring with the geotechnical engineer.*

## **A GEOTECHNICAL ENGINEERING REPORT IS SUBJECT TO MISINTERPRETATION**

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a geotechnical engineering report. To help avoid these problems, the geotechnical engineer should be retained to work with other appropriate design professionals to explain relevant geotechnical findings and to review the adequacy of their plans and specifications relative to geotechnical issues.

## **BORING LOGS SHOULD NOT BE SEPARATED FROM THE ENGINEERING REPORT**

Final boring logs are developed by geotechnical engineers based upon their interpretation of field logs (assembled by site personnel) and laboratory evaluation of field samples. Only final boring logs customarily are included in geotechnical engineering reports. *These logs should not under any circumstances be redrawn* for inclusion in architectural or other design drawings, because drafters may commit errors or omissions in the transfer process. Although photographic reproduction eliminates this problem, it does nothing to minimize the possibility of contractors misinterpreting the logs during bid preparation. When this occurs, delays, disputes and unanticipated costs are the all-too-frequent result.

To minimize the likelihood of boring log misinterpretation, *give contractors ready access to the complete geotechnical engineering report* prepared or authorized for their use. Those

who do not provide such access may proceed under the *mistaken* impression that simply disclaiming responsibility for the accuracy of subsurface information always insulates them from attendant liability. Providing the best available information to contractors helps prevent costly construction problems and the adversarial attitudes which aggravate them to disproportionate scale.

## **READ RESPONSIBILITY CLAUSES CLOSELY**

Because geotechnical engineering is based extensively on judgment and opinion, it is far less exact than other design disciplines. This situation has resulted in wholly unwarranted claims being lodged against geotechnical consultants. To help prevent this problem, geotechnical engineers have developed model clauses for use in written transmittals. These are *not* exculpatory clauses designed to foist geotechnical engineers' liabilities onto someone else. Rather, they are definitive clauses which identify where geotechnical engineers' responsibilities begin and end. Their use helps all parties involved recognize their individual responsibilities and take appropriate action. Some of these definitive clauses are likely to appear in your geotechnical engineering report, and you are encouraged to read them closely. your geotechnical engineer will be pleased to give full and frank answers to your questions.

## **OTHER STEPS YOU CAN TAKE TO REDUCE RISK**

Your consulting geotechnical engineer will be pleased to discuss other techniques which can be employed to mitigate risk. In addition, ASFE as developed a variety of materials which may be beneficial. Contact ASFE for a complimentary copy of its publications directory.

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# Tetra Tech Boring Log Descriptive Terminology

## Key to Soil Symbols and Terms

12/06/12



### SOIL CLASSIFICATION CHART

MAJOR DIVISIONS			SYMBOLS		TYPICAL DESCRIPTIONS
			GRAPH	LETTER	
COARSE GRAINED SOILS	GRAVEL AND GRAVELLY SOILS	CLEAN GRAVELS (LITTLE OR NO FINES)		GW	Well-graded gravels, gravel sand mixtures, little or no fines.
		GRAVELS WITH FINES		GP	Poorly graded gravels, gravel-sand mixtures, little or no fines.
		MORE THAN 50% OF COARSE FRACTION RETAINED ON NO. 4 SIEVE GRAVELS WITH FINES (APPRECIABLE AMOUNT OF FINES)		GM	Silty gravels, gravel-sand-silt mixtures.
	SAND AND SANDY SOILS	CLEAN SANDS (LITTLE OR NO FINES)		SW	Well-graded sands, gravelly sands, little or no fines.
		MORE THAN 50% OF COARSE FRACTION PASSING ON NO. 4 SIEVE SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES)		SM	Silty sands, sand-silt mixtures.
		SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES)		SC	Clayey sands, sand-clay mixtures.
FINE GRAINED SOILS	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity.
				CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.
				OL	Organic silts and organic silty clays of low plasticity.
	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts.
				CH	Inorganic clays of high plasticity, fat clays.
				OH	Organic clays of medium to high plasticity, organic silts.
HIGHLY ORGANIC SOILS				PT	Peat and other highly organic soils.

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS

#### Notes

See Soil Boring Information Special Provision.

SPT (Standard Penetration Test-ASTM D1586):

The number of blows of a 140 lb (63.6 kg) hammer falling 2.5 ft (750 mm) used to drive a 2 in (50 mm)

O.D. Split Spoon sampler for a total of 1.5 ft (0.45 m) of penetration.

Written as follows:

first 0.5 ft (0.15 m) - second 0.5 ft (0.15 m) - third 0.5 ft (0.15 m)

(ex: 1-3-9)

Note: if the number of blows exceeds 50 before 0.5 ft (0.15 m) of penetration is achieved, the actual penetration rounded to the nearest 0.1 ft (0.03 m) follows the number of blows in parentheses (ex: 12-24-50 (0.09 m), 34-50 (0.4 ft), or 100 (0.3 ft)). WR denotes a zero blow count with the weight of the rods only.

WH denotes a zero blow count with the weight of the rods plus the weight of the hammer.

MC=Moisture Content, LL=Liquid limit, PL=Plastic Limit  
-200%=percent soil passing 200 sieve, DD=Dry Density

Soil Classifications are Based on the Unified Soil Classification System, ASTM D2487 and D2488. Also included are the AASHTO group classifications (M145). Descriptions are based on visual observation, except where they have been modified to reflect results of laboratory tests as deemed appropriate.

Example soil description: Sandy FAT CLAY (CH), soft, wet, brown. (A-7)

#### Order of Descriptors

- Group Name
- Consistency or Relative Density
- Moisture Condition
- Color
- Particle size descriptor(s) (coarse grained soils only)
- Angularity of coarse grained soils
- Other relevant notes

#### Criteria For Descriptors

##### Consistency of Fine Grained Soils

Consistency	N-Value (uncorrected)
Very Soft	< 2
Soft	2 - 4
Medium Stiff	5 - 8
Stiff	9 - 15
Very Stiff	16 - 30
Hard	> 30

##### Apparent Density of Coarse Grained Soils

Relative Density	N-Value (uncorrected)
Very Loose	< 4
Loose	4 - 10
Medium Dense	11 - 30
Dense	31 - 50
Very Dense	> 50

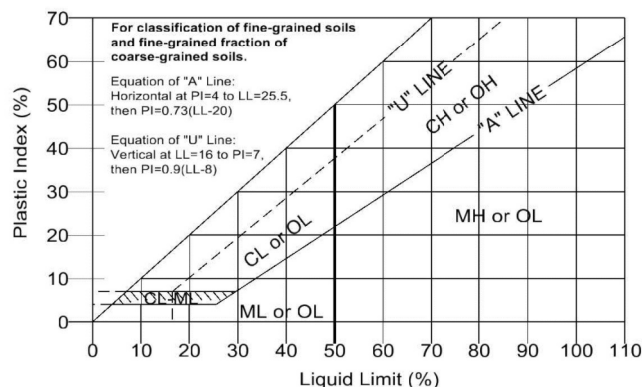
#### Moisture Condition

- Dry -Absence of moisture, dusty, dry to the touch.
- Moist -Damp, but no visible water.
- Wet -Visible free water.

#### Definition of Particle Size Ranges

Soil Component	Size Range
Boulder	> 12 in (300 mm)
Cobble	3 in (75 mm) - 12 in (300 mm)
Gravel	No. 4 Sieve (4.75 mm) to 3 in (75 mm)
Sand	No. 200 (0.075 mm) to No. 4 Sieves (4.75 mm)
Silt	< No. 200 Sieve (0.075 mm)*
Clay	< No. 200 Sieve (0.075 mm)*

\*Atterberg limits and chart below to differentiate between silt and clay.



#### Angularity of Coarse-Grained Particles

- Angular -Particles have sharp edges and relative plane sides with unpolished surfaces.
- Subangular -Particles are similar to angular description, but have rounded edges.
- Subrounded-Particles have nearly plane sides, but have no edges.
- Rounded -Particles have smoothly curved sides and well-rounded corners and edges.

# Tetra Tech Boring Log Descriptive Terminology

## Key to Rock Symbols and Terms

12/06/12



Rock Type	Symbol	Rock Type	Symbol	Rock Type	Symbol
Argillite		Dolomite		Quartzite	
Basalt		Gneiss		Rhyolite	
Bedrock (other)		Granitic		Sandstone	
Breccia		Limestone		Schist	
Claystone		Siltstone		Shale	
		Conglomerate			

### Order of Descriptors

- Rock Type
- Color
- Grain size (if applicable)
- Stratification/Foliation (as applicable)
- Field Hardness
- Other relevant notes

### Criteria For Descriptors

*Grain Size*

Description	Characteristic
Coarse Grained	-Individual grains can be easily distinguished by eye
Fine Grained	-Individual grains can be distinguished with difficulty

### Stratum Thickness

Thickly Bedded	3-10 ft (1-3 m)
Medium Bedded	1-3 ft (300 mm - 1 m)
Thinly Bedded	2-12 in (50-300 mm)
Very Thinly Bedded	< 2 in (50 mm)

### Rock Field Hardness

Very Soft	-Can be carved with knife. Can be excavated readily with point of rock hammer. Can be scratched readily by fingernail.
Soft	-Can be grooved or gouged readily by knife or point of rock hammer. Can be excavated in fragments from chips to several inches in size by moderate blows of the point of a rock hammer.
Medium	-Can be grooved or gouged 0.05 in (2 mm) deep by firm pressure of knife or rock hammer point. Can be excavated in small chips to pieces about 1 in (25 mm) maximum size by hard blows of the point of a rock hammer.
Moderately hard	-Can be scratched with knife or pick. Gouges or grooves to 0.25 in (6 mm) can be excavated by hard blow of rock hammer. Hand specimen can be detached by moderate blows.
Hard	-Can be scratched with knife or pick only with difficulty. Hard hammer blows required to detach hand specimen.
Very Hard	-Cannot be scratched with knife or sharp rock hammer point. Breaking of hand specimens requires several hard blows of a rock hammer.

### Notes:

UCS = Unconfined Compressive Strength obtained from laboratory testing at the given depth.

**See Soil Boring Information Special Provision.**

## Miscellaneous Soil/Rock Symbols and Terms

	Concrete
	Asphalt
	Water
	Boulders and Cobbles
	Coal
	Fill
	Millings
	Topsoil

### Explanation of Text Fields In Boring Logs:

Material Description: Lithologic Description of soil or rock encountered.

Remarks: Comments on drilling, including method, bit type, and problems encountered.  
Unless stated on logs as being surveyed by district survey, all locations are considered approximate.

### General Notes

- Descriptions on these boring logs apply only at the specific boring, and at the time the borings were made. These logs are not warranted to be representative of subsurface conditions at other locations or times.
- Water level observations apply only at the specific boring, and at the time the borings were made. Due to the variability of groundwater measurements given the type of drilling used, and the stratification of the soil in the boring, these logs are not warranted to be representative of groundwater conditions at other locations or times.
- Other terms may be used as descriptors, as defined by the profession.

### Operation Types:

	Auger
	Casing Advancer
	Core Barrel
	Drive Casing

### Sample Types:

	Split Spoon
	Shelby
	Bulk Sample
	Grab Sample
	Cone Penetrometer
	Vane Shear
	Special Samplers
	Testpit

**-Soil and Rock descriptions are based on visual observation, except where they have been modified to reflect results of laboratory tests as deemed appropriate.**

### Example Rock Log

*SANDSTONE, gray, fine grained, thickly bedded, hard field hardness.*



# CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES

ASTM Designation: D 2487 – 83  
(Based on Unified Soil Classification System)

MAJOR DIVISIONS		GROUP SYMBOL	GROUP NAME		
Coarse-Grained Soils More than 50% retained on No. 200 sieve	Gravels More than 50% coarse fraction retained on No. 4 sieve	Clean Gravels Less than 5% fines $Cu \geq 4$ and $1 \leq Cc \leq 3^E$	GW Well graded gravel <sup>F</sup>		
		$Cu < 4$ and/or $1 > Cc > 3^E$	GP Poorly graded gravel <sup>F</sup>		
		Gravels with Fines More than 12% fines Fines classify as ML or MH	GM Silty gravel <sup>F GH</sup>		
		Fines classify as CL or CH	GC Clayey gravel <sup>F GH</sup>		
	Sands 50% or more of coarse fraction passes No. 4 sieve	Clean Sands Less than 5% fines $Cu \geq 6$ and $1 \leq Cc \leq 3^E$	SW Well-graded sand <sup>I</sup>		
		$Cu < 6$ and/or $1 > Cc > 3^E$	SP Poorly graded sand <sup>I</sup>		
		Sands with Fines More than 12% fines Fines classify as ML or MH	SM Silty Sand <sup>G HI</sup>		
		Fines classify as CL or CH	SC Clayey sand <sup>G HI</sup>		
		Fine-Grained Soils 50% or more passes the No. 200 sieve	Silts and Clays Liquid limit less than 50	Inorganic PI > 7 and plots on or above "A" line	CL Lean clay <sup>K LM</sup>
				Inorganic PI < 4 or plots below "A" line	ML Silt <sup>K LM</sup>
Silts and Clays Liquid limit 50 or more	Organic $\frac{\text{Liquid limit} - \text{oven dried}}{\text{Liquid limit} - \text{not dried}} < 0.75$		OL Organic clay <sup>K LMN</sup> Organic silt <sup>K LMO</sup>		
	Inorganic PI plots on or above "A" line		CH Fat clay <sup>K LM</sup>		
	Inorganic PI plots below "A" line		MH Elastic silt <sup>K LM</sup>		
	Organic $\frac{\text{Liquid limit} - \text{oven dried}}{\text{Liquid limit} - \text{not dried}} < 0.75$		OH Organic clay <sup>K LMO</sup> Organic silt <sup>K LMO</sup>		
Highly organic soils	Primarily organic matter, dark in color, and organic odor	PT	Peat		

<sup>A</sup> Based on the material passing the 3-in. (75-mm) sieve.

<sup>B</sup> If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.

<sup>C</sup> Gravels with 5 to 12% require dual symbols:  
GW-GM well-graded gravel with silt  
GW-GC well-graded gravel with clay  
GP-GM poorly graded gravel with silt  
GP-GC poorly graded gravel with clay

<sup>D</sup> Sands with 5 to 12% fines require dual symbols:  
SW-SM well-graded sand with silt  
SW-SC well-graded sand with clay  
SP-SM poorly graded sand with silt  
SP-SC poorly graded sand with clay

<sup>E</sup>  $Cu = D_{60}/D_{10}$   $Cc = (D_{30})^2 / (D_{10} \times D_{60})$

<sup>F</sup> If soil contains  $\geq 15\%$  sand, add "with sand" to group name.

<sup>G</sup> If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.

<sup>H</sup> If fines are organic, add "with organic fines" to group name.

<sup>I</sup> If soil contains  $\geq 15\%$  gravel, add "with gravel" to group name.  
If soil contains  $\geq 15\%$  gravel, add "with gravel" to group name.

<sup>J</sup> If Atterberg limits plot in hatched area, soil is a CL-ML, silty clay.

<sup>K</sup> If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel", whichever is predominant.

<sup>L</sup> If solid contains  $\geq 30\%$  plus No. 200, predominantly sand, add "sandy" to group name.

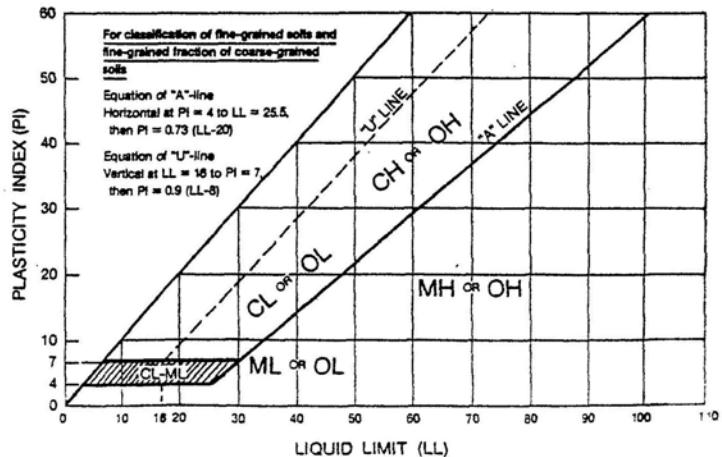
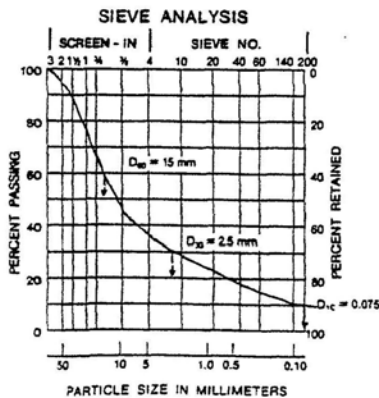
<sup>M</sup> If soil contains  $\geq 30\%$  plus No. 200, predominantly gravel, add "gravelly" to group name.

<sup>N</sup> PI  $\geq 4$  and plots on or above "A" line.

<sup>O</sup> PI < 4 or plots below "A" line.

<sup>P</sup> PI plots on or above "A" line.

<sup>Q</sup> PI plots below "A" line.



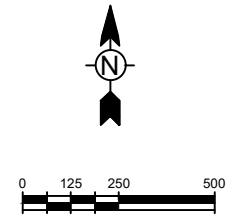
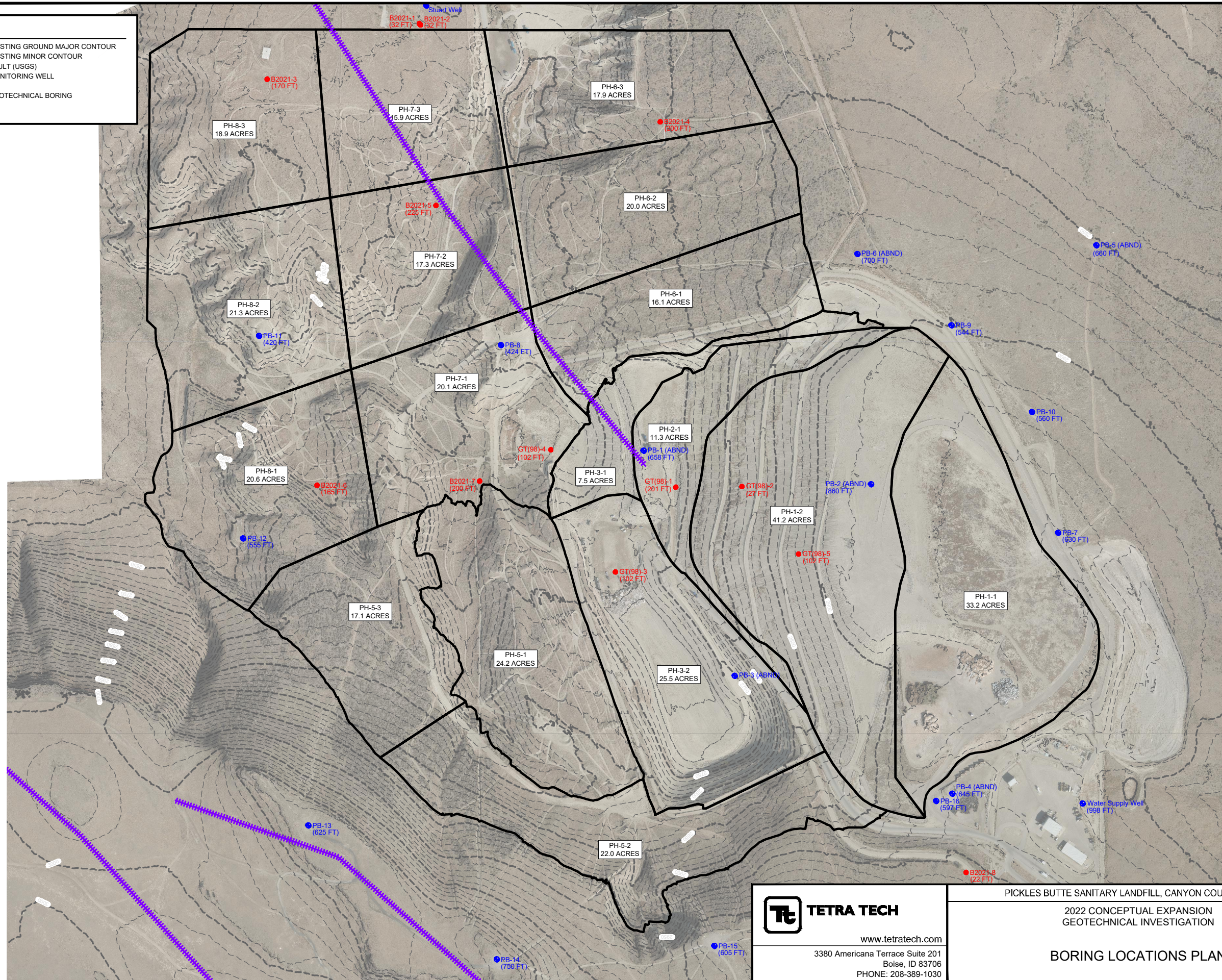
$$C_u = \frac{D_{60}}{D_{10}} = \frac{15}{0.075} = 200 \quad C_c = \frac{(D_{30})^2}{D_{12} \times 10_{36}} + \frac{(2.5)}{0.075 \times 15} = 5.6$$




8/1/2022 3:05 PM - O:\T-Z\TTMISSOULA\114-57\1040-PICKLES BUTTE LANDFILL\07-CAD\SHEETFILES\GEOTECH\1040-1 BORING LOCATIONS.DWG

**LEGEND**

- EXISTING GROUND MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- ||||| FAULT (USGS)
- ID NO. (DEPTH) MONITORING WELL
- ID NO. (DEPTH) GEOTECHNICAL BORING



 <b>TETRA TECH</b> <a href="http://www.tetrattech.com">www.tetrattech.com</a> 3380 Americana Terrace Suite 201 Boise, ID 83706 PHONE: 208-389-1030	PICKLES BUTTE SANITARY LANDFILL, CANYON COUNTY, IDAHO 2022 CONCEPTUAL EXPANSION GEOTECHNICAL INVESTIGATION  <b>BORING LOCATIONS PLAN</b>	Project No.: 114-571040-2022 Date: 7/29/2022 Designed By: SEF/MAM Figure <b>1040-1</b>
	Bar Measures 1 inch	

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## **APPENDIX B: Logs of Exploratory Borings**

Figures 1 through 8

# Figure No. 1 LOG OF BORING



## Boring B2021-1

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.502927
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.624204
<b>Date Started:</b> 11/15/21	<b>Date Finished:</b> 11/15/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2740.4 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
0.3			100		3-3-4		TOPSOIL, moist, tan/brown.	0.3						
2740.1			100		2-3-3		Poorly-Graded SAND with silt (SP-SM), loose, moist, brown to gray, fine to medium grained, subangular.	9		NV/NP		12	110	
5.3			100		2-3-5			5.3						
2735.1			100		3-6-9		Poorly-Graded SAND (SP), loose to medium dense, moist, gray to tan, medium grained, subangular to angular.	8						
9-13-13			100					6						
11.2			100		8-11-13			11.2						
2729.2			100				Silty SAND (SM), medium dense, moist, gray to tan, fine grained, medium plasticity, Pockets of clay.	5						
14.1			100		10-13-15			14.1						
2726.3			100				Poorly-Graded SAND (SP), medium dense, slightly moist, gray, fine to medium grained, subangular to angular, medium plasticity, Small pockets of grey clay.							
20			100		10-12-13			24.1						
2720.4			100					24.1						
25			100		13-21-23			2716.3		NV/NP		6	113	Cc= 0.03
2715.4			100				Poorly-Graded SAND with silt (SP-SM), dense to very dense, slightly moist, gray, fine to medium grained.							
30			100		13-25-34			31.5						
2710.4			100					2708.9						
Boring Depth: 31.5 ft, Elevation: 2708.9 ft														

<b>Water Level Observations</b>		Remarks:
<input type="checkbox"/> <b>During Drilling:</b> Not Encountered <input checked="" type="checkbox"/> <b>After Drilling:</b> Not Recorded	<input type="checkbox"/> <b>During Drilling:</b> Not Encountered <input checked="" type="checkbox"/> <b>After Drilling:</b> Not Recorded	

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2525 Palmer St  
 59808  
 Phone: 406-543-3045  
 Fax:

# Figure No. 2 LOG OF BORING



Sheet 1 of 1

**Boring B2021-2**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.501658
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.713829
<b>Date Started:</b> 11/16/21	<b>Date Finished:</b> 11/16/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Top of Boring Elevation:</b> 2739.0 ft
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	Elev. (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
5			100		2-1-3		Silty SAND (SM), very loose, slightly moist, brown to tan, fine grained, subangular to angular.	2.3	2736.7						
			100		2-1-1		Poorly-Graded SAND with silt (SP-SM), very loose to very dense, slightly moist to moist, brown to gray, fine to medium grained, angular to subangular.								
10			100		3-3-4										
			100		2-4-6										
15			100		7-10-14										
			100		10-15-20										
20			100		7-11-17										
			150		11-17-21										
25			100		11-16-21										
30			100		15-25-34										
Boring Depth: 31.5 ft, Elevation: 2707.5								31.5	2707.5						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Encountered	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded		<input checked="" type="checkbox"/> After Drilling: Not Recorded	

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**Boring B2021-3**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.500874
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.716768
<b>Date Started:</b> 11/16/21	<b>Date Finished:</b> 11/22/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
5					2-3-7		Slightly moist, tan. SILT (ML), stiff, slightly moist, light tan, low plasticity.	0.7 2737.0						
10					7-9-9		Silty SAND (SM), loose to medium dense, slightly moist to slightly moist, light tan, very fine grained.	8.0 2729.7						
15					11-11-12									
20				93	10-12-13				3					
25				80	11-15-15					NV/NP		29		Friction Angle= 25.86 degrees Cohesion= 0 ksf Cc= 0.04
30				100	10-12-14				3					
35				100	11-14-21									
40				93	10-14-16									
45				100	12-12-12		SILT (ML), very stiff, slightly moist, gray, low plasticity. Silty SAND (SM), medium dense to dense, slightly moist, tan to gray, fine grained, subangular to angular.	41.1 2696.6 41.9 2695.8						
50							SILT (ML), very stiff, slightly moist, gray, low plasticity. Silty SAND (SM), medium dense to	47.0 2690.7 47.7 2690.0						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Encountered	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.500874
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.716768
<b>Date Started:</b> 11/16/21	<b>Date Finished:</b> 11/22/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2737.7 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
55 2682.7			100		4-18-19		dense, slightly moist, tan to gray, fine grained, subangular to angular.	52.0 2685.7						
60 2677.7			100				SILT (ML), very stiff, slightly moist, gray to tan, low plasticity, Hard consolidated pieces.	56.2 2681.5						
65 2672.7			100				Poorly-Graded SAND with silt (SP), medium dense to dense, slightly moist, tan to gray, fine grained, subangular to angular.			NV/NP		19	100	Friction Angle= 20.21 degrees Cohesion= 0.282 ksf UCS= 0.143 ksf
70 2667.7			100		15-25-50					NV/NP		8		
75 2662.7			100				Sandy SILT (ML), stiff, dry, gray to red, fine grained, Broken siltstone.	76.5 2661.2						
80 2657.7			75				Silty SAND (SM), medium dense to dense, slightly moist, tan to gray, fine grained, subangular to angular.	78.5 2659.2						Friction Angle= 32.81 degrees Cohesion= 0.413 ksf
85 2652.7			100		4-11-50		Poorly-Graded SAND (SP), very dense, dry, salt & pepper, fine to medium grained, subangular to angular.	82.0 2655.7	2			24		
90 2647.7			100		23-40-50									
95 2642.7			0		50/0.2ft		Poorly-Graded SAND with silt (SP-SM), very stiff, dry, tan, fine to medium grained, subangular, Large amounts of broken sandstone.	95.0 2642.7						
100 2637.7			0				Silty SAND (SM), very dense, dry, gray to red, fine to coarse grained.	100.0 2637.7						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Encountered	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 3 LOG OF BORING

**Boring B2021-3**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.500874
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.716768
<b>Date Started:</b> 11/16/21	<b>Date Finished:</b> 11/22/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83 <b>Top of Boring Elevation:</b> 2737.7 ft
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
105 2632.7							subangular, Mixed with large pieces of siltstone.							
110 2627.7			143		31 - 50/0.2ft									
115 2622.7							Silty SAND (SM), very dense, dry to moist, salt & pepper to gray, fine to medium grained, subangular to angular, Minimal pieces of sandstone. Decreasing with depth.	115.0 2622.7		NV/NP		16	104	
120 2617.7			88		47 - 50/0.3ft				4					
125 2612.7														
130 2607.7														
135 2602.7							Poorly-Graded SAND with silt (SP-SM), very stiff, dry, tan, fine to coarse grained, subangular, Large amounts of broken sandstone and siltstone.	135.0 2602.7						
140 2597.7			100		14 - 33 - 50		Poorly-Graded SAND (SP), very dense, dry to moist, salt & pepper to gray, fine to medium grained, subangular to angular, Minimal pieces of sandstone..	138.6 2599.1						
145 2592.7														
150 2587.7			100		16 - 33 - 50		Silty CLAY (CL-ML), hard, very moist, gray, high plasticity.	146.5 2591.2						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Encountered	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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 59808  
 Phone: 406-543-3045  
 Fax:

# Figure No. 3 LOG OF BORING



Sheet 4 of 4

Boring B2021-3

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.500874
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.716768
<b>Date Started:</b> 11/16/21	<b>Date Finished:</b> 11/22/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83 <b>Top of Boring Elevation:</b> 2737.7 ft
<b>Driller:</b> Holt Services <b>Logger:</b> Matt Adams		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
		<b>Location:</b> Refer to site map.	

Depth (ft)	Elev. (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	Elev. (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
155	2582.7															
160	2577.7			100		16 - 24 - 36										
165	2572.7															
170	2567.7								170.0	2567.7						

Boring Depth: 170.0 ft, Elevation: 2567.7 ft

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<b>Water Level Observations</b>	<input type="checkbox"/> During Drilling: Not Encountered <input checked="" type="checkbox"/> After Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded	<input checked="" type="checkbox"/> During Drilling: Not Recorded	



# Figure No. 4 LOG OF BORING

**Boring B2021-4**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.665364
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.688388
<b>Date Started:</b> 12/8/21	<b>Date Finished:</b> 12/14/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
0.7							TOPSOIL, moist, dark brown.	0.7						
5					2-9-7		Silty SAND (SM), medium dense, moist to slightly moist, tan, fine grained, angular.	2796.5						
10					5-9-7									
15					5-12-14		SILT (ML), very stiff, slightly moist, tan, low plasticity.	15.0						
20					18-37-48		Silty SAND (SM), medium dense, moist to slightly moist, tan, fine grained.	20.0						
25					16-35-48		Silty CLAY (CL-ML), very stiff, slightly moist, tan, medium plasticity.	25.2						
30					16-27-33		SILT (ML), very stiff, slightly moist, tan, low plasticity.	27.7						
35					15-30-34									
40					11-23-18		Silty SAND (SM), medium dense, moist to slightly moist, tan, fine grained, angular to subangular.	40.0						
45					9-13-13		Silty CLAY (CL-ML), very stiff, slightly moist, tan to black, medium plasticity, Broken pieces of consolidated clay and sit.	41.0						
50							Poorly-Graded SAND with silt (SP-SM).	2756.2						
								50.0		NV/NP		6		Friction Angle= 27.04

<b>Water Level Observations</b>	<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded	

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# Figure No. 4 LOG OF BORING



## Boring B2021-4

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.665364
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.688388
<b>Date Started:</b> 12/8/21	<b>Date Finished:</b> 12/14/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
55 2742.2			100		9-20-41		medium dense to very dense, slightly moist, tan to salt & pepper, fine to medium grained, subangular to angular.	2747.2						degrees Cohesion= 0.123 ksf
60 2737.2			80		2-5-18			2						
65 2732.2														
70 2727.2			67		6-13-23									
75 2722.2							Silty SAND (SM), medium dense, moist to slightly moist, tan, fine grained, angular to subangular.	73.0 2724.2						
80 2717.2			80		2-7-23									
85 2712.2														
90 2707.2			100		13-40-50		Poorly-Graded SAND (SP), stiff, dry, tan to yellow, fine to medium grained, angular to subangular.	87.0 2710.2						
95 2702.2							Silty SAND (SM), hard, moist, tan to brown, fine grained, angular to subangular, Broken pieces of consolidated clay.	90.0 2707.2		NV	NP	38		Friction Angle= 22.83 degrees Cohesion= 0.198 ksf
100 2697.2			100		9-18-20			22						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 4 LOG OF BORING

**Boring B2021-4**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.665364
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.688388
<b>Date Started:</b> 12/8/21	<b>Date Finished:</b> 12/14/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2797.2 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
105 2692.2							Sandy SILT (ML), very stiff, slightly moist, tan, low plasticity.	104.0 2693.2						
105.0 2692.2							Silty CLAY (CL-ML), hard, moist, tan to brown, medium plasticity, Broken pieces of consolidated clay.	105.0 2692.2						
110 2687.2			100		6-12-20									
115 2682.2														
120 2677.2			100		31-70/0.4ft		Sandy SILT (ML), very stiff, slightly moist, tan, low plasticity.	117.5 2679.7						
120 2677.2							Silty SAND (SM), medium dense to very dense, slightly moist, tan to salt & pepper, fine to medium grained, subangular to angular.	120.0 2677.2		NV/NP		49		Friction Angle= 29.51 degrees Cohesion= 0.588 ksf
125 2672.2														
130 2667.2			100		9-21-26		Poorly-Graded SAND (SP), dense to very dense, slightly moist, salt & pepper, fine to medium grained, angular to subangular.	129.0 2668.2						
135 2662.2														
140 2657.2			100		30-48-44				2					
145 2652.2														
150 2647.2			111		31-50/0.4ft		Sandy SILT (ML), very stiff, slightly moist, tan to brown, low plasticity.	145.0 2652.2						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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**Boring B2021-4**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.665364
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.688388
<b>Date Started:</b> 12/8/21	<b>Date Finished:</b> 12/14/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2797.2 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
155 2642.2							Poorly-Graded SAND (SP), dense to very dense, slightly moist, salt & pepper, fine to medium grained, angular to subangular.	155.0 2642.2						
160 2637.2	Hand		111		29 - 50/0.4ft		Sandy SILT (ML), very stiff, slightly moist, tan to brown, low plasticity.	157.0 2640.2						
165 2632.2							Poorly-Graded SAND (SP), dense to very dense, slightly moist, salt & pepper, fine to medium grained, angular to subangular.	159.0 2638.2						
170 2627.2	Hand		88		50 - 50/0.3ft									
175 2622.2	Hand						Silty SAND (SM), very stiff, dry, gray, fine grained, angular to subangular.	175.0 2622.2						
180 2617.2	Hand						Poorly-Graded SAND (SP), dense to very dense, slightly moist, salt & pepper, fine to medium grained, angular to subangular.	177.0 2620.2						
185 2612.2							Silty SAND (SM), very stiff, dry, gray to gray, fine grained, angular to subangular.	183.0 2614.2						
190 2607.2	Hand						Poorly-Graded SAND with silt (SP-SM), medium dense to very dense, slightly moist, tan to salt & pepper, fine to medium grained, subangular to angular.	190.0 2607.2						
195 2602.2														
200 2597.2														

Boring Depth: 200.0 ft, Elevation: 2597.2 ft

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 5 LOG OF BORING

**Boring B2021-5**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.499133
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.713491
<b>Date Started:</b> 12/14/21	<b>Date Finished:</b> 12/19/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2661.6 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
0.7							TOPSOIL, moist, brown.	0.7						
2660.9					6-8-5		Sandy SILT (ML), stiff, slightly moist, tan, fine grained, angular to subangular.	2660.9						
5			100					4						
2656.6														
10			100		12-21-43		Poorly-Graded SAND (SP), medium dense to very dense, moist, tan to red, fine to medium grained, angular to subangular.	10.0						
2651.6								2651.6						
15			100		5-7-16			3						
2646.6														
20			100		10-21-26									
2641.6														
25			100											
2636.6														
30			100		10-27-40		Silty CLAY (CL-ML), medium stiff, slightly moist, white to gray, high plasticity.	27.0						
2631.6								2634.6						
35			100		10-22-35		Poorly-Graded SAND (SP), medium dense to very dense, slightly moist, salt & pepper to red, fine to medium grained, angular to subangular.	29.0						
2626.6								2632.6						
40			150		27-33-45/0.0ft		SILT (ML), hard, slightly moist, tan to gray, low plasticity.	37.0						
2621.6								2624.6						
45			100		23-39-42		Poorly-Graded SAND (SP), medium dense to very dense, slightly moist, salt & pepper to red, fine to medium grained, angular to subangular.	42.0						
2616.6								2619.6						
50			100				SILT (ML), hard, slightly moist, tan to gray, low plasticity.	44.0						
2611.6								2617.6						
							Silty SAND (SM), medium dense to very dense, slightly moist, gray to brown, fine	45.0						
								2616.6						
								50.0	54	24				Friction Angle= 14.95

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 5 LOG OF BORING

**Boring B2021-5**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.499133
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.713491
<b>Date Started:</b> 12/14/21	<b>Date Finished:</b> 12/19/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2661.6 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
55			100		27 - 35 - 30		grained, angular to subangular.	2611.6						degrees
2606.6							Silty CLAY (CL-ML), hard, slightly moist, tan, high plasticity.	51.0						Cohesion= 0.489 ksf
60			100		34 - 50/0.1ft		Poorly-Graded SAND (SP), medium dense to very dense, slightly moist, gray to tan, fine to medium grained, angular to subangular.	2610.6						Cc= 0.06
2606.6							Silty SAND (SM), medium stiff, slightly moist, tan, fine grained.	54.0						
65			100				Poorly-Graded SAND (SP), medium dense to very dense, slightly moist, gray to tan, fine to medium grained, angular to subangular.	2607.6						
2596.6							Poorly-Graded SAND (SP), medium dense to very dense, slightly moist, gray to tan, fine to medium grained, angular to subangular.	55.0						
70			100		10 - 30 - 20		Poorly-Graded SAND with silt (SP-SM), very dense, moist, gray, fine grained, Varying amounts of silt. Thin veins of silty clay.	2606.6						
2591.6							SILT with sand (ML), hard, slightly moist, white to gray, non plastic, Broken pieces of consolidated clay.	60.0	4					
75			100				Silty SAND (SM), very stiff, slightly moist, tan, fine grained.	2601.6						
2586.6							CLAY with sand (CL), hard, slightly moist, white to gray, non plastic, Broken pieces of consolidated clay.	65.5						
80			100		10 - 18 - 27			2596.1						
2581.6								71.5	29	NV	NP	77	112	Friction Angle= 19.09 degrees
85			100					2590.1						Cohesion= 0.037 ksf
90			100		49 - 50/0.3ft		Silty SAND (SM), very dense, slightly moist, tan to red, fine grained, angular to subangular.	73.5						
2576.6								2588.1						
95			100					86.0						
2566.6								2575.6						
100			115		21 - 46 - 50/0.3ft									
2561.6									11					

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 5 LOG OF BORING

**Boring B2021-5**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.499133
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.713491
<b>Date Started:</b> 12/14/21	<b>Date Finished:</b> 12/19/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2661.6 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
105 2556.6							Silty CLAY (CL-ML), very stiff, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	102.0 2559.6						
110 2551.6			100		30 - 50/0.1ft		Silty SAND (SM), very dense, slightly moist, tan to red, fine grained, angular to subangular.	110.0 2551.6						
115 2546.6							Silty CLAY (CL-ML), very stiff, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	111.0 2550.6						
120 2541.6			100		9 - 17 - 36		Silty SAND (SM), medium dense to very dense, slightly moist, gray to brown, fine grained, angular to subangular.	115.5 2546.1						
125 2536.6							Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	116.5 2545.1						
130 2531.6			107		26 - 50 - 50/0.4ft		Sandy SILT (ML), hard, slightly moist, red to brown, fine grained, low plasticity, Very fine sand. Some consolidated clay mixed.	126.0 2535.6						
135 2526.6							Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	127.0 2534.6						
140 2521.6			111		42 - 50/0.4ft		Silty SAND (SM), very dense, slightly moist, tan, very fine grained, Very fine sand. Some consolidated clay mixed. Less clay with depth.	129.5 2532.1						
145 2516.6							Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	131.5 2530.1						
150 2511.6			107		8 - 17 - 50/0.4ft		Silty SAND (SM), very dense, slightly moist, tan, low plasticity, Some consolidated silt. Seams of varying clay content.	134.5 2527.1						
							Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	140.0 2521.6						
							Sandy SILT (ML), hard, slightly moist, tan, low plasticity, Some consolidated silt. Seams of varying clay content.	141.0 2520.6						
							Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	143.0 2518.6						
							Sandy SILT (ML), hard, slightly moist, tan, low plasticity, Some consolidated silt. Seams of varying clay content.	145.0 2516.6						
							Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	147.0 2514.6						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 5 LOG OF BORING

**Boring B2021-5**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.499133
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.713491
<b>Date Started:</b> 12/14/21	<b>Date Finished:</b> 12/19/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2661.6 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
155 2506.6							pieces of consolidated clay.	156.0 2505.6						
160 2501.6	Hand		83		46 - 50/0.1ft		Sandy SILT (ML), hard, slightly moist, tan, low plasticity, Some consolidated silt. Seams of varying clay content.	157.0 2504.6						
165 2496.6							Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	160.0 2501.6						
170 2491.6	Hand		100		9 - 17 - 50		Sandy SILT (ML), hard, slightly moist, tan, low plasticity, Some consolidated silt. Seams of varying clay content.	163.5 2498.1						
175 2486.6							Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay. Higher silt content than previous.	164.5 2497.1						
180 2481.6	Hand						CLAY (CL), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	167.0 2494.6						
185 2476.6							Sandy SILT (ML), hard, slightly moist, tan, low plasticity, Some consolidated silt.	170.0 2491.6						
190 2471.6	Hand						CLAY (CL), hard, slightly moist, gray to blue, high plasticity, Broken pieces of consolidated clay.	180.0 2481.6						
195 2466.6							Silty SAND (SM), slightly moist, tan, fine grained, angular to subangular.							
200 2461.6	Hand						Silty CLAY (CL-ML), hard, slightly moist, gray to blue, high plasticity, Varying levels of silt content.							
							Silty SAND (SM), slightly moist, tan, fine grained, angular to subangular.							
							CLAY (CL), hard, slightly moist to moist, gray to blue, high plasticity, consolidated clay.	200.0 2461.6						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 5 LOG OF BORING



Sheet 5 of 5

**Boring B2021-5**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.499133
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.713491
<b>Date Started:</b> 12/14/21	<b>Date Finished:</b> 12/19/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests					
Elev. (ft)								Elev. (ft)											
205																			
2456.6																			
210																			
2451.6																			
215																			
2446.6																			
220																			
2441.6																			
225																			
2436.6								225.0											

Boring Depth: 225.0 ft, Elevation: 2436.6 ft

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<b>Water Level Observations</b>	<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded	

# Figure No. 6 LOG OF BORING

**Boring B2021-6**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.495196
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.715718
<b>Date Started:</b> 11/22/21	<b>Date Finished:</b> 12/2/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2636.7 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
0.6							TOPSOIL, very moist, brown.	2636.1						
5					4-5-5		Silty SAND (SM), loose to medium dense, slightly moist, tan to red, fine grained, subangular.							
10			67											
10			73		7-7-7				6					
15							Poorly-Graded SAND (SP), very dense, slightly moist, gray, fine to medium grained, subangular.	15.0						
20					11-31-42			21.0						
25			100				Silty SAND (SM), loose to medium dense, slightly moist, gray, fine grained, subangular.	2615.7						
25			100		12-22-42			18						
30							Poorly-Graded SAND (SP), very dense, slightly moist, gray, fine to medium grained, subangular.	27.0						
35							Silty SAND (SM), loose to medium dense, slightly moist to moist, gray, fine grained, Pieces of siltstone increasing with depth.	2609.7						
40					8-18-37			33.0						
45			100					22						
50					39-42-50									
50			100				Sandy SILT (ML), hard, slightly moist, gray, fine grained.	48.0						
50								2588.7						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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**Boring B2021-6**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.495196
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.715718
<b>Date Started:</b> 11/22/21	<b>Date Finished:</b> 12/2/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Top of Boring Elevation:</b> 2636.7 ft
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
55 2581.7			100		14-28-43									
60 2576.7			100		6-13-27			76.0 2560.7	25					UCS= 7.246 ksf
65 2571.7			100											
70 2566.7			100		7-20-27									
75 2561.7			100											
80 2556.7			91		8-18-50/0.1ft		CLAY (CH), hard, slightly moist, very dark gray, high plasticity, Almost claystone very consolidated.			67	19	91		
85 2551.7			100											
90 2546.7			100		9-14-40									
95 2541.7			100											
100 2536.7			100		11-23-26					56	22	90		UCS= 15.661 ksf

<b>Water Level Observations</b>	<input type="checkbox"/> During Drilling: Not Recorded <input checked="" type="checkbox"/> After Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded	

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# Figure No. 6 LOG OF BORING



## Boring B2021-6

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.495196
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.715718
<b>Date Started:</b> 11/22/21	<b>Date Finished:</b> 12/2/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83 <b>Top of Boring Elevation:</b> 2636.7 ft
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
105 2531.7							Sandy SILT (ML), hard, slightly moist, gray, medium plasticity.	102.0 2534.7						
110 2526.7			100		9 - 19 - 28		Silty CLAY (CL-ML), hard, slightly moist, very dark gray, high plasticity, Almost claystone very consolidated.	102.8 2533.9	47	22	91	100		
115 2521.7							CLAY with sand (CL), hard, slightly moist, gray, medium plasticity.	106.0 2530.7						
120 2516.7			100		10 - 18 - 33		Silty CLAY (CL-ML), hard, slightly moist, very dark gray, high plasticity, Almost claystone very consolidated.	106.9 2529.8	21					
125 2511.7							Sandy SILT (ML), hard, slightly moist, gray, medium plasticity.	110.8 2525.9						
130 2506.7			115		28 - 47 - 50/0.3ft		Silty CLAY (CL-ML), hard, slightly moist, very dark gray to blue, high plasticity, Almost claystone very consolidated.	112.0 2524.7	22					
135 2501.7														
140 2496.7			100		6 - 16 - 31									
145 2491.7														
150 2486.7			107		11 - 19 - 50/0.4ft									

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 6 LOG OF BORING



Sheet 4 of 4

**Boring B2021-6**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.495196
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.715718
<b>Date Started:</b> 11/22/21	<b>Date Finished:</b> 12/2/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
155 2481.7														
160 2476.7			115		29 - 50 - 50/0.3ft									
165 2471.7								165.0						

Boring Depth: 165.0 ft, Elevation: 2471.7 ft

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<b>Water Level Observations</b>	<input type="checkbox"/> During Drilling: Not Recorded <input checked="" type="checkbox"/> After Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Encountered	<input checked="" type="checkbox"/> After Drilling: Not Recorded	

# Figure No. 7 LOG OF BORING

**Boring B2021-7**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.49528
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.712592
<b>Date Started:</b> 12/2/21	<b>Date Finished:</b> 12/7/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2659.5 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
5					2-2-3		Slightly moist, dark brown. Silty SAND (SM), loose to dense, very moist, tan, fine grained, angular to subangular.	0.6 2658.9	4					
2654.5			60											
10					10-8-5									
2649.5			67											
15					8-18-18									
2644.5			80					16.4 2643.1						
20							Poorly-Graded SAND (SP), dense, moist, tan, fine to medium grained, angular to subangular.							
2639.5														
25					13-40-50									
2634.5			100				Silty SAND (SM), loose to dense, very moist, tan, fine grained, angular to subangular.	25.0 2634.5						
30					26-50/0.1ft									
2629.5			0				Poorly-Graded SAND (SP), dense, moist, gray, fine to medium grained, angular to subangular.	30.3 2629.2						
35					35-50/0.3ft									
2624.5			0				Silty SAND (SM), loose to dense, very moist, tan, fine grained, angular to subangular.	31.3 2628.2						
40					16-28-50/0.4ft									
2619.5			107				Poorly-Graded SAND (SP), dense, moist, gray, fine to medium grained, angular to subangular.	32.3 2627.2						
45					19-37-48									
2614.5			100				Silty SAND (SM), loose to dense, very moist, tan, fine grained, angular to subangular.	33.8 2625.7						
50							Poorly-Graded SAND (SP), dense, moist, gray, fine to medium grained, angular to subangular.	39.6 2619.9	23	NV/NP	23	112	UCS= 0.511 ksf	
2609.5							Silty SAND (SM), very dense, slightly	41.4 2618.1						
							Poorly-Graded SAND (SP), dense, moist, gray, fine to medium grained, angular to subangular.	43.6 2615.9						
							Silty CLAY (CL-ML), very stiff, moist, tan, high plasticity, Broken pieces of consolidated clay.	46.1 2613.4						
								50.0						

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Encountered	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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**Boring B2021-7**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.49528
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.712592
<b>Date Started:</b> 12/2/21	<b>Date Finished:</b> 12/7/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2659.5 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
55 2604.5			100		29-49-37		moist, tan, fine grained, angular to subangular, Broken pieces of siltstone and sandstone.	2609.5						
55.6 2603.9							Silty CLAY (CL-ML), hard, moist, tan, high plasticity, Broken pieces of consolidated clay.	54.0 2605.5						
60 2599.5			107		21-41-50/0.4ft		Silty SAND (SM), very dense, slightly moist, tan, fine grained, angular to subangular, Broken pieces of siltstone and sandstone.	58.5 2601.0	12	NV/NP	84	104	UCS= 1.817 ksf	
65 2594.5							Silty CLAY (CL-ML), hard, moist, tan, high plasticity, Broken pieces of consolidated clay..							
70 2589.5			100		9-23-35		Silty SAND (SM), very dense, slightly moist, tan, fine grained, angular to subangular, Broken pieces of siltstone and sandstone.	66.0 2593.5						
75 2584.5							Sandy SILT (ML), hard, moist, tan, high plasticity, Broken pieces of consolidated clay..							
80 2579.5			0		78-70/0.2ft		CLAY (CL), hard, moist, tan, high plasticity.	80.0 2579.5						
85 2574.5							Silty SAND (SM), very dense, slightly moist, tan, fine grained, angular to subangular, Broken pieces of siltstone and sandstone.	85.0 2574.5						
90 2569.5			0		70/0.3ft		Silty CLAY (CL-ML), hard, moist, tan, high plasticity, Broken pieces of consolidated clay..							
95 2564.5														
100 2559.5			100		28-28-28		CLAY (CL), hard, moist, tan, high plasticity.	97.7 2561.8	20					

<b>Water Level Observations</b>	<input type="checkbox"/> During Drilling: Not Encountered	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded	<input checked="" type="checkbox"/> After Drilling: Not Recorded	

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# Figure No. 7 LOG OF BORING



## Boring B2021-7

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.49528
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.712592
<b>Date Started:</b> 12/2/21	<b>Date Finished:</b> 12/7/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	
<b>Top of Boring Elevation:</b> 2659.5 ft			

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
105 2554.5														
110 2549.5			100		6-12-22									
115 2544.5														
120 2539.5			77		22-41-50/0.3ft					33	23			Friction Angle= 18.02 degrees Cohesion= 0.053 ksf Cc= 0.38
125 2534.5						SILT (ML), hard, dry, tan, low plasticity, Broken pieces.	121.5 2538.0							
125 2534.5						Silty CLAY (CL-ML), hard, moist, gray, high plasticity, Broken pieces of consolidated clay..	122.2 2537.3							
130 2529.5			100		12-33-48		Sandy SILT (ML), hard, dry, tan, low plasticity, Broken pieces.	128.5 2531.0	19					
135 2524.5							Silty CLAY (CL-ML), hard, moist, gray, high plasticity, Broken pieces of consolidated clay..	129.1 2530.4						
140 2519.5			100		9-18-50				24					
145 2514.5							CLAY (CL), hard, moist, gray to blue, high plasticity.	145.0 2514.5						
150 2509.5			100		9-18-31									

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Encountered	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded	<input checked="" type="checkbox"/> After Drilling: Not Recorded		

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# Figure No. 7 LOG OF BORING



Sheet 4 of 4

**Boring B2021-7**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.49528
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.712592
<b>Date Started:</b> 12/2/21	<b>Date Finished:</b> 12/7/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Top of Boring Elevation:</b> 2659.5 ft
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
155 2504.5														
160 2499.5			107		21 - 48 - 50/0.4ft									
165 2494.5														
170 2489.5			100		14 - 18 - 28									
175 2484.5														
180 2479.5														
185 2474.5														
190 2469.5														
195 2464.5														
200 2459.5								200.0						

Boring Depth: 200.0 ft, Elevation: 2459.5 ft

<b>Water Level Observations</b>		<input type="checkbox"/> During Drilling: Not Encountered	Remarks:
<input type="checkbox"/> After Drilling: Not Recorded	<input type="checkbox"/> After Drilling: Not Recorded		

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**Boring B2021-8**

<b>Project:</b> Pickles Butte Sanitary Landfill - Canyon County, ID		<b>Rig:</b> TS150 Crawler	<b>Boring Location N:</b> 43.48988
<b>Project Number:</b> 114-571040-2022		<b>Hammer:</b> Auto	<b>Coordinates E:</b> -116.703147
<b>Date Started:</b> 11/15/21	<b>Date Finished:</b> 11/15/21	<b>Boring Diameter:</b> 6 in	<b>System:</b> Decimal Degrees <b>Datum:</b> NAD83 <b>Top of Boring Elevation:</b> 2956.6 ft
<b>Driller:</b> Holt Services		<b>Drilling Fluid:</b> None	<b>Abandonment Method:</b> Grout
<b>Logger:</b> Matt Adams		<b>Location:</b> Refer to site map.	

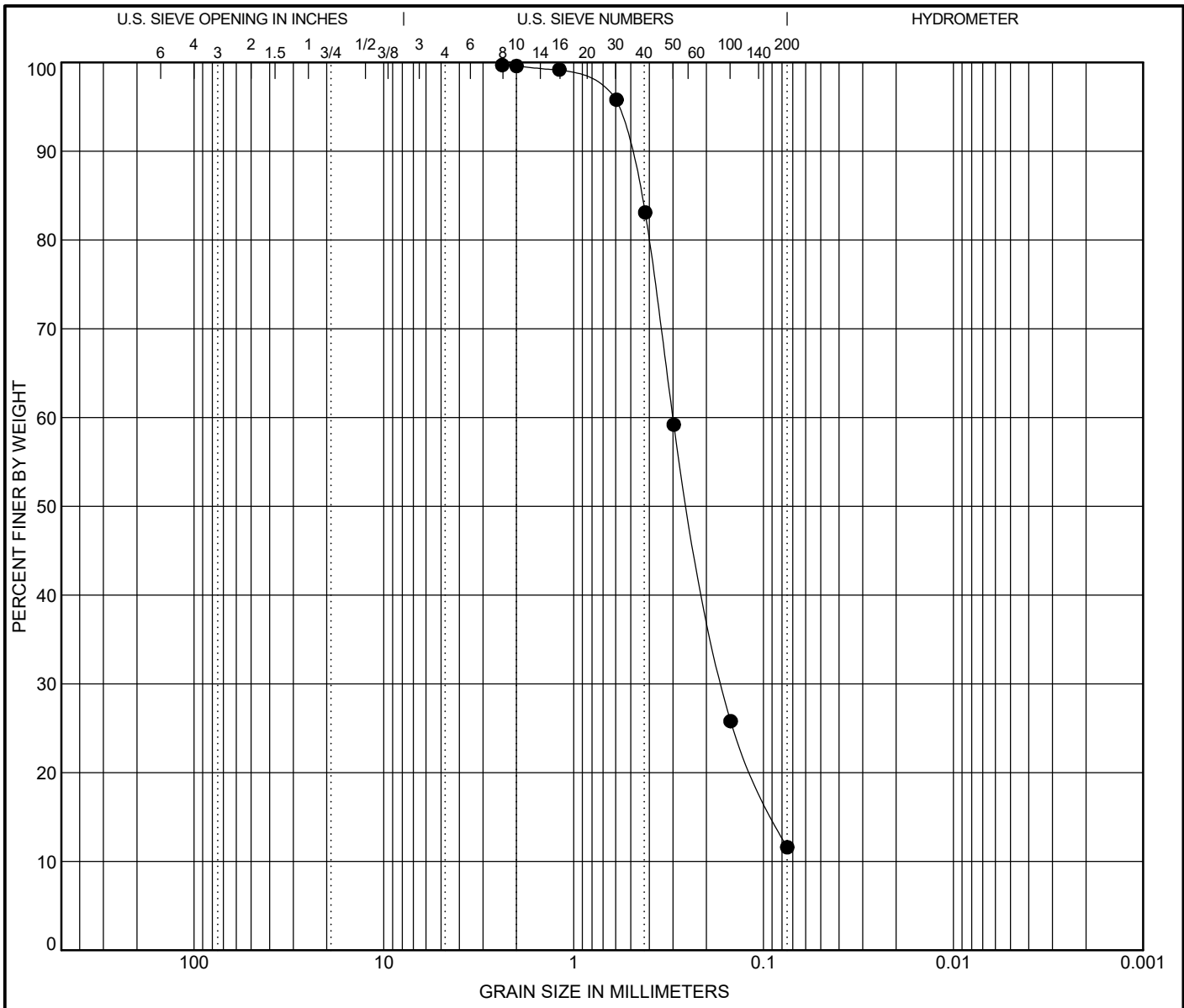
Depth (ft)	Operation	Sample Type	Recovery (%)	RQD (%)	Blow Count	Lithology	Material Description	Depth (ft)	MC (%)	LL	PL	-200 (%)	DD (pcf)	Remarks and Other Tests
Elev. (ft)								Elev. (ft)						
0.6			100		5-5-12	TOPSOIL, moist, brown.		0.6	11					
2956.0			100		10-16-13	SILT with sand (ML), very stiff, slightly moist to moist, tan.		2956.0		NV	NP	84	97	
11			100		8-8-10			11						
10			100		7-9-11	Silty SAND (SM), medium dense, slightly moist, tan to gray, fine grained, subangular, scattered gravel.		10.1	12					
2946.6			100		6-7-9			2946.5	6					
15			87		9-13-15	Poorly-Graded SAND (SP), medium dense, slightly moist, tan to yellow, fine to medium grained, subangular to angular.		20.0	5					
2941.6			87					2936.6						
20			87					21.5						
2936.6			87					2935.1						
Boring Depth: 21.5 ft, Elevation: 2935.1 ft														

TT LOG OF BORING - MDT - REVISED - 2009+ - GDT - 7/27/22 09:44 - N:\GEO\TECH\REPORTS\REPORT 2022\PICKLES BUTTE LANDFILL\LAB - LOGS\BORING LOGS.GPJ

<b>Water Level Observations</b>	<input type="checkbox"/> During Drilling: Not Encountered <input checked="" type="checkbox"/> After Drilling: Not Recorded	Remarks:
<input checked="" type="checkbox"/> After Drilling: Not Recorded	<input checked="" type="checkbox"/> After Drilling: Not Recorded	

## **APPENDIX C: Laboratory Testing**

Figures 9 through 56



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 8	99.7
No. 10	99.6
No. 16	99.2
No. 30	95.8
No. 40	83.1
No. 50	59.2
No. 100	25.8
No. 200	11.6

**Specimen Identification**  
B2021-1 - (3 - 6 ft)

Classification					
<b>POORLY GRADED SAND with</b>					
<b>SILT(SP-SM)</b>					
LL	PL	PI	Cc	Cu	
NV	NV	NP	1.27	4.33	

% Gravel	% Sand	% Silt	% Clay
0	88	12	

D100	D60	D30	D10
2.38	0.3	0.163	

### GRAIN SIZE DISTRIBUTION

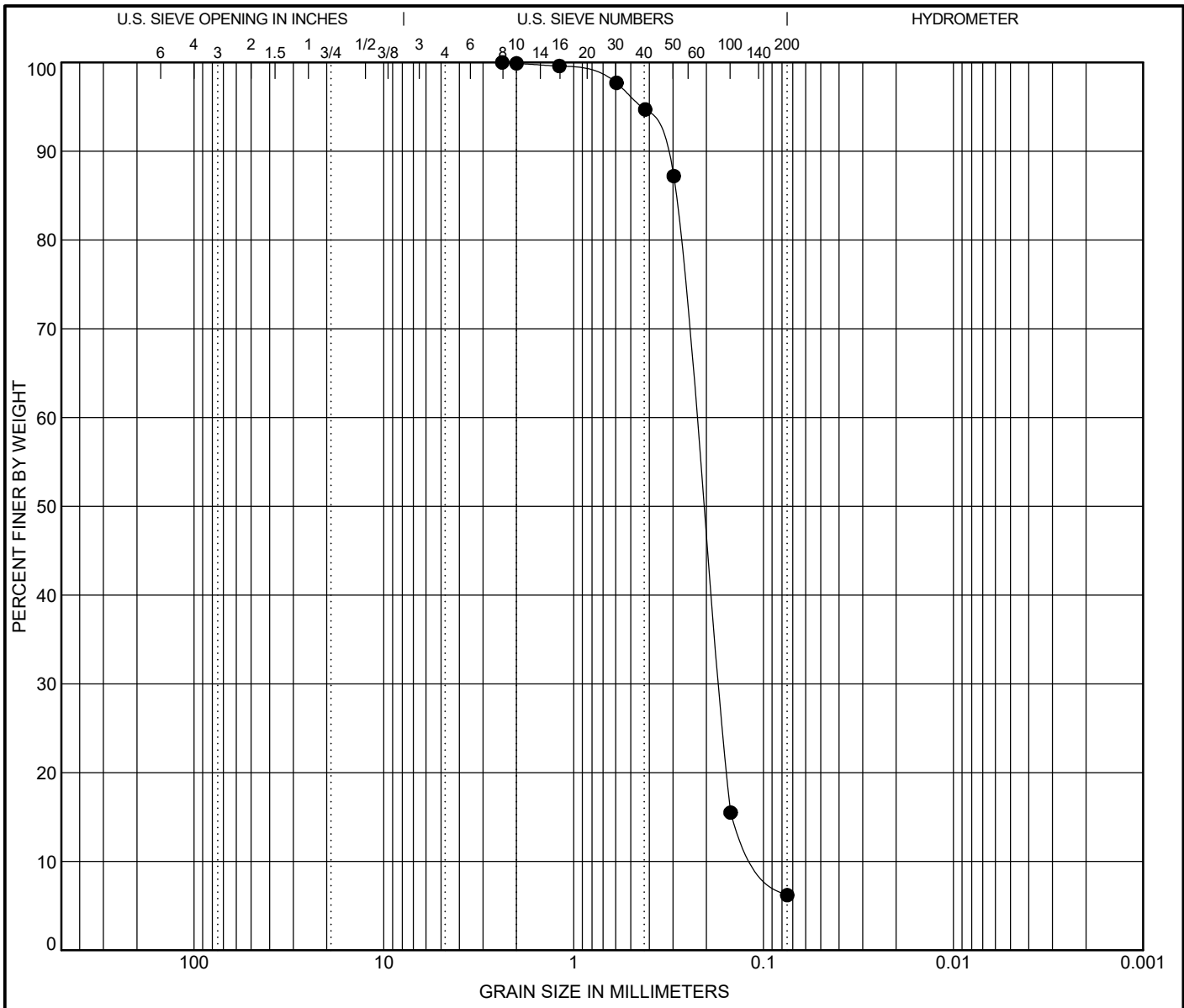


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 9

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 8	100
No. 10	99.9
No. 16	99.6
No. 30	97.7
No. 40	94.7
No. 50	87.2
No. 100	15.5
No. 200	6.2

**Specimen Identification**  
**B2021-1 - (25 - 27 ft)**

Classification					
<b>POORLY GRADED SAND with</b>					
<b>SILT(SP-SM)</b>					
LL	PL	PI	Cc	Cu	
NV	NV	NP	1.29	2.30	

% Gravel	% Sand	% Silt	% Clay
0	94	6	

D100	D60	D30	D10
2.38	0.229	0.171	0.099

### GRAIN SIZE DISTRIBUTION

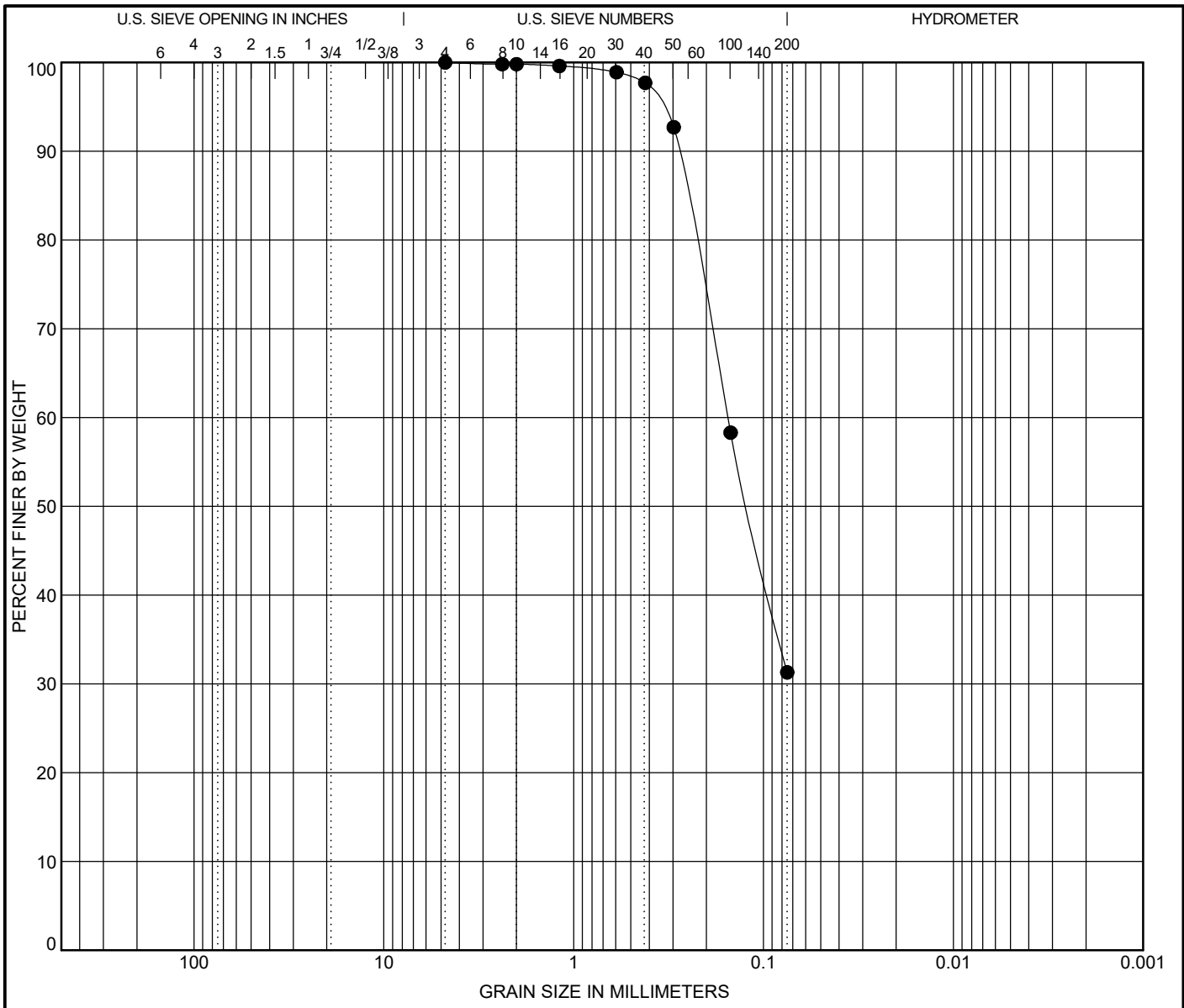


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 10

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	99.8
No. 10	99.8
No. 16	99.6
No. 30	98.9
No. 40	97.7
No. 50	92.7
No. 100	58.3
No. 200	31.3

**Specimen Identification**  
**B2021-3 - (25 - 27 ft)**

Classification				
<b>SILTY SAND(SM)</b>				
LL	PL	PI	Cc	Cu
<b>NV</b>	<b>NV</b>	<b>NP</b>		

% Gravel	% Sand	% Silt	% Clay
0	69	31	

D100	D60	D30	D10
4.75	0.154		

**GRAIN SIZE DISTRIBUTION**

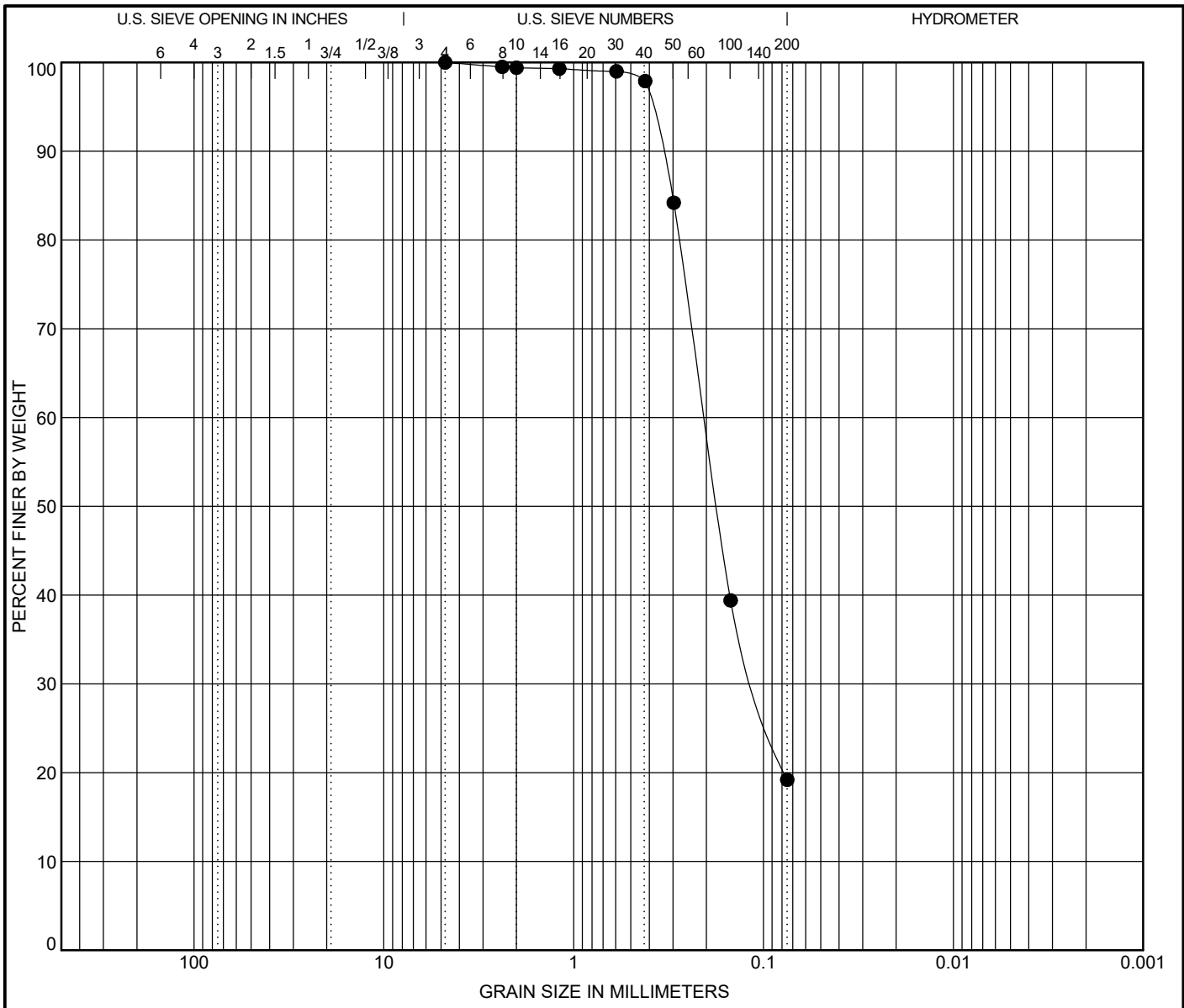


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 11

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	99.5
No. 10	99.4
No. 16	99.3
No. 30	99
No. 40	97.9
No. 50	84.2
No. 100	39.4
No. 200	19.2

**Specimen Identification**  
**B2021-3 - (60 - 62 ft)**

Classification				
<b>SILTY SAND(SM)</b>				
LL	PL	PI	Cc	Cu
<b>NV</b>	<b>NV</b>	<b>NP</b>		

% Gravel	% Sand	% Silt	% Clay
0	81	19	

D100	D60	D30	D10
4.75	0.205	0.108	

**GRAIN SIZE DISTRIBUTION**

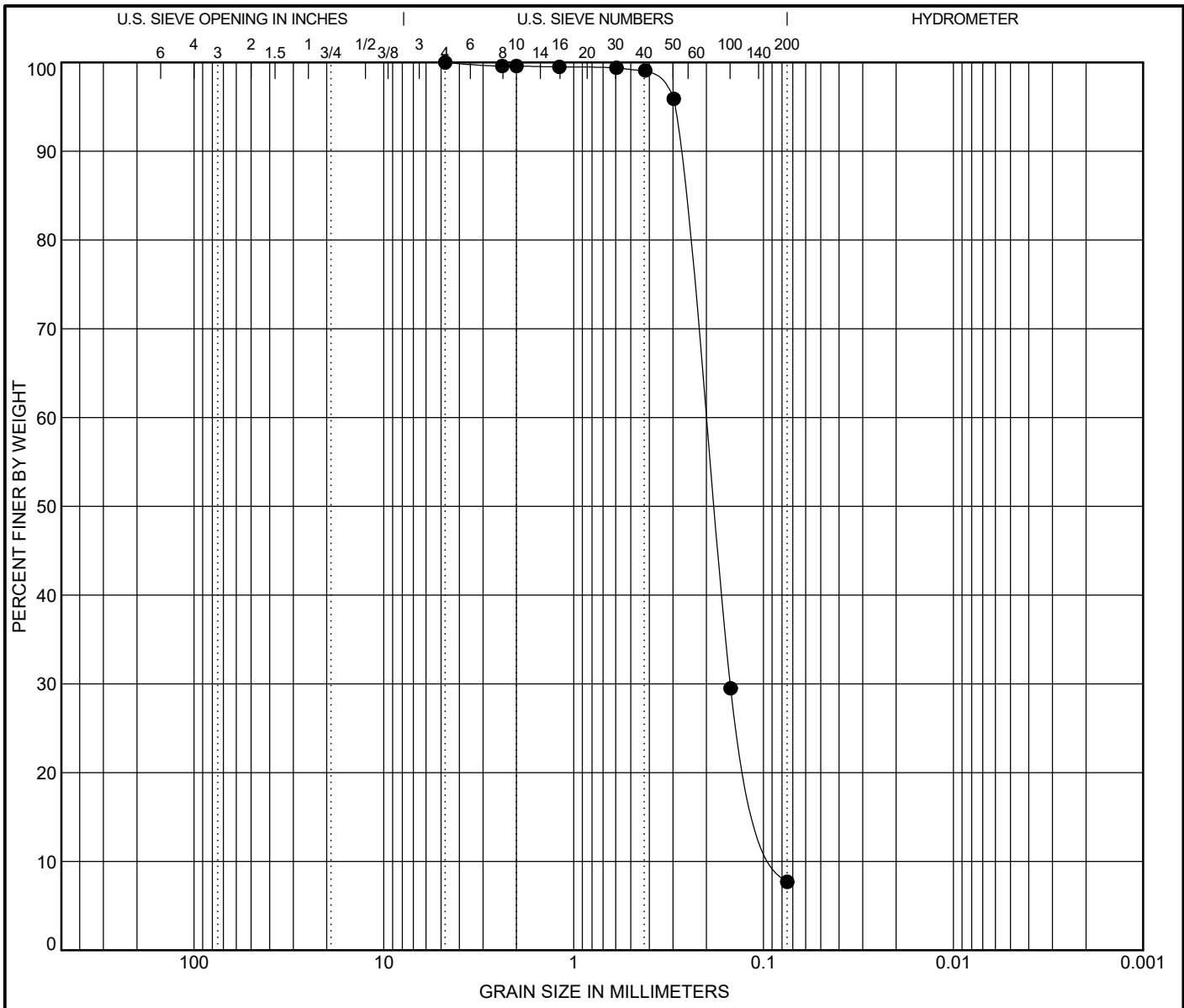


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 12

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	99.6
No. 10	99.6
No. 16	99.5
No. 30	99.4
No. 40	99.1
No. 50	95.9
No. 100	29.5
No. 200	7.7

**Specimen Identification**  
**B2021-3 - (61 - 65 ft)**

Classification					
<b>POORLY GRADED SAND with</b>					
<b>SILT(SP-SM)</b>					
LL	PL	PI	Cc	Cu	
NV	NV	NP	1.36	2.54	

% Gravel	% Sand	% Silt	% Clay
0	92	8	

D100	D60	D30	D10
4.75	0.205	0.15	0.081

### GRAIN SIZE DISTRIBUTION



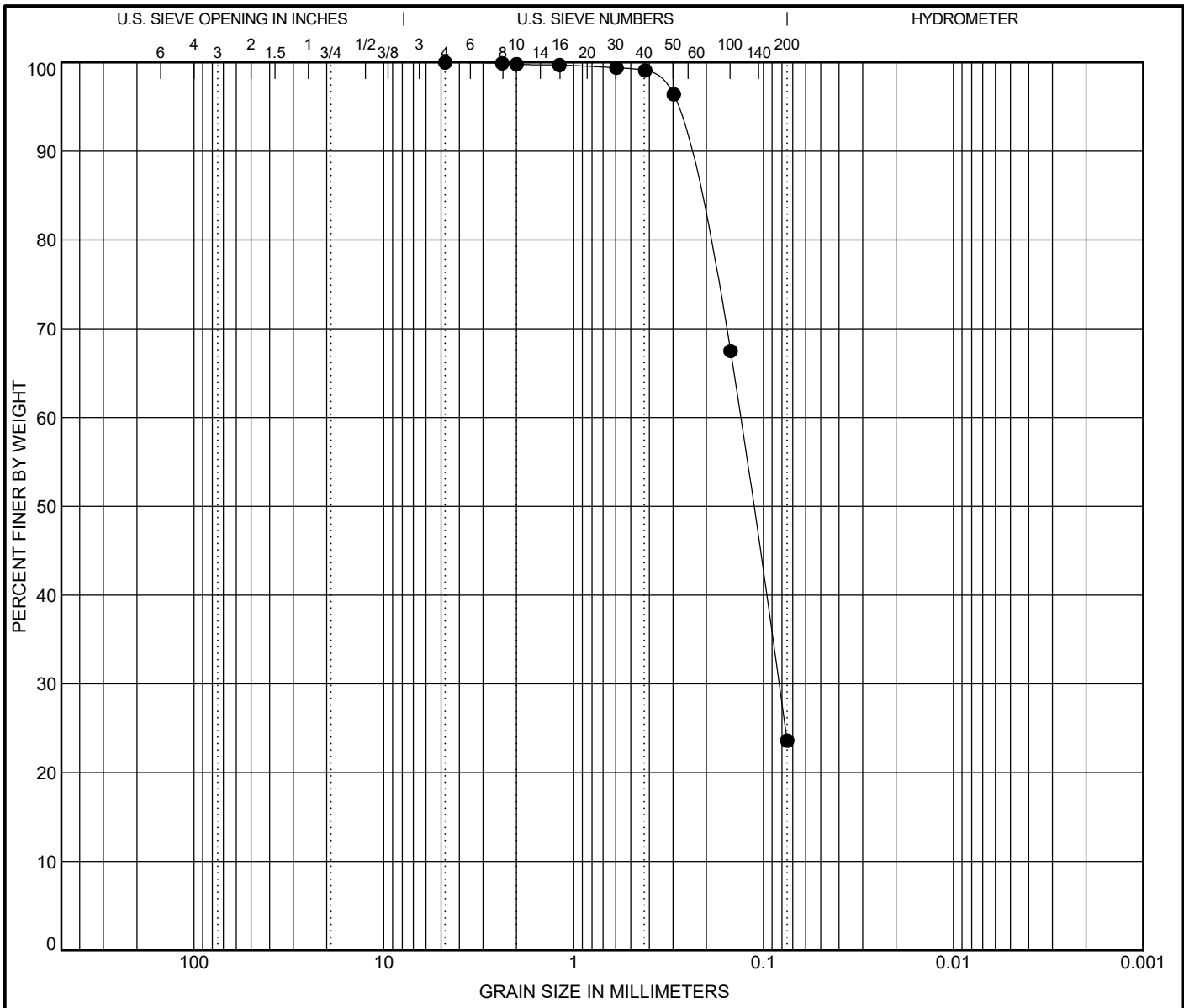
Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 13

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)





COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	99.9
No. 10	99.8
No. 16	99.7
No. 30	99.4
No. 40	99.1
No. 50	96.4
No. 100	67.5
No. 200	23.6

**Specimen Identification**  
**B2021-3 - (80 - 82 ft)**

Classification				
<b>SILTY SAND(SM)</b>				
LL	PL	PI	Cc	Cu
<b>NV</b>	<b>NV</b>	<b>NP</b>		

% Gravel	% Sand	% Silt	% Clay
0	76	24	

D100	D60	D30	D10
4.75	0.133	0.083	

**GRAIN SIZE DISTRIBUTION**

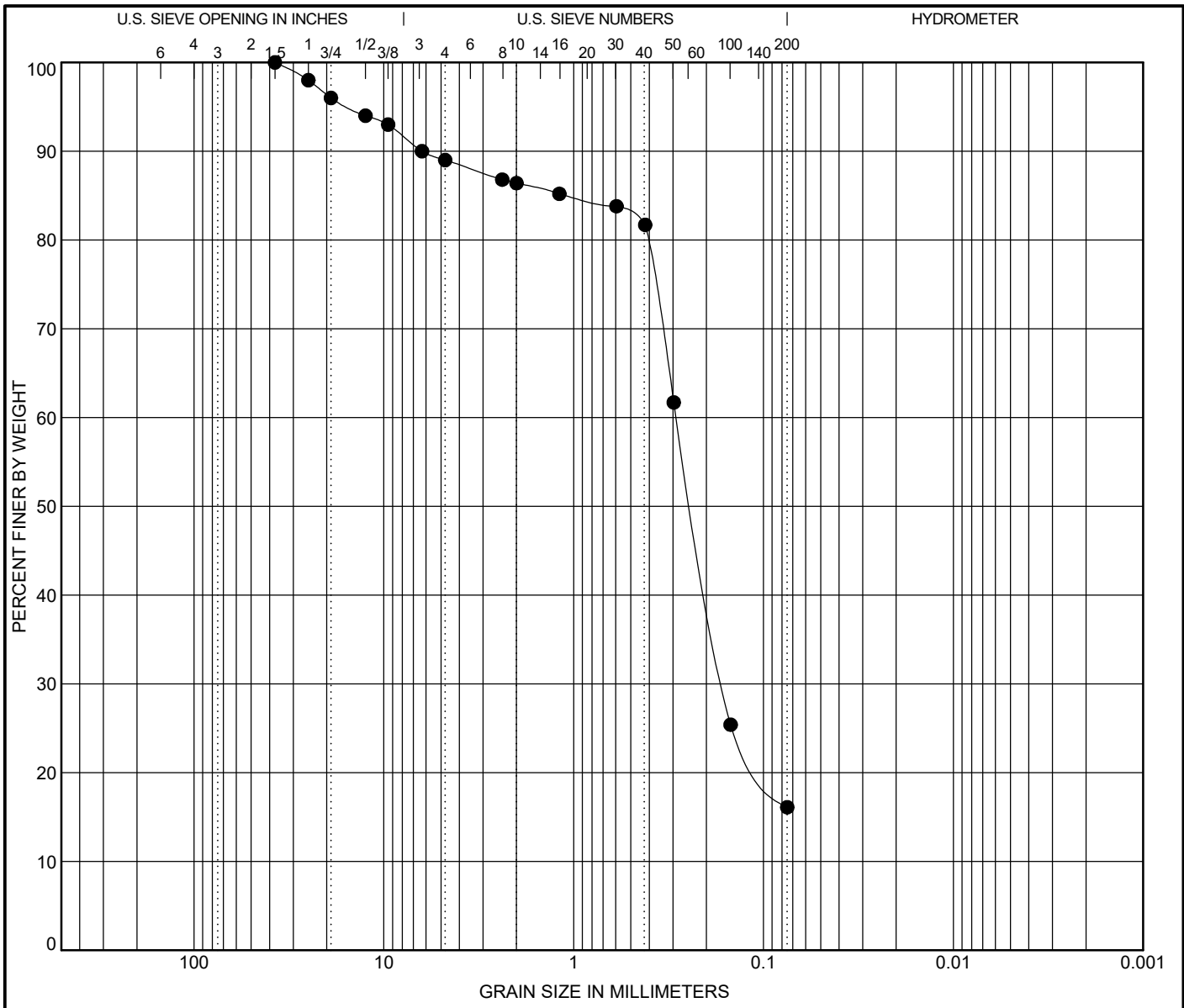


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 14

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
1.5 in	100
1 in	98
3/4 in	96
1/2 in	94
3/8 in	93
1/4 in	90
No. 4	89
No. 8	86.8
No. 10	86.4
No. 16	85.2
No. 30	83.8
No. 40	81.7
No. 50	61.7
No. 100	25.4
No. 200	16.1

**Specimen Identification**  
B2021-3 - (116 - 120 ft)

Classification				
<b>SILTY SAND(SM)</b>				
LL	PL	PI	Cc	Cu
NV	NV	NP		

% Gravel	% Sand	% Silt	% Clay
11	73	16	

D100	D60	D30	D10
37.5	0.288	0.163	

### GRAIN SIZE DISTRIBUTION

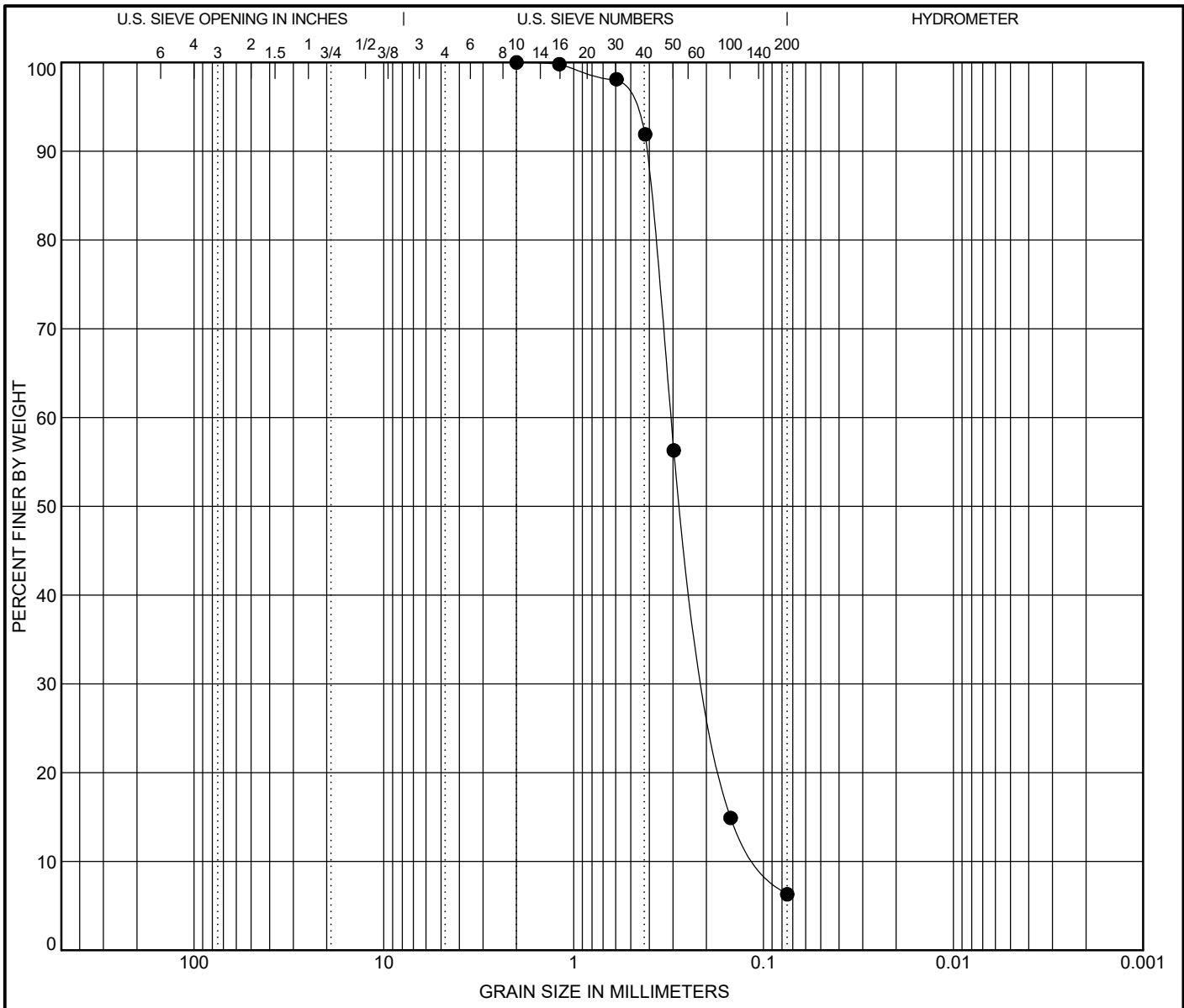


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 15

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 10	100
No. 16	99.8
No. 30	98.1
No. 40	91.9
No. 50	56.3
No. 100	14.9
No. 200	6.3

**Specimen Identification**  
B2021-4 - (50 - 51.5 ft)

Classification					
<b>POORLY GRADED SAND with</b>					
<b>SILT(SP-SM)</b>					
LL	PL	PI	Cc	Cu	
NV	NV	NP	1.18	3.06	

% Gravel	% Sand	% Silt	% Clay
0	94	6	

D100	D60	D30	D10
2	0.308	0.192	0.101

### GRAIN SIZE DISTRIBUTION

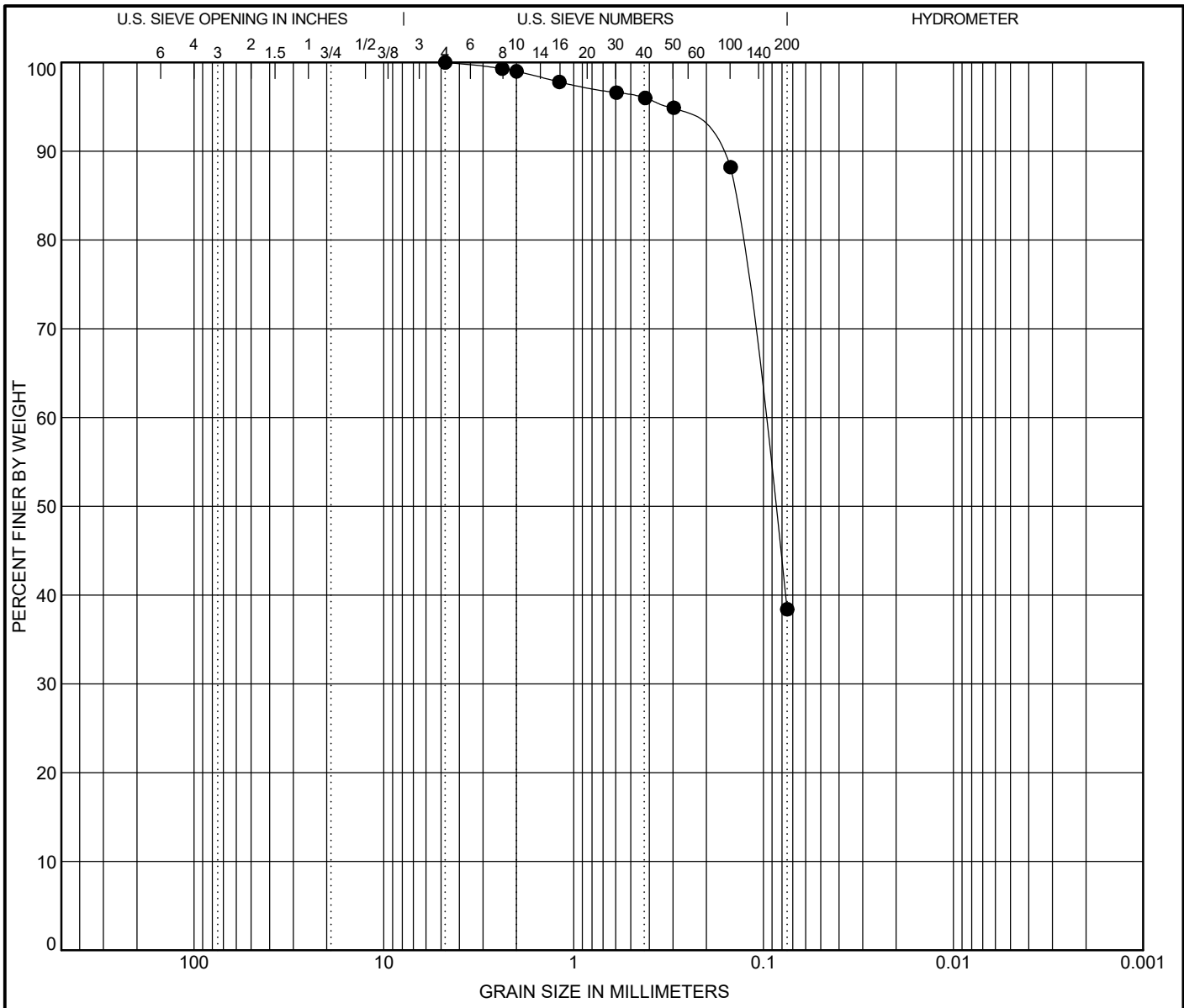


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 16

BORING LOGS.GPJ 6-20-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	99.3
No. 10	99
No. 16	97.8
No. 30	96.6
No. 40	96
No. 50	94.9
No. 100	88.2
No. 200	38.4

**Specimen Identification**  
B2021-4 - (90 - 91.5 ft)

Classification				
<b>SILTY SAND(SM)</b>				
LL	PL	PI	Cc	Cu
NV	NV	NP		

% Gravel	% Sand	% Silt	% Clay
0	62	38	

D100	D60	D30	D10
4.75	0.101		

### GRAIN SIZE DISTRIBUTION

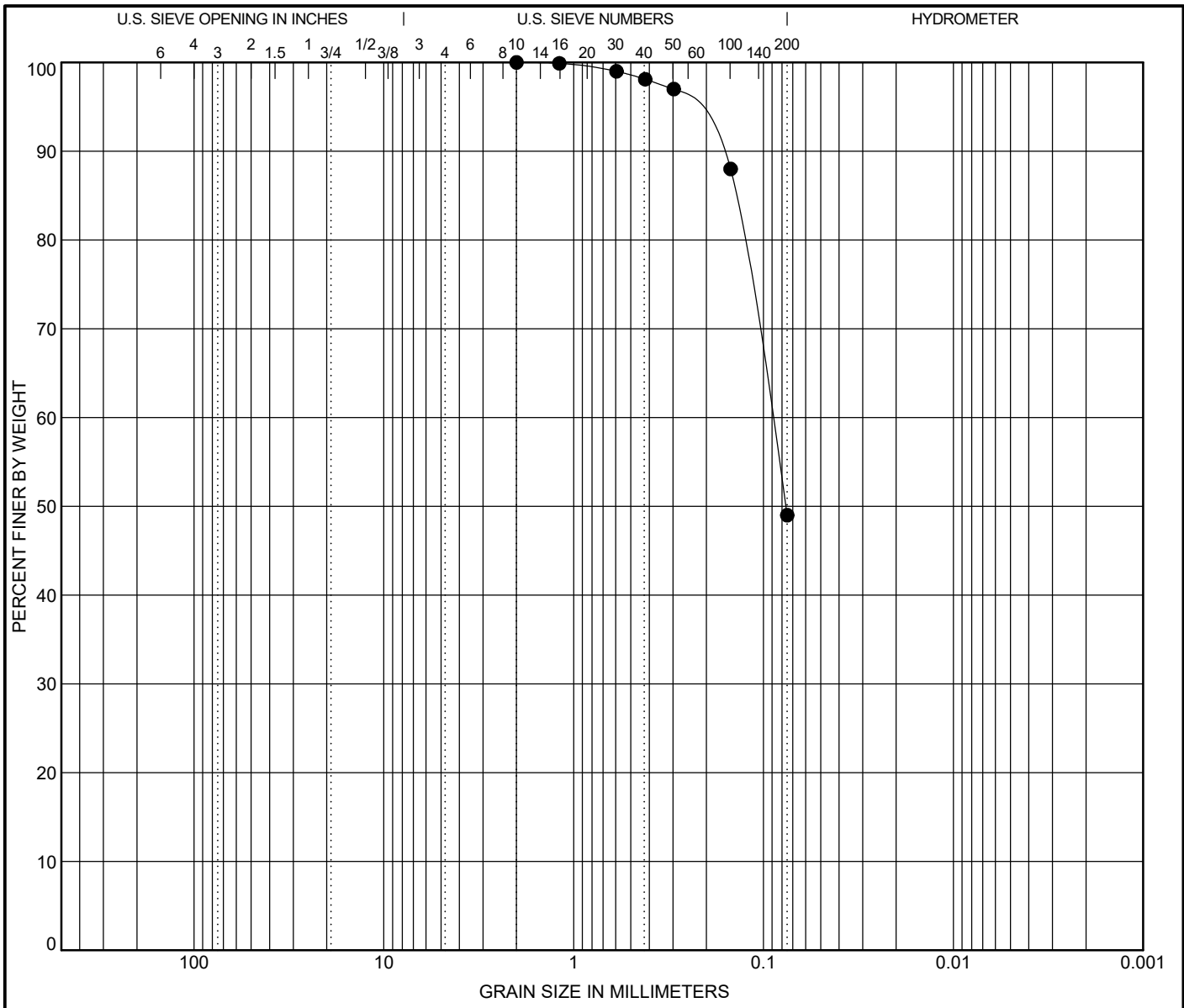


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 17

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 10	100
No. 16	99.9
No. 30	99
No. 40	98.1
No. 50	97
No. 100	88
No. 200	49

**Specimen Identification**  
**B2021-4 - (120 - 120.9 ft)**

Classification				
<b>SILTY SAND(SM)</b>				
LL	PL	PI	Cc	Cu
<b>NV</b>	<b>NV</b>	<b>NP</b>		

% Gravel	% Sand	% Silt	% Clay
0	51	49	

D100	D60	D30	D10
2	0.091		

**GRAIN SIZE DISTRIBUTION**

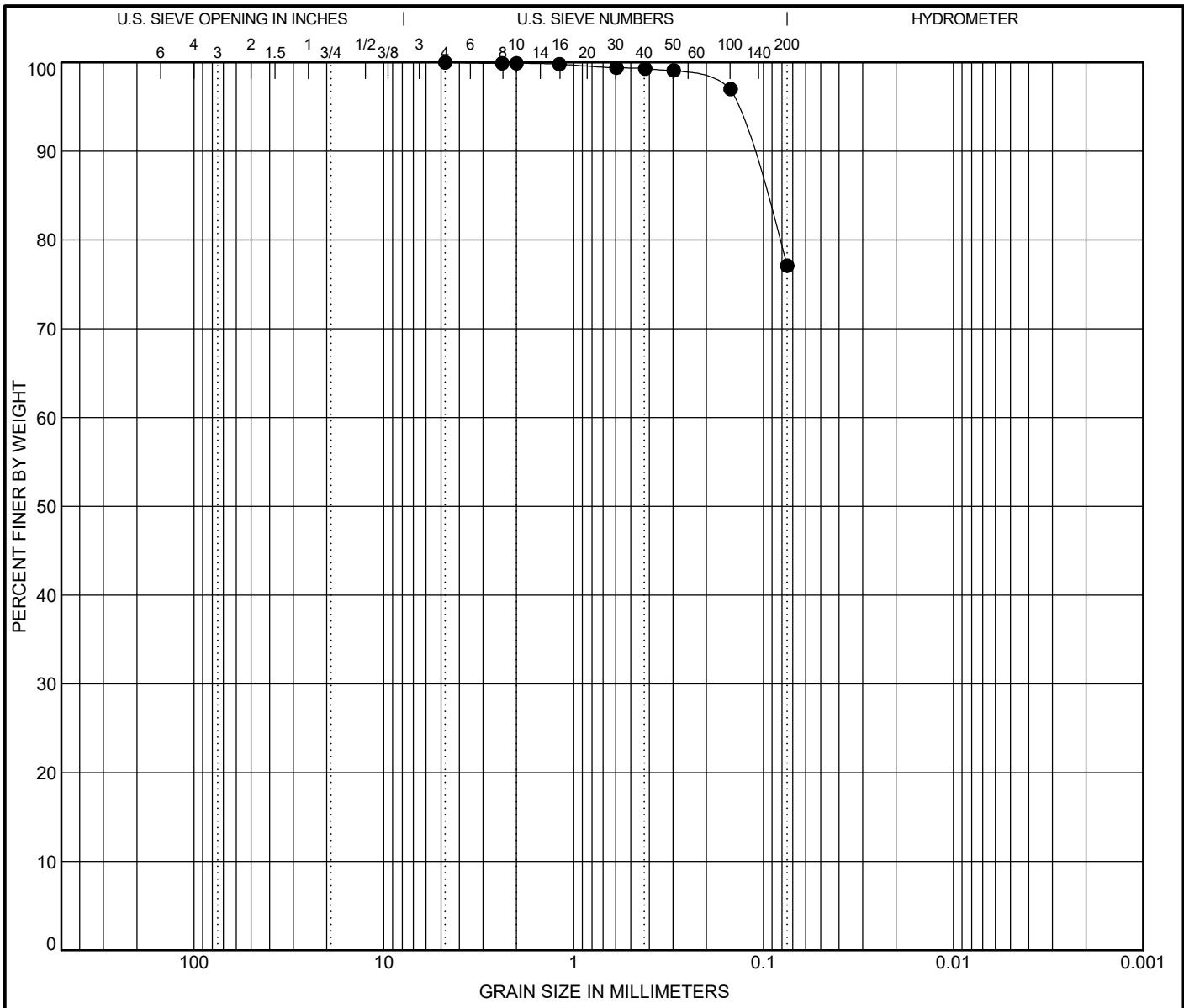


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 18

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	99.9
No. 10	99.9
No. 16	99.8
No. 30	99.4
No. 40	99.3
No. 50	99.1
No. 100	97
No. 200	77.1

**Specimen Identification**  
B2021-5 - (69 - 70 ft)

Classification				
<b>SILT with SAND(ML)</b>				
LL	PL	PI	Cc	Cu
<b>27</b>	<b>20</b>	<b>7</b>		

% Gravel	% Sand	% Silt	% Clay
0	23	77	

D100	D60	D30	D10
4.75			

### GRAIN SIZE DISTRIBUTION

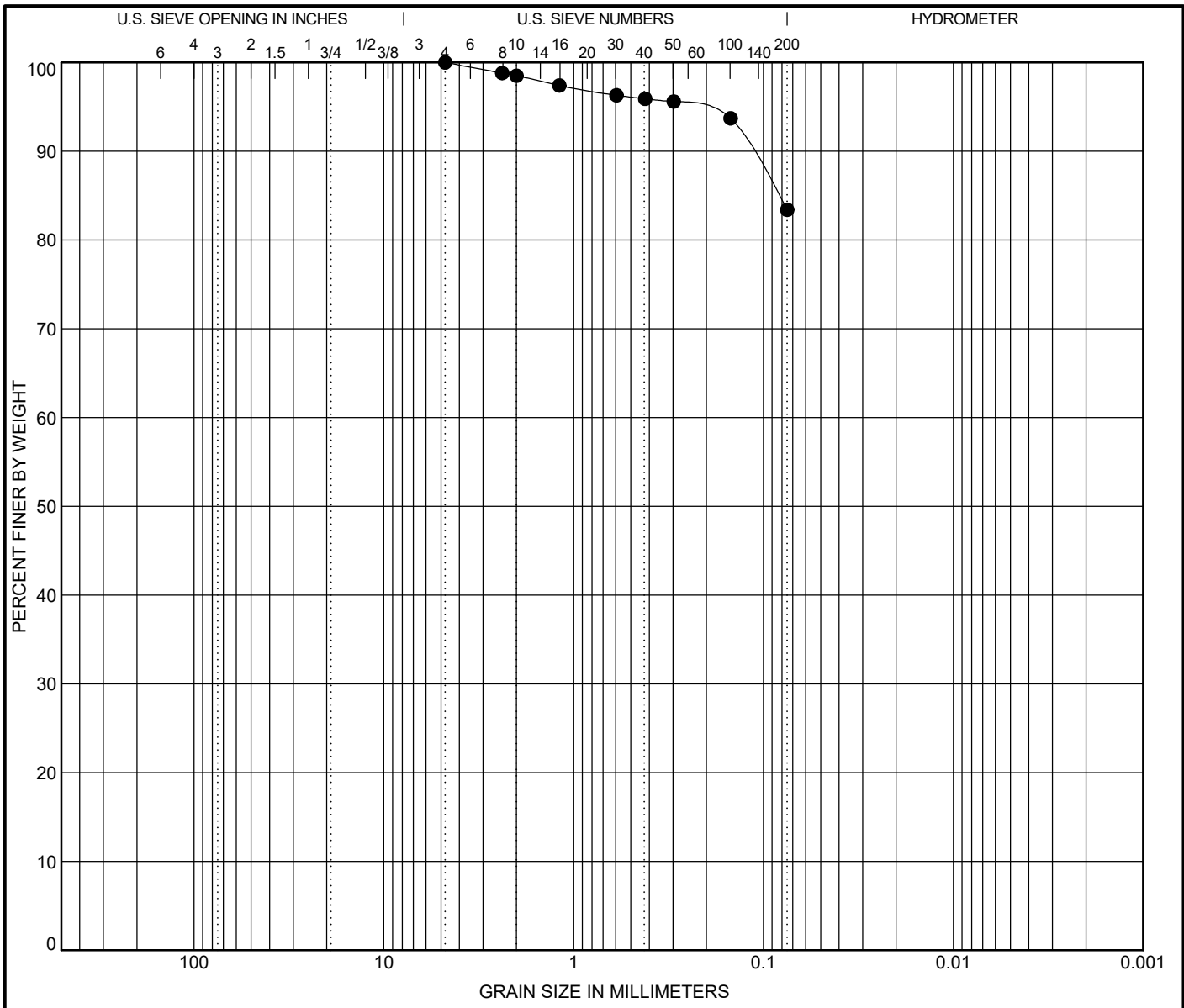


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 19

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	98.8
No. 10	98.5
No. 16	97.4
No. 30	96.3
No. 40	95.9
No. 50	95.6
No. 100	93.7
No. 200	83.4

**Specimen Identification**  
B2021-5 - (80 - 81.5 ft)

Classification					
<b>LEAN CLAY with SAND(CL)</b>					
LL	PL	PI	Cc	Cu	
<b>35</b>	<b>21</b>	<b>14</b>			

% Gravel	% Sand	% Silt	% Clay
0	17	83	

D100	D60	D30	D10
4.75			

### GRAIN SIZE DISTRIBUTION

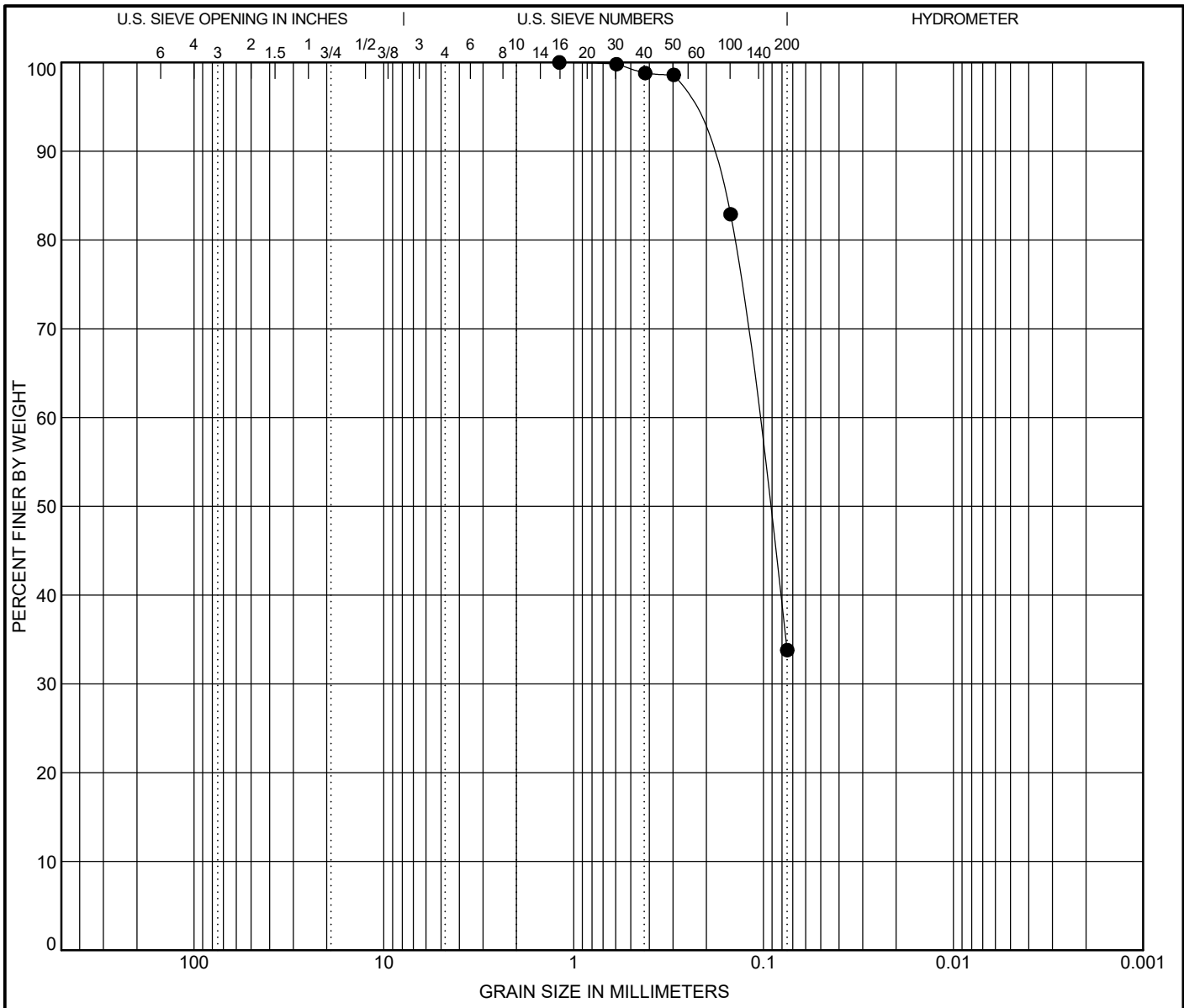


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 20

BORING LOGS.GPJ 6-20-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 16	100
No. 30	99.8
No. 40	98.8
No. 50	98.6
No. 100	82.9
No. 200	33.8

**Specimen Identification**  
B2021-5 - (90 - 91.5 ft)

Classification				
<b>SILTY SAND(SM)</b>				
LL	PL	PI	Cc	Cu
<b>NV</b>	<b>NV</b>	<b>NP</b>		

% Gravel	% Sand	% Silt	% Clay
0	66	34	

D100	D60	D30	D10
1.19	0.108		

### GRAIN SIZE DISTRIBUTION



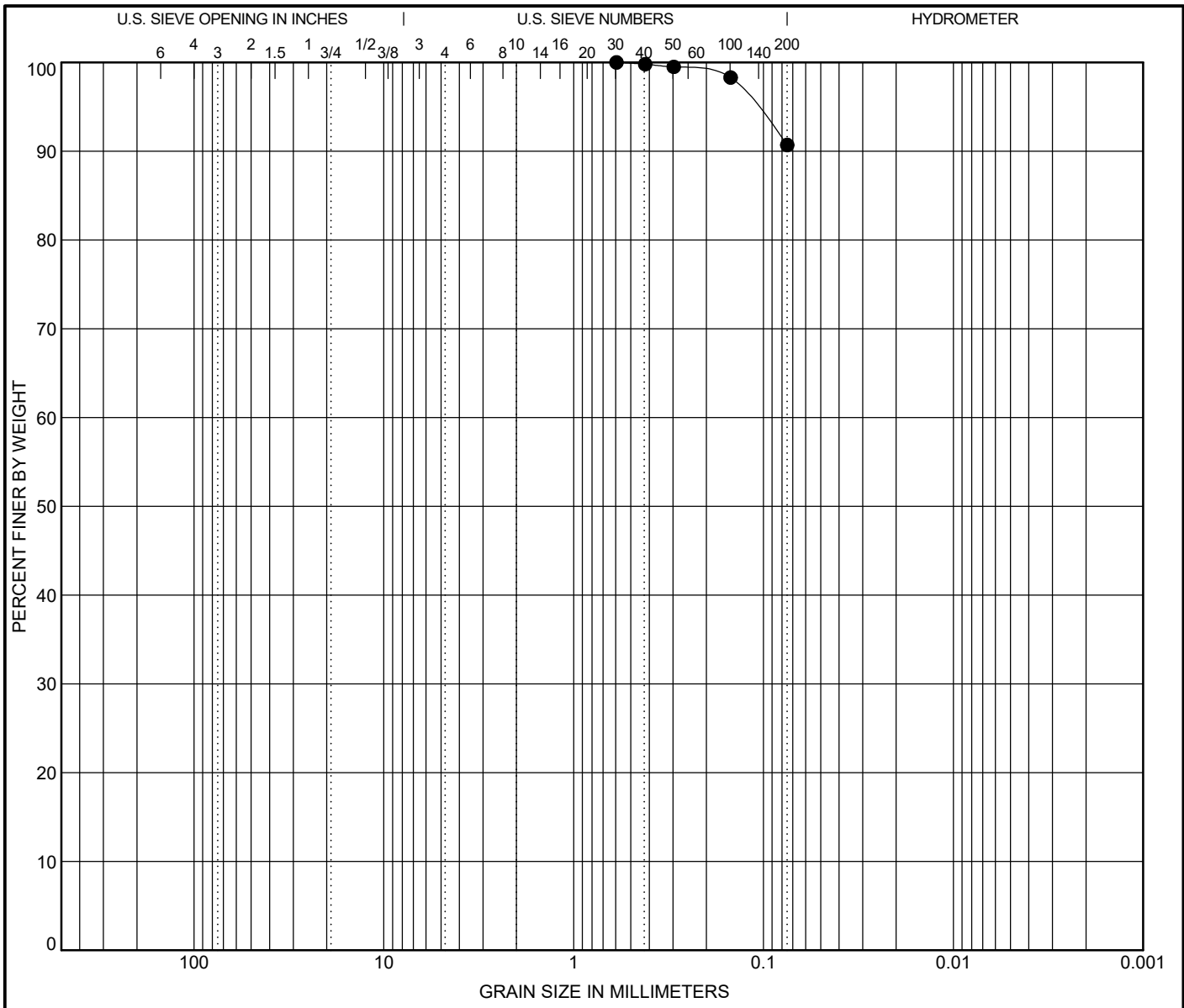
Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 21

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)





COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 30	100
No. 40	99.8
No. 50	99.5
No. 100	98.3
No. 200	90.7

**Specimen Identification**  
**B2021-6 - (79 - 81 ft)**

Classification				
<b>FAT CLAY(CH)</b>				
LL	PL	PI	Cc	Cu
<b>67</b>	<b>19</b>	<b>48</b>		

% Gravel	% Sand	% Silt	% Clay
0	9	91	

D100	D60	D30	D10
0.595			

**GRAIN SIZE DISTRIBUTION**

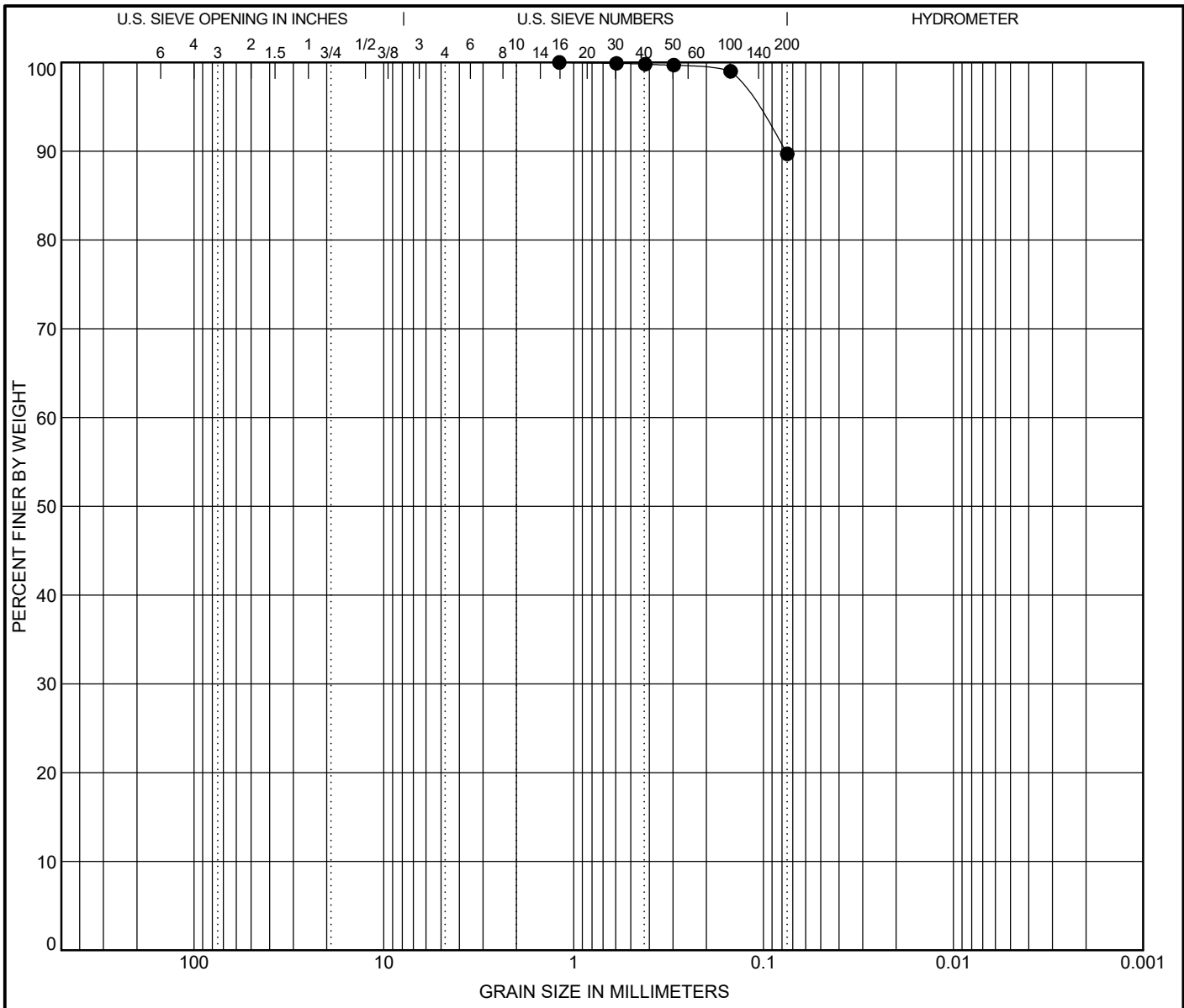


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 22

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 16	100
No. 30	99.9
No. 40	99.8
No. 50	99.7
No. 100	99
No. 200	89.7

**Specimen Identification**  
B2021-6 - (99 - 102 ft)

Classification				
<b>FAT CLAY(CH)</b>				
LL	PL	PI	Cc	Cu
<b>56</b>	<b>22</b>	<b>34</b>		

% Gravel	% Sand	% Silt	% Clay
0	10	90	

D100	D60	D30	D10
1.19			

### GRAIN SIZE DISTRIBUTION

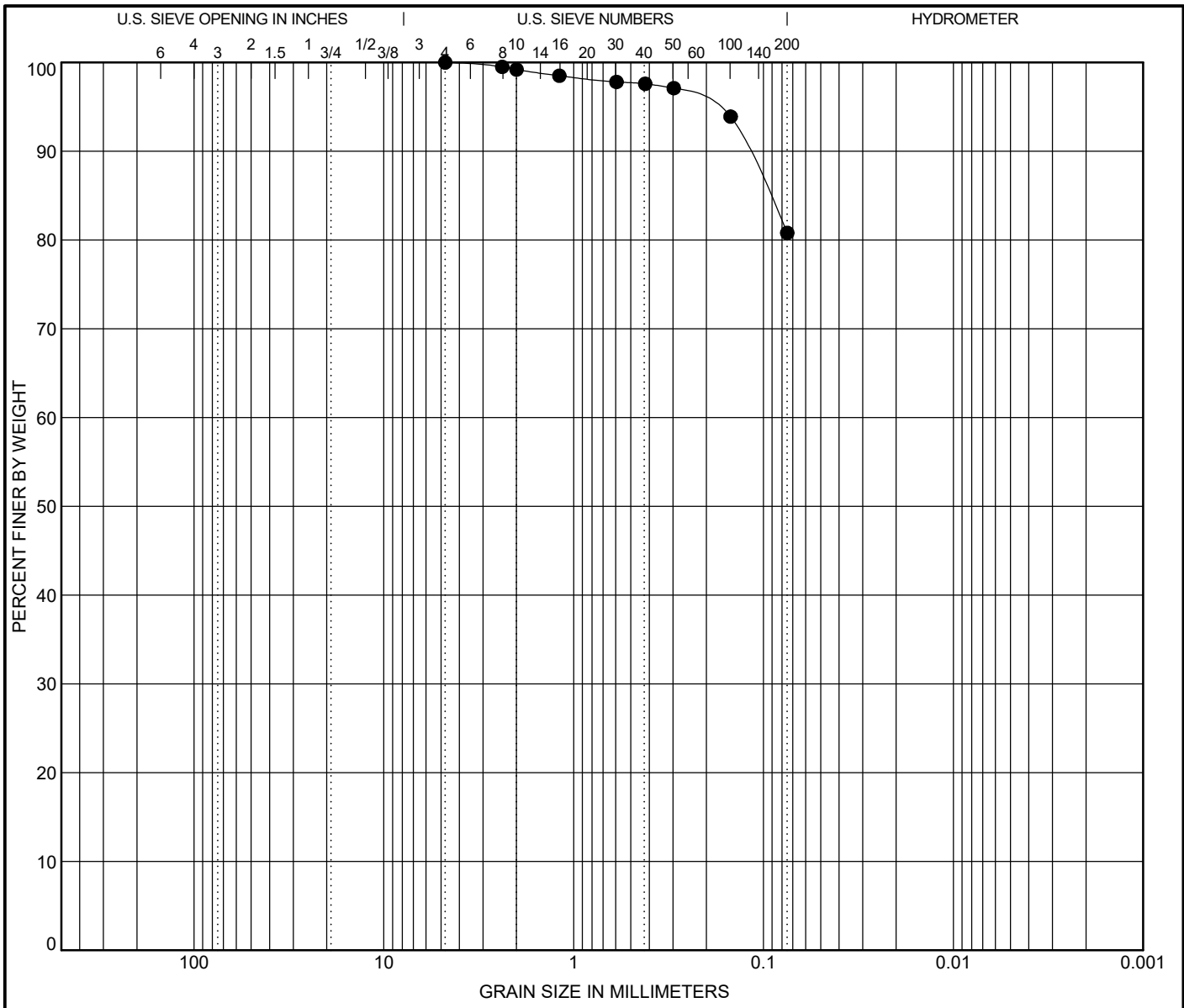


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 23

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	99.5
No. 10	99.2
No. 16	98.5
No. 30	97.8
No. 40	97.6
No. 50	97.1
No. 100	93.9
No. 200	80.8

**Specimen Identification**  
**B2021-6 - (106 - 107 ft)**

Classification					
<b>LEAN CLAY with SAND(CL)</b>					
LL	PL	PI	Cc	Cu	
<b>47</b>	<b>22</b>	<b>25</b>			

% Gravel	% Sand	% Silt	% Clay
0	19	81	

D100	D60	D30	D10
4.75			

### GRAIN SIZE DISTRIBUTION

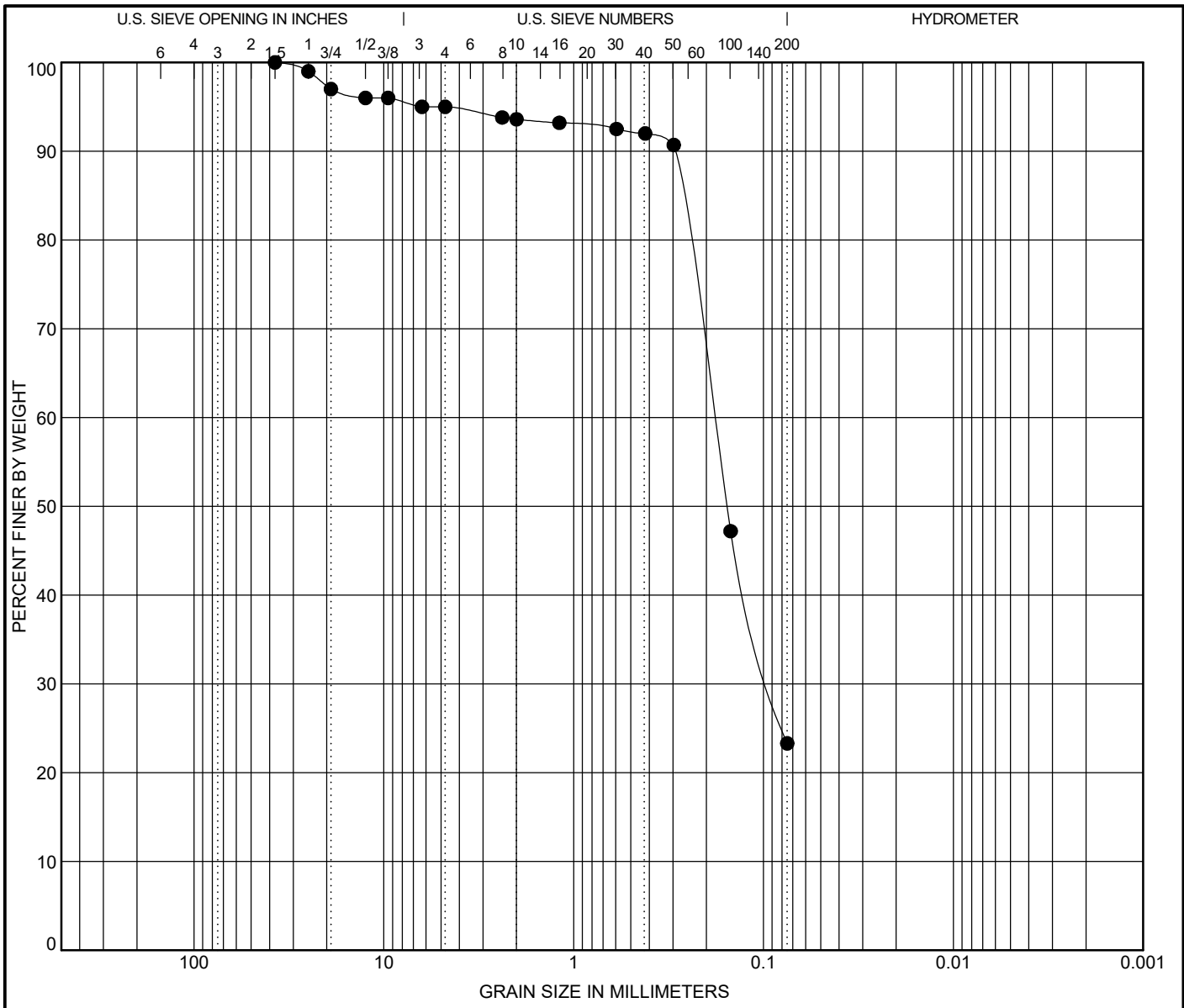


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 24

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
1.5 in	100
1 in	99
3/4 in	97
1/2 in	96
3/8 in	96
1/4 in	95
No. 4	95
No. 8	93.8
No. 10	93.6
No. 16	93.2
No. 30	92.5
No. 40	92
No. 50	90.7
No. 100	47.2
No. 200	23.3

**Specimen Identification**  
B2021-7 - (39 - 41 ft)

Classification				
<b>SILTY SAND(SM)</b>				
LL	PL	PI	Cc	Cu
NV	NV	NP		

% Gravel	% Sand	% Silt	% Clay
5	72	23	

D100	D60	D30	D10
37.5	0.183	0.091	

### GRAIN SIZE DISTRIBUTION

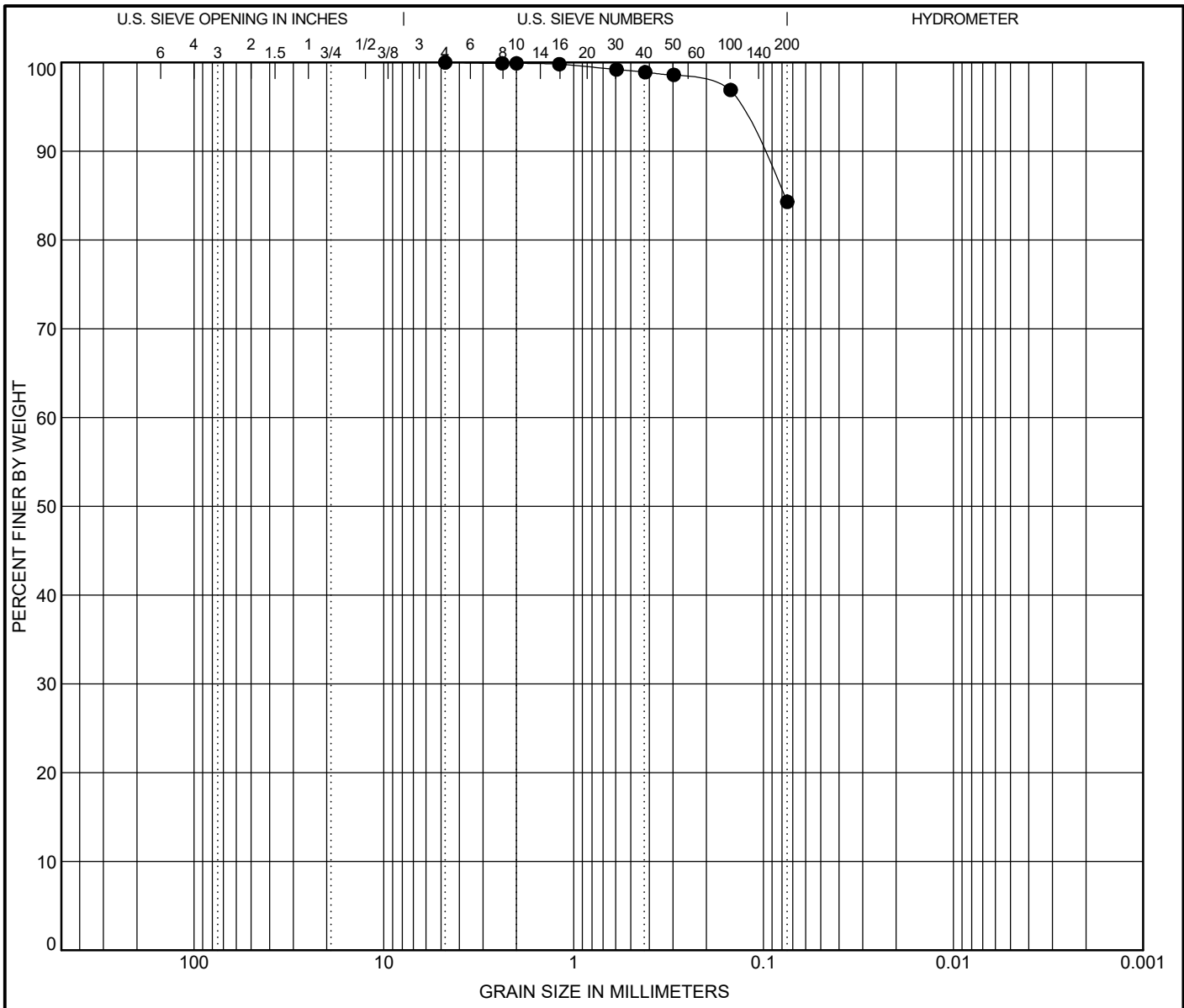


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 25

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 4	100
No. 8	99.9
No. 10	99.9
No. 16	99.8
No. 30	99.2
No. 40	98.9
No. 50	98.6
No. 100	96.9
No. 200	84.3

**Specimen Identification**  
B2021-7 - (59 - 60 ft)

Classification				
<b>SILT with SAND(ML)</b>				
LL	PL	PI	Cc	Cu
<b>NV</b>	<b>NV</b>	<b>NP</b>		

% Gravel	% Sand	% Silt	% Clay
0	16	84	
D100	D60	D30	D10
4.75			

### GRAIN SIZE DISTRIBUTION

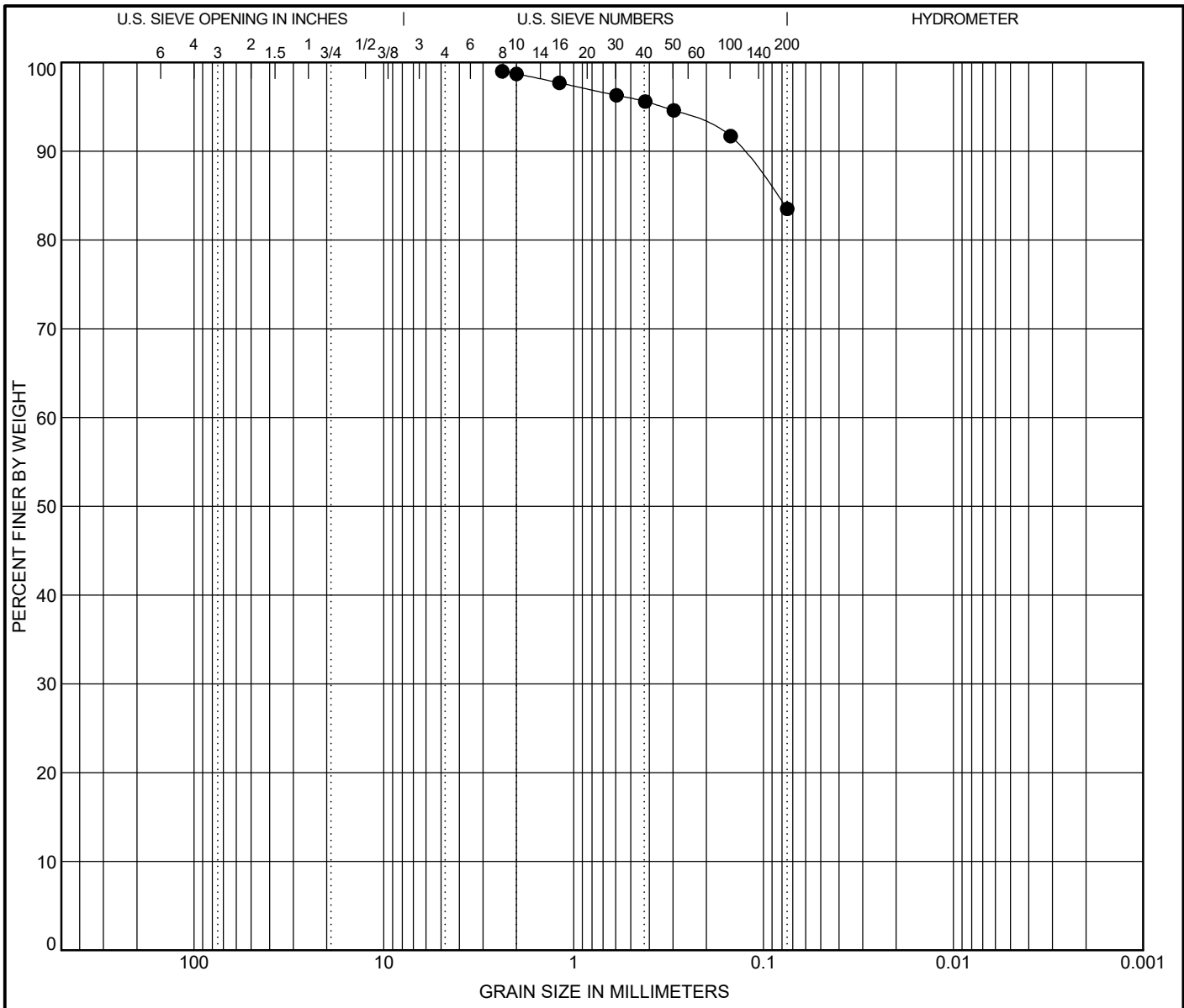
Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022



Figure No. 26

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

SIEVE SIZE	% PASSING
No. 8	99
No. 10	98.7
No. 16	97.7
No. 30	96.3
No. 40	95.6
No. 50	94.6
No. 100	91.7
No. 200	83.5

**Specimen Identification**  
**B2021-8 - (1 - 4 ft)**

Classification				
<b>SILT with SAND(ML)</b>				
LL	PL	PI	Cc	Cu
<b>NV</b>	<b>NV</b>	<b>NP</b>		

% Gravel	% Sand	% Silt	% Clay
0	15	84	

D100	D60	D30	D10
2.38			

**GRAIN SIZE DISTRIBUTION**

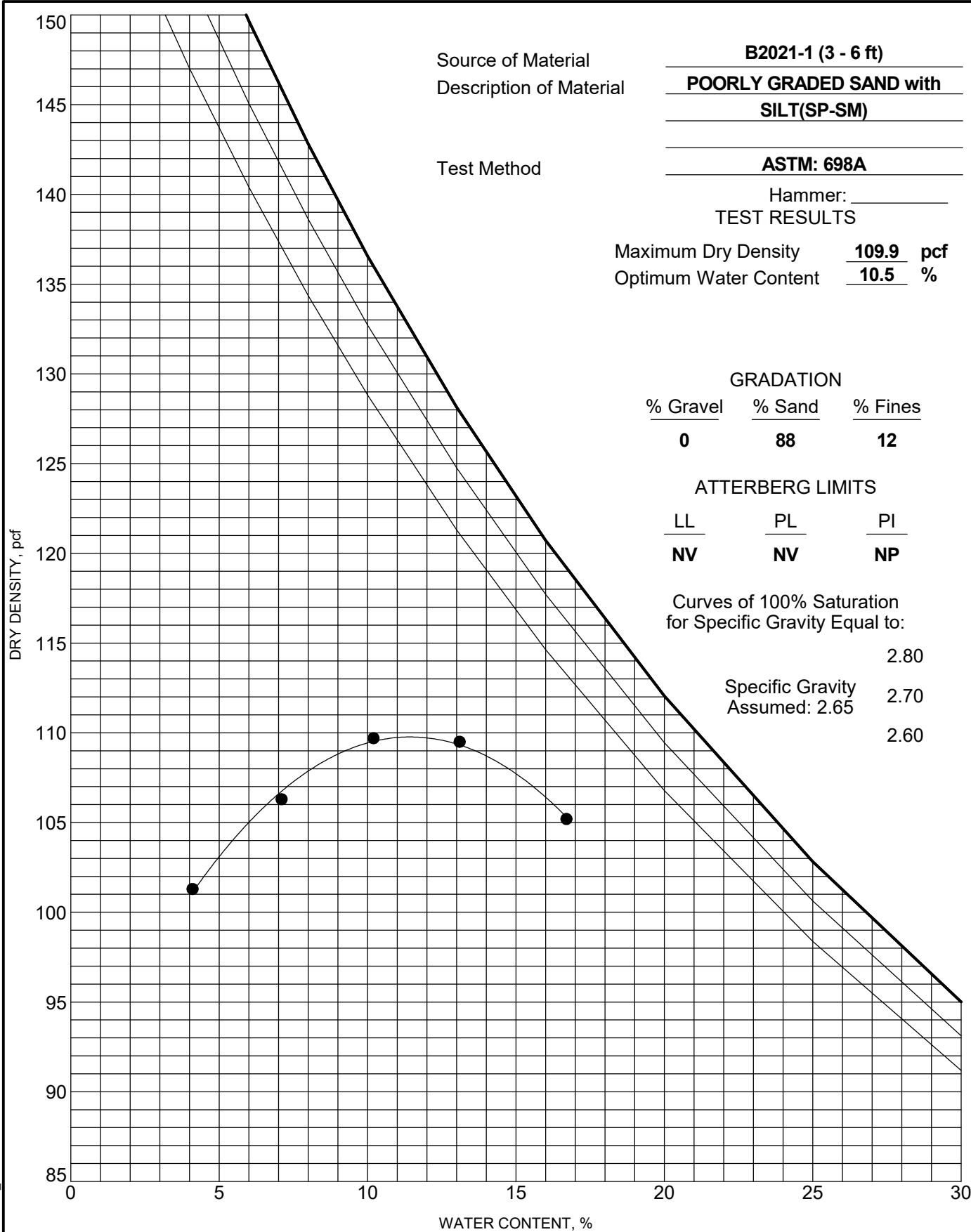


Project: Pickles Butte Sanitary Landfill - Canyon County, ID  
 Location: Refer to site map.  
 Number: 114-571040-2022

Figure No. 27

BORING LOGS.GPJ 6-9-22 TT\_US GRAIN SIZE (SIEVE DATA)

Revised 1-23-08 (MAT)



BORING LOGS: GPJ 6-9-22 TT - COMPACTION W/CURVE



**MOISTURE-DENSITY RELATIONSHIP**

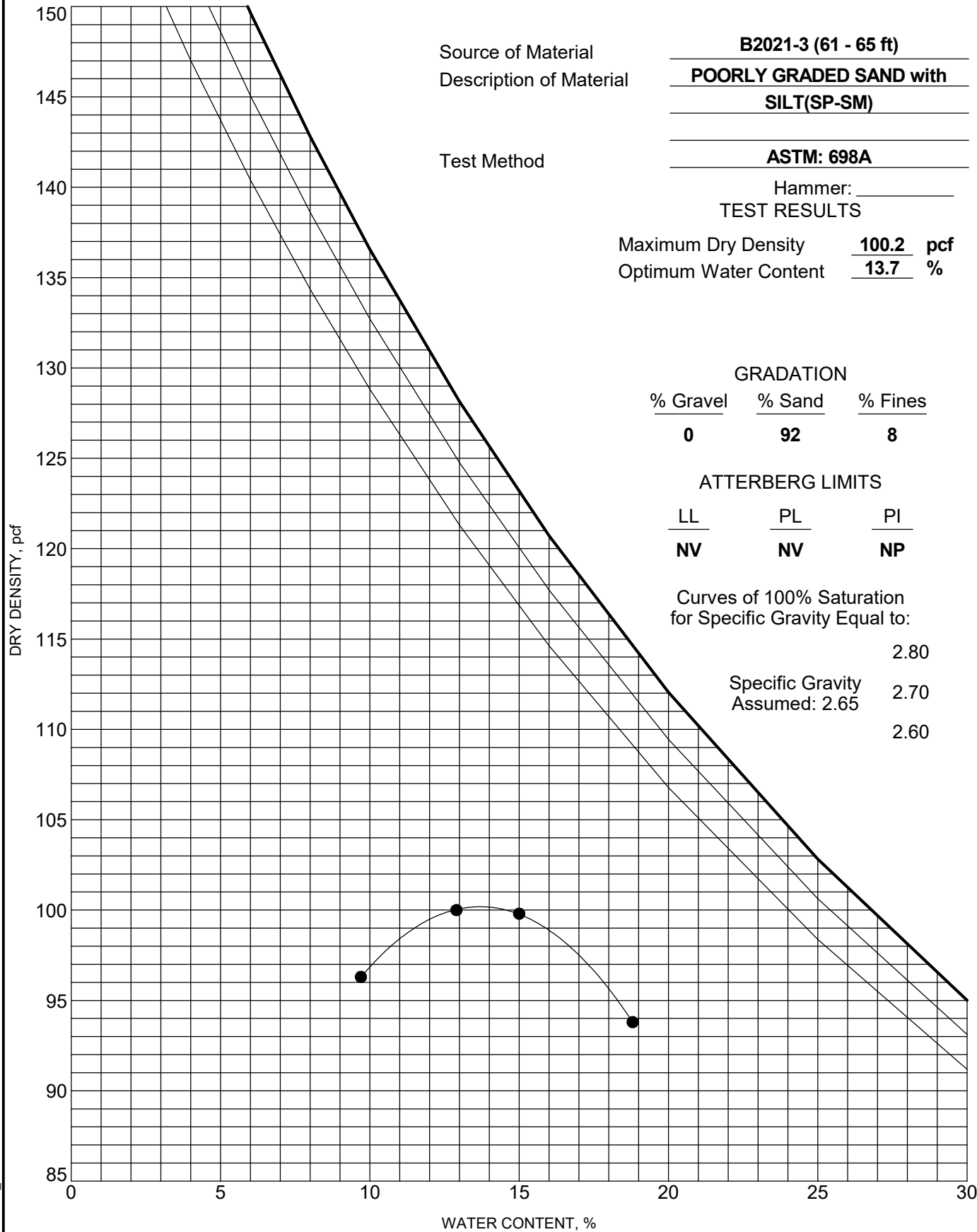
Project: Pickles Butte Sanitary Landfill - Canyon County, ID

Location: Refer to site map.

Number: 114-571040-2022

Figure No. 28

Revised 1-23-08 (MAT)



BORING LOGS.GPJ 6-9-22 TT\_COMPACTON W/CURVE



**MOISTURE-DENSITY RELATIONSHIP**

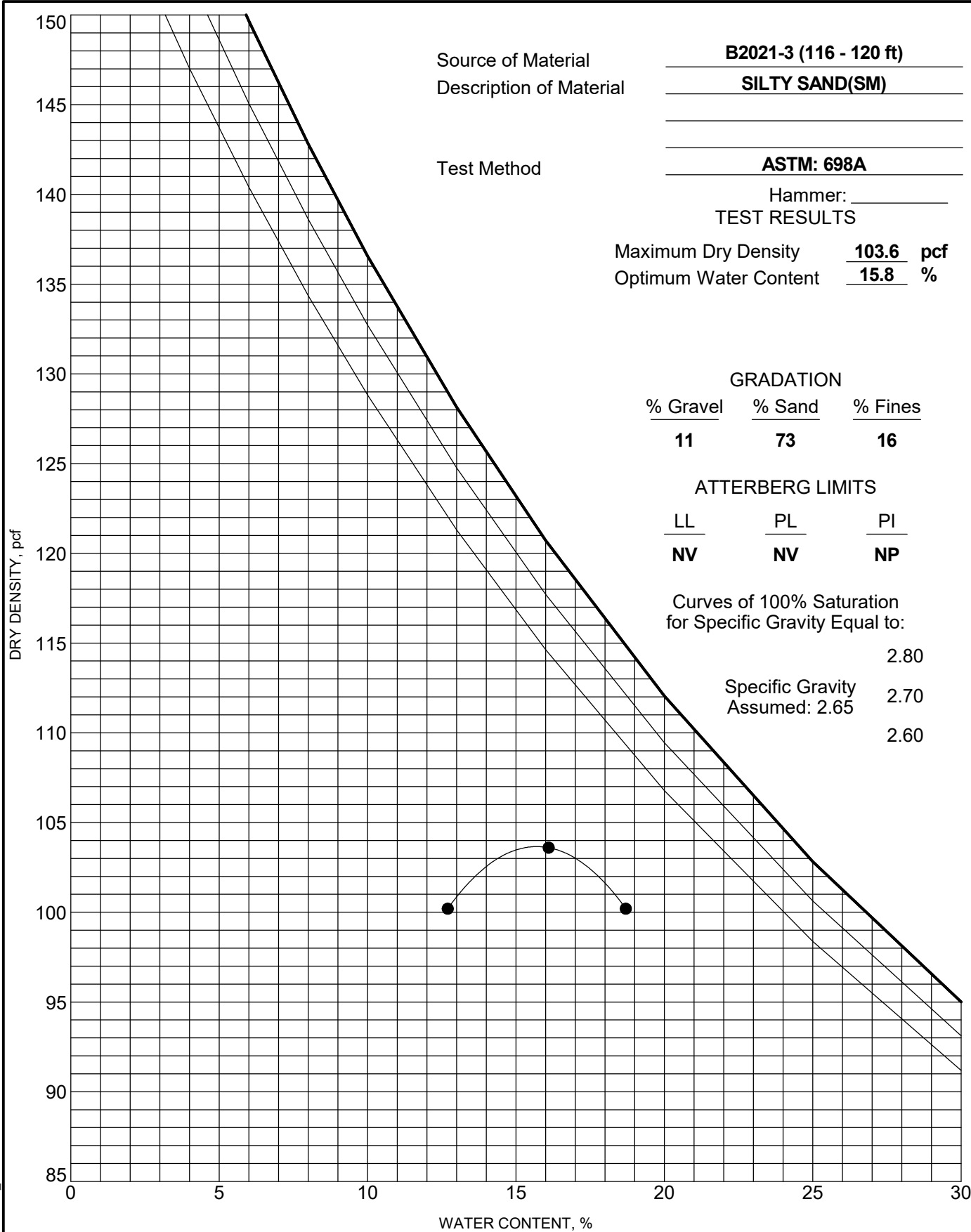
Project: Pickles Butte Sanitary Landfill - Canyon County, ID

Location: Refer to site map.

Number: 114-571040-2022

Figure No. 29





BORING LOGS.GPJ 6-9-22 TT\_COMPACTON W/CURVE



**MOISTURE-DENSITY RELATIONSHIP**

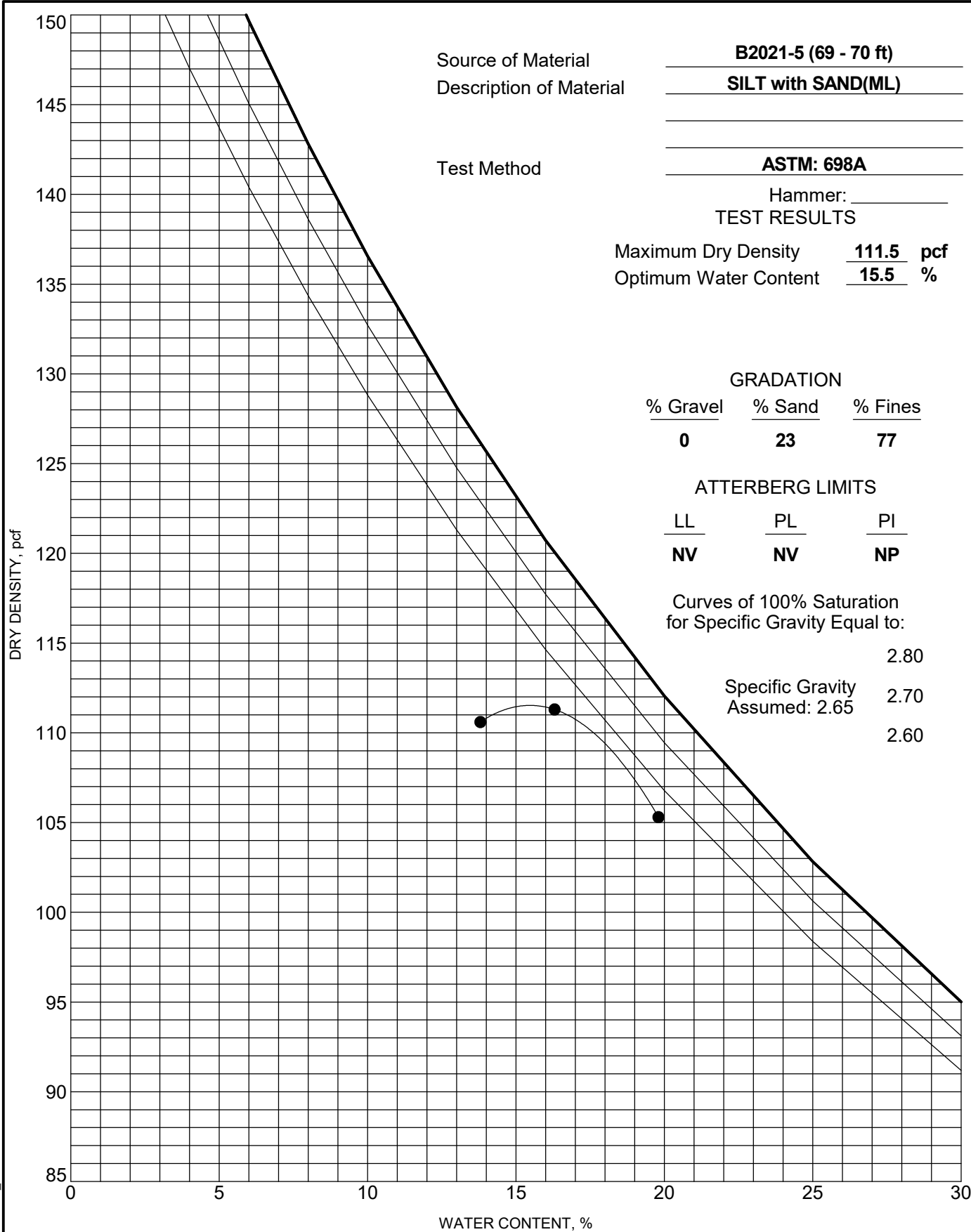
Project: Pickles Butte Sanitary Landfill - Canyon County, ID

Location: Refer to site map.

Number: 114-571040-2022

Figure No. 30

Revised 1-23-08 (MAT)



Source of Material  
Description of Material

**B2021-5 (69 - 70 ft)**  
**SILT with SAND(ML)**

Test Method

**ASTM: 698A**

Hammer: \_\_\_\_\_  
**TEST RESULTS**

Maximum Dry Density **111.5 pcf**  
Optimum Water Content **15.5 %**

**GRADATION**

% Gravel	% Sand	% Fines
<b>0</b>	<b>23</b>	<b>77</b>

**ATTERBERG LIMITS**

LL	PL	PI
<b>NV</b>	<b>NV</b>	<b>NP</b>

Curves of 100% Saturation  
for Specific Gravity Equal to:

2.80
Specific Gravity Assumed: 2.65
2.70
2.60

BORING LOGS.GPJ 6-9-22 TT\_COMPACTON W/CURVE



**MOISTURE-DENSITY RELATIONSHIP**

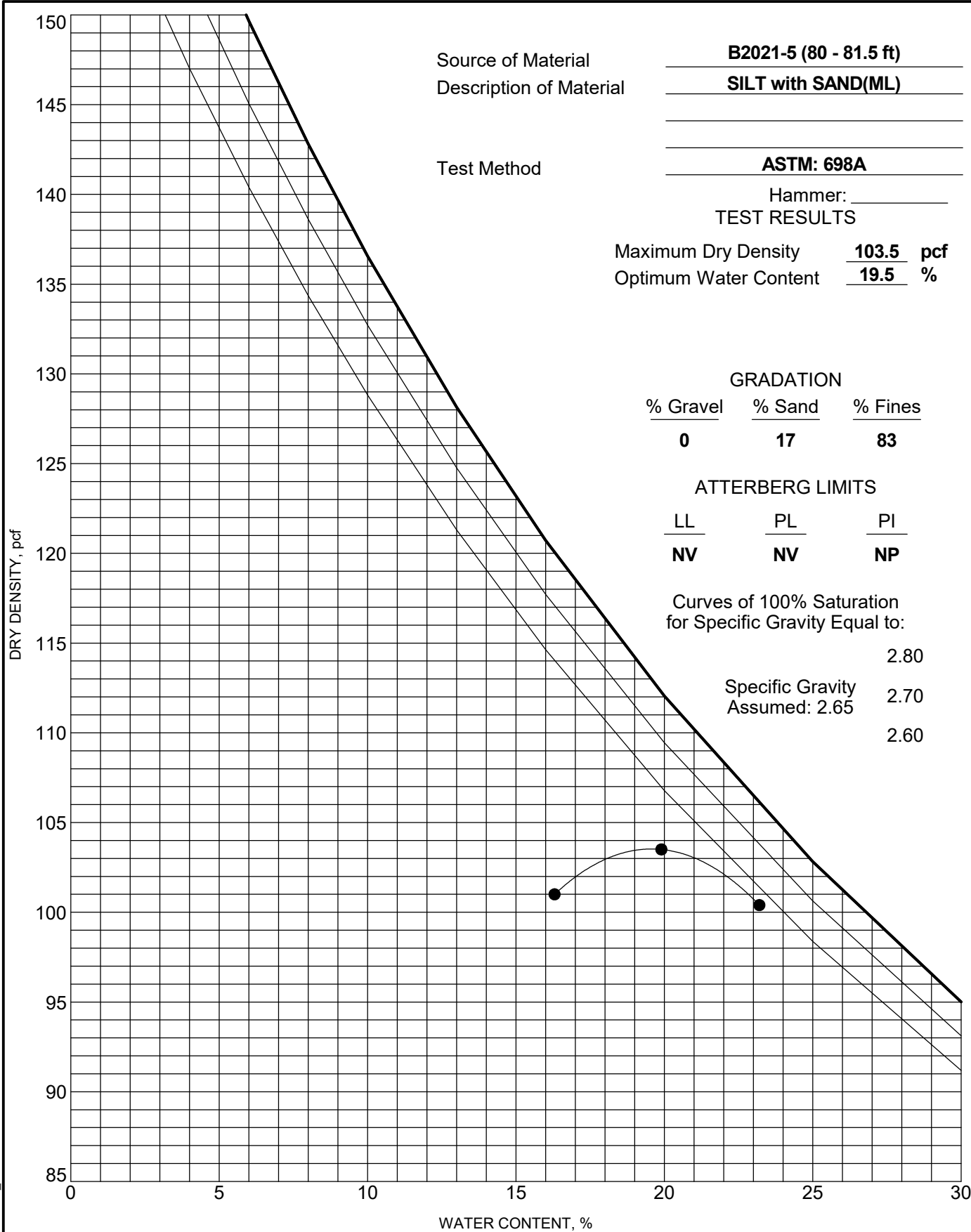
Project: Pickles Butte Sanitary Landfill - Canyon County, ID

Location: Refer to site map.

Number: 114-571040-2022

Figure No. 31

Revised 1-23-08 (MAT)



BORING LOGS.GPJ 6-9-22 TT\_COMPACTON W/CURVE



**MOISTURE-DENSITY RELATIONSHIP**

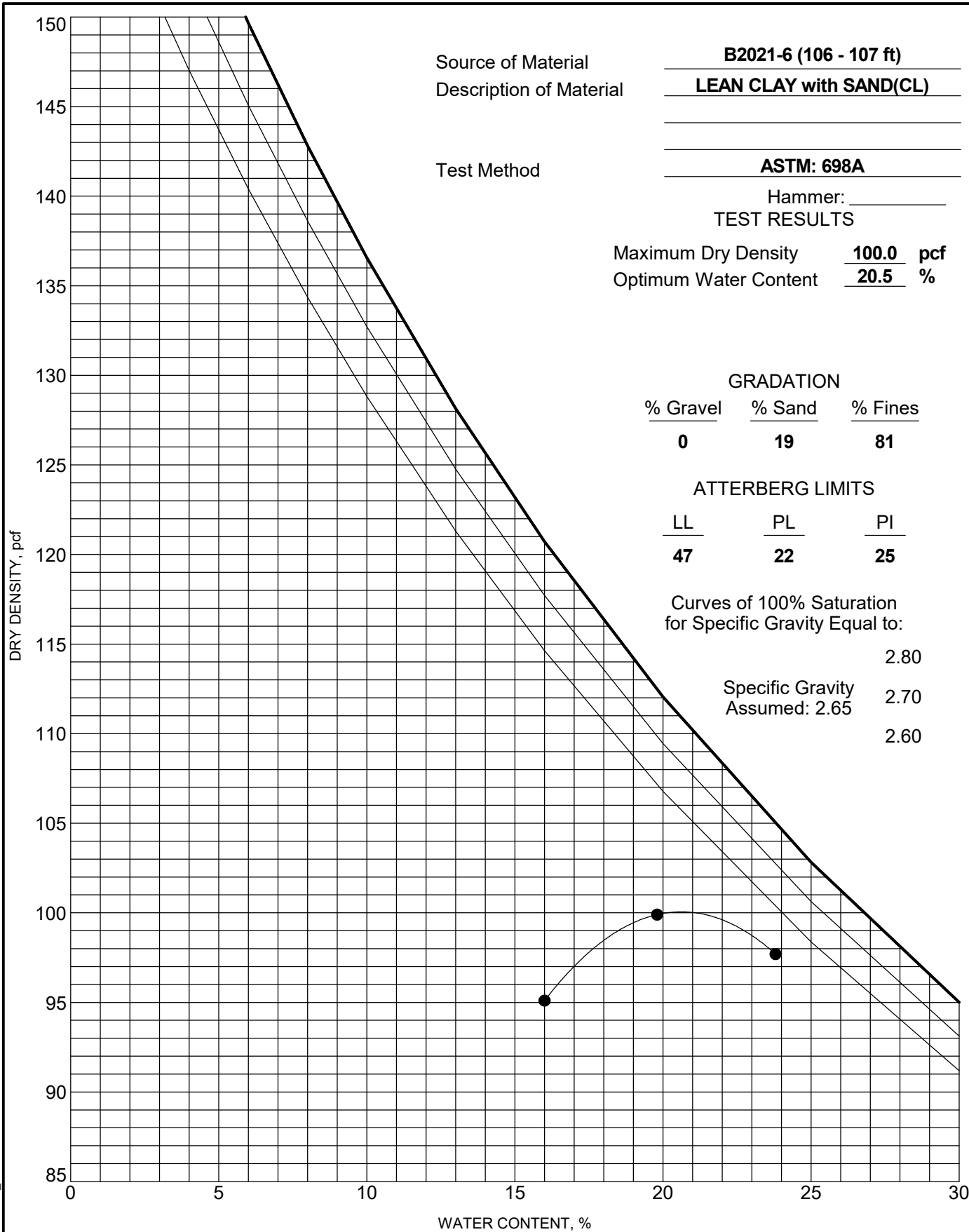
Project: Pickles Butte Sanitary Landfill - Canyon County, ID

Location: Refer to site map.

Number: 114-571040-2022

Figure No. 32

Revised 1-23-08 (MAT)



BORING LOGS.GPJ 6-9-22 TT\_COMPACTON W/CURVE



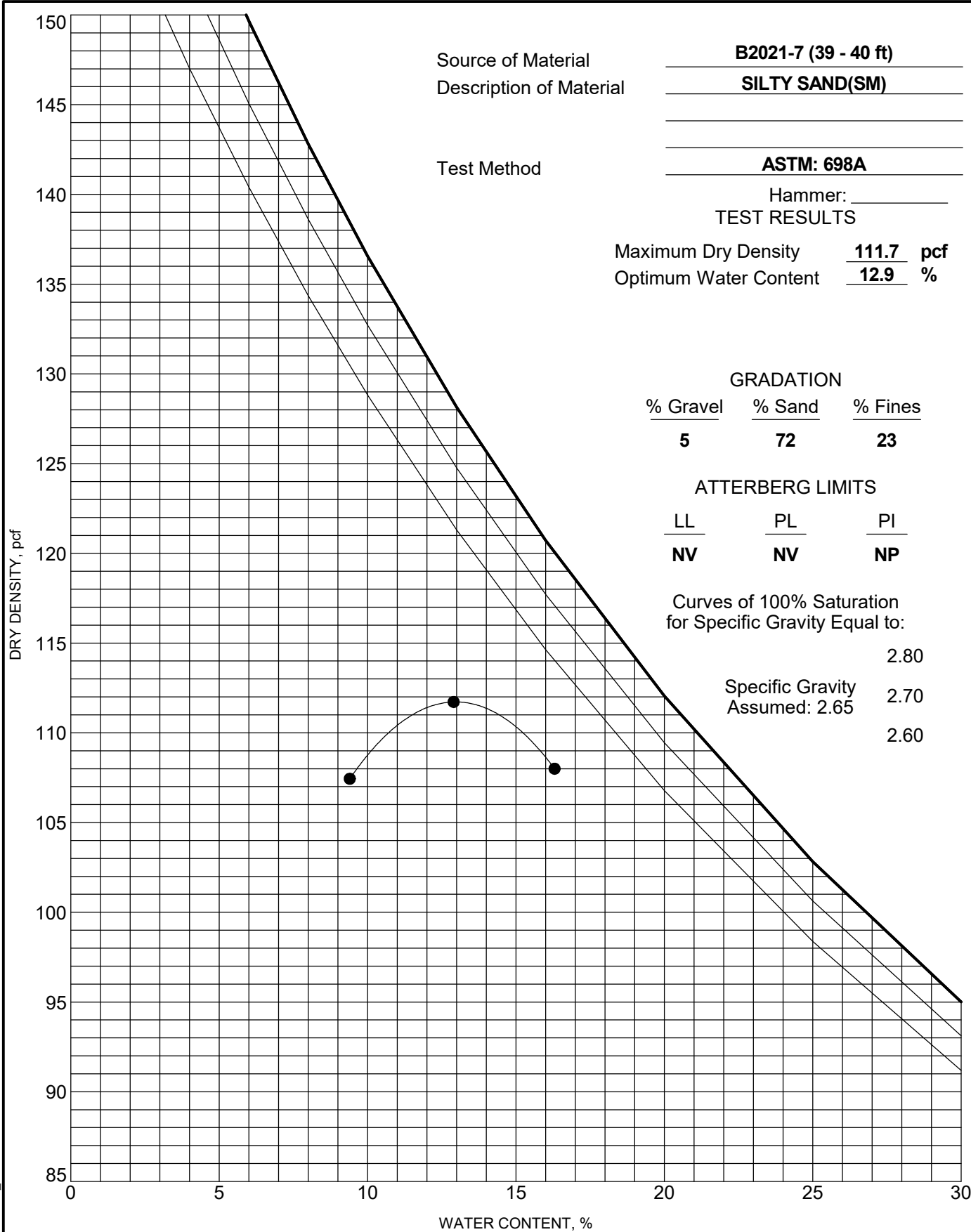
**MOISTURE-DENSITY RELATIONSHIP**

Project: Pickles Butte Sanitary Landfill - Canyon County, ID

Location: Refer to site map.

Number: 114-571040-2022

Figure No. 33



Source of Material  
Description of Material

**B2021-7 (39 - 40 ft)**  
**SILTY SAND(SM)**

Test Method

**ASTM: 698A**

Hammer: \_\_\_\_\_  
**TEST RESULTS**

Maximum Dry Density **111.7 pcf**  
Optimum Water Content **12.9 %**

**GRADATION**

% Gravel	% Sand	% Fines
<b>5</b>	<b>72</b>	<b>23</b>

**ATTERBERG LIMITS**

LL	PL	PI
<b>NV</b>	<b>NV</b>	<b>NP</b>

Curves of 100% Saturation  
for Specific Gravity Equal to:

2.80
Specific Gravity Assumed: 2.65
2.70
2.60

BORING LOGS.GPJ 6-9-22 TT\_COMPACTON W/CURVE



**MOISTURE-DENSITY RELATIONSHIP**

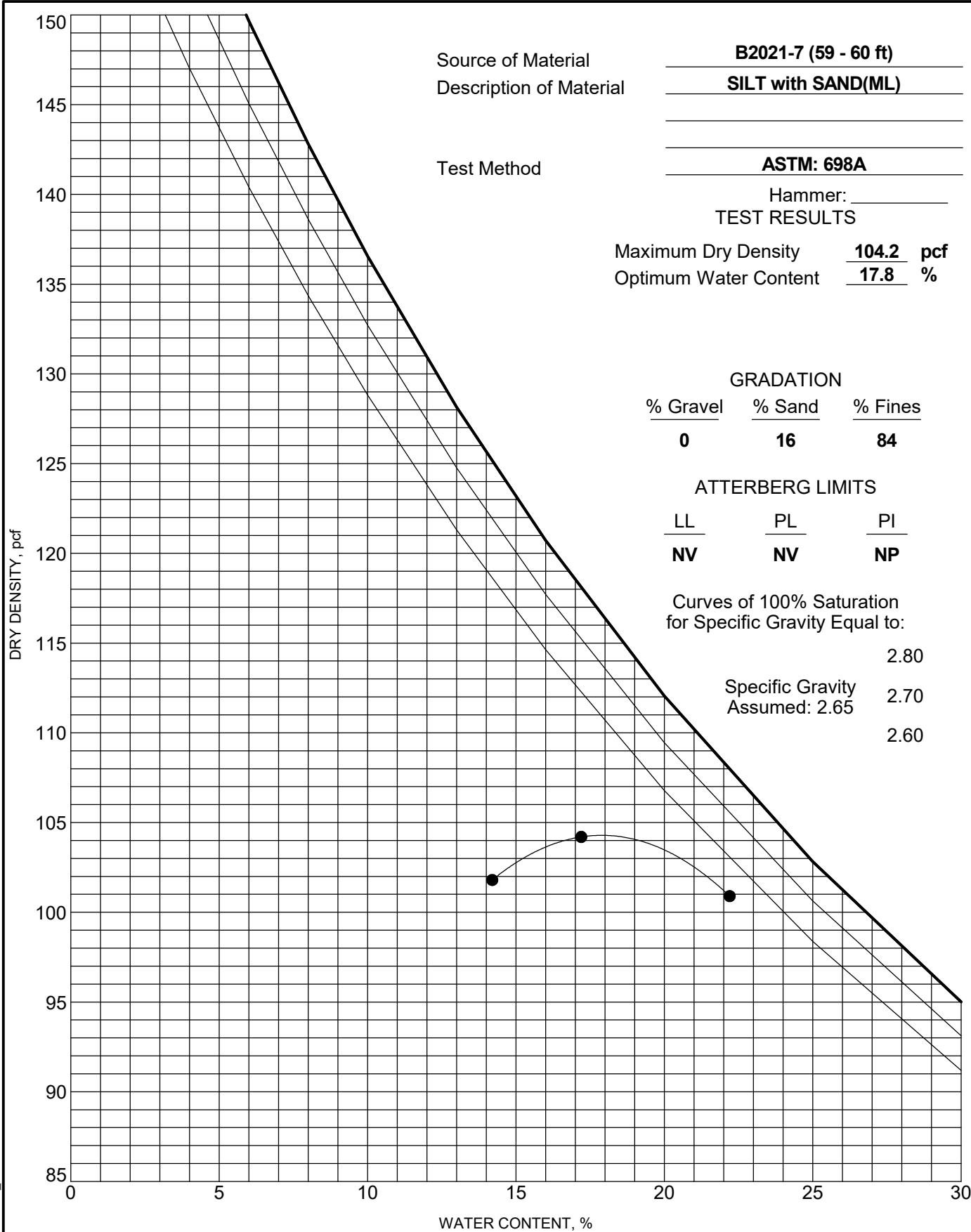
Project: Pickles Butte Sanitary Landfill - Canyon County, ID

Location: Refer to site map.

Number: 114-571040-2022

Figure No. 34

Revised 1-23-08 (MAT)



Source of Material  
Description of Material

**B2021-7 (59 - 60 ft)**  
**SILT with SAND(ML)**

Test Method

**ASTM: 698A**

Hammer: \_\_\_\_\_  
**TEST RESULTS**

Maximum Dry Density **104.2 pcf**  
Optimum Water Content **17.8 %**

**GRADATION**

% Gravel	% Sand	% Fines
<b>0</b>	<b>16</b>	<b>84</b>

**ATTERBERG LIMITS**

LL	PL	PI
<b>NV</b>	<b>NV</b>	<b>NP</b>

Curves of 100% Saturation  
for Specific Gravity Equal to:

2.80
Specific Gravity Assumed: 2.70
2.60

BORING LOGS.GPJ 6-9-22 TT\_COMPACTON W/CURVE



**MOISTURE-DENSITY RELATIONSHIP**

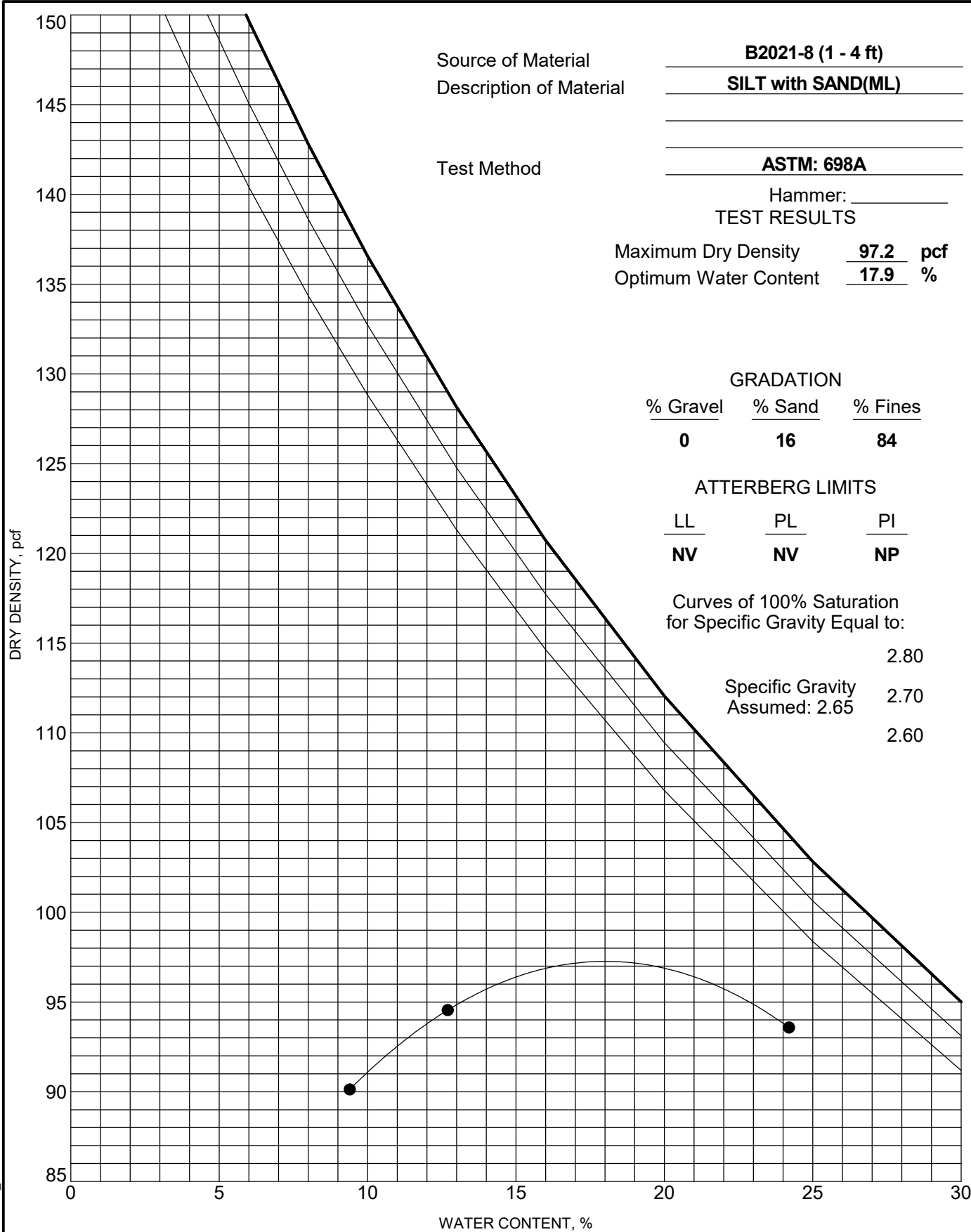
Project: Pickles Butte Sanitary Landfill - Canyon County, ID

Location: Refer to site map.

Number: 114-571040-2022

Figure No. 35

Revised 1-23-08 (MAT)



BORING LOGS: GPJ 6-9-22 TT-COMPACTION W/CURVE



**MOISTURE-DENSITY RELATIONSHIP**

Project: Pickles Butte Sanitary Landfill - Canyon County, ID

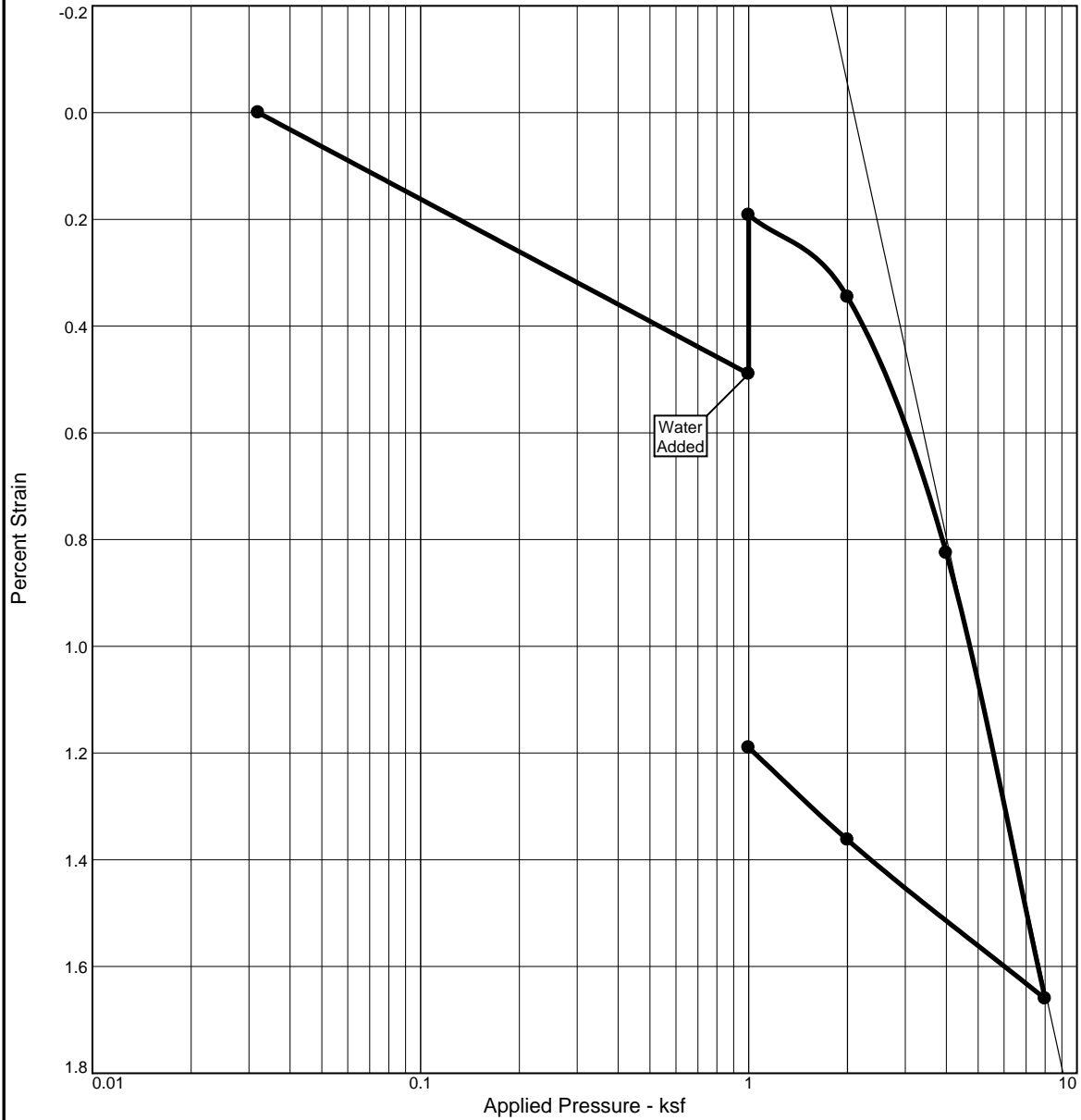
Location: Refer to site map.

Number: 114-571040-2022

Figure No. 36

Revised 1-23-08 (MAT)

# CONSOLIDATION TEST REPORT



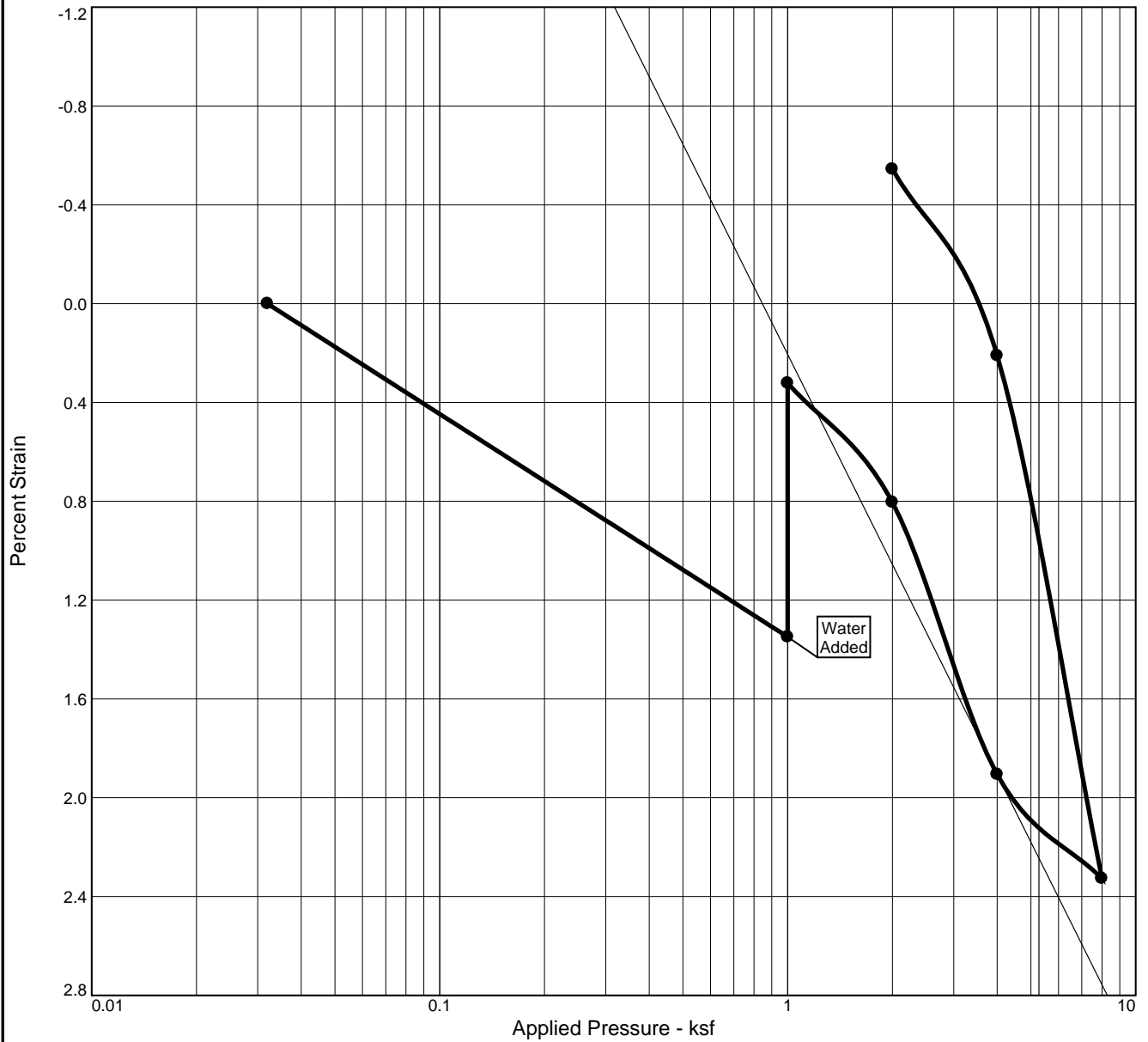
Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (ksf)	P <sub>c</sub> (ksf)	C <sub>c</sub>	C <sub>s</sub>	Swell Press. (ksf)	Swell %	e <sub>0</sub>
Sat.	Moist.											
24.8 %	3.5 %	120.1	NV	NP	2.65		3.0	0.04	0.01	2.6	0.3	0.375

MATERIAL DESCRIPTION	USCS	AASHTO
Silty Sand	SM	

<p><b>Project No.</b> 1145710402022</p> <p><b>Project:</b> Pickles Butte</p> <p><b>Source of Sample:</b> B2021-3      <b>Depth:</b> 25-27 ft</p> <p style="text-align: center;"><b>Tetra Tech</b></p> <p style="text-align: center;"><b>Missoula, MT</b></p>	<p><b>Remarks:</b></p> <p style="text-align: right;"><b>Figure 37</b></p>
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# CONSOLIDATION TEST REPORT

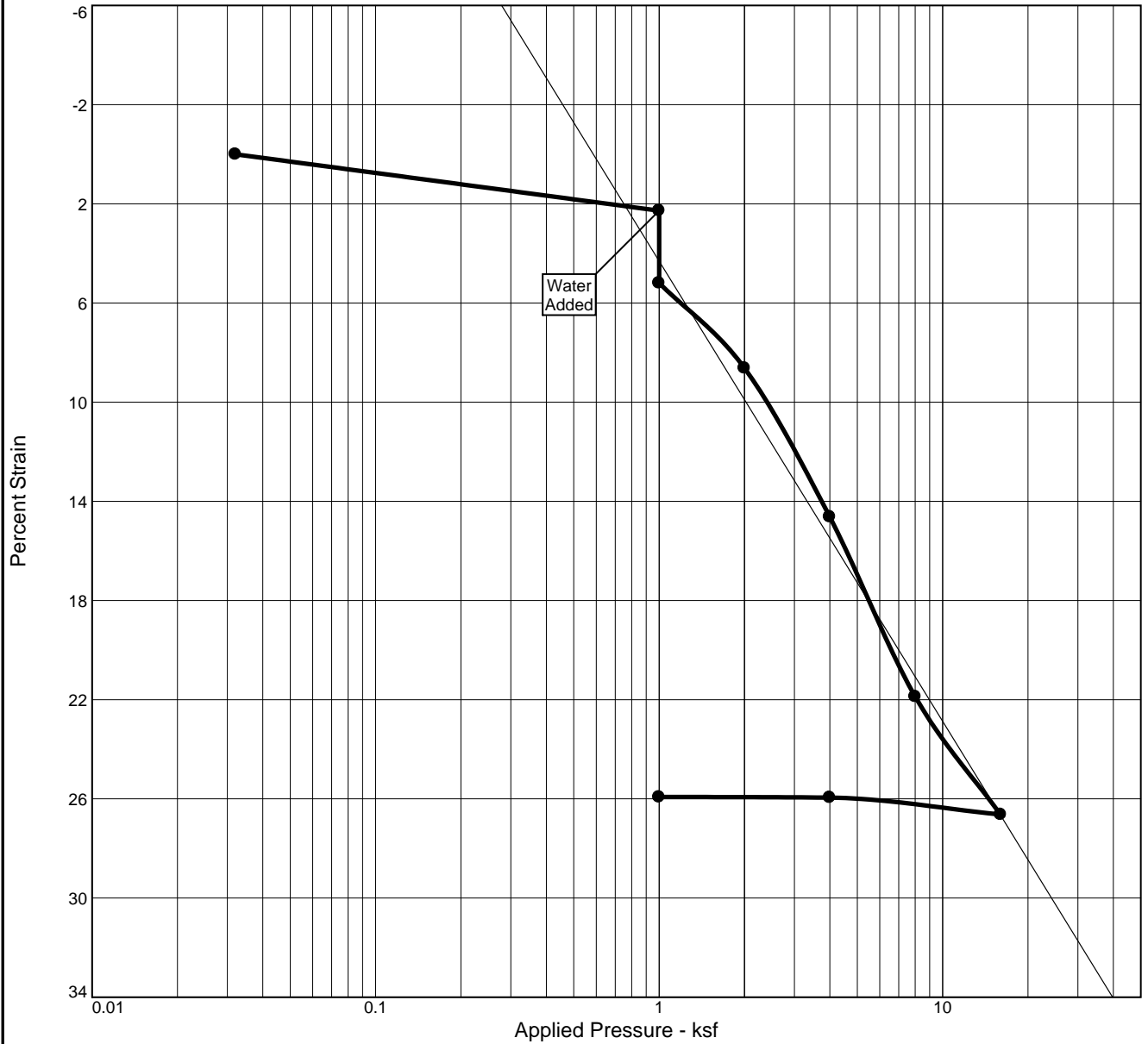


Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (ksf)	P <sub>C</sub> (ksf)	C <sub>C</sub>	C <sub>s</sub>	Swell Press. (ksf)	Swell %	e <sub>o</sub>
Sat.	Moist.											
63.8 %	23.7 %	90.1	54	30	2.65		4.8	0.06	0.09	2.8	1.0	0.984

MATERIAL DESCRIPTION										USCS	AASHTO
Silty Clay										CL-ML	

<p><b>Project No.</b> 1145710402022</p> <p><b>Project:</b> Pickles Butte</p> <p><b>Source of Sample:</b> B2021-5      <b>Depth:</b> 50-51.5 ft</p> <p style="text-align: center;"><b>Tetra Tech</b></p> <p style="text-align: center;"><b>Missoula, MT</b></p>	<p><b>Remarks:</b></p>
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# CONSOLIDATION TEST REPORT

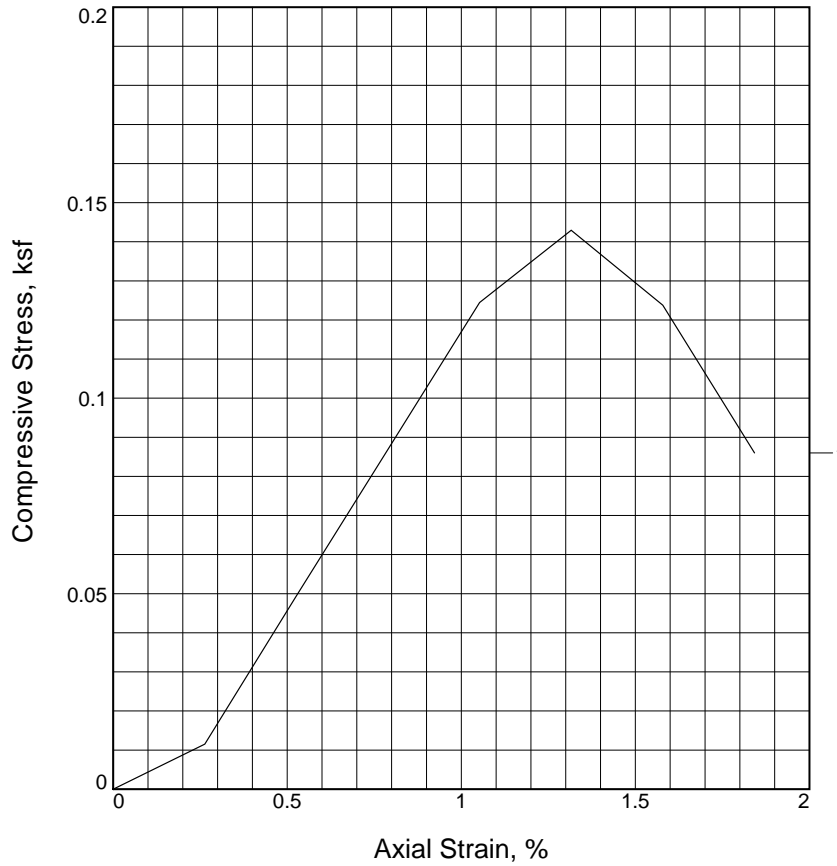


Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (ksf)	P <sub>C</sub> (ksf)	C <sub>C</sub>	C <sub>s</sub>	Swell Press. (ksf)	Clpse. %	e <sub>o</sub>
Sat.	Moist.											
52.0 %	20.4 %	83.5	33	10	2.65		1.5	0.38	0.01	0	2.9	1.038

MATERIAL DESCRIPTION										USCS	AASHTO
Silty Clay										CL-ML	

<p><b>Project No.</b> 1145710402022</p> <p><b>Project:</b> Pickles Butte</p> <p><b>Source of Sample:</b> B2021-7      <b>Depth:</b> 120-121.3 ft</p> <p style="text-align: center;"><b>Tetra Tech</b></p> <p style="text-align: center;"><b>Missoula, MT</b></p>	<p><b>Remarks:</b></p>
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# UNCONFINED COMPRESSION TEST



Sample No.	1		
Unconfined strength, ksf	0.143		
Undrained shear strength, ksf	0.071		
Failure strain, %	1.3		
Strain rate, in./min.	0.030		
Water content, %	8.3		
Wet density, pcf	103.1		
Dry density, pcf	95.2		
Saturation, %	29.7		
Void ratio	0.7369		
Specimen diameter, in.	2.790		
Specimen height, in.	5.700		
Height/diameter ratio	2.04		

**Description:** bulk

LL = NV    PL = NV    PI = NV    Assumed GS= 2.65    Type: SP

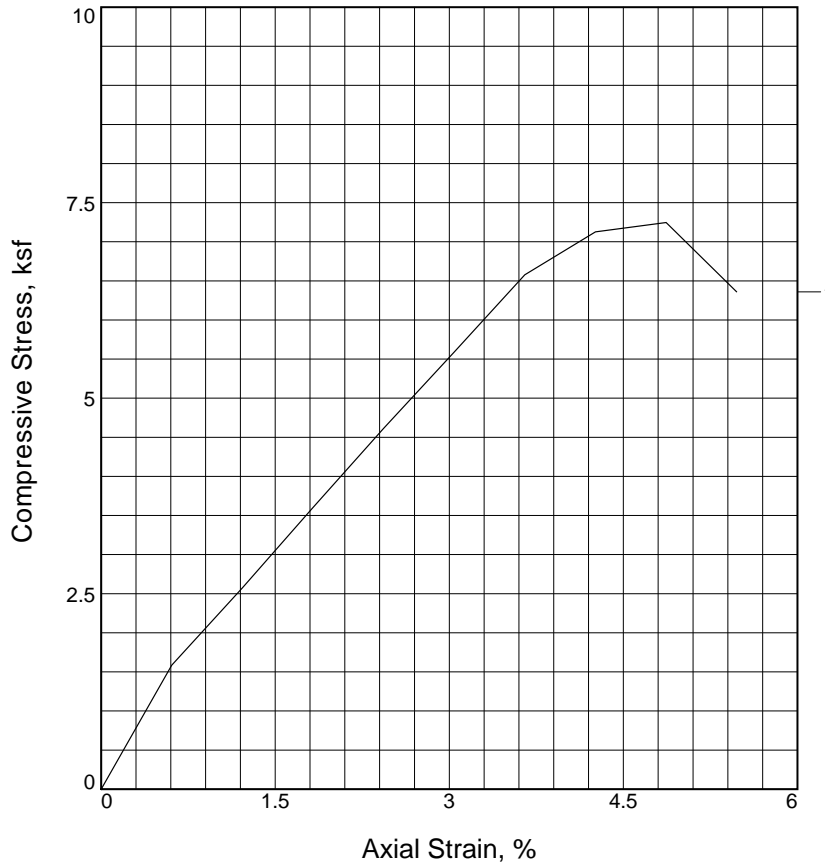
**Project No.:** 1145710402022  
**Date Sampled:**  
**Remarks:**

**Project:** Pickles Butte  
**Source of Sample:** B2021-3  
**Depth:** 61-65 ft

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UNCONFINED COMPRESSION TEST  
 Tetra Tech  
 Missoula, MT

# UNCONFINED COMPRESSION TEST



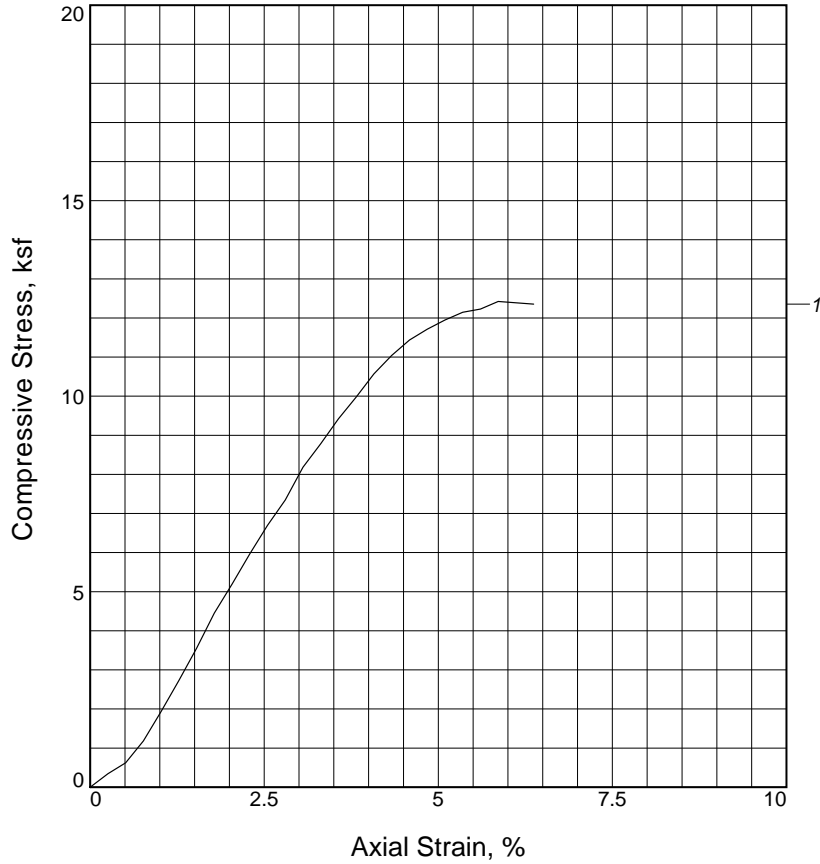
Sample No.	1			
Unconfined strength, ksf	7.246			
Undrained shear strength, ksf	3.623			
Failure strain, %	4.9			
Strain rate, in./min.	0.060			
Water content, %	24.0			
Wet density, pcf	119.4			
Dry density, pcf	96.3			
Saturation, %	88.5			
Void ratio	0.7184			
Specimen diameter, in.	2.450			
Specimen height, in.	4.930			
Height/diameter ratio	2.01			

**Description:** Special

LL = N/A	PL = N/A	PI = N/A	Assumed GS= 2.65	Type: ML
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<p><b>Project No.:</b> 1145710402022</p> <p><b>Date Sampled:</b></p> <p><b>Remarks:</b></p>	<p><b>Project:</b> Pickles Butte</p> <p><b>Source of Sample:</b> B2021-6</p> <p style="text-align: right;"><b>Depth:</b> 57-58 ft</p> <hr/> <p style="text-align: center;">UNCONFINED COMPRESSION TEST Tetra Tech Missoula, MT</p>
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# UNCONFINED COMPRESSION TEST



Sample No.	1		
Unconfined strength, ksf	12.421		
Undrained shear strength, ksf	6.211		
Failure strain, %	5.9		
Strain rate, in./min.	0.020		
Water content, %	24.6		
Wet density, pcf	124.9		
Dry density, pcf	100.2		
Saturation, %	100.3		
Void ratio	0.6508		
Specimen diameter, in.	1.918		
Specimen height, in.	3.925		
Height/diameter ratio	2.05		

**Description:** Special

**LL = 67    PL = 19    PI = 48    Assumed GS= 2.65    Type: CH**

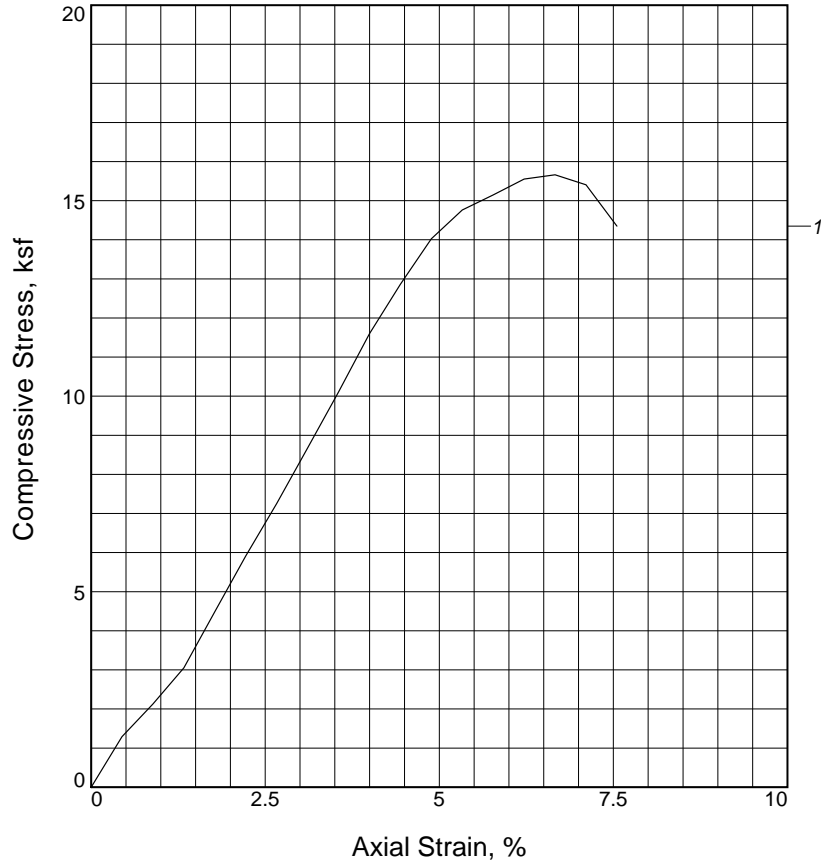
**Project No.:** 1145710402022  
**Date Sampled:**  
**Remarks:**

**Figure** 42

**Project:** Pickles Butte  
**Source of Sample:** B2021-6  
**Depth:** 79-81 ft

UNCONFINED COMPRESSION TEST  
 Tetra Tech  
 Missoula, MT

# UNCONFINED COMPRESSION TEST



Sample No.	1		
Unconfined strength, ksf	15.661		
Undrained shear strength, ksf	7.831		
Failure strain, %	6.7		
Strain rate, in./min.	0.050		
Water content, %	22.8		
Wet density, pcf	122.8		
Dry density, pcf	100.0		
Saturation, %	92.4		
Void ratio	0.6550		
Specimen diameter, in.	2.473		
Specimen height, in.	5.629		
Height/diameter ratio	2.28		

**Description:** Special

**LL = 56**    **PL = 22**    **PI = 34**    **Assumed GS= 2.65**    **Type: CH**

**Project No.:** 1145710402022

**Date Sampled:**

**Remarks:**

**Project:** Pickles Butte

**Source of Sample:** B2021-6

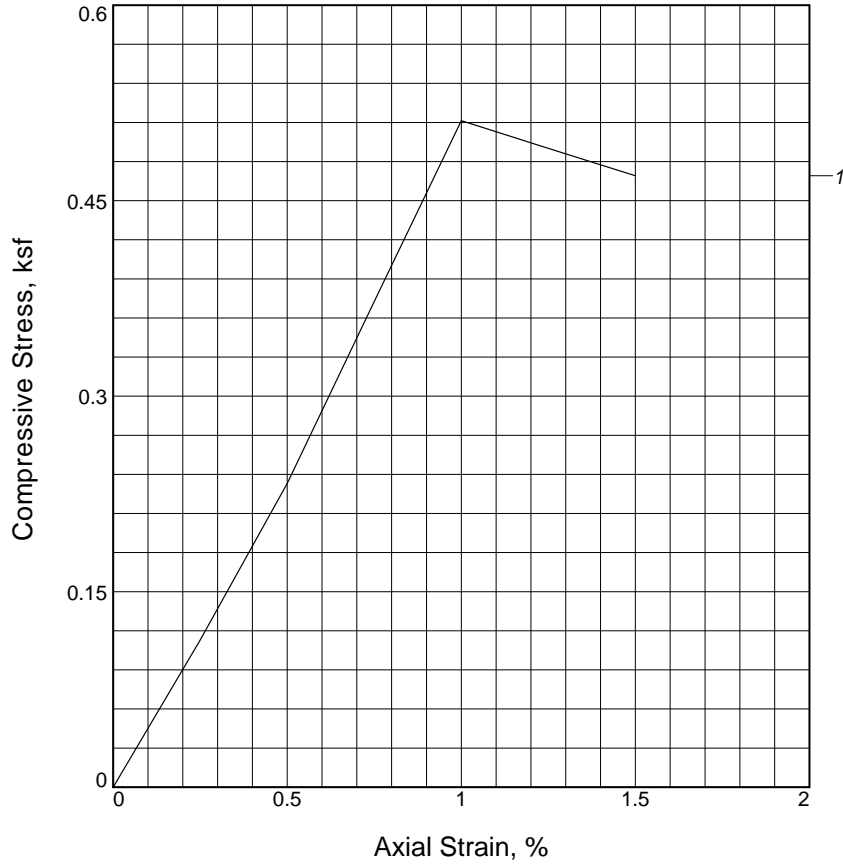
**Depth:** 99-102 ft

UNCONFINED COMPRESSION TEST

Tetra Tech  
Missoula, MT

**Figure** 43

# UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, ksf	0.511			
Undrained shear strength, ksf	0.256			
Failure strain, %	1.0			
Strain rate, in./min.	0.030			
Water content, %	4.5			
Wet density, pcf	109.9			
Dry density, pcf	105.2			
Saturation, %	20.8			
Void ratio	0.5722			
Specimen diameter, in.	2.710			
Specimen height, in.	6.000			
Height/diameter ratio	2.21			

**Description:** grab

LL = NV    PL = NV    PI = NV    Assumed GS= 2.65    Type: SP

**Project No.:** 1145710402022

**Date Sampled:**

**Remarks:**

**Project:** 'Pickles Butte'

**Source of Sample:** B2021-7

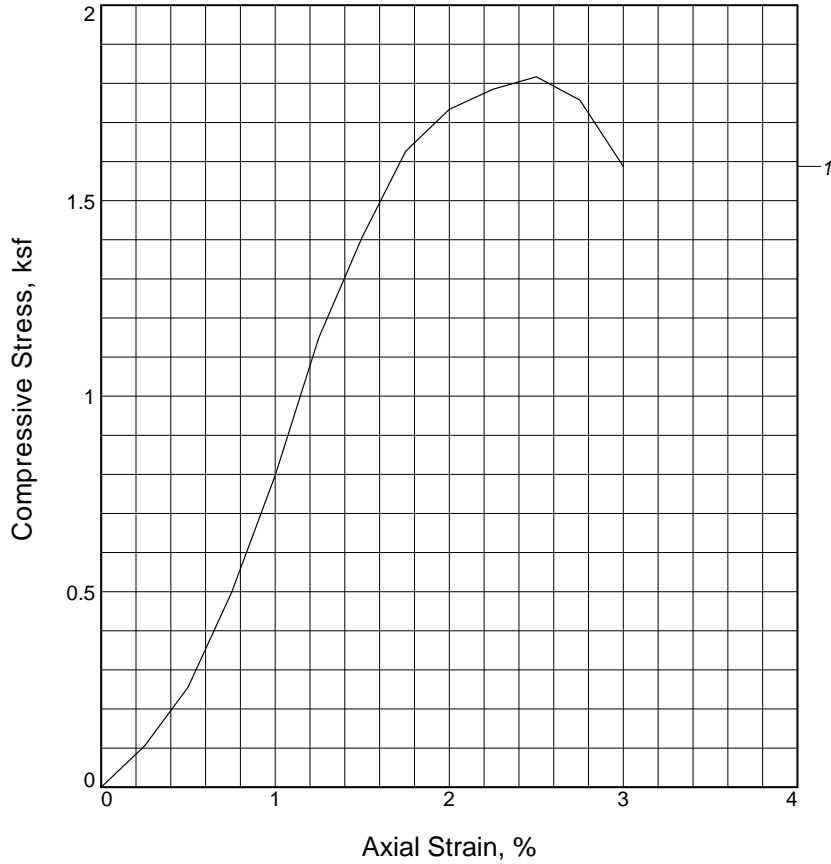
**Depth:** 39-40 ft

UNCONFINED COMPRESSION TEST

Tetra Tech  
Missoula, MT

**Figure**    44

# UNCONFINED COMPRESSION TEST



Sample No.	1		
Unconfined strength, ksf	1.817		
Undrained shear strength, ksf	0.908		
Failure strain, %	2.5		
Strain rate, in./min.	0.030		
Water content, %	19.9		
Wet density, pcf	112.4		
Dry density, pcf	93.8		
Saturation, %	68.9		
Void ratio	0.7646		
Specimen diameter, in.	2.800		
Specimen height, in.	6.000		
Height/diameter ratio	2.14		

**Description:** grab

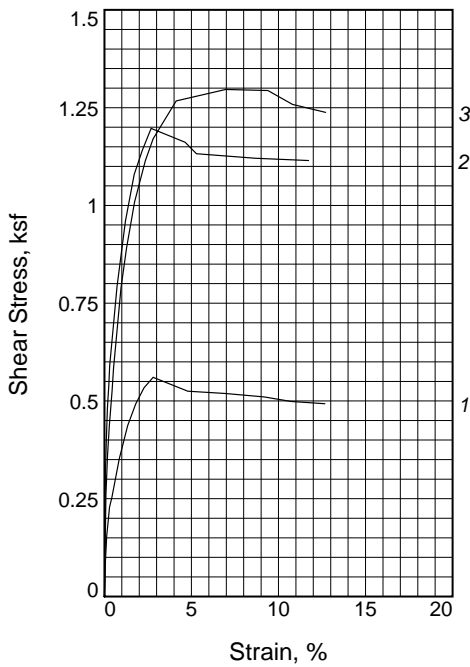
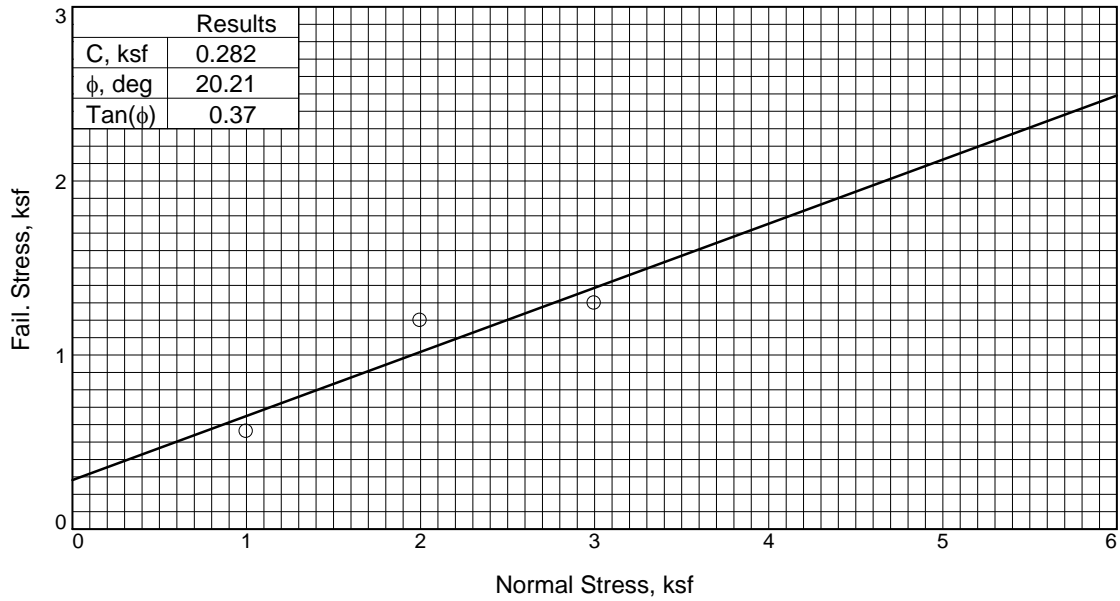
LL = NV    PL = NV    PI = NV    Assumed GS= 2.65    Type: ML

**Project No.:** 1145710402022  
**Date Sampled:**  
**Remarks:**

**Project:** Pickles Butte  
**Source of Sample:** B2021-7  
**Depth:** 59-60 ft

UNCONFINED COMPRESSION TEST  
 Tetra Tech  
 Missoula, MT





Sample No.	1	2	3	
Initial	Water Content, %	12.2	11.6	12.3
	Dry Density, pcf	104.5	106.4	101.5
	Saturation, %	55.7	55.5	51.6
	Void Ratio	0.5829	0.5554	0.6306
	Diameter, in.	2.500	2.500	2.500
	Height, in.	1.210	1.200	1.259
At Test	Water Content, %	16.4	17.4	18.2
	Dry Density, pcf	104.6	106.6	104.8
	Saturation, %	74.7	83.4	83.5
	Void Ratio	0.5816	0.5524	0.5787
	Diameter, in.	2.500	2.500	2.500
	Height, in.	1.209	1.198	1.219
Normal Stress, ksf	1.000	2.000	3.000	
Fail. Stress, ksf	0.560	1.197	1.297	
Strain, %	2.8	2.7	7.0	
Ult. Stress, ksf				
Strain, %				
Strain rate, in./min.	0.001	0.001	0.001	

**Sample Type:** Shelby  
**Description:** Silty Sand

**Assumed Specific Gravity=** 2.65  
**Remarks:** Remolded

**Project:** Pickles Butte

**Source of Sample:** B2021-3

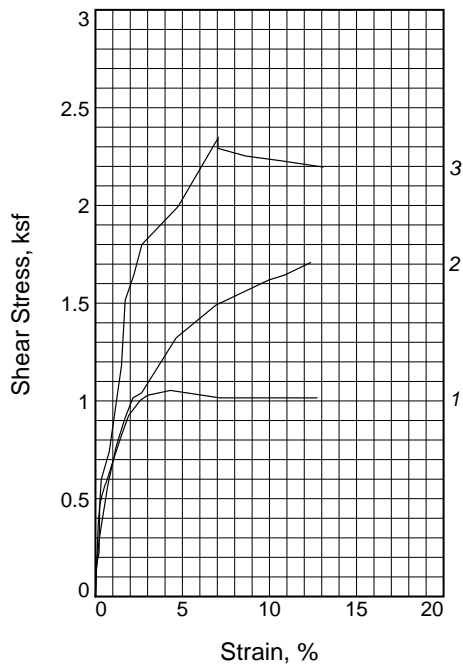
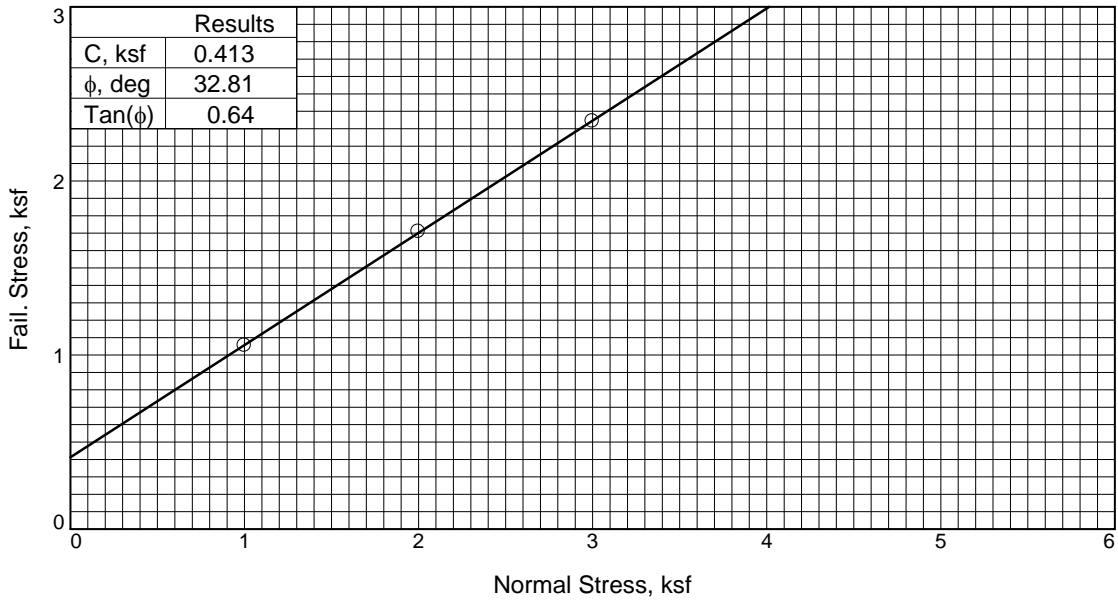
**Proj. No.:** 1145710402022

**Depth:** 60-62 ft

**Date Sampled:**

DIRECT SHEAR TEST REPORT

Tetra Tech  
 Missoula, MT



Sample No.	1	2	3	
Initial	Water Content, %	13.7	12.8	13.0
	Dry Density, pcf	104.1	92.2	84.3
	Saturation, %	61.7	42.7	35.9
	Void Ratio	0.5892	0.7944	0.9626
	Diameter, in.	2.410	2.410	2.400
	Height, in.	0.934	1.068	1.240
At Test	Water Content, %	21.2	22.3	20.2
	Dry Density, pcf	105.2	96.7	84.8
	Saturation, %	98.1	83.1	56.4
	Void Ratio	0.5722	0.7104	0.9499
	Diameter, in.	2.410	2.410	2.400
	Height, in.	0.924	1.018	1.232
Normal Stress, ksf	1.000	2.000	3.000	
Fail. Stress, ksf	1.054	1.708	2.343	
Strain, %	4.3	12.4	7.0	
Ult. Stress, ksf				
Strain, %				
Strain rate, in./min.	0.001	0.001	0.001	

**Sample Type:** Shelby  
**Description:** Silty Sand

**Assumed Specific Gravity=** 2.65  
**Remarks:** Remolded

**Project:** Pickles Butte

**Source of Sample:** B2021-3

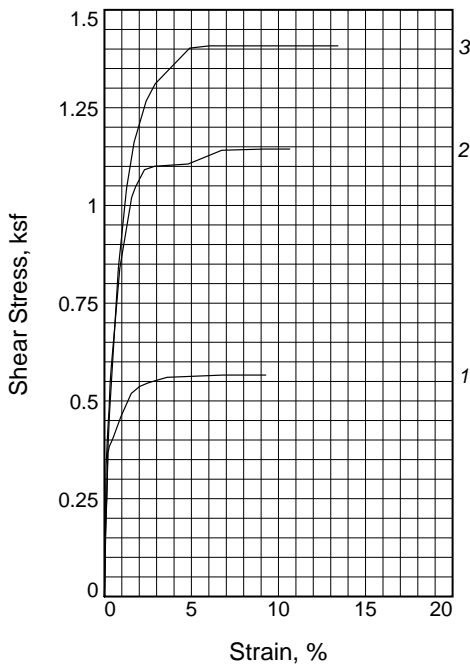
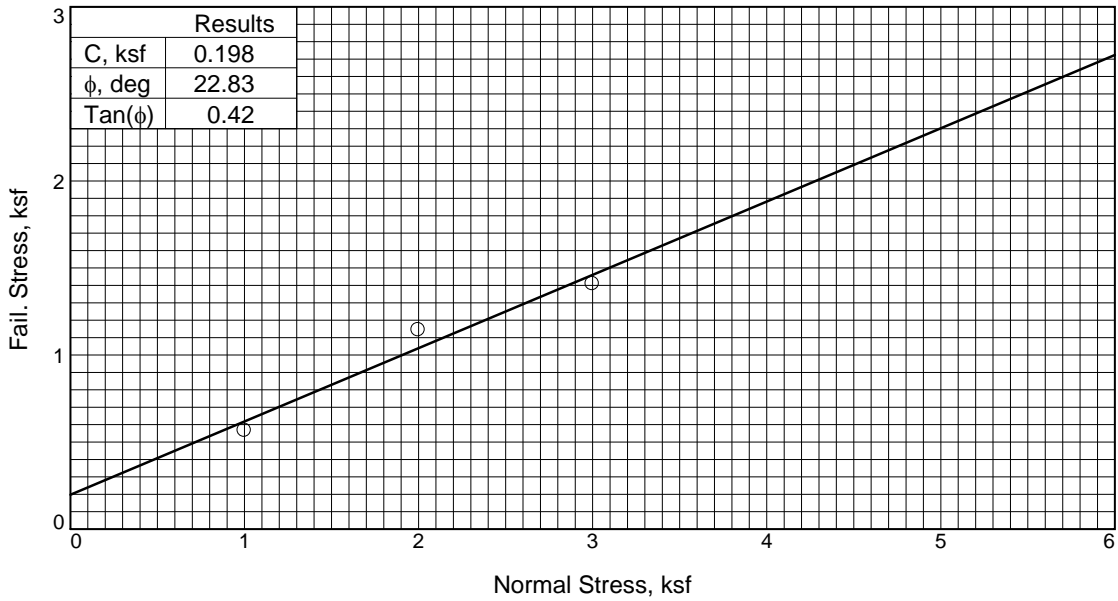
**Proj. No.:** 1145710402022

**Depth:** 80-82 ft

**Date Sampled:**

DIRECT SHEAR TEST REPORT

Tetra Tech  
 Missoula, MT



Sample No.	1	2	3	
Initial	Water Content, %	15.0	15.0	15.0
	Dry Density, pcf	97.7	89.6	96.1
	Saturation, %	57.4	47.0	55.1
	Void Ratio	0.6932	0.8458	0.7217
	Diameter, in.	2.500	2.500	2.500
	Height, in.	1.210	1.310	1.210
At Test	Water Content, %	29.0	29.5	28.0
	Dry Density, pcf	97.8	89.9	96.3
	Saturation, %	111.2	93.0	103.2
	Void Ratio	0.6910	0.8400	0.7180
	Diameter, in.	2.500	2.500	2.500
	Height, in.	1.208	1.306	1.207
Normal Stress, ksf	1.000	2.000	3.000	
Fail. Stress, ksf	0.566	1.144	1.408	
Strain, %	6.8	9.2	6.0	
Ult. Stress, ksf				
Strain, %				
Strain rate, in./min.	0.001	0.001	0.001	

**Sample Type:** MC

**Description:** Silty Sand

**LL=** NV

**PI=** NP

**Assumed Specific Gravity=** 2.65

**Remarks:**

**Project:** Pickles Butte

**Source of Sample:** B2021-4

**Proj. No.:** 1145710402022

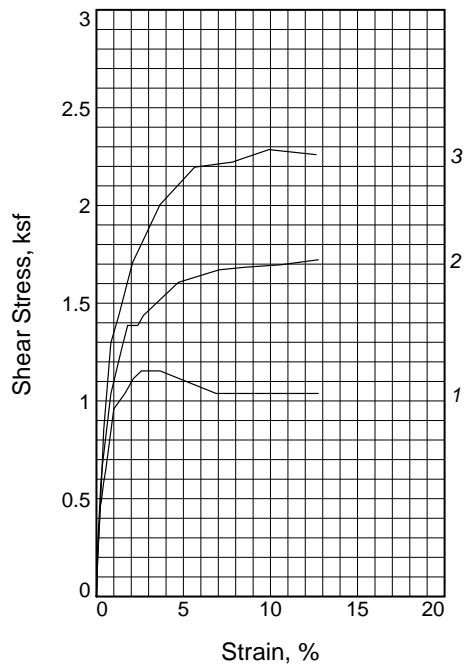
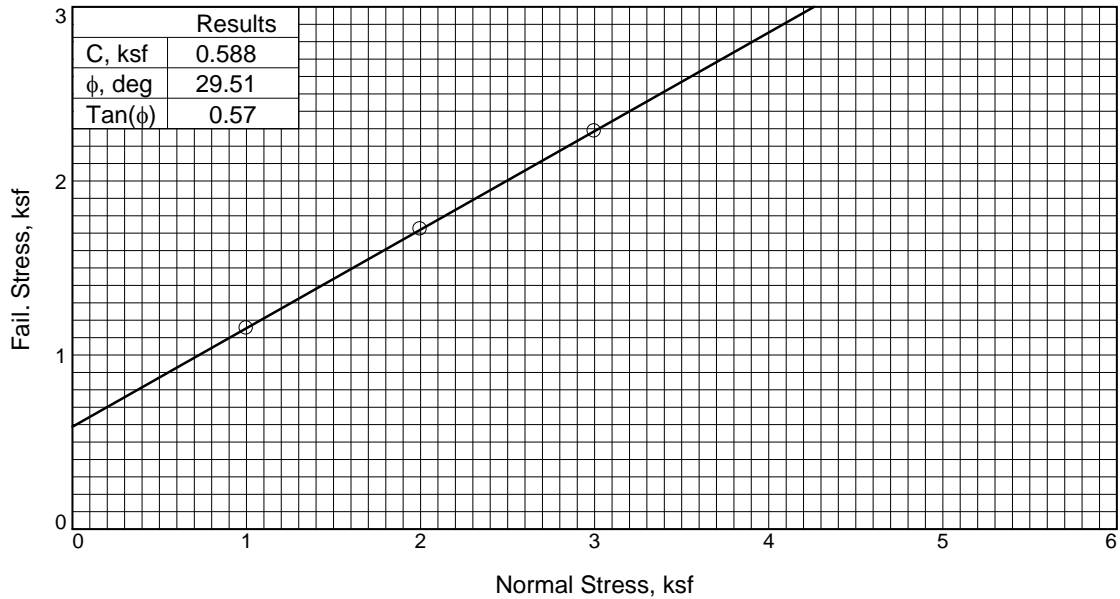
**Depth:** 90-91.5 ft

**Date Sampled:**

DIRECT SHEAR TEST REPORT

Tetra Tech  
Missoula, MT

**Figure** 48



Sample No.	1	2	3	
Initial	Water Content, %	6.9	6.2	6.2
	Dry Density, pcf	89.6	94.1	95.0
	Saturation, %	21.8	21.8	22.3
	Void Ratio	0.8457	0.7582	0.7415
	Diameter, in.	2.400	2.400	2.410
	Height, in.	1.150	1.138	1.122
At Test	Water Content, %	28.7	27.7	25.8
	Dry Density, pcf	90.0	96.2	100.9
	Saturation, %	90.8	101.9	107.0
	Void Ratio	0.8377	0.7195	0.6390
	Diameter, in.	2.400	2.400	2.410
	Height, in.	1.145	1.113	1.056
Normal Stress, ksf	1.000	2.000	3.000	
Fail. Stress, ksf	1.153	1.723	2.285	
Strain, %	2.6	12.8	9.9	
Ult. Stress, ksf				
Strain, %				
Strain rate, in./min.	0.001	0.001	0.001	

**Sample Type:** MC

**Description:** Silty Sand

**Assumed Specific Gravity=** 2.65

**Remarks:** Remolded

**Project:** Pickles Butte

**Source of Sample:** B2021-4

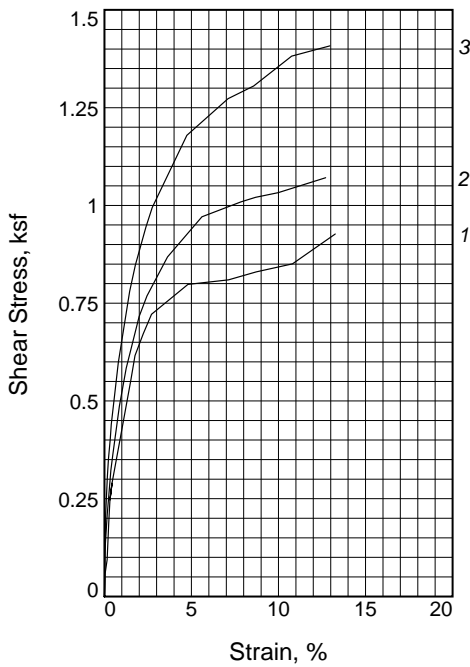
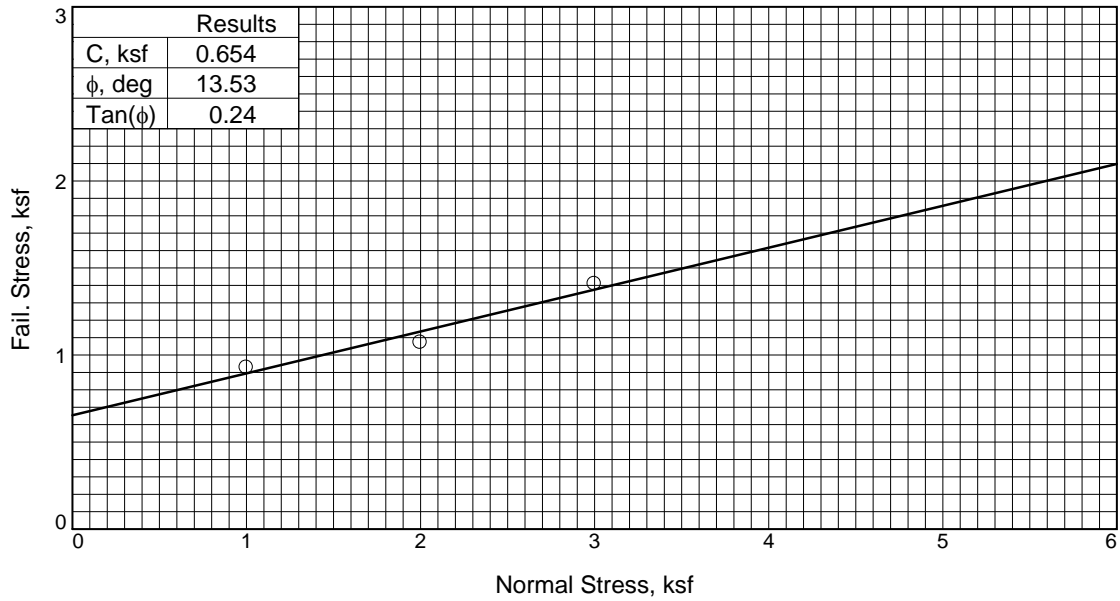
**Proj. No.:** 1145710402022

**Depth:** 120-120.9 ft

**Date Sampled:**

DIRECT SHEAR TEST REPORT

Tetra Tech  
Missoula, MT



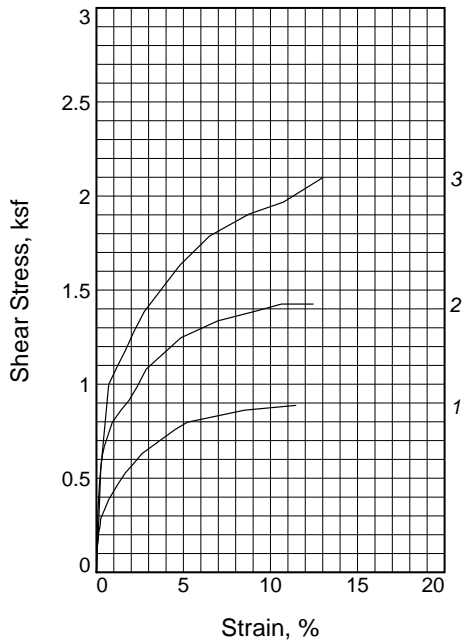
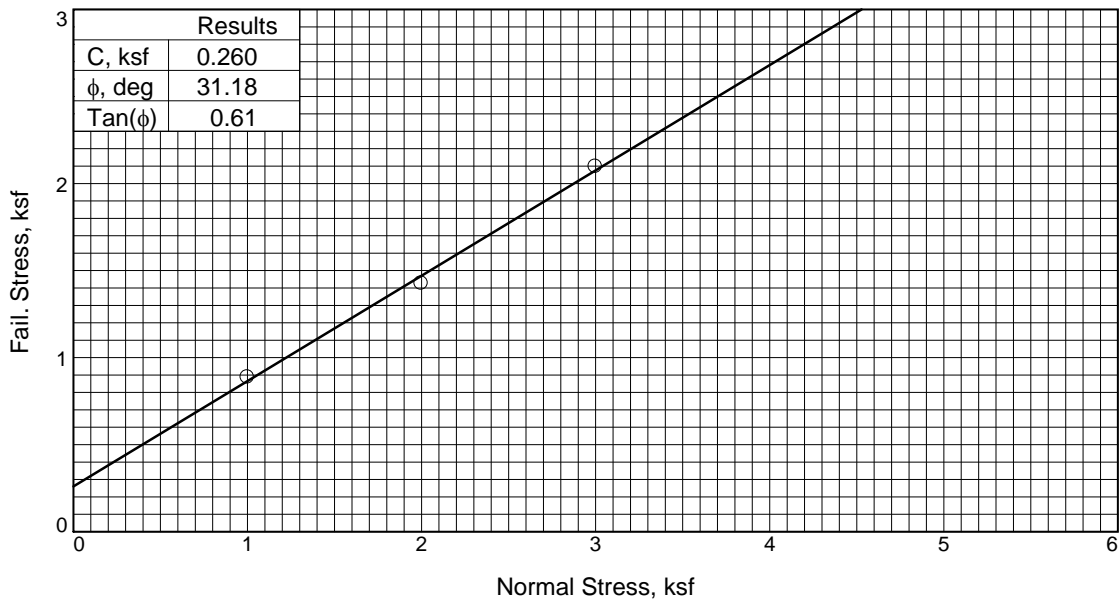
Sample No.	1	2	3	
Initial	Water Content, %	11.3	11.3	11.2
	Dry Density, pcf	99.2	98.3	98.8
	Saturation, %	44.6	43.7	43.8
	Void Ratio	0.6682	0.6829	0.6750
	Diameter, in.	2.500	2.500	2.500
	Height, in.	1.200	1.190	1.206
At Test	Water Content, %	27.5	25.7	27.1
	Dry Density, pcf	101.9	102.9	102.0
	Saturation, %	117.0	112.1	115.6
	Void Ratio	0.6233	0.6075	0.6217
	Diameter, in.	2.500	2.500	2.500
	Height, in.	1.168	1.137	1.168
Normal Stress, ksf	1.000	2.000	3.000	
Fail. Stress, ksf	0.927	1.071	1.408	
Strain, %	13.3	12.7	13.0	
Ult. Stress, ksf				
Strain, %				
Strain rate, in./min.	0.001	0.001	0.001	

**Sample Type:** MC  
**Description:** Lean Clay With Sand  
**Assumed Specific Gravity=** 2.65  
**Remarks:** Remolded

**Project:** Pickles Butte  
**Source of Sample:** B2021-5  
**Proj. No.:** 1145710402022      **Depth:** 80.0-81.5 ft

**Date Sampled:**

DIRECT SHEAR TEST REPORT  
Tetra Tech  
Missoula, MT



Sample No.	1	2	3	
Initial	Water Content, %	18.0	18.2	18.3
	Dry Density, pcf	80.6	84.6	78.3
	Saturation, %	45.3	50.4	43.7
	Void Ratio	1.0522	0.9546	1.1118
	Diameter, in.	2.410	2.410	2.400
	Height, in.	1.240	1.190	1.250
At Test	Water Content, %	25.0	24.1	24.1
	Dry Density, pcf	82.7	87.5	82.3
	Saturation, %	66.2	71.7	63.1
	Void Ratio	1.0009	0.8905	1.0104
	Diameter, in.	2.410	2.410	2.400
	Height, in.	1.209	1.151	1.190
Normal Stress, ksf	1.000	2.000	3.000	
Fail. Stress, ksf	0.887	1.426	2.098	
Strain, %	11.5	10.6	13.0	
Ult. Stress, ksf				
Strain, %				
Strain rate, in./min.	0.001	0.001	0.001	

**Sample Type:** MC  
**Description:** Silty Sand

**Assumed Specific Gravity=** 2.65  
**Remarks:** Remolded

**Figure** 51

**Project:** Pickles Butte

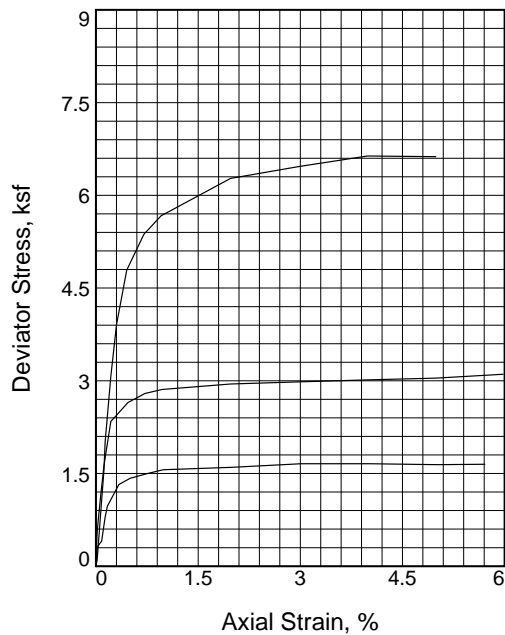
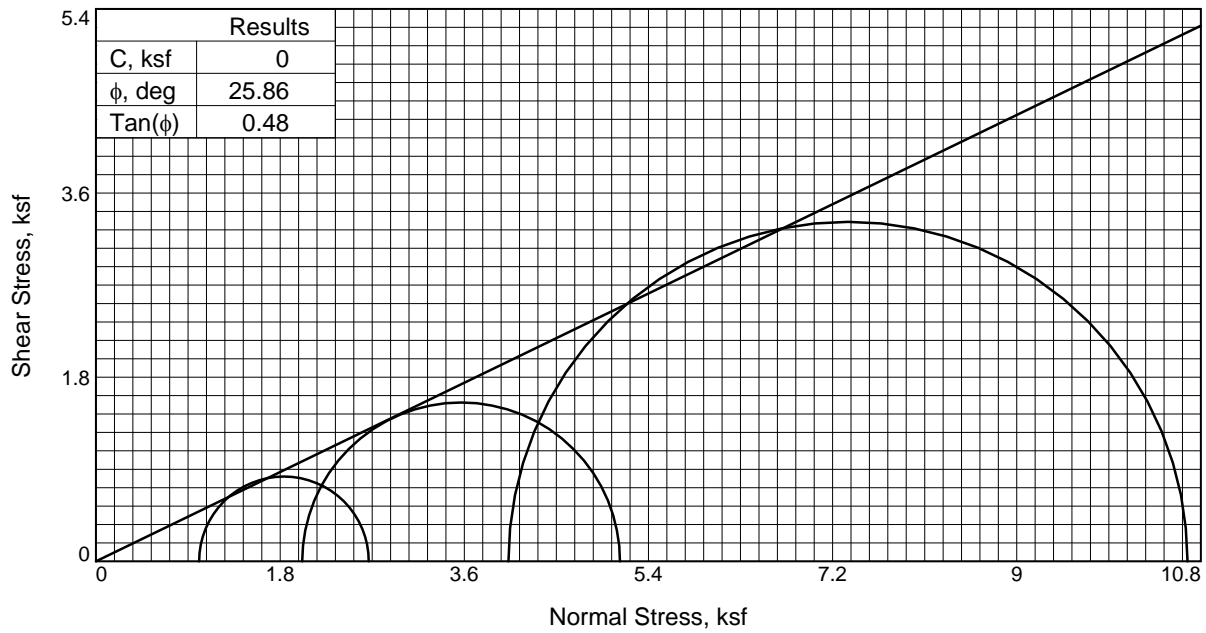
**Source of Sample:** B2021-5

**Proj. No.:** 1145710402022

**Depth:** 90-91.5 ft

**Date Sampled:**

DIRECT SHEAR TEST REPORT  
 Tetra Tech  
 Missoula, MT



Sample No.	1	2	3	
Initial	Water Content, %	5.0	5.0	5.0
	Dry Density, pcf	100.9	100.9	100.9
	Saturation, %	20.7	20.7	20.7
	Void Ratio	0.6394	0.6394	0.6394
	Diameter, in.	2.803	2.803	2.803
At Test	Height, in.	6.001	6.001	6.001
	Water Content, %	22.7	21.8	20.9
	Dry Density, pcf	101.4	102.9	104.6
	Saturation, %	95.4	95.2	95.0
	Void Ratio	0.6312	0.6074	0.5820
Diameter, in.	2.803	2.869	2.945	
	Height, in.	5.972	5.616	5.247
Strain rate, in./min.	0.001	0.001	0.001	
Back Pressure, psi	85.000	85.000	85.000	
Cell Pressure, psi	92.000	99.000	113.000	
Fail. Stress, ksf	1.66	3.11	6.64	
Ult. Stress, ksf				
$\sigma_1$ Failure, ksf	2.67	5.12	10.67	
$\sigma_3$ Failure, ksf	1.01	2.02	4.03	

**Type of Test:**

Consolidated Undrained

**Description:** Silty Sand

**Assumed Specific Gravity=**

2.65 **Remarks:**

**Project:** Pickles Butte

**Source of Sample:** B2021-3

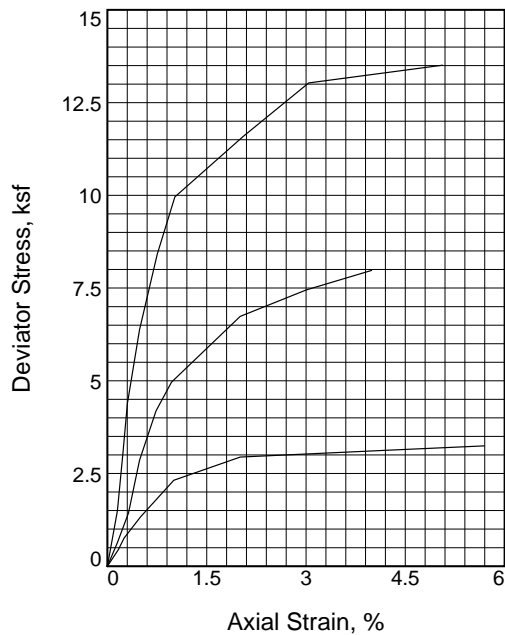
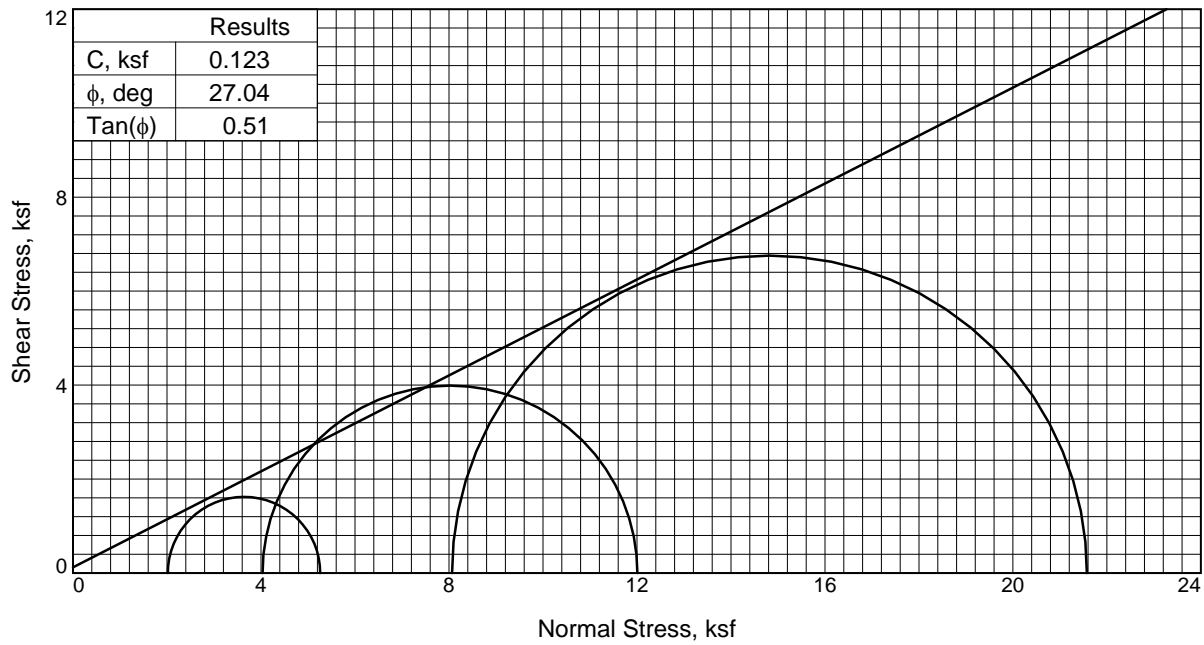
**Proj. No.:** 1145710402022

**Depth:** 25-27 ft

**Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

Tetra Tech  
Missoula, MT



Sample No.	1	2	3	
Initial	Water Content, %	5.0	5.0	5.0
	Dry Density, pcf	100.4	100.4	100.4
	Saturation, %	20.5	20.5	20.5
	Void Ratio	0.6481	0.6481	0.6481
	Diameter, in.	2.801	2.801	2.801
At Test	Height, in.	6.001	6.001	6.001
	Water Content, %	23.2	22.3	20.9
	Dry Density, pcf	100.7	102.2	104.5
	Saturation, %	95.5	95.3	95.0
	Void Ratio	0.6431	0.6195	0.5836
1	Diameter, in.	2.800	2.865	2.895
	Height, in.	5.986	5.638	5.397
	Strain rate, in./min.	0.001	0.001	0.001
	Back Pressure, psi	103.000	103.000	103.000
	Cell Pressure, psi	117.000	131.000	159.000
	Fail. Stress, ksf	3.24	7.98	13.51
	Ult. Stress, ksf			
	$\sigma_1$ Failure, ksf	5.26	12.01	21.57
	$\sigma_3$ Failure, ksf	2.02	4.03	8.06

**Type of Test:**

Consolidated Undrained

**Description:** Poorly Graded Sand with Silt

**Assumed Specific Gravity=** 2.65

**Remarks:**

**Project:** Pickles Butte

**Source of Sample:** B2021-4

**Proj. No.:** 1145710402022

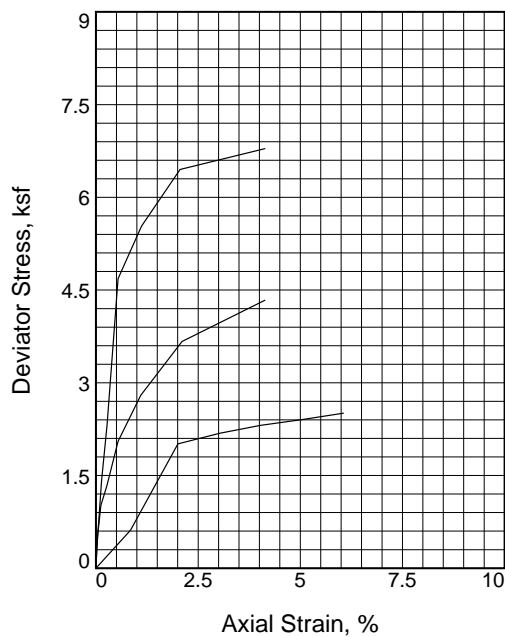
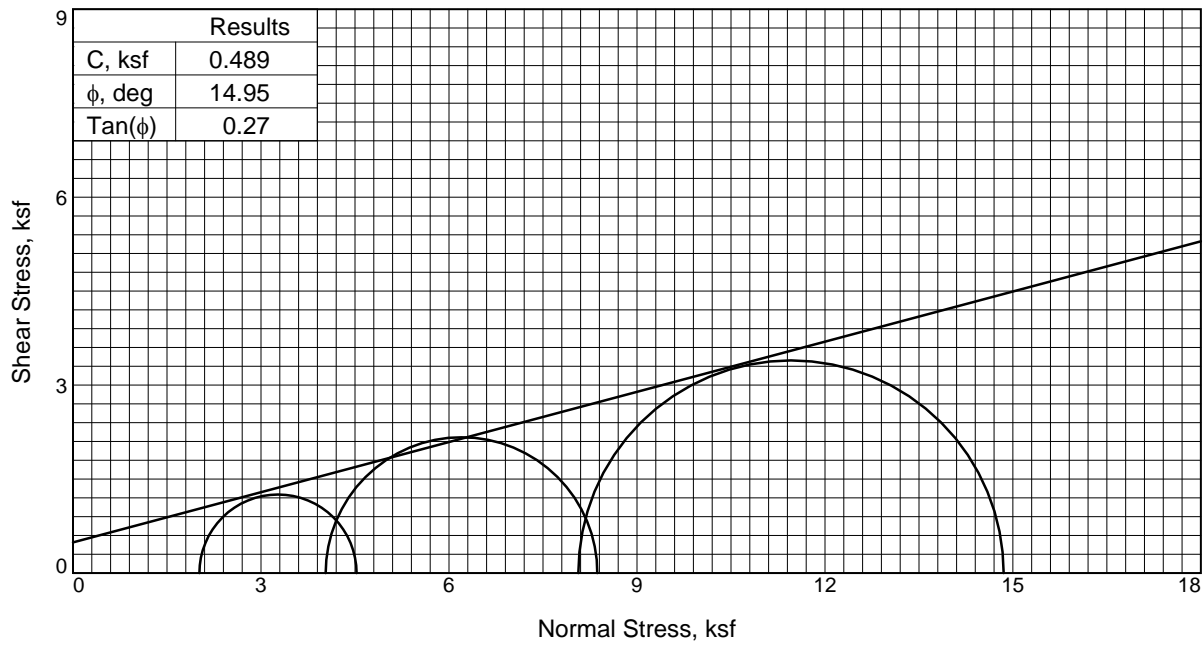
**Depth:** 50-51.5 ft

**Date Sampled:**

TRIAxIAL SHEAR TEST REPORT

Tetra Tech  
Missoula, MT





Sample No.	1	2	3	
Initial	Water Content, %	23.0	23.0	23.0
	Dry Density, pcf	90.1	90.1	90.1
	Saturation, %	73.0	73.0	73.0
	Void Ratio	0.8354	0.8354	0.8354
	Diameter, in.	2.800	2.800	2.800
At Test	Height, in.	6.030	6.030	6.030
	Water Content, %	27.4	23.7	21.3
	Dry Density, pcf	95.2	100.9	104.9
	Saturation, %	98.4	98.2	98.0
	Void Ratio	0.7372	0.6404	0.5770
Strain rate, in./min.	Diameter, in.	2.747	2.776	2.793
	Height, in.	5.930	5.481	5.206
	Back Pressure, psi	63.000	63.000	63.000
Cell Pressure, psi	77.000	91.000	119.000	
Fail. Stress, ksf	2.51	4.34	6.79	
Ult. Stress, ksf				
$\sigma_1$ Failure, ksf	4.52	8.37	14.85	
$\sigma_3$ Failure, ksf	2.02	4.03	8.06	

**Type of Test:**

Consolidated Undrained

**Description:** Silty Clay

**Assumed Specific Gravity=** 2.65

**Remarks:**

**Project:** Pickles Butte

**Source of Sample:** B2021-5

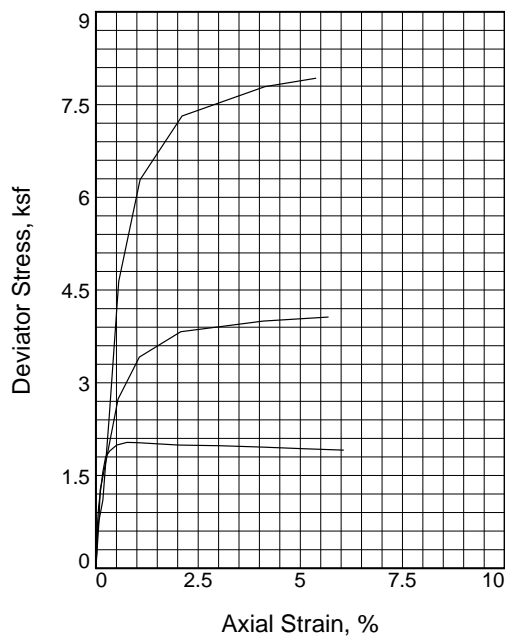
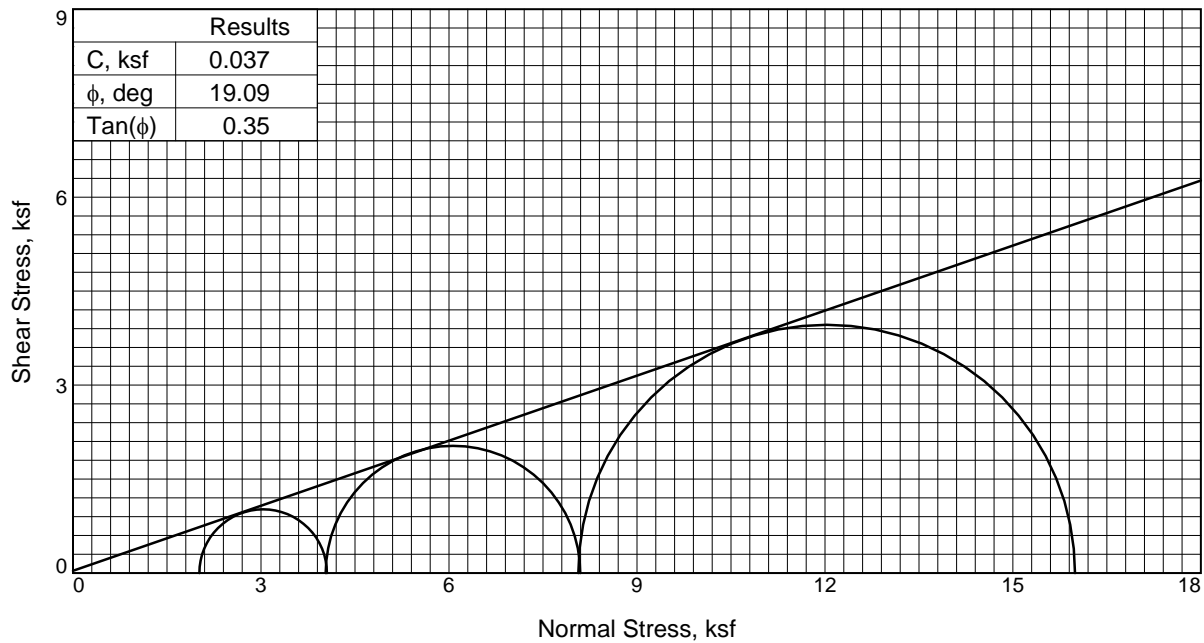
**Proj. No.:** 1145710402022

**Depth:** 50-51.5 ft

**Date Sampled:**

TRIAxIAL SHEAR TEST REPORT

Tetra Tech  
Missoula, MT



Sample No.	1	2	3	
Initial	Water Content, %	16.2	16.2	16.2
	Dry Density, pcf	101.9	101.9	101.9
	Saturation, %	69.1	69.1	69.1
	Void Ratio	0.6231	0.6231	0.6231
	Diameter, in.	2.790	2.790	2.790
At Test	Height, in.	6.000	6.000	6.000
	Water Content, %	22.2	21.2	19.2
	Dry Density, pcf	102.4	104.1	107.8
	Saturation, %	95.7	95.5	95.0
	Void Ratio	0.6160	0.5892	0.5344
1	Diameter, in.	2.800	2.873	2.924
	Height, in.	5.930	5.541	5.164
	Strain rate, in./min.	0.001	0.001	0.001
	Back Pressure, psi	53.000	53.000	53.000
	Cell Pressure, psi	67.000	81.000	109.000
	Fail. Stress, ksf	2.03	4.06	7.93
	Ult. Stress, ksf			
	$\sigma_1$ Failure, ksf	4.05	8.09	15.99
	$\sigma_3$ Failure, ksf	2.02	4.03	8.06

**Type of Test:**

Consolidated Undrained

**Description:** Silt

**Assumed Specific Gravity=** 2.65

**Remarks:**

**Project:** Pickles Butte

**Source of Sample:** B2021-5

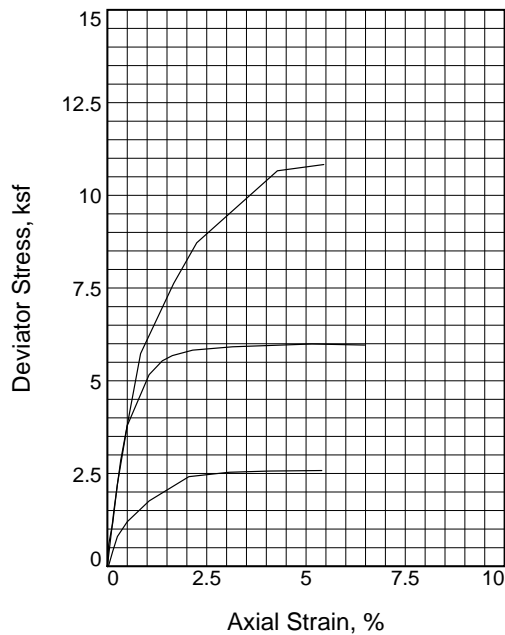
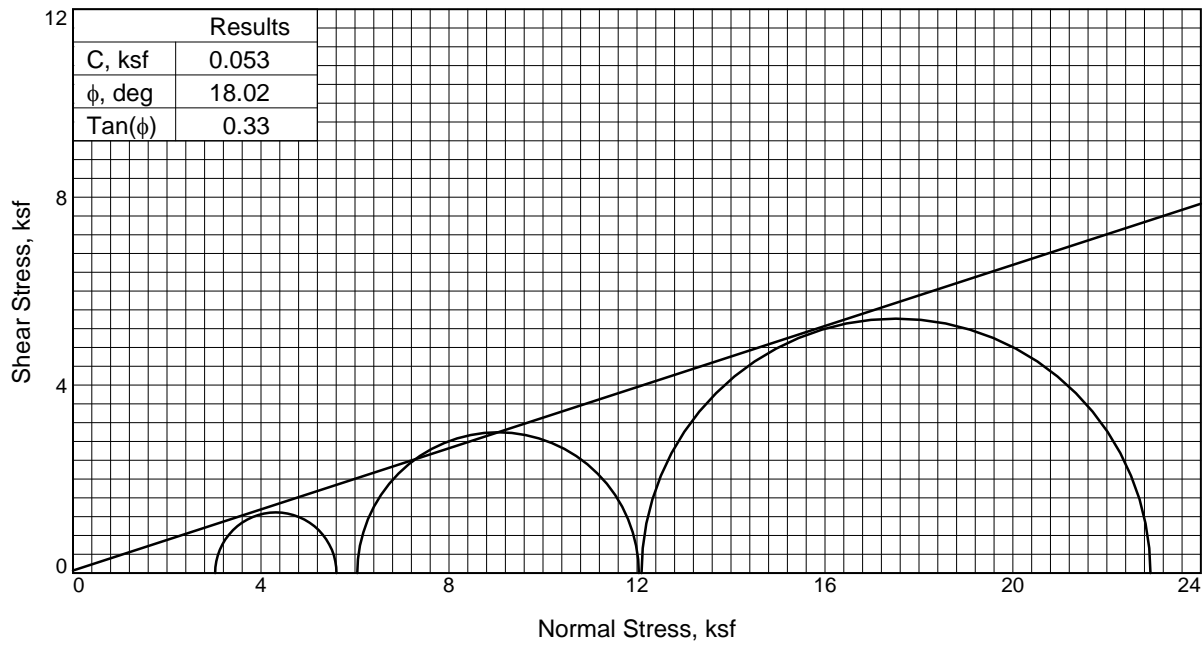
**Proj. No.:** 1145710402022

**Depth:** 69-70 ft

**Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

Tetra Tech  
Missoula, MT



Sample No.	1	2	3	
Initial	Water Content, %	18.1	18.1	18.1
	Dry Density, pcf	85.7	85.7	85.7
	Saturation, %	51.4	51.4	51.4
	Void Ratio	0.9314	0.9314	0.9314
	Diameter, in.	2.801	2.801	2.801
At Test	Height, in.	6.020	6.020	6.020
	Water Content, %	24.5	24.5	24.5
	Dry Density, pcf	98.3	98.3	98.3
	Saturation, %	95.0	95.0	95.0
	Void Ratio	0.6826	0.6826	0.6826
Strain rate, in./min.	Diameter, in.	2.618	2.694	2.795
	Height, in.	6.004	5.670	5.268
Back Pressure, psi	0.001	0.001	0.001	
Cell Pressure, psi	65.000	65.000	65.000	
Fail. Stress, ksf	86.000	107.000	149.000	
Ult. Stress, ksf	2.58	5.99	10.83	
$\sigma_1$ Failure, ksf				
$\sigma_3$ Failure, ksf	5.61	12.04	22.93	
	3.02	6.05	12.10	

**Type of Test:**

Consolidated Undrained

**Description:** Clay

**Assumed Specific Gravity=** 2.65

**Remarks:**

**Project:** Pickles Butte

**Source of Sample:** B2021-7

**Proj. No.:** 1145710402022

**Depth:** 120-121.3 ft

**Date Sampled:**

TRIAxIAL SHEAR TEST REPORT

Tetra Tech  
Missoula, MT



















# SUMMARY OF LABORATORY RESULTS

PROJECT NUMBER 114-571040-2022

PROJECT NAME Pickles Butte Sanitary Landfill - Canyon County, ID

Boring Number	Date Drilled	Latitude	Longitude	Elevation (feet)	Depth (feet)	Soil Class (USCS)	LL (%)	PI (%)	Liquidity Index	10 Mesh (%)	40 Mesh (%)	200 Mesh (%)	In-Place Density (pcf)	Maximum Dry Density (pcf)	Percent Natural Moisture	Percent Optimum Moisture	Friction Angle (degrees)	Cohesion (ksf)	Unconfined Compressive Strength (ksf)	Splitting Tensile Strength (psi)	Cc	pH	Resistivity (ohm-cm)	Sulfate Content (%)	California Bearing Ratio	
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	130 - 131.5										19											
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	139 - 140																					
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	140 - 141.5										24											
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	149 - 150																					
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	150 - 151.5																					
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	160 - 161.4																					
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	169 - 170																					
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	170 - 171.5																					
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	179 - 180																					
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	189 - 190																					
B2021-7	12/7/2021	43.495280	-116.712592	2659.5036	199 - 200																					
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	0 - 1.5										11											
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	1 - 4		NV	NP		98.7	95.6	83.5	97	97.2		17.9										
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	2 - 3.5																					
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	4 - 5.5																					
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	8 - 10																					
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	10 - 11.5																					
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	11 - 15																					
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	15 - 16.5																					
B2021-8	11/15/2021	43.489880	-116.703147	2956.6206	20 - 21.5																					

LAB SUMMARY TT - LAB SUMMARY.GDT - 7/29/22 12:00 - N:\GEO\TECH\REPORTS\REPORT 2022\PICKLES BUTTE LANDFILL\LAB\_LOGS\BORING LOGS.GPJ

## **APPENDIX D: Static Slope Stability Analyses**

Slope Stability Cross Sections - Figures 1D through 5D

Slope Stability Stability Analyses Printouts Figures 6D through 43D

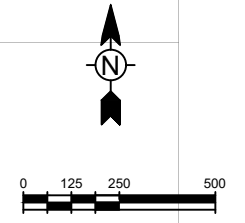
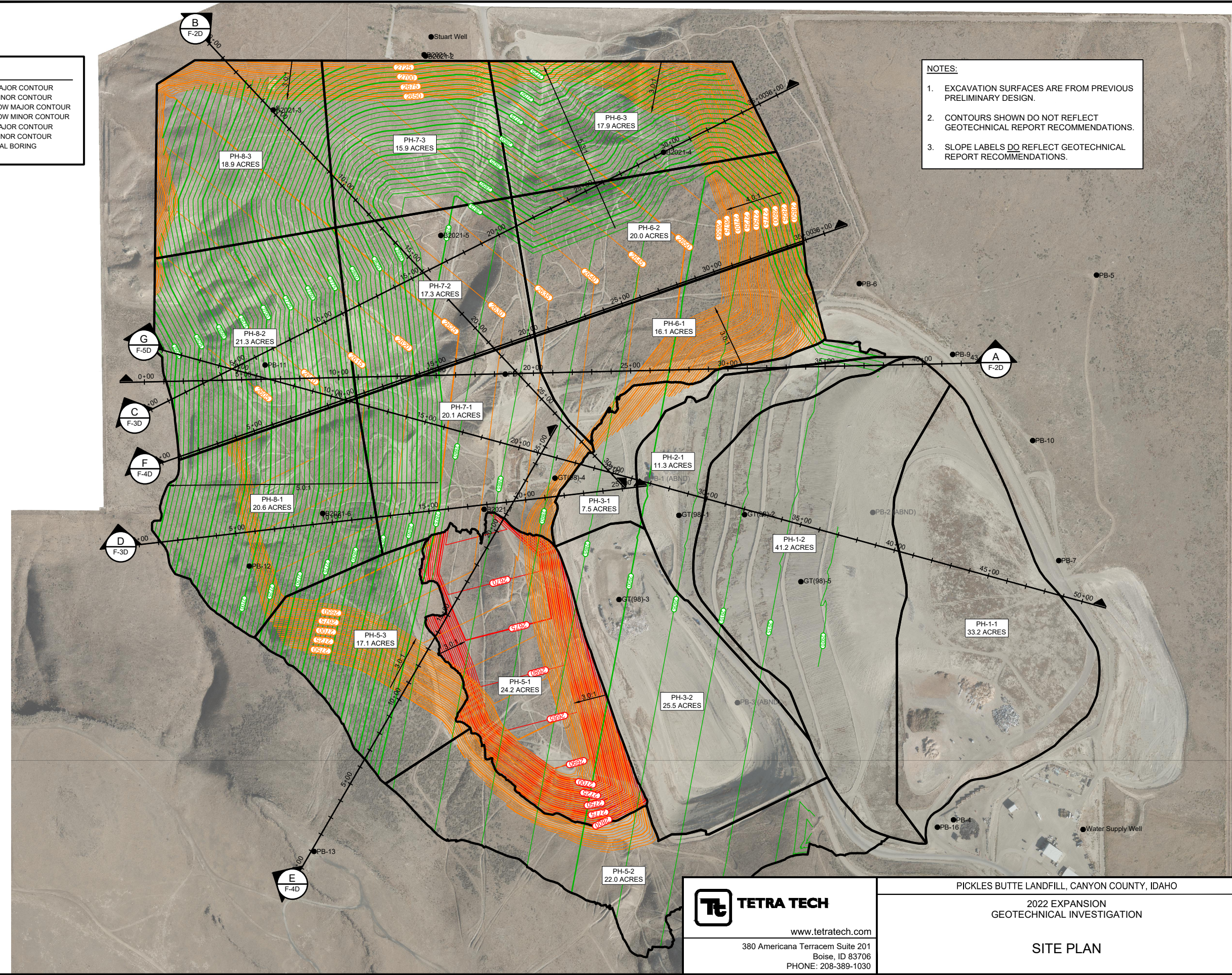
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**LEGEND**

- PROPOSED CUT MAJOR CONTOUR
- PROPOSED CUT MINOR CONTOUR
- PROPOSED BORROW MAJOR CONTOUR
- PROPOSED BORROW MINOR CONTOUR
- PROPOSED FILL MAJOR CONTOUR
- PROPOSED FILL MINOR CONTOUR
- B2021-# 2021 GEOTECHNICAL BORING

**NOTES:**

1. EXCAVATION SURFACES ARE FROM PREVIOUS PRELIMINARY DESIGN.
2. CONTOURS SHOWN DO NOT REFLECT GEOTECHNICAL REPORT RECOMMENDATIONS.
3. SLOPE LABELS DO REFLECT GEOTECHNICAL REPORT RECOMMENDATIONS.



**TETRA TECH**  
 www.tetrattech.com  
 380 Americana Terracem Suite 201  
 Boise, ID 83706  
 PHONE: 208-389-1030

PICKLES BUTTE LANDFILL, CANYON COUNTY, IDAHO  
 2022 EXPANSION  
 GEOTECHNICAL INVESTIGATION

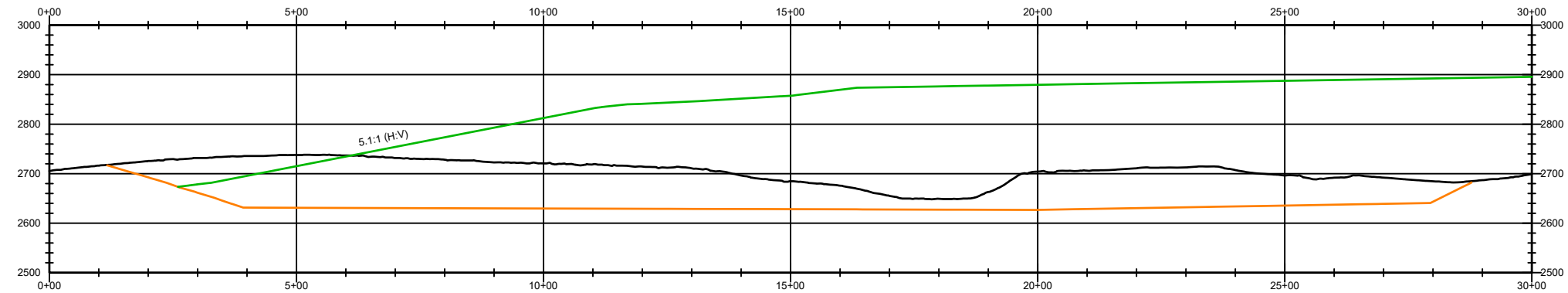
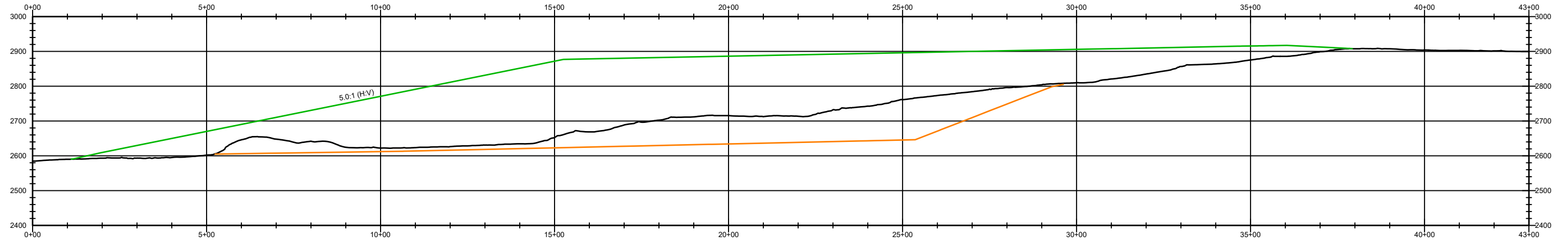
**SITE PLAN**

Project No.: 114-571040-2022  
 Date: 7/29/2022  
 Designed By: SG  
 Figure 1D

Copyright Tetra Tech

Bar Measures 1 inch

7/29/2022 12:34 PM - O:\T-Z\T\MISSOULA\114-571040-PICKLES BUTTE LANDFILL\07-CAD\SHEETFILES\GEOTECH\F-00-GEOTECH INVESTIGATION FIGURES.DWG



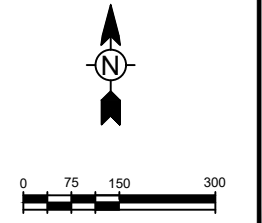
LEGEND	
	EXISTING GROUND
	PROPOSED CUT
	PROPOSED BORROW
	PROPOSED FILL

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PICKLES BUTTE LANDFILL, CANYON COUNTY, IDAHO  
2022 EXPANSION  
GEOTECHNICAL INVESTIGATION

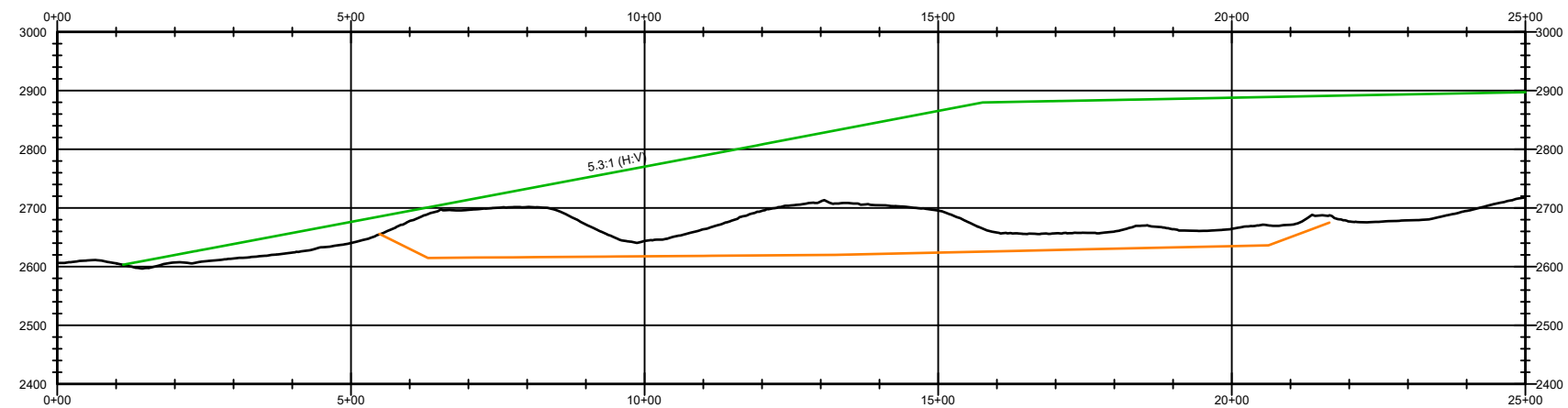
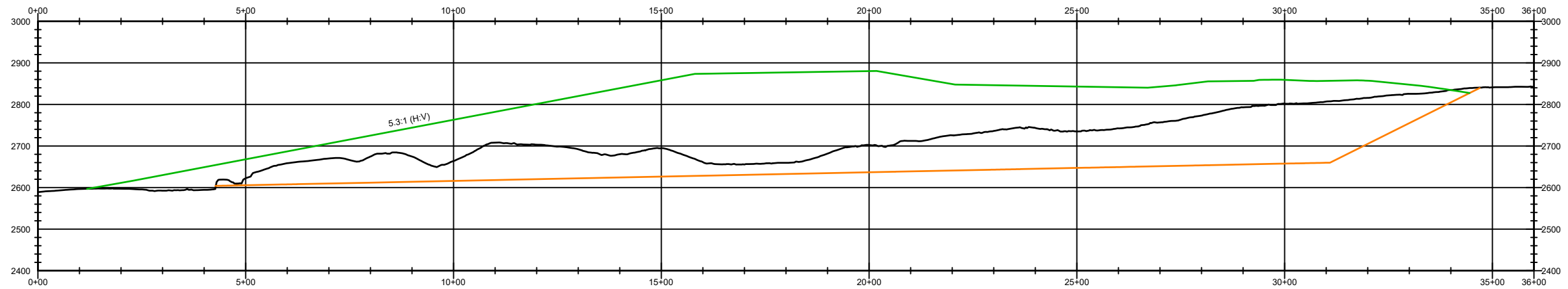
**PROFILES A & B**

Project No.:	114-571040-2022
Date:	7/29/2022
Designed By:	SG
Figure	2D

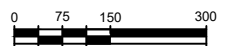


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LEGEND	
	EXISTING GROUND
	PROPOSED CUT
	PROPOSED BORROW
	PROPOSED FILL



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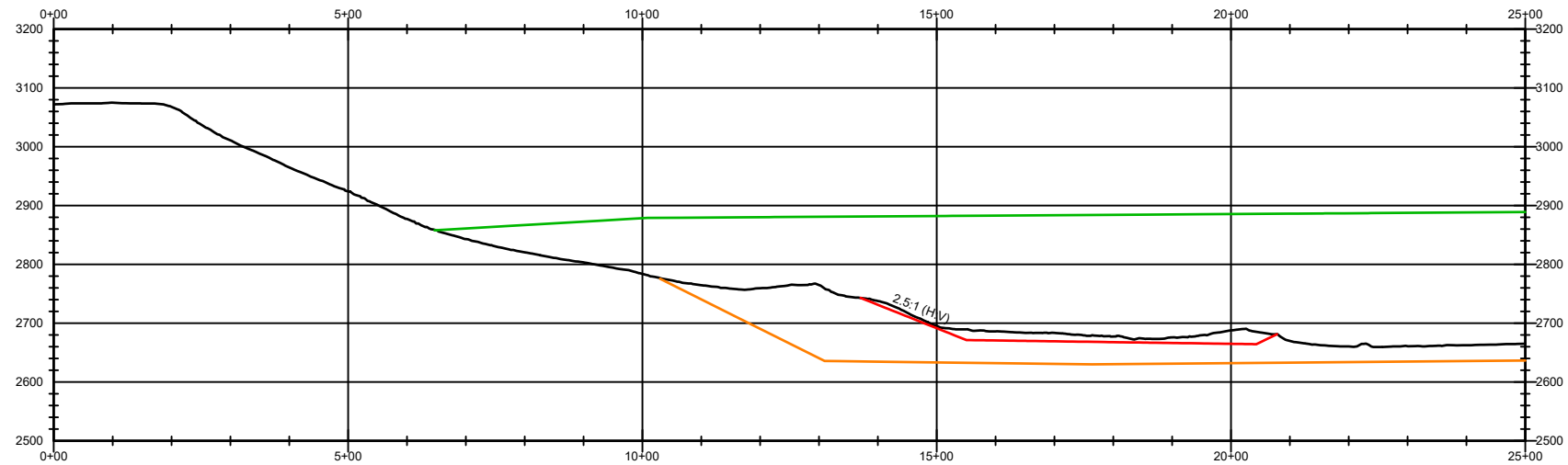
PICKLES BUTTE LANDFILL, CANYON COUNTY, IDAHO  
2022 EXPANSION  
GEOTECHNICAL INVESTIGATION  
**PROFILES C & D**

Project No.:	114-571040-2022
Date:	7/29/2022
Designed By:	SG
Figure	3D

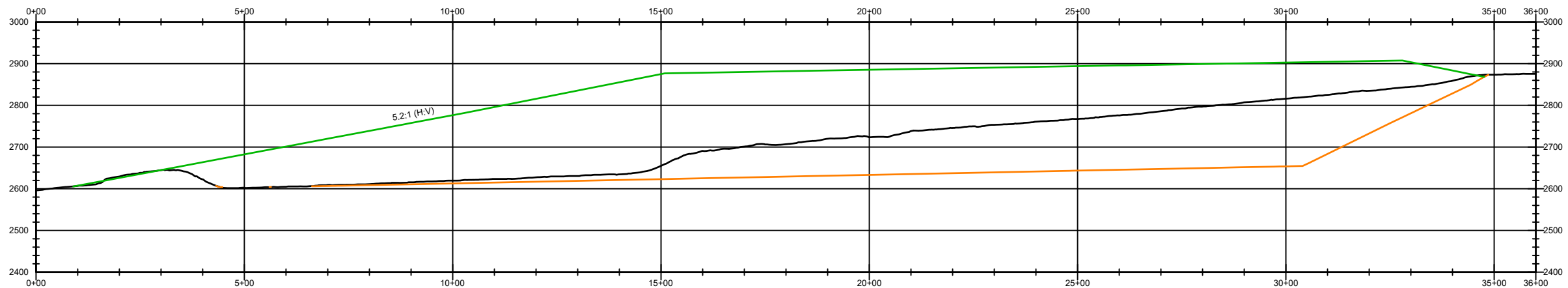
Bar Measures 1 inch

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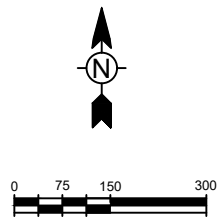


E SECTION E  
F-1D SCALE: 1" = 300'



F SECTION F  
F-1D SCALE: 1" = 300'

LEGEND	
	EXISTING GROUND
	PROPOSED CUT
	PROPOSED BORROW
	PROPOSED FILL



**Tt TETRA TECH**  
 www.tetrattech.com  
 380 Americana Terracem Suite 201  
 Boise, ID 83706  
 PHONE: 208-389-1030

PICKLES BUTTE LANDFILL, CANYON COUNTY, IDAHO  
 2022 EXPANSION  
 GEOTECHNICAL INVESTIGATION  
**PROFILES E & F**

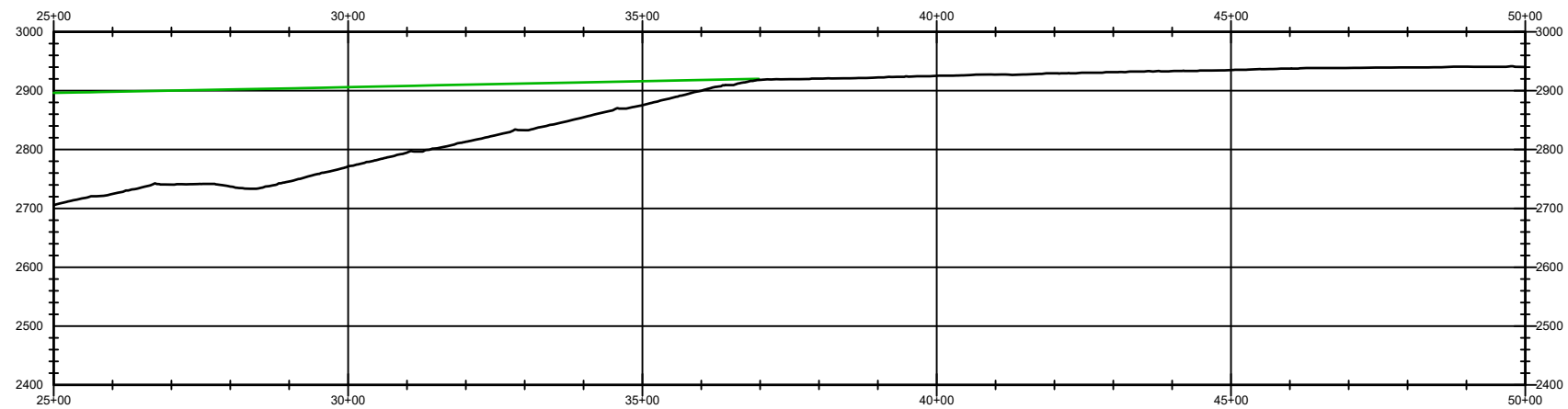
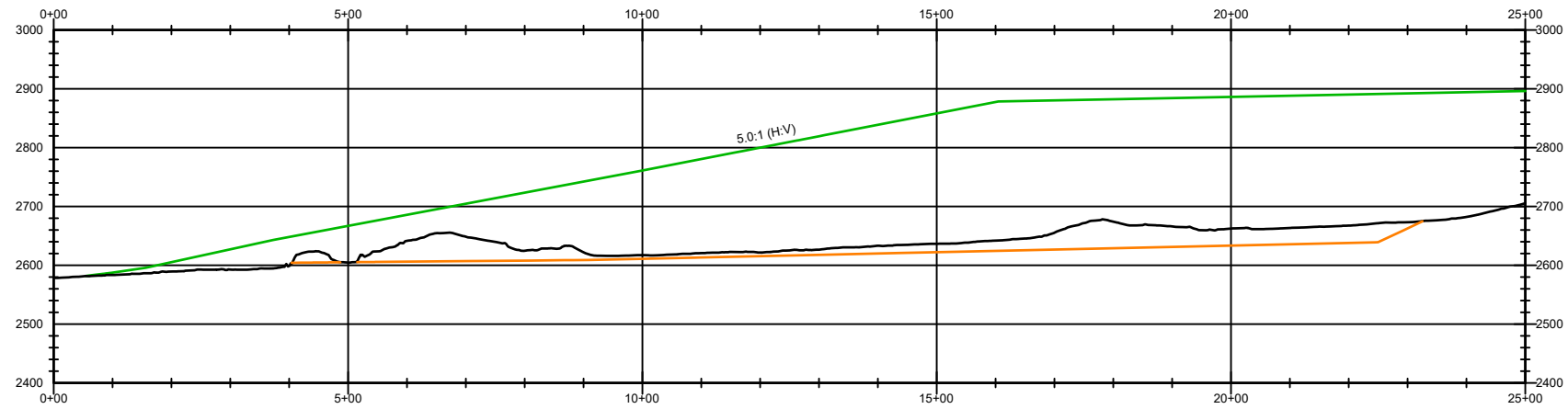
Project No.: 114-571040-2022  
 Date: 7/29/2022  
 Designed By: SG  
 Figure  
**4D**

Bar Measures 1 inch

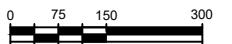
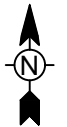
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SECTION G  
SCALE: 1" = 300'



LEGEND	
	EXISTING GROUND
	PROPOSED CUT
	PROPOSED BORROW
	PROPOSED FILL

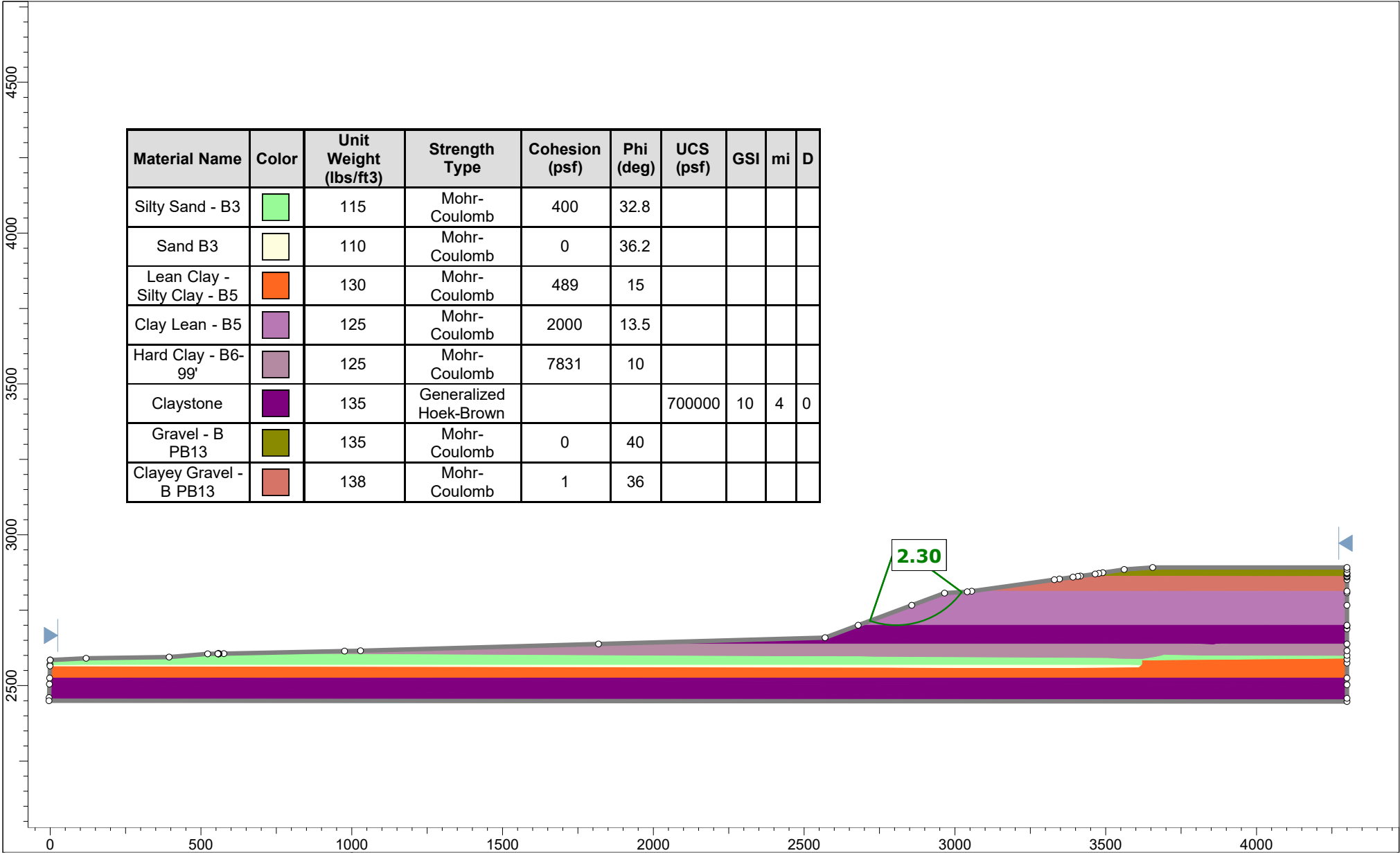
**TETRA TECH**  
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380 Americana Terracem Suite 201  
Boise, ID 83706  
PHONE: 208-389-1030


PICKLES BUTTE LANDFILL, CANYON COUNTY, IDAHO  
2022 EXPANSION  
GEOTECHNICAL INVESTIGATION  
**PROFILE G**

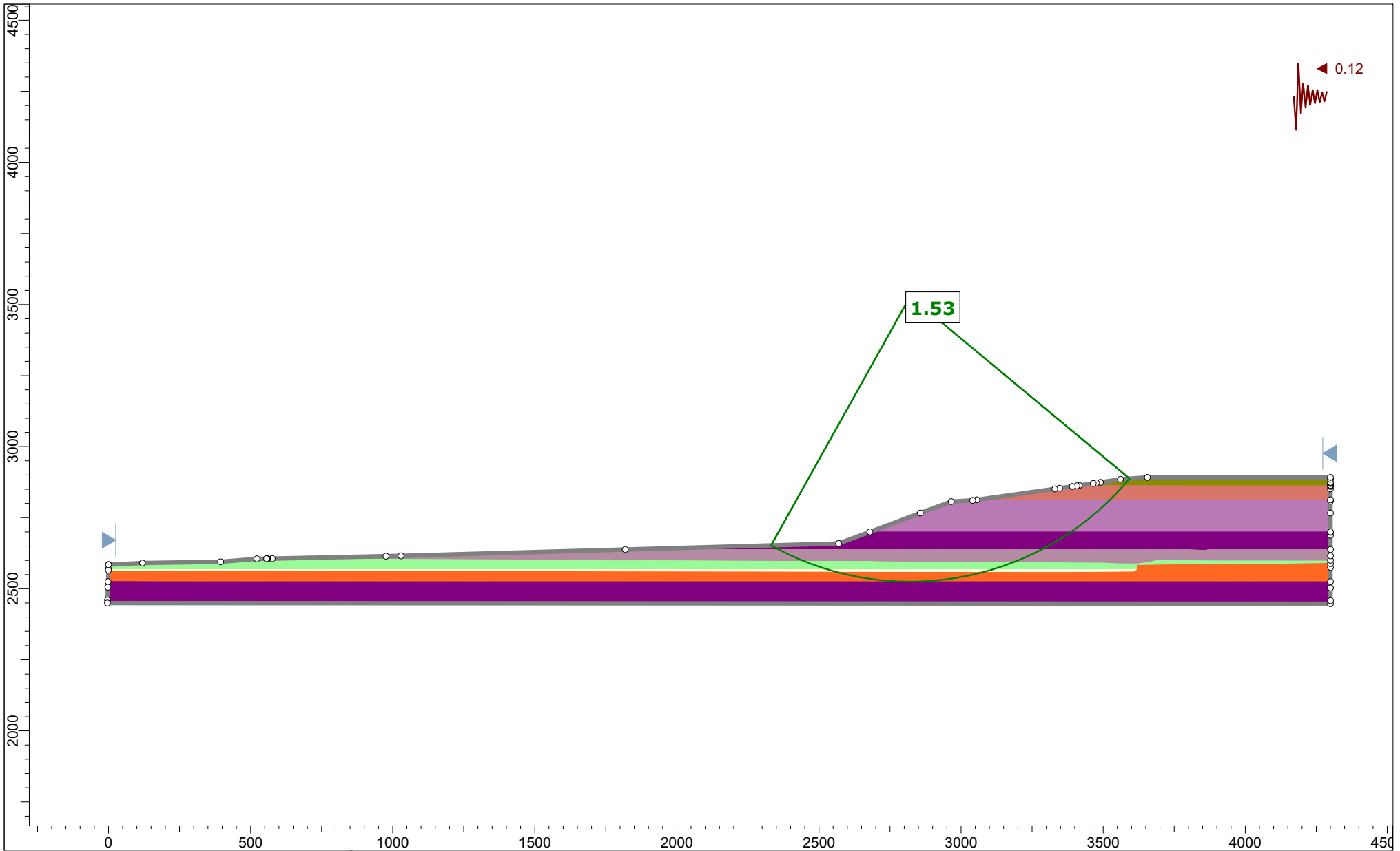
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Date:	7/29/2022
Designed By:	SG
Figure	5D


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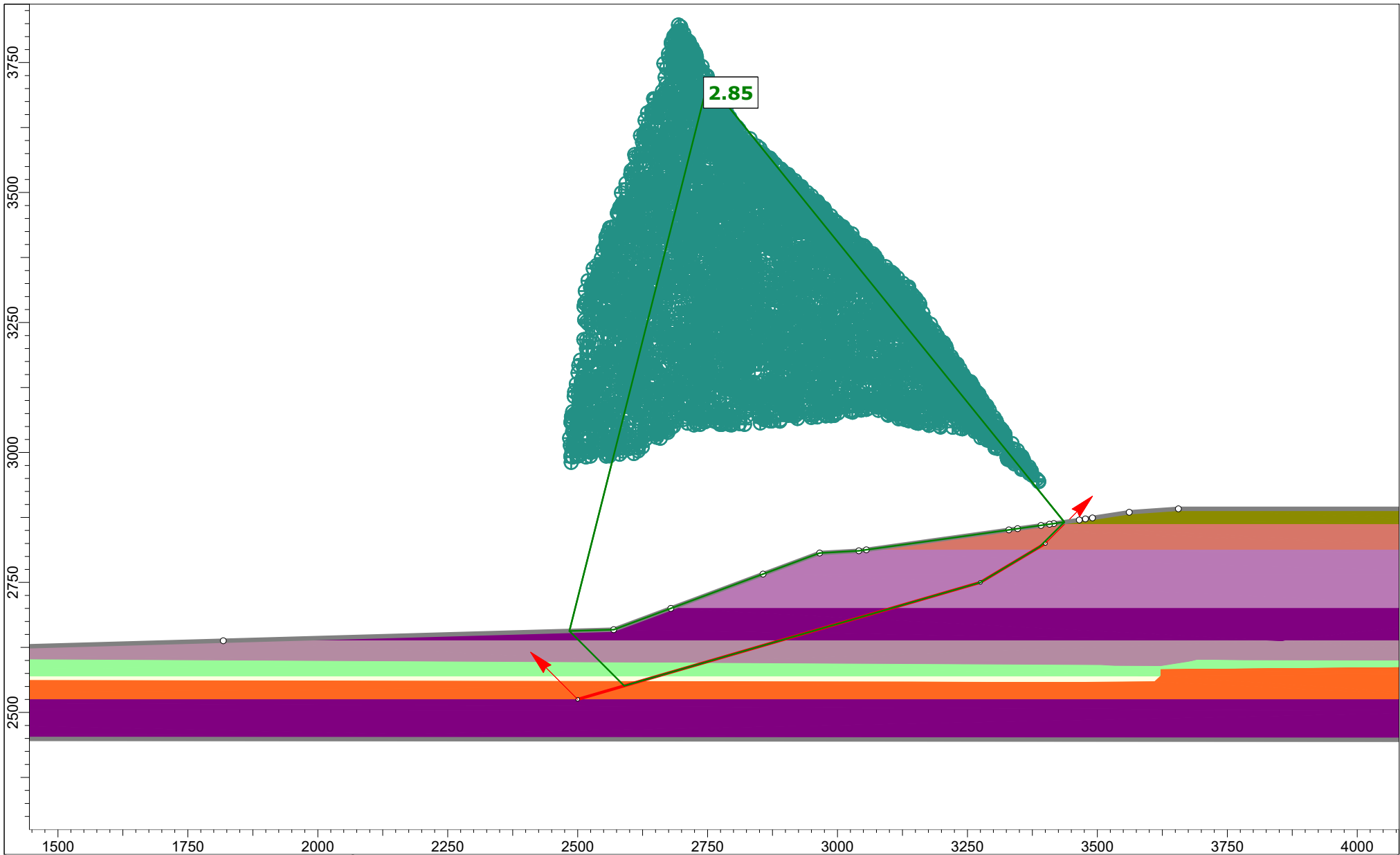
Bar Measures 1 inch



	<i>Project</i> Pickles Butte	Figure 6D
	<i>Group</i> SECTION A	<i>Scenario</i> Proposed Excavation 3H:1V
	<i>Drawn By</i> SG	<i>Company</i> Tetra Tech
	<i>Date</i> 7/27/2022	<i>File Name</i> Static Loading

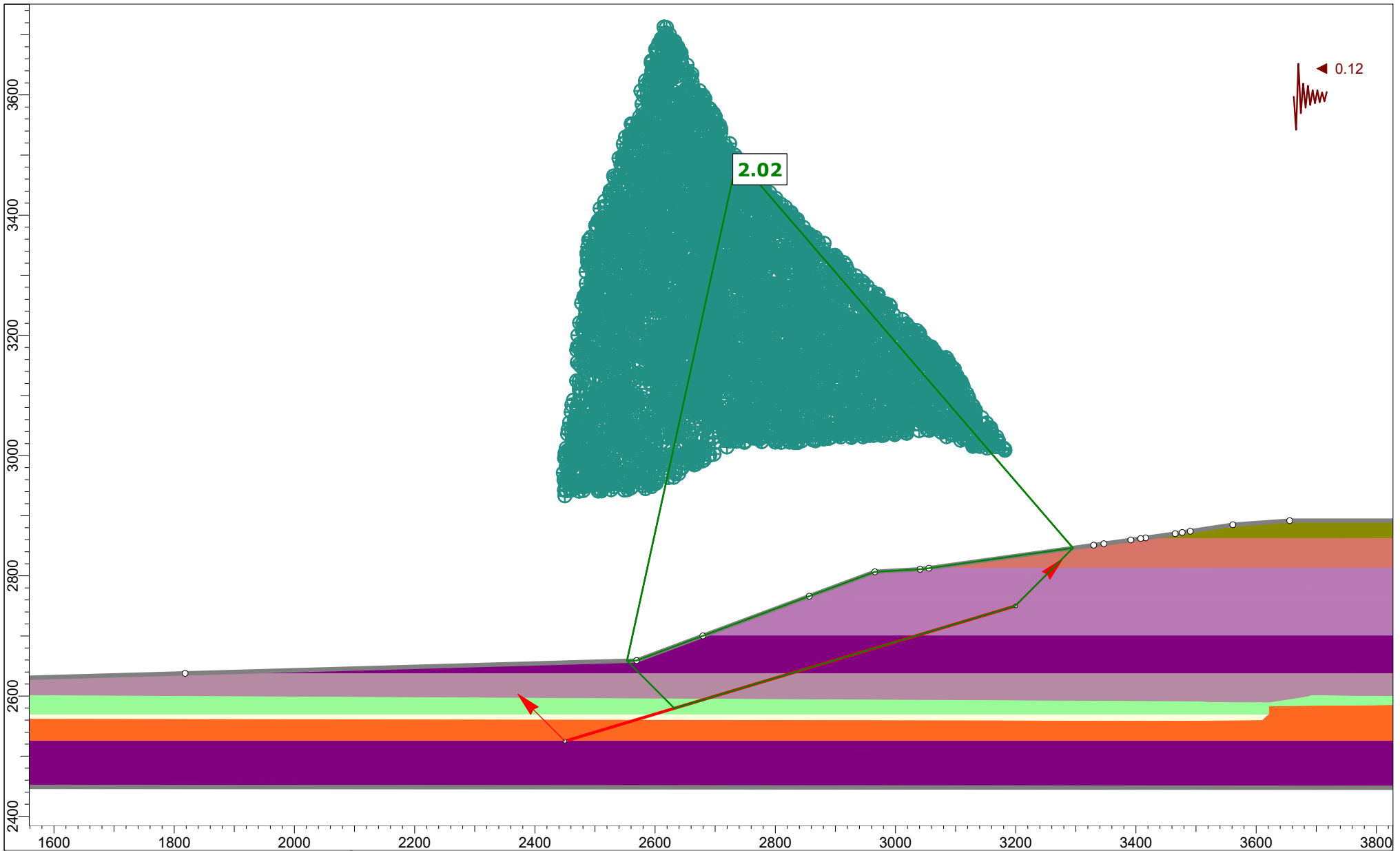



	<i>Project</i> Pickles Butte		Figure 7D	
	<i>Group</i> SECTION A		<i>Scenario</i> Proposed Excavation 3H:1V	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/27/2022		<i>File Name</i> Seismic Loading	
	SLIDEINTERPRET 9.023			

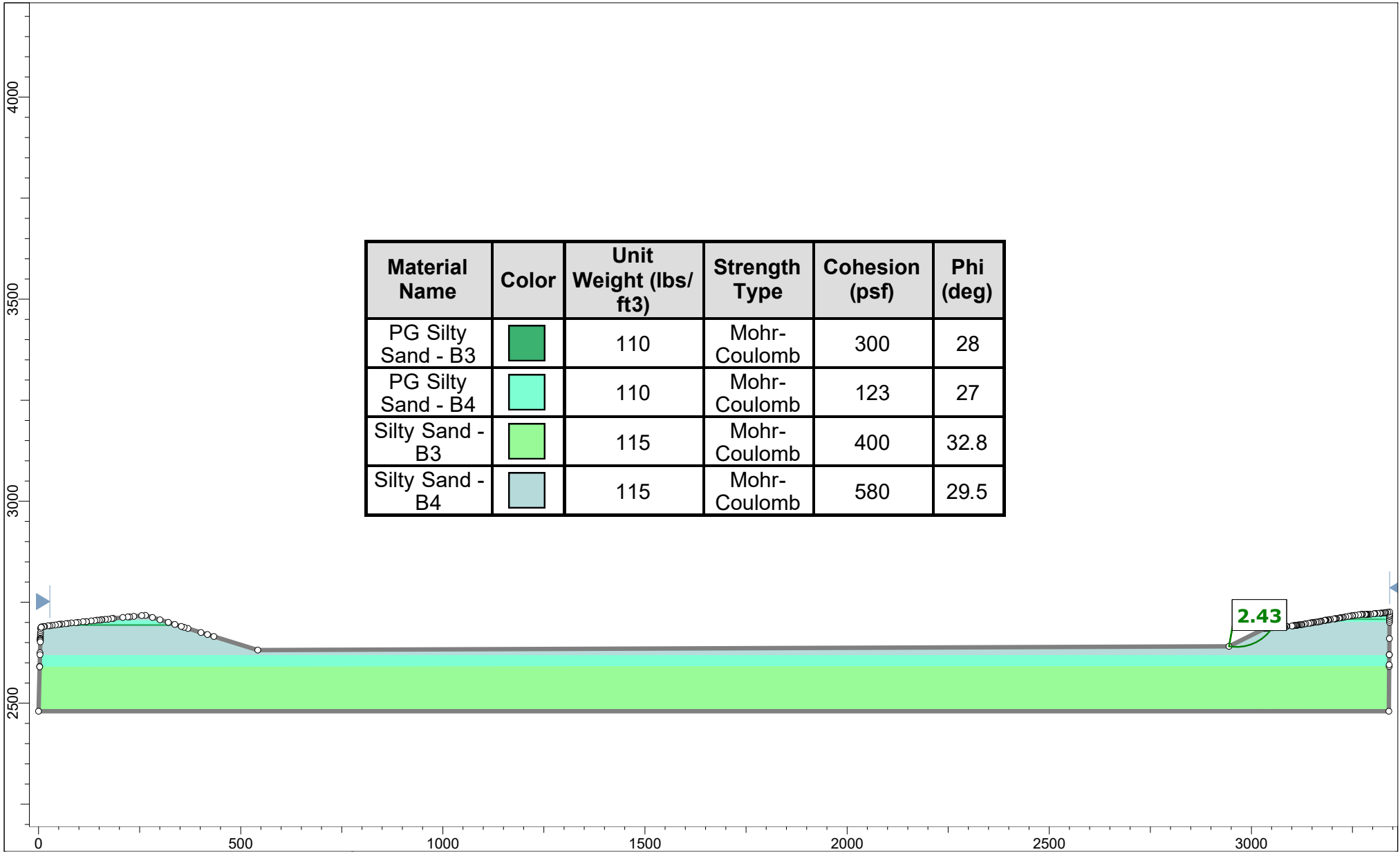



SLIDEINTERPRET 9.023

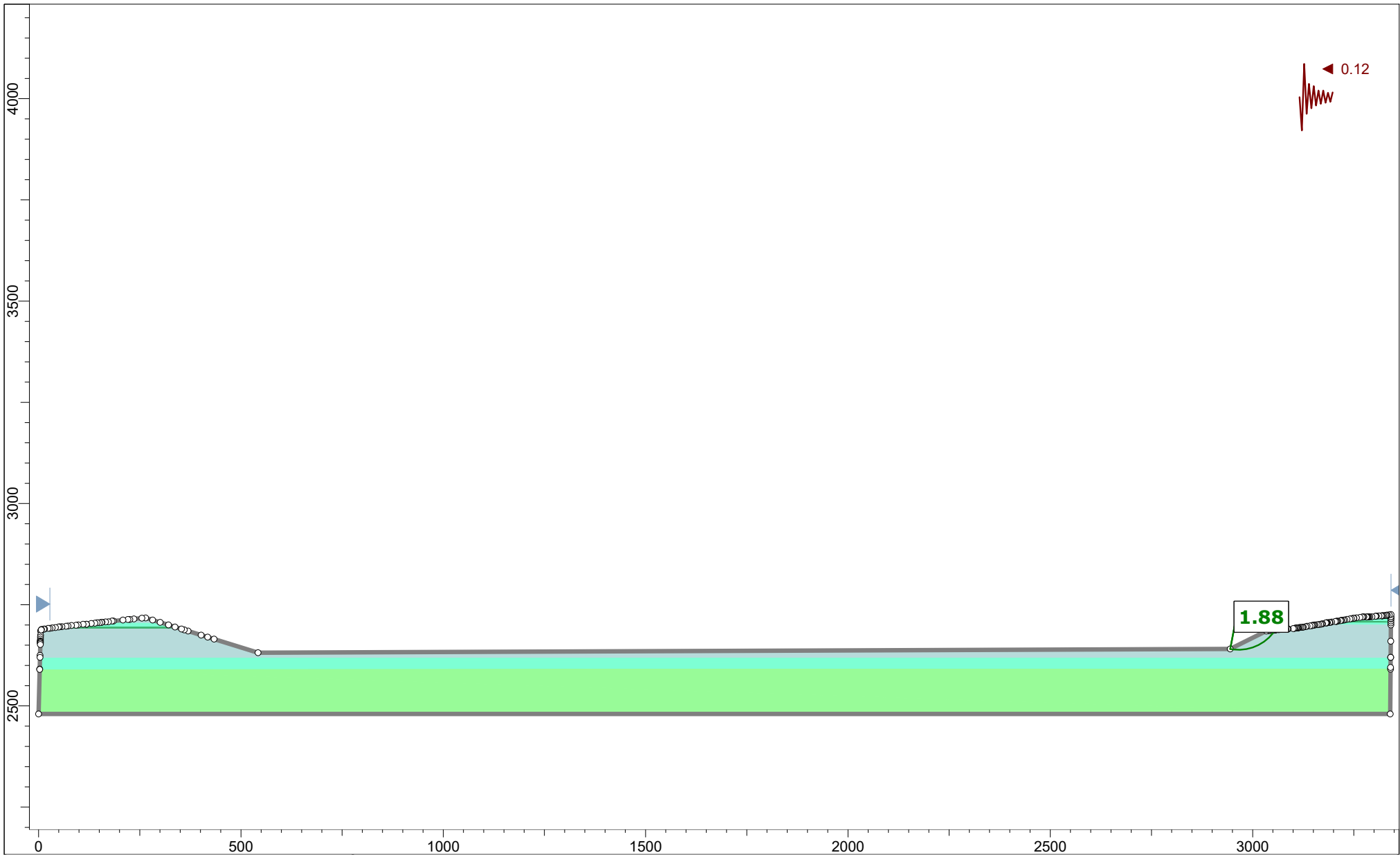
<i>Project</i>		Pickles Butte		Figure 8D	
<i>Group</i>		SECTION A	<i>Scenario</i>		Proposed Excavation 3H:1V
<i>Drawn By</i>		SG	<i>Company</i>		Tetra Tech
<i>Date</i>		7/28/2022	<i>File Name</i>		Static Loading - Block Failure




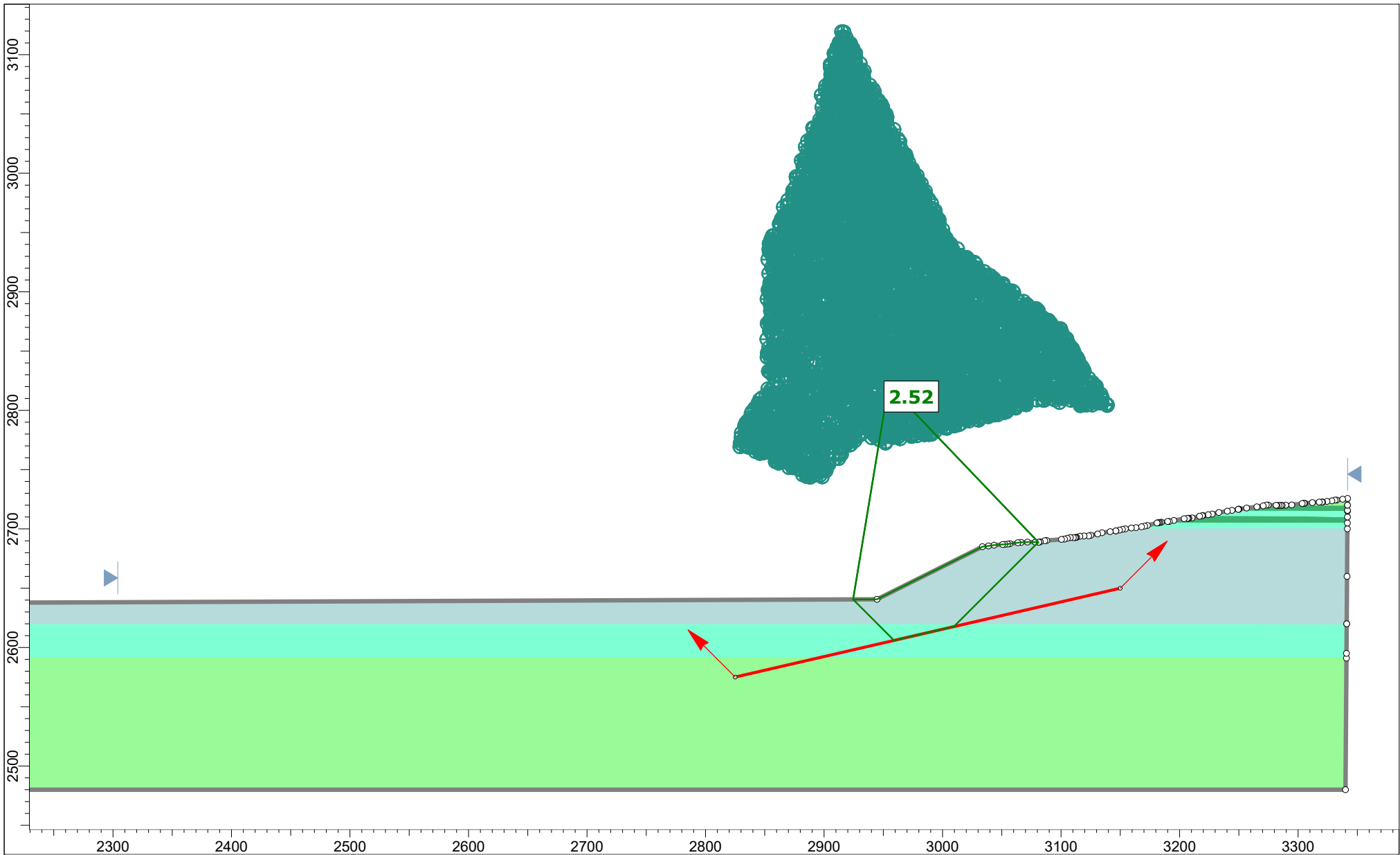
	Project		Pickles Butte		Figure 9D	
	Group		SECTION A		Scenario	
	Drawn By		SG		Company	
	Date		7/28/2022		Tetra Tech	
					File Name	
				Seismic Loading - Block		




	<i>Project</i> Pickles Butte		<b>Figure 10D</b>	
	<i>Group</i> SECTION B		<i>Scenario</i> Proposed Excavation 2.27H:1V	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/27/2022		<i>File Name</i> Static Loading	

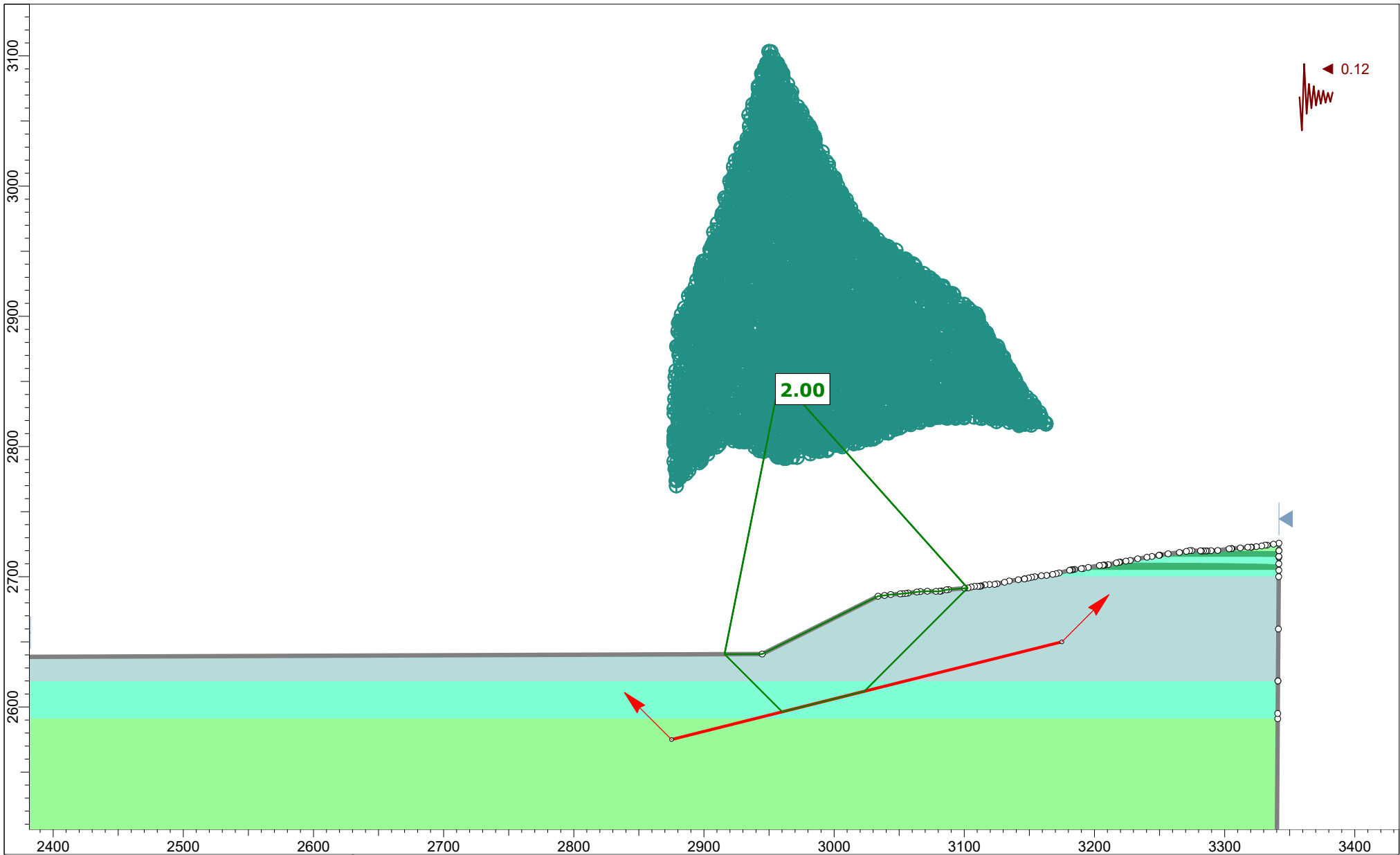



	<i>Project</i> Pickles Butte		<b>Figure 11D</b>	
	<i>Group</i> SECTION B		<i>Scenario</i> Proposed Excavation 2.27H:1V	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/27/2022		<i>File Name</i> Seismic Loading	

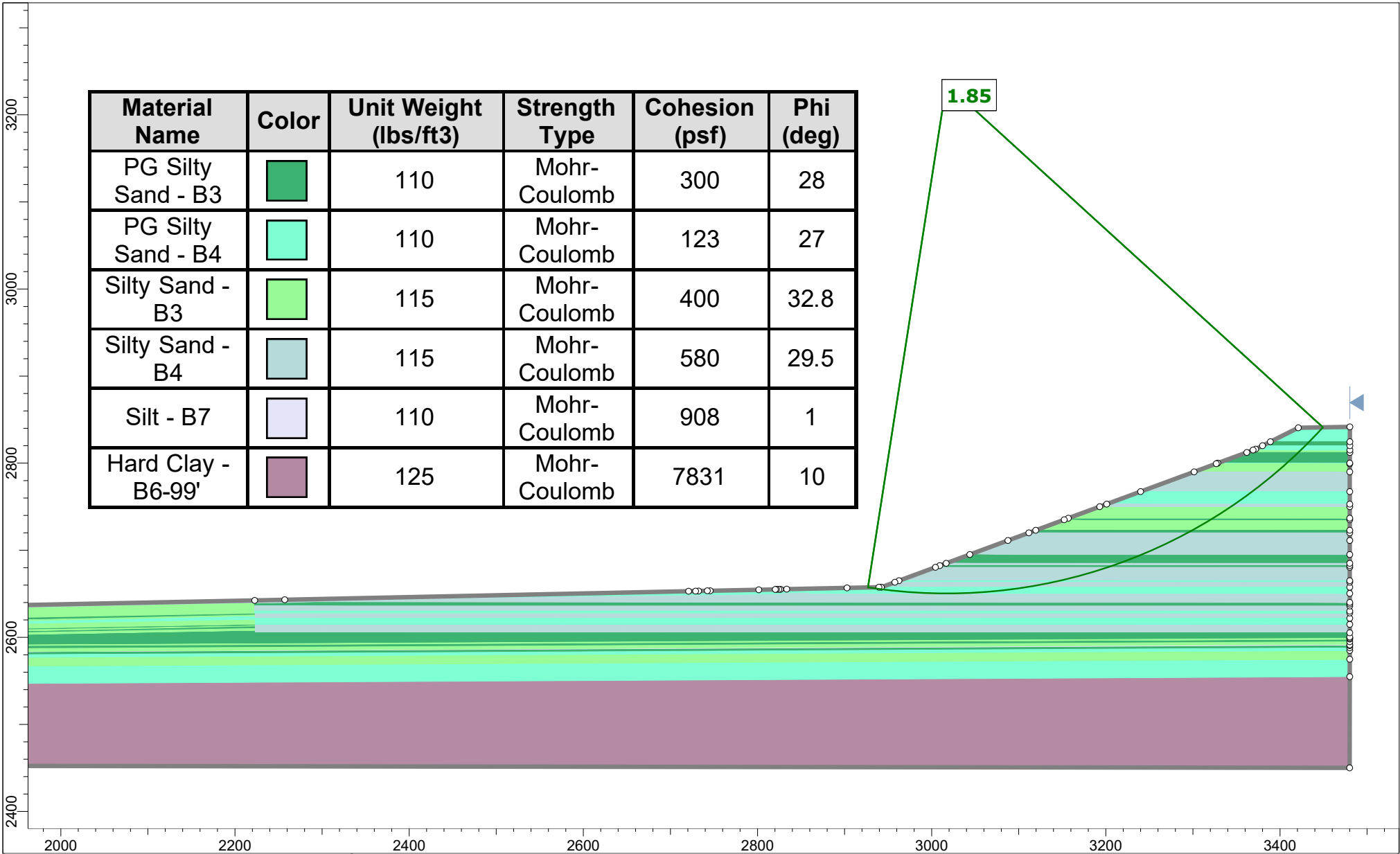



	Project		Pickles Butte		Figure 12D		
	Group		SECTION B		Scenario		
	Drawn By		SG		Company		
	Date		7/28/2022		File Name		
				Proposed Excavation 2.27H:1V		Tetra Tech	
				Static Loading - Block Failure			

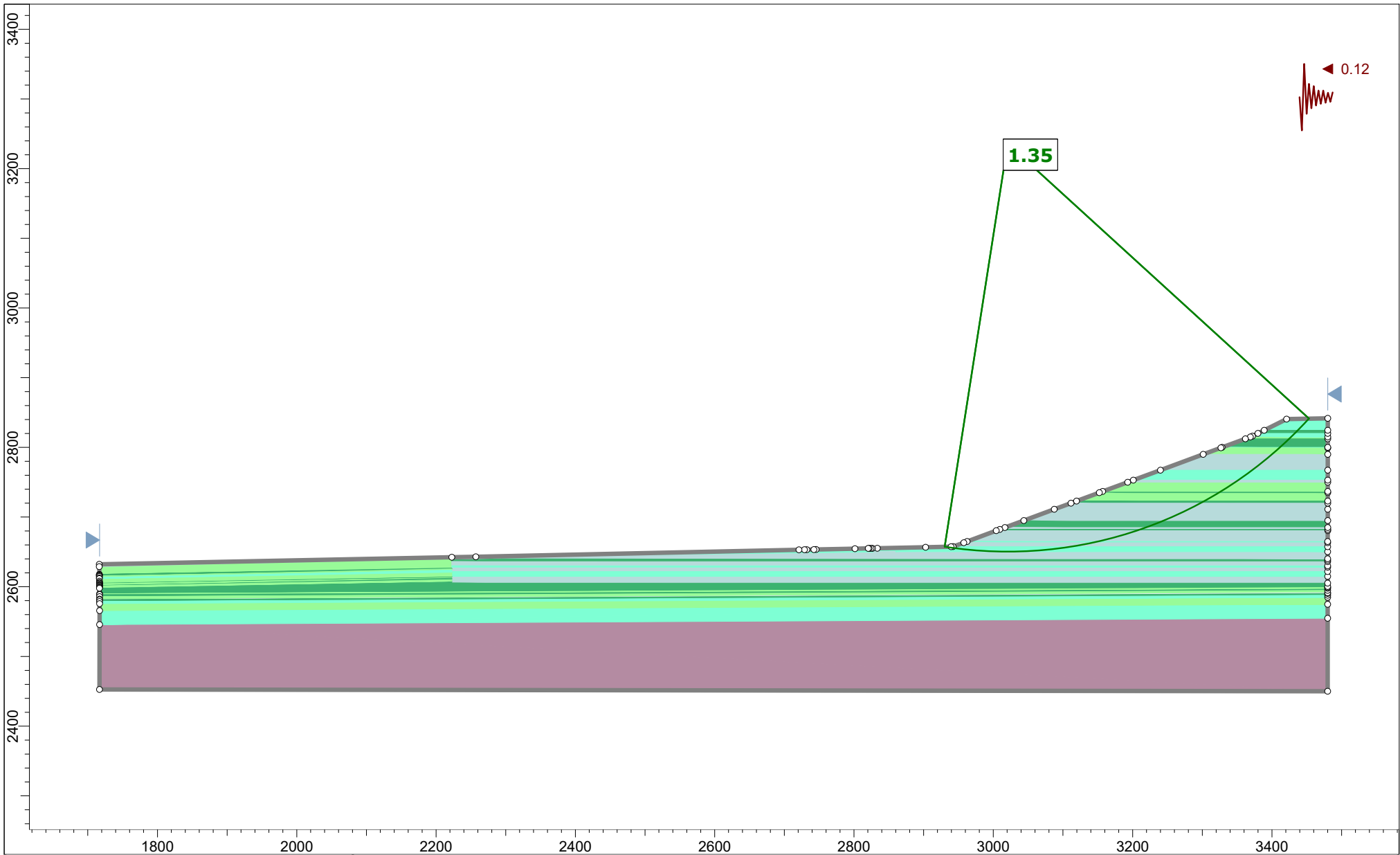





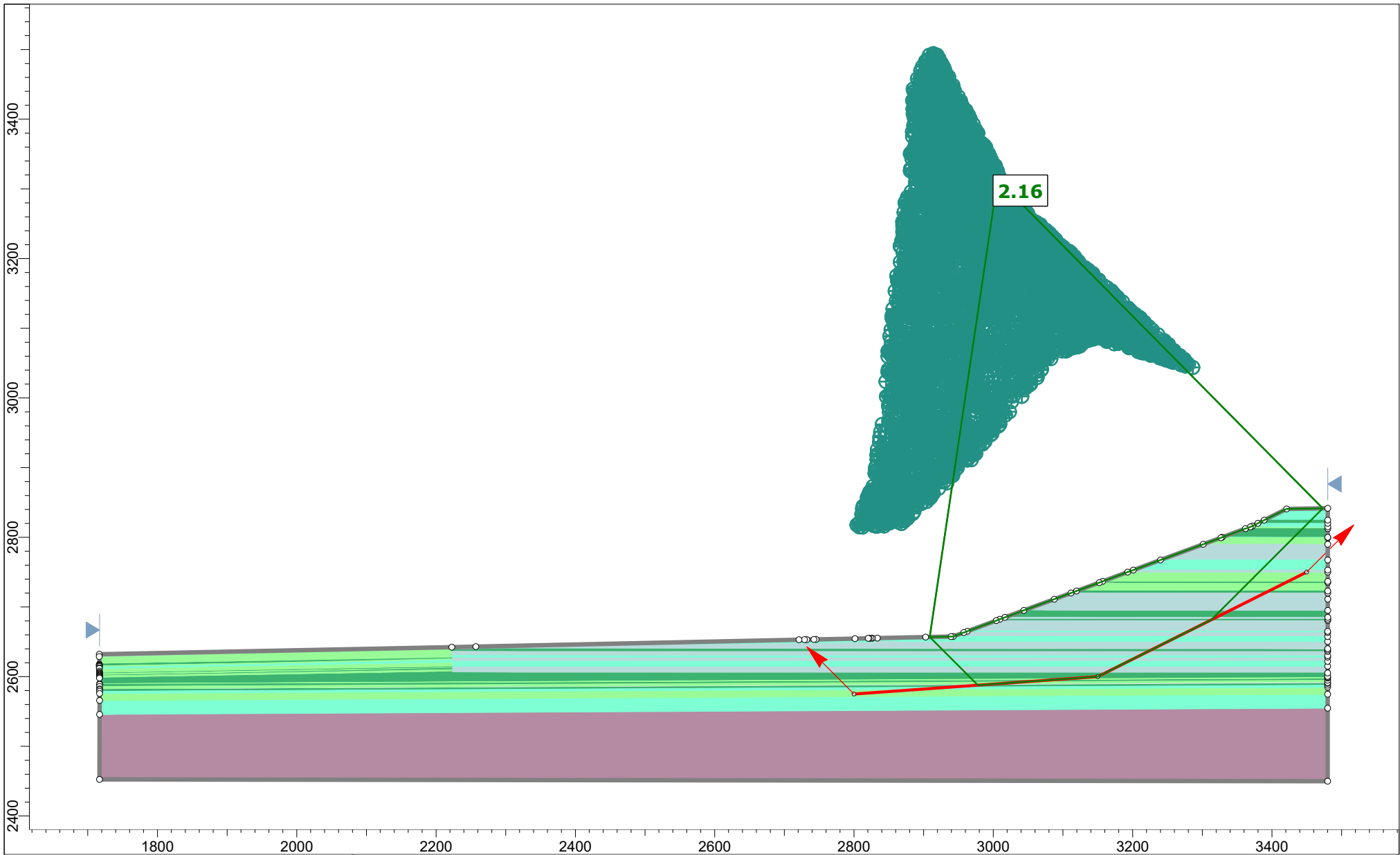
	Project		Pickles Butte		Figure 13D		
	Group		SECTION B		Scenario		
	Drawn By		SG		Company		
	Date		7/28/2022		File Name		
				Proposed Excavation 2.27H:1V		Tetra Tech	
				Seismic Loading - Block			




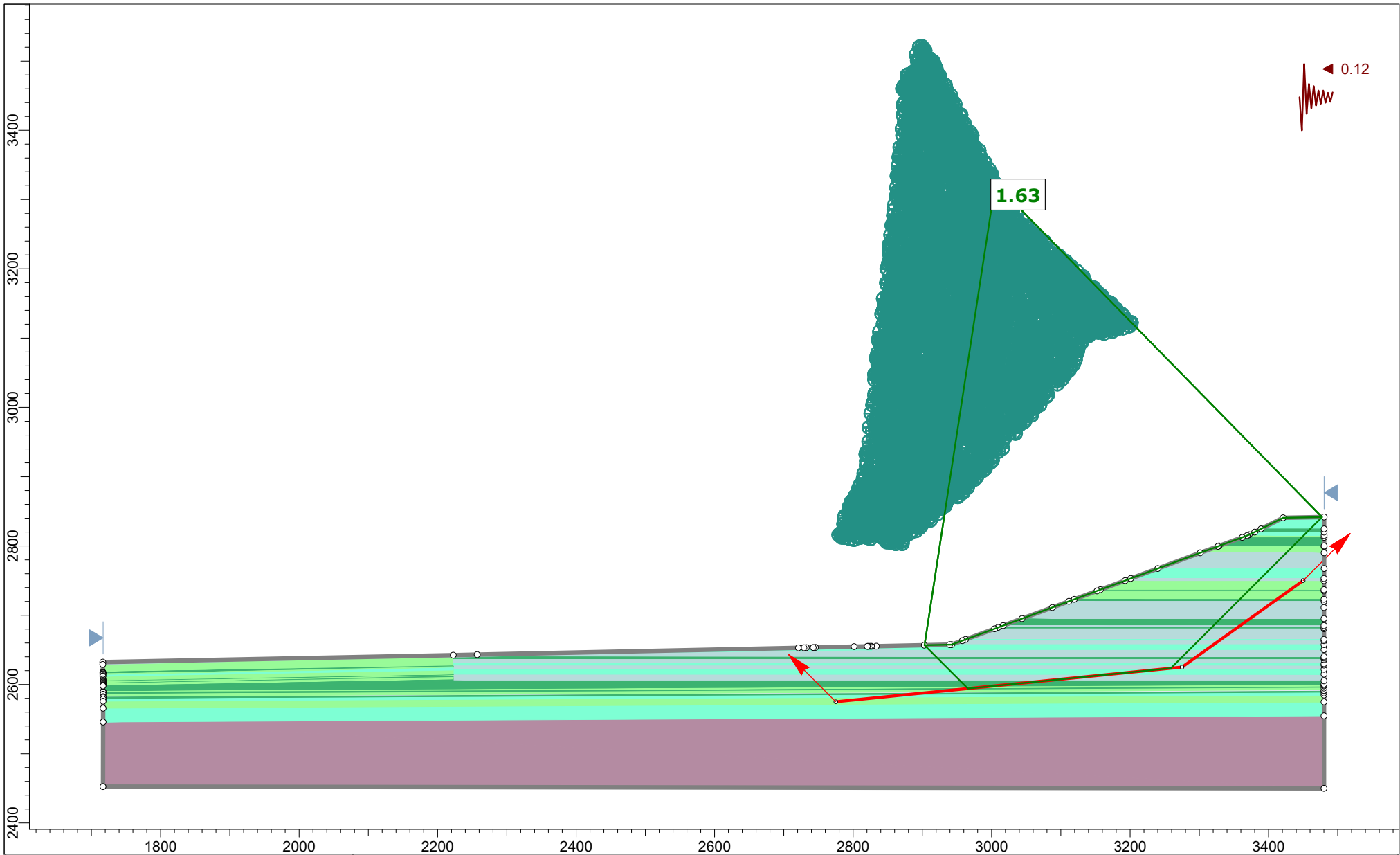
	Project		Pickles Butte		<b>Figure 14D</b>
	Group		SECTION C		
	Drawn By		SG		
	Date		7/27/2022		
	Scenario		Proposed Excavation 2.85H:1V		
		Company		Tetra Tech	
		File Name		Static Loading	












	<i>Project</i> Pickles Butte		<b>Figure 15D</b>
	<i>Group</i> SECTION C	<i>Scenario</i> Proposed Excavation 2.85H:1V	
	<i>Drawn By</i> SG	<i>Company</i> Tetra Tech	
	<i>Date</i> 7/27/2022	<i>File Name</i> Seismic Loading	

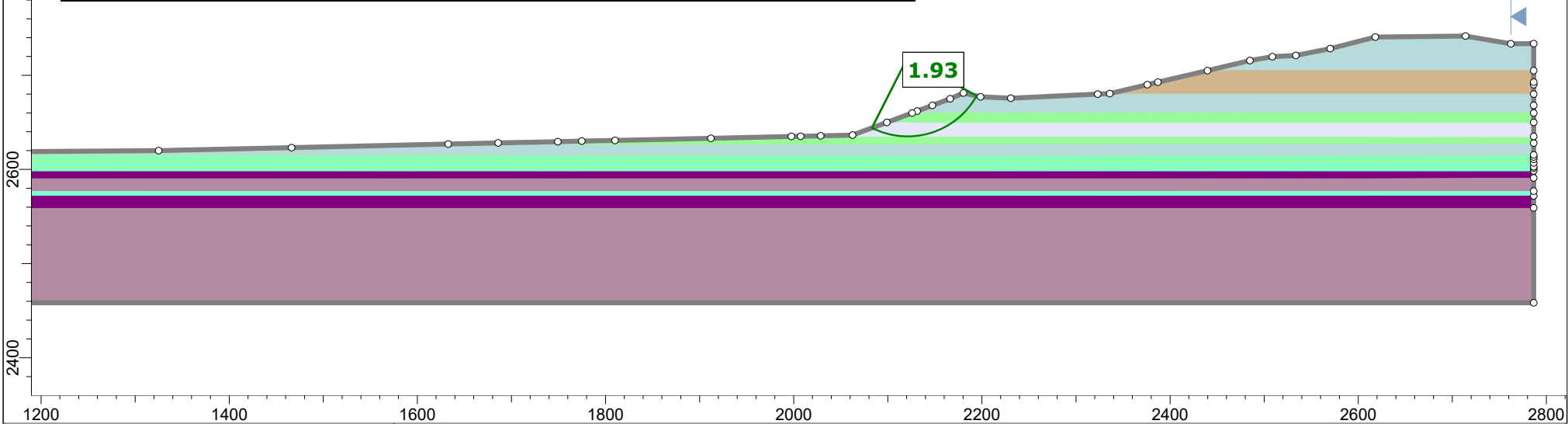



	<i>Project</i> Pickles Butte		<b>Figure 16D</b>	
	<i>Group</i> SECTION C		<i>Scenario</i> Proposed Excavation 2.85H:1V	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/28/2022		<i>File Name</i> Static Loading - Block	

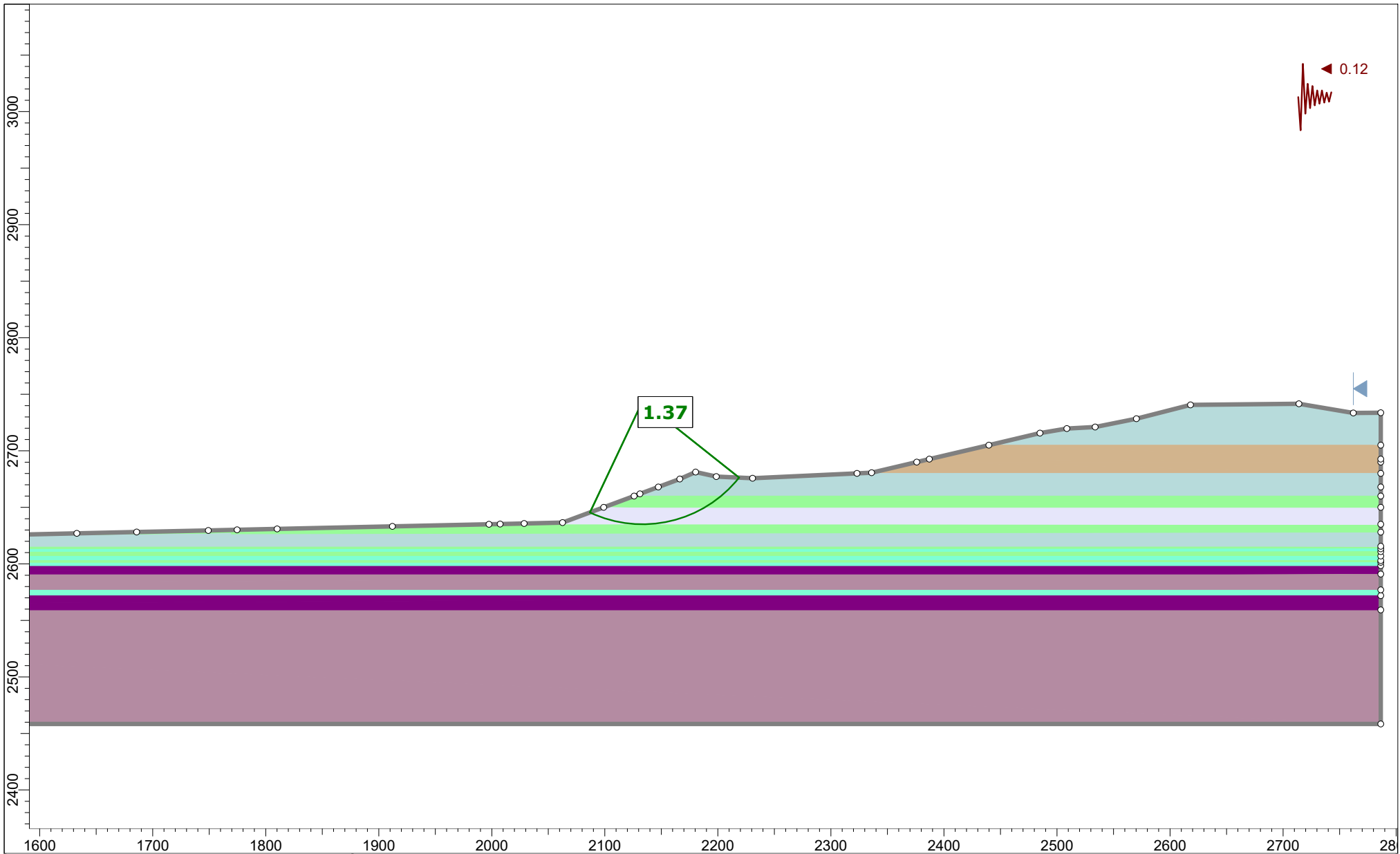



	<i>Project</i> Pickles Butte		<b>Figure 17D</b>	
	<i>Group</i> SECTION C		<i>Scenario</i> Proposed Excavation 2.85H:1V	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/28/2022		<i>File Name</i> Seismic Loading - Block Failure	

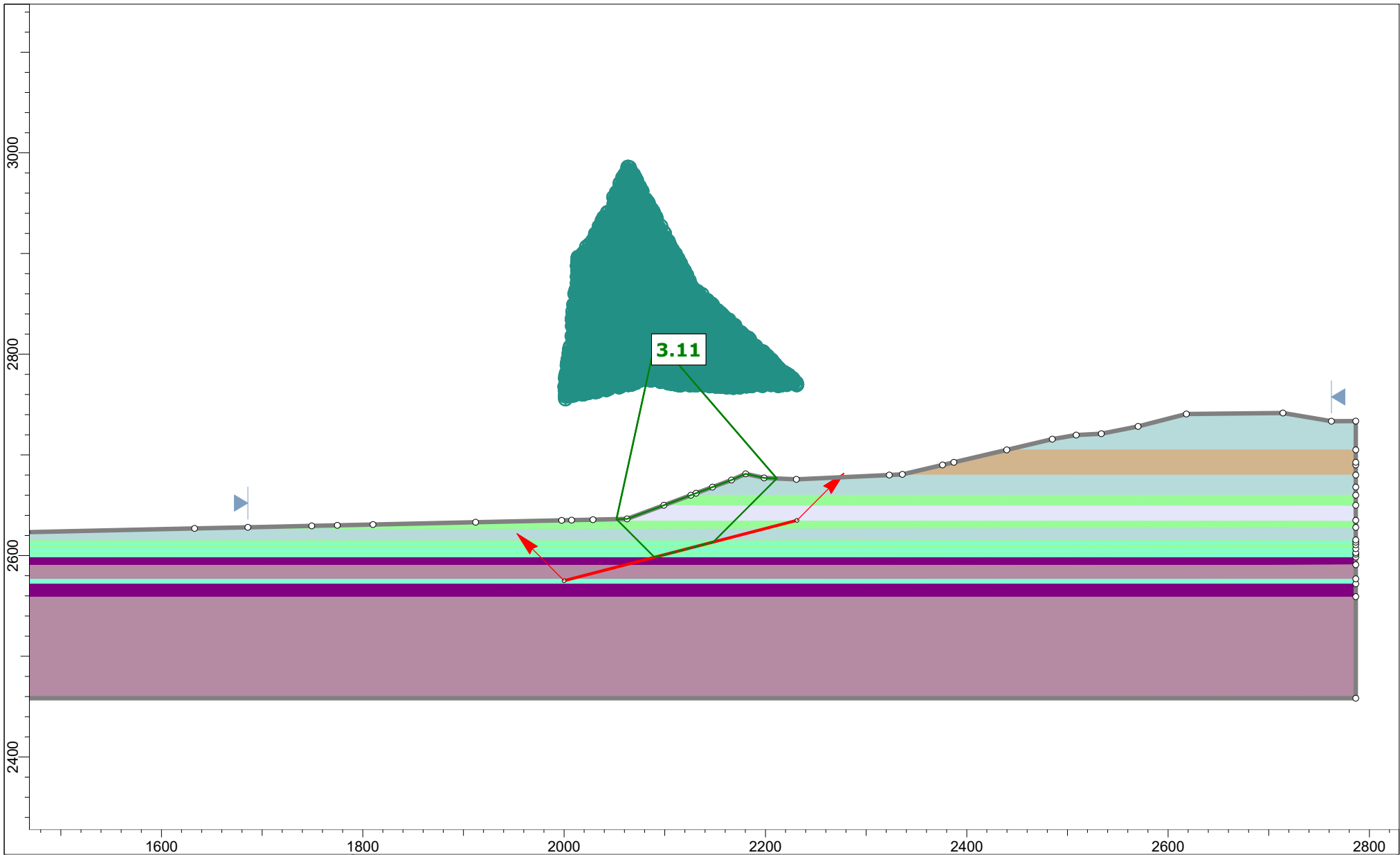
Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D
PG Silty Sand - B3		110	Mohr-Coulomb	300	28				
PG Silty Sand - B4		110	Mohr-Coulomb	123	27				
Silty Sand - B3		115	Mohr-Coulomb	400	32.8				
Silty Sand - B4		115	Mohr-Coulomb	580	29.5				
Silt - B7		110	Mohr-Coulomb	908	1				
Hard Clay - B6-99'		125	Mohr-Coulomb	7831	10				
Claystone		135	Generalized Hoek-Brown			700000	10	4	0
Sand/Gravel Interbedded - B PB13		135	Mohr-Coulomb	0	37				



	Project		Pickles Butte		Figure 18D		
	Group		SECTION D		Scenario		
	Drawn By		SG		Company		
	Date		7/27/2022		File Name		
				Proposed Excavation 2.87H:1V		Tetra Tech	
						Static Loading	



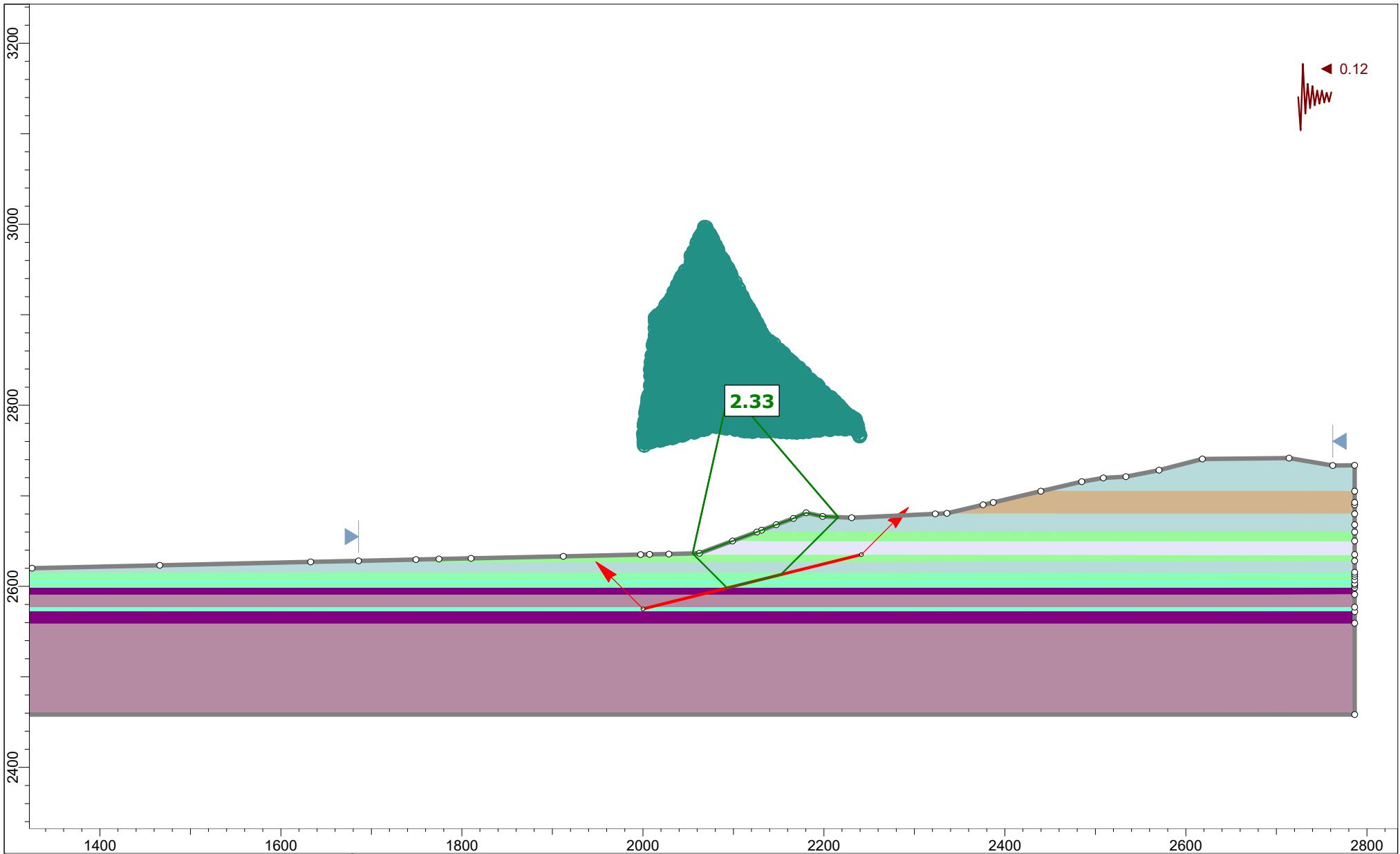
	<i>Project</i> Pickles Butte		<b>Figure 19D</b>	
	<i>Group</i> SECTION D		<i>Scenario</i> Proposed Excavation 2.87H:1V	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/27/2022		<i>File Name</i> Seismic Loading	












SLIDEINTERPRET 9.023

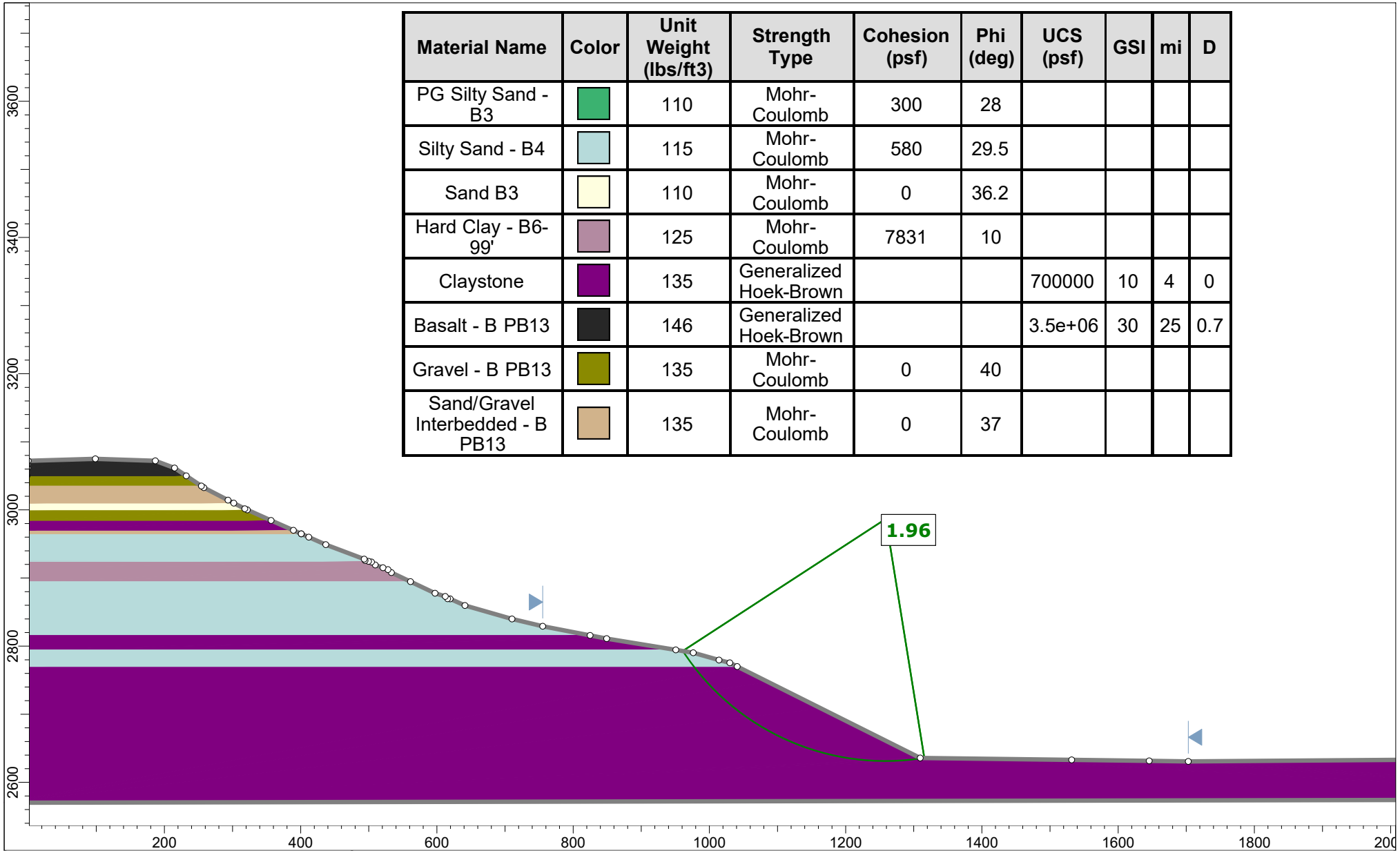
<i>Project</i>	Pickles Butte		<b>Figure 20D</b>
<i>Group</i>	SECTION D	<i>Scenario</i>	Proposed Excavation 2.87H:1V
<i>Drawn By</i>	SG	<i>Company</i>	Tetra Tech
<i>Date</i>	7/28/2022	<i>File Name</i>	Static Loading - Block





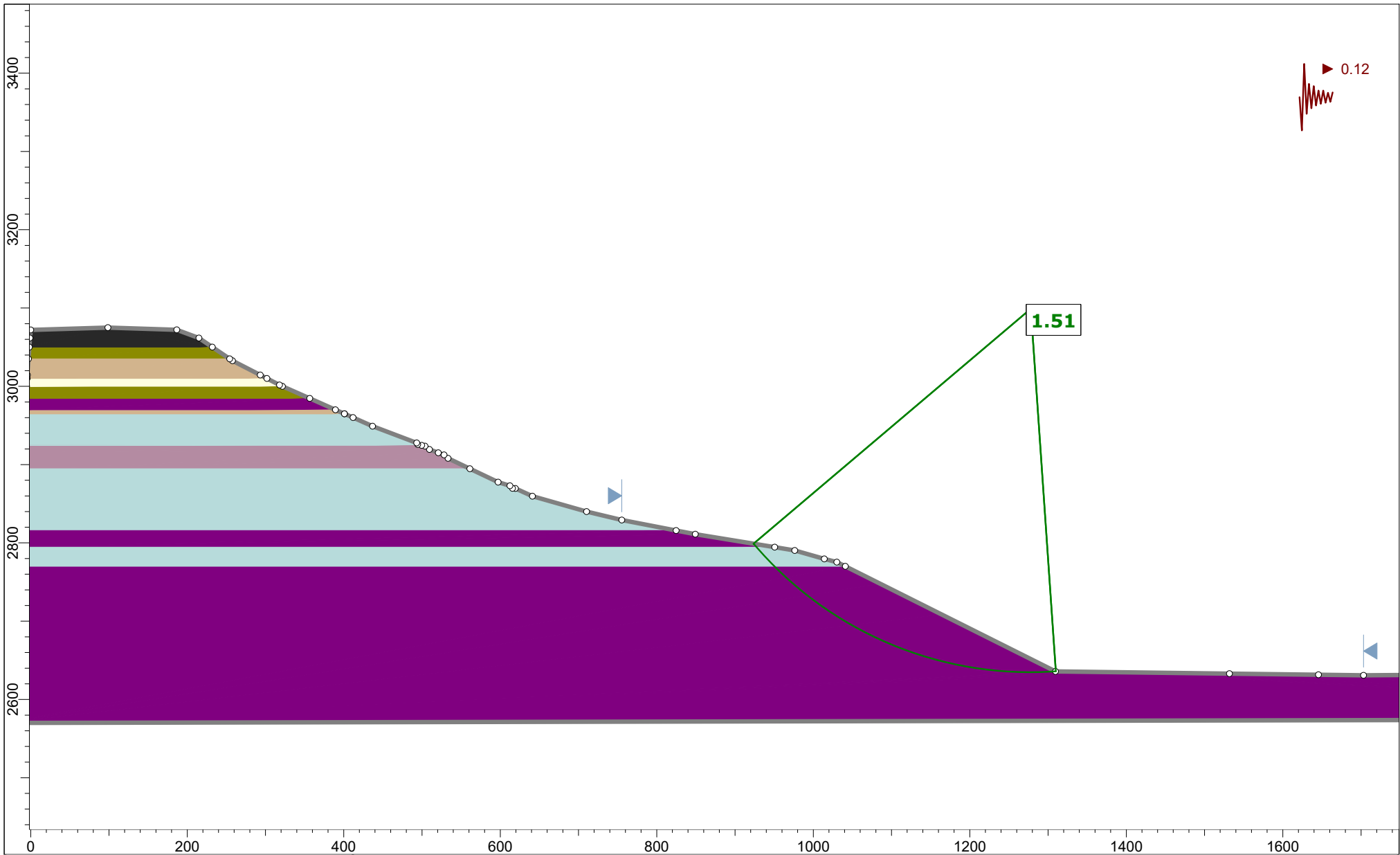
	Project		Pickles Butte		Figure 21D		
	Group		SECTION D		Scenario		
	Drawn By		SG		Company		
	Date		7/28/2022		File Name		
				Proposed Excavation 2.87H:1V		Tetra Tech	
				Seismic Loading - Block Failure			


Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D
PG Silty Sand - B3		110	Mohr-Coulomb	300	28				
Silty Sand - B4		115	Mohr-Coulomb	580	29.5				
Sand B3		110	Mohr-Coulomb	0	36.2				
Hard Clay - B6-99'		125	Mohr-Coulomb	7831	10				
Claystone		135	Generalized Hoek-Brown			700000	10	4	0
Basalt - B PB13		146	Generalized Hoek-Brown			3.5e+06	30	25	0.7
Gravel - B PB13		135	Mohr-Coulomb	0	40				
Sand/Gravel Interbedded - B PB13		135	Mohr-Coulomb	0	37				

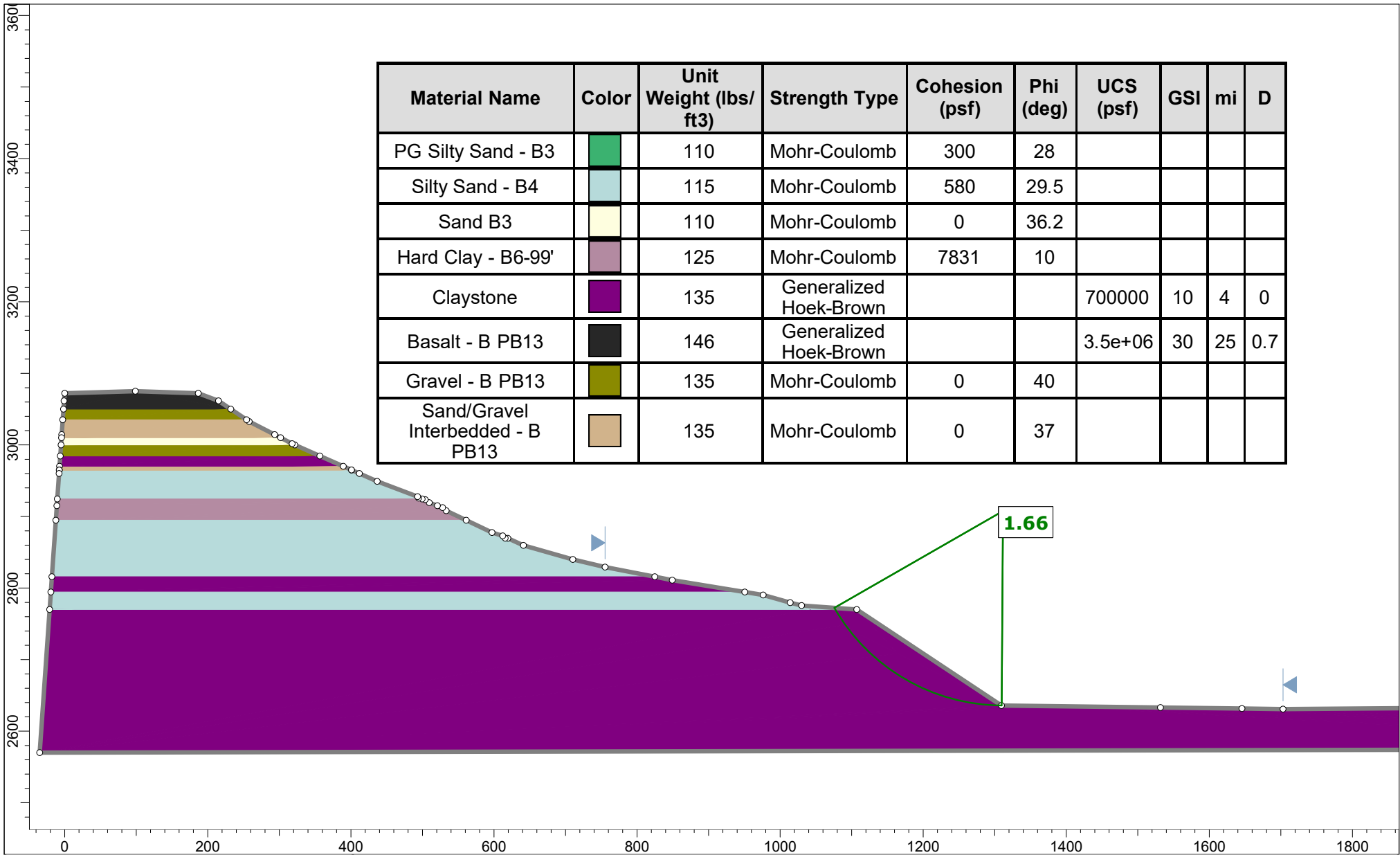


SLIDEINTERPRET 9.023

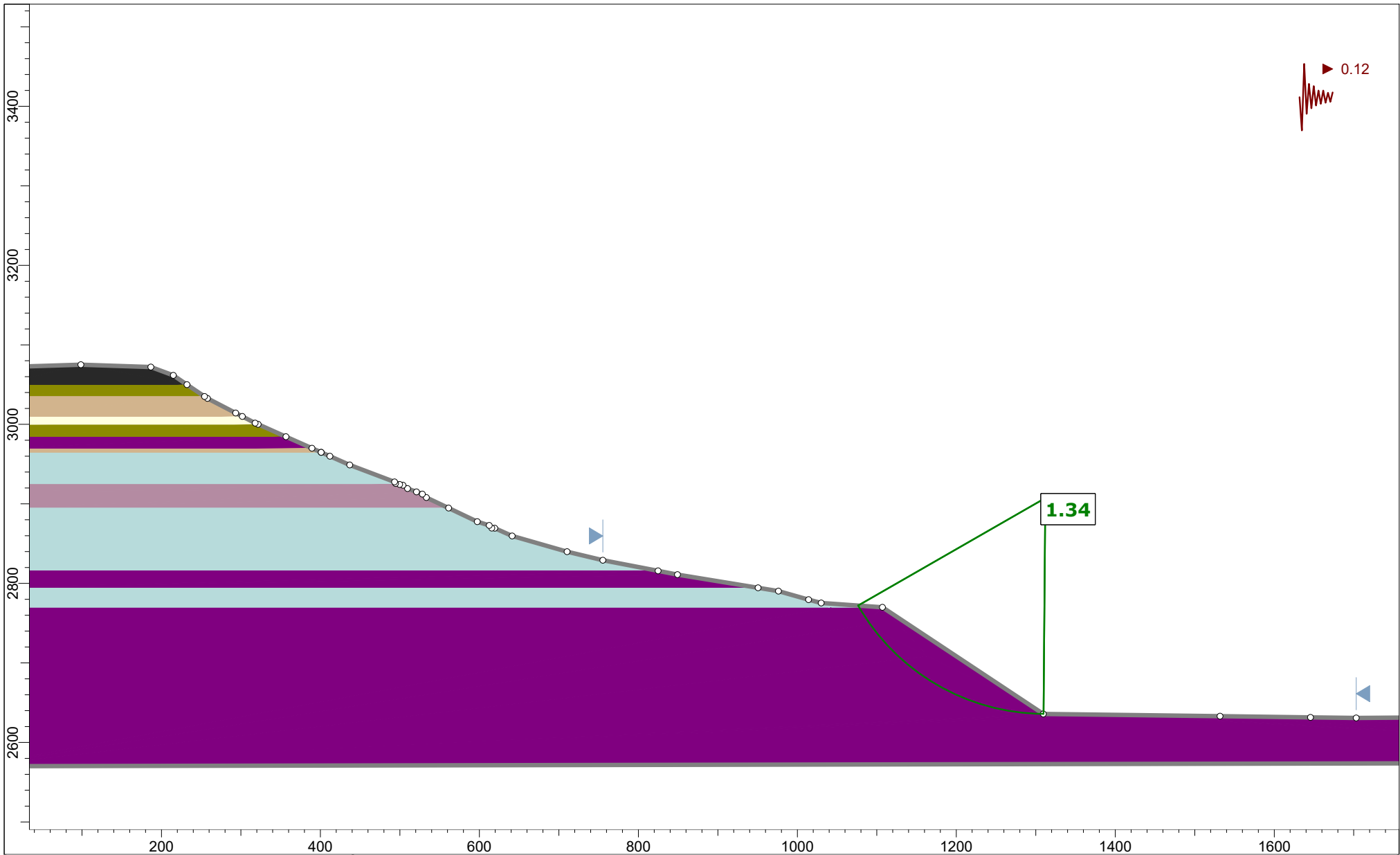
Project	Pickles Butte		Figure 22D
Group	SECTION E	Scenario	Proposed Excavation 2.27H:1V
Drawn By	SG	Company	Tetra Tech
Date	7/27/2022	File Name	Static Loading



	Project		Pickles Butte		Figure 23D	
	Group		SECTION E		Scenario	
	Drawn By		SG		Company	
	Date		7/27/2022		File Name	
					Proposed Excavation 2.27H:1V	
				Tetra Tech		
				Seismic Loading		

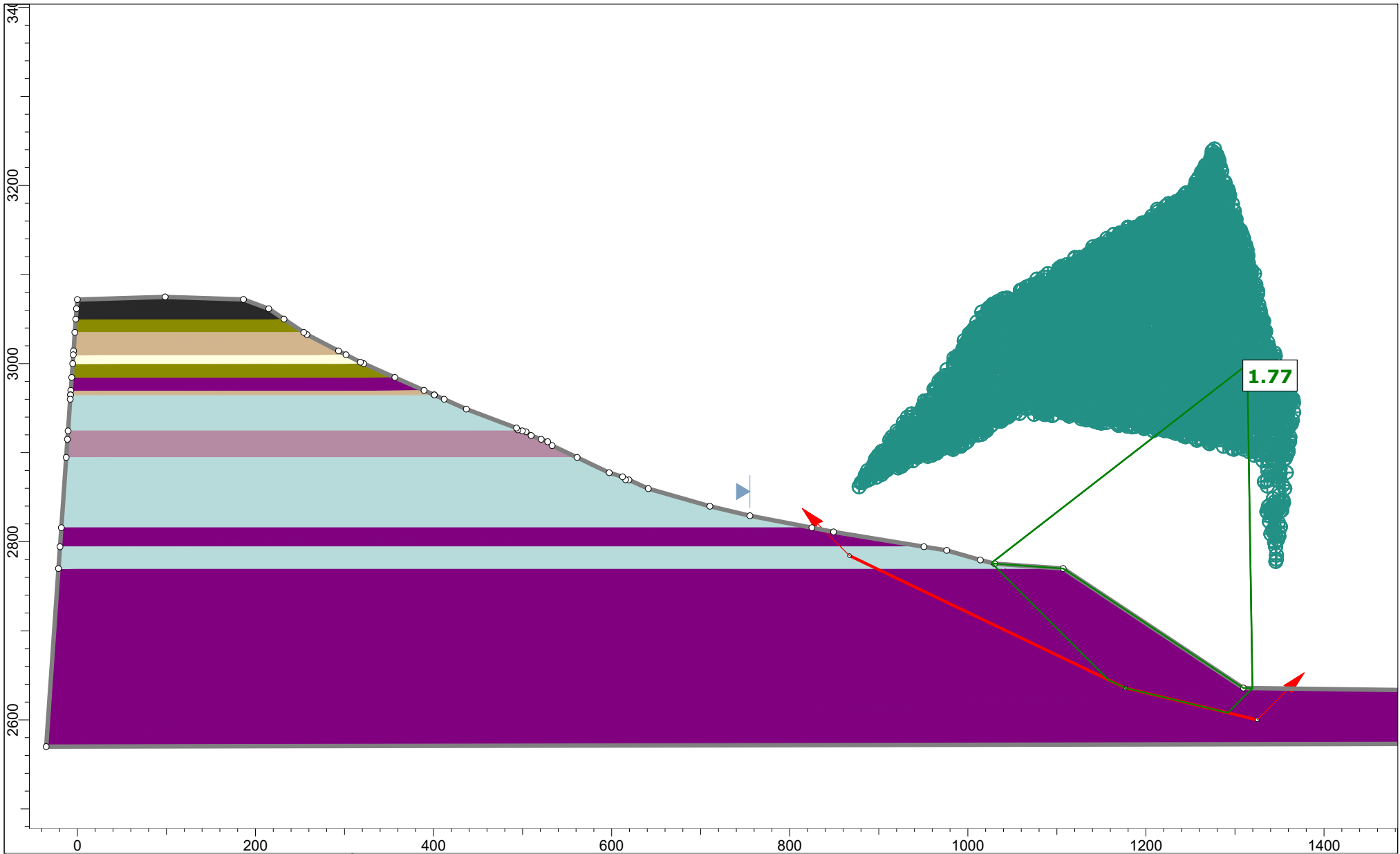



Project		Pickles Butte		Figure 24D	
Group	SECTION E	Scenario	Proposed Excavation 1.87H:1V		
Drawn By	SG	Company	Tetra Tech		
Date	7/27/2022	File Name	Static Loading		

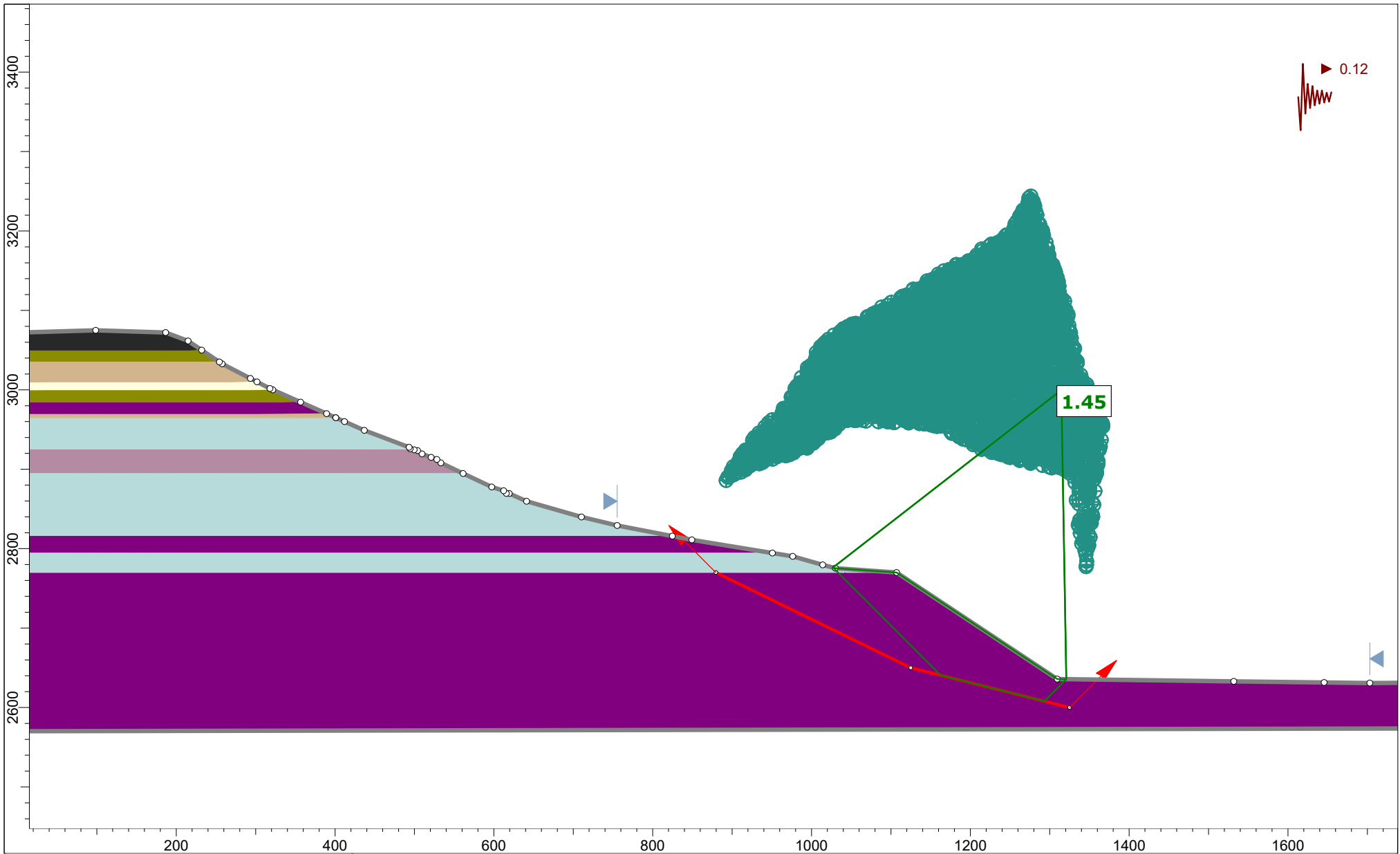



SLIDEINTERPRET 9.023

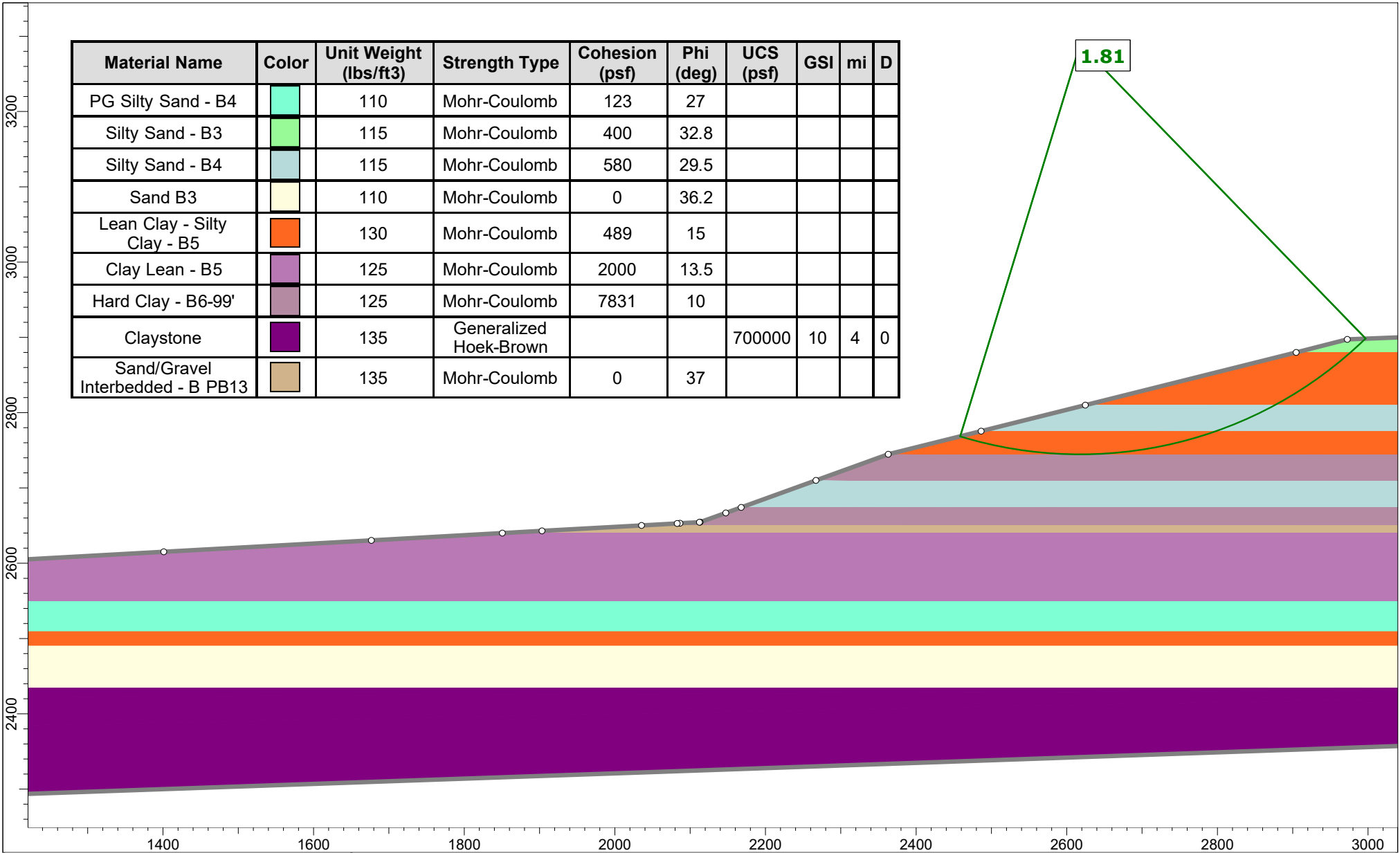
<i>Project</i>	Pickles Butte		<b>Figure 25D</b>
<i>Group</i>	SECTION E	<i>Scenario</i>	Proposed Excavation 1.87H:1V
<i>Drawn By</i>	SG	<i>Company</i>	Tetra Tech
<i>Date</i>	7/27/2022	<i>File Name</i>	Seismic Loading



	Project		Pickles Butte		Figure 26D		
	Group		SECTION E		Scenario		
	Drawn By		SG		Company		
	Date		7/28/2022		File Name		
				Proposed Excavation 1.87H:1V		Tetra Tech	
				Static Loading - Block			

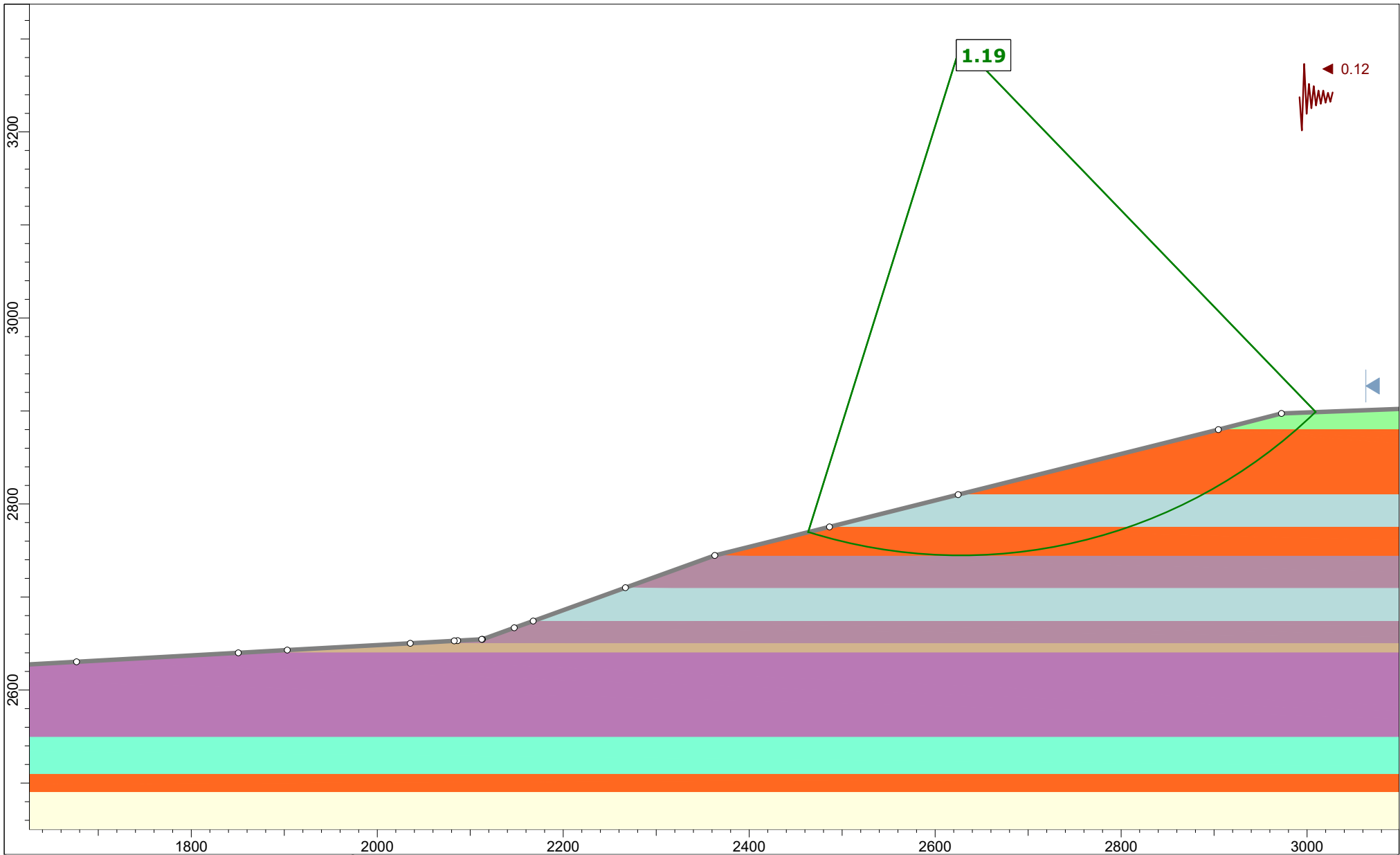



	Project		Pickles Butte		Figure 27D	
	Group		SECTION E		Scenario	
	Drawn By		SG		Company	
	Date		7/28/2022		Tetra Tech	
					File Name	
				Seismic Loading - Block		

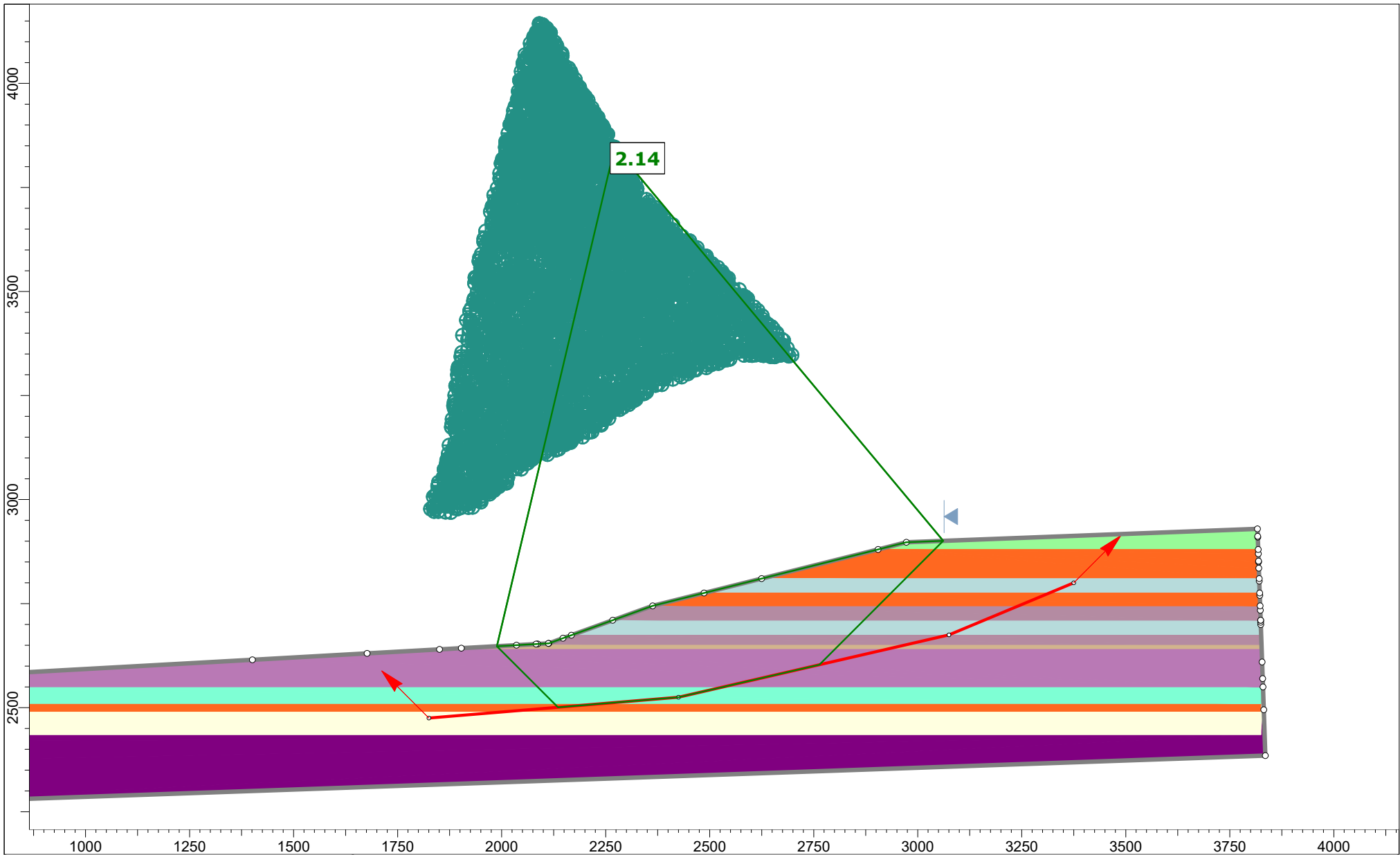



	<i>Project</i> Pickles Butte	Figure 28D
	<i>Group</i> SECTION F	<i>Scenario</i> Proposed Excavation 3H:1V Lower, 4H:1V Upper
	<i>Drawn By</i> SG	<i>Company</i> Tetra Tech
	<i>Date</i> 7/28/2022	<i>File Name</i> Static Loading

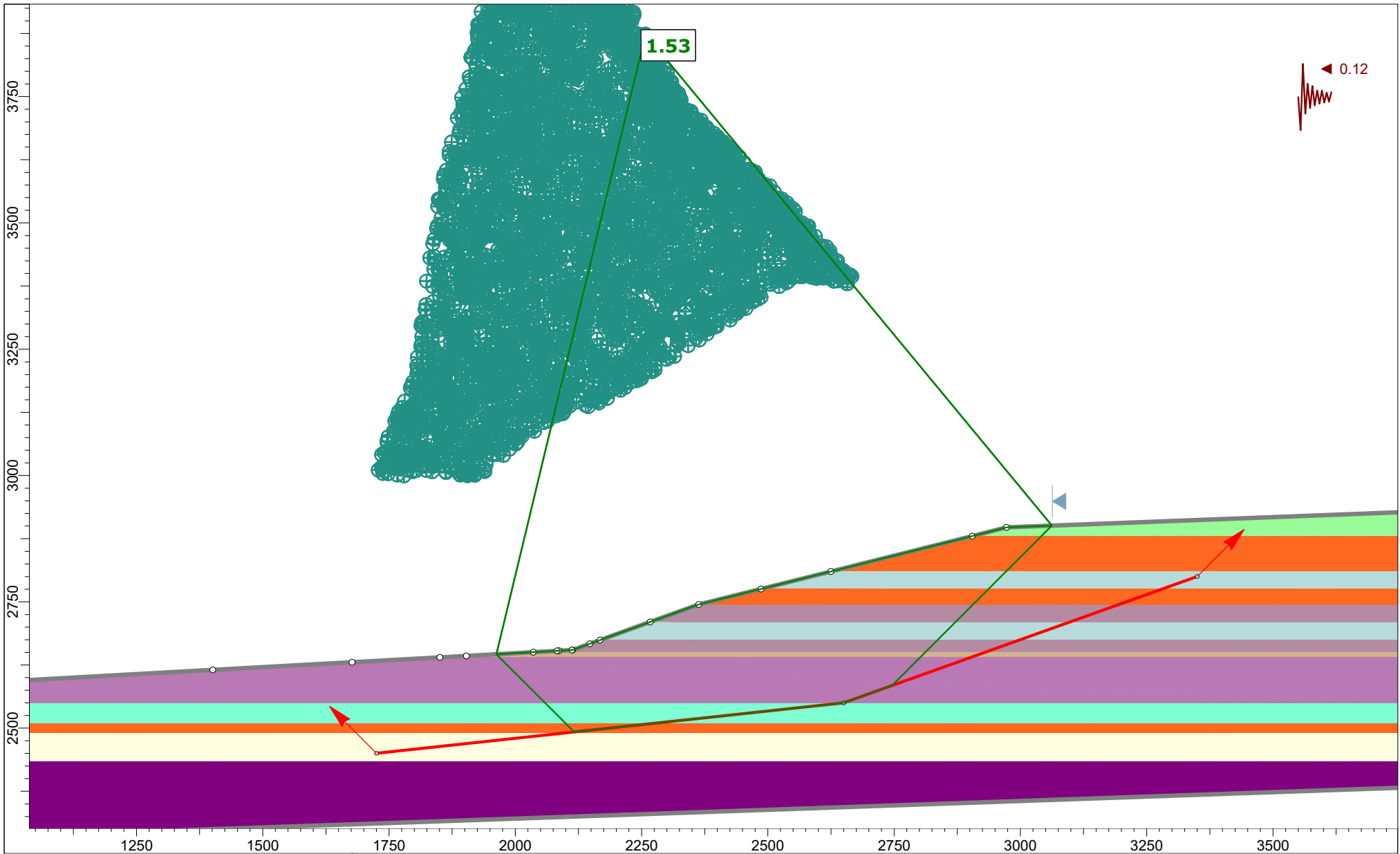





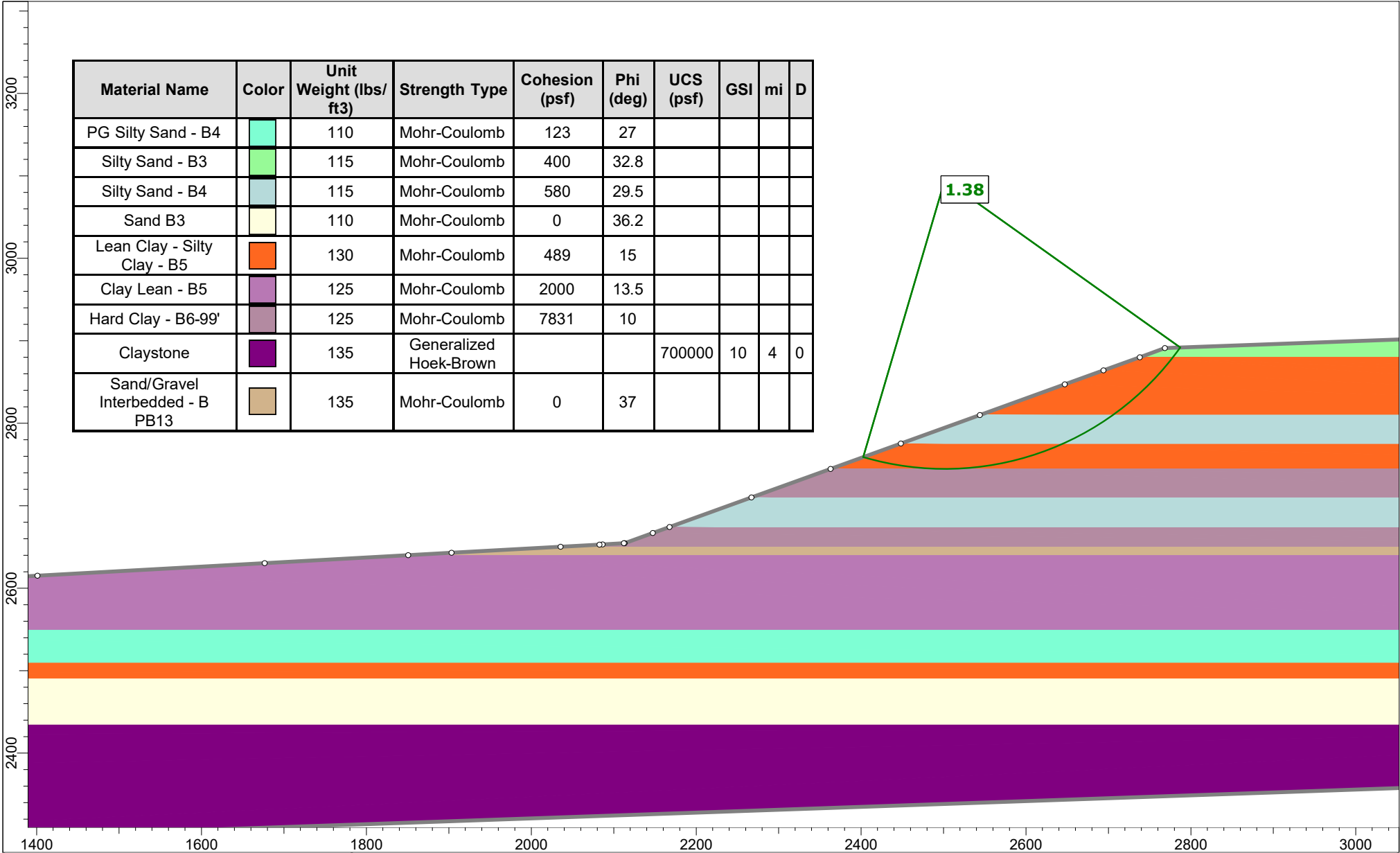
	Project		Pickles Butte		Figure 29D	
	Group		SECTION F		Scenario	
	Drawn By		SG		Company	
	Date		7/28/2022		File Name	
					Proposed Excavation 3H:1V Lower, 4H:1V Upper	
				Tetra Tech		
				Seismic Loading		



	<i>Project</i> Pickles Butte		<b>Figure 30D</b>	
	<i>Group</i> SECTION F		<i>Scenario</i> Proposed Excavation 3H:1V Lower, 4H:1V Upper	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/28/2022		<i>File Name</i> Static Loading - Block Failure	

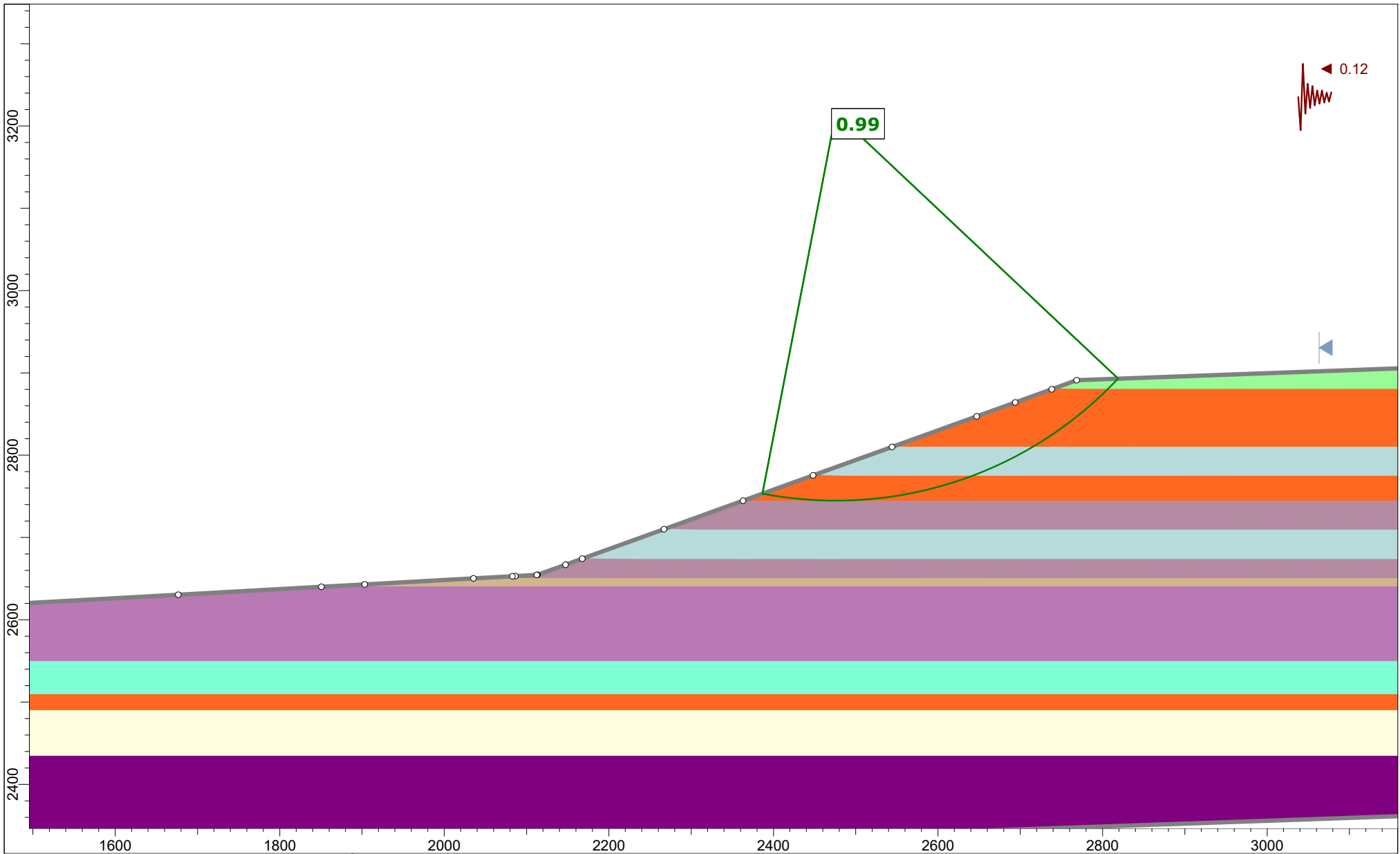



	<i>Project</i> Pickles Butte		<b>Figure 31D</b>
	<i>Group</i> SECTION F	<i>Scenario</i> Proposed Excavation 3H:1V Lower, 4H:1V Upper	
	<i>Drawn By</i> SG	<i>Company</i> Tetra Tech	
	<i>Date</i> 7/28/2022	<i>File Name</i> Static Loading - Block Failure	

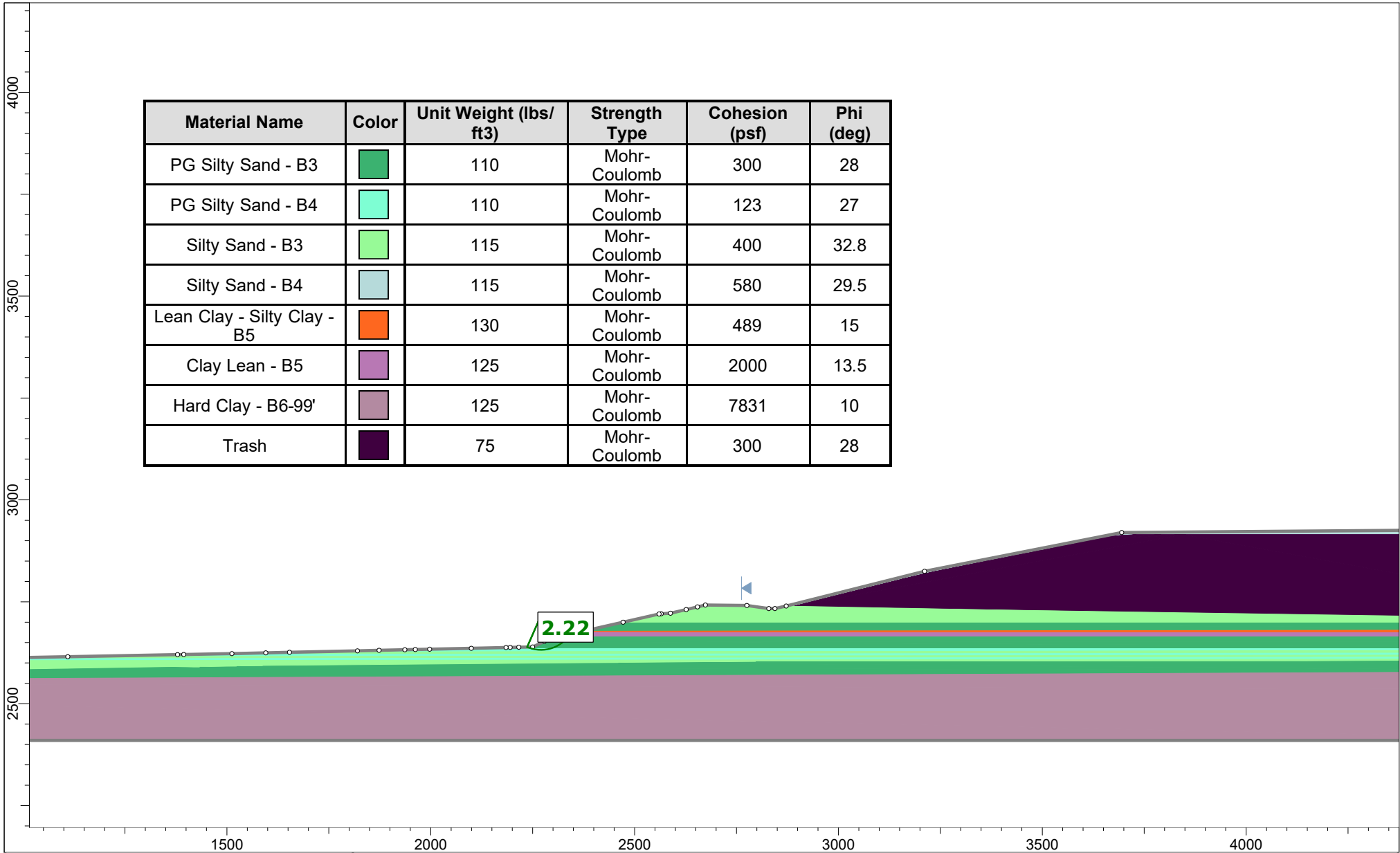


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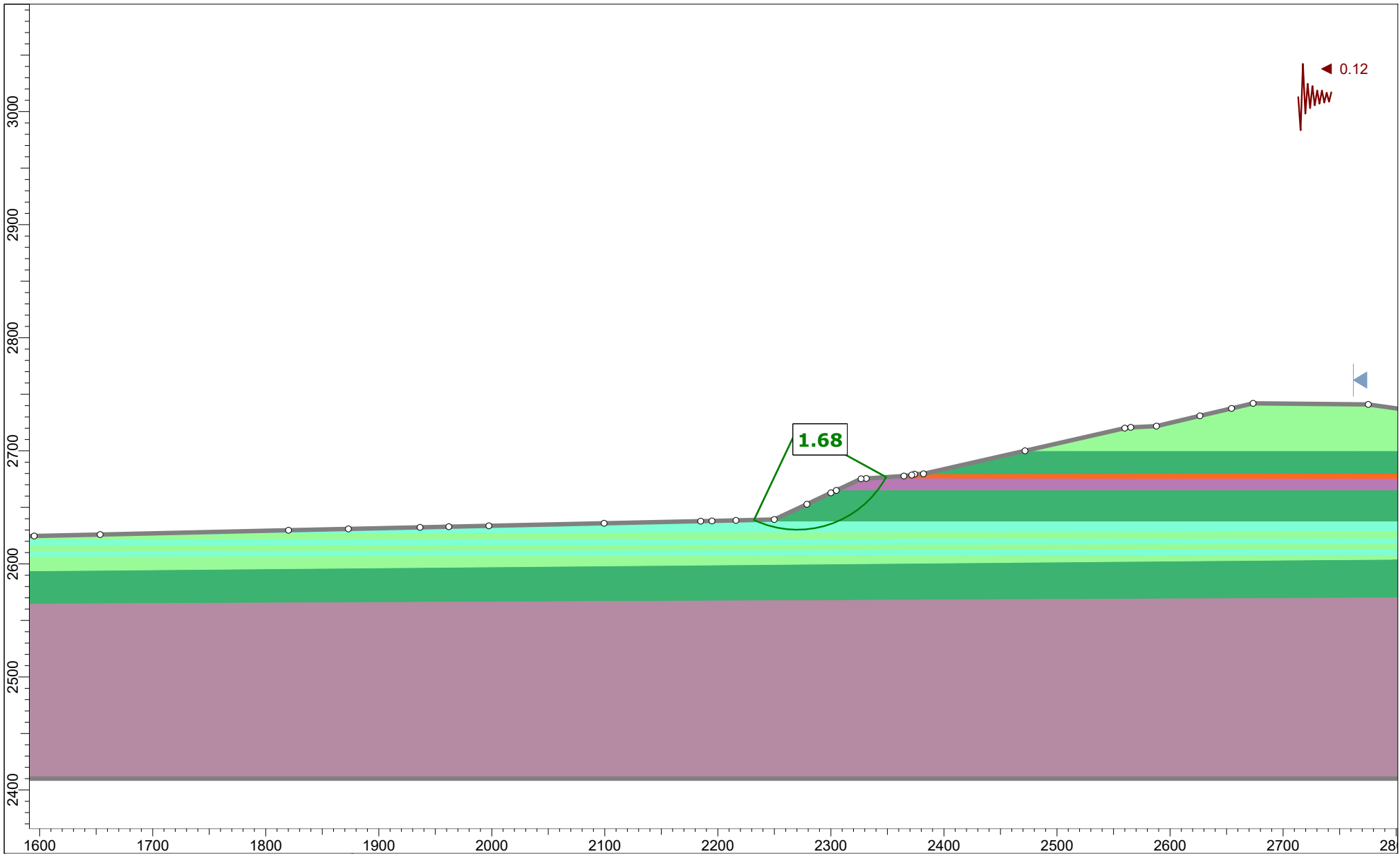
	Project	Pickles Butte		Figure 32D
	Group	SECTION F	Scenario	Proposed Excavation 3H:1V
	Drawn By	SG	Company	Tetra Tech
	Date	7/28/2022	File Name	Static Loading
	SLIDEINTERPRET 9.023			




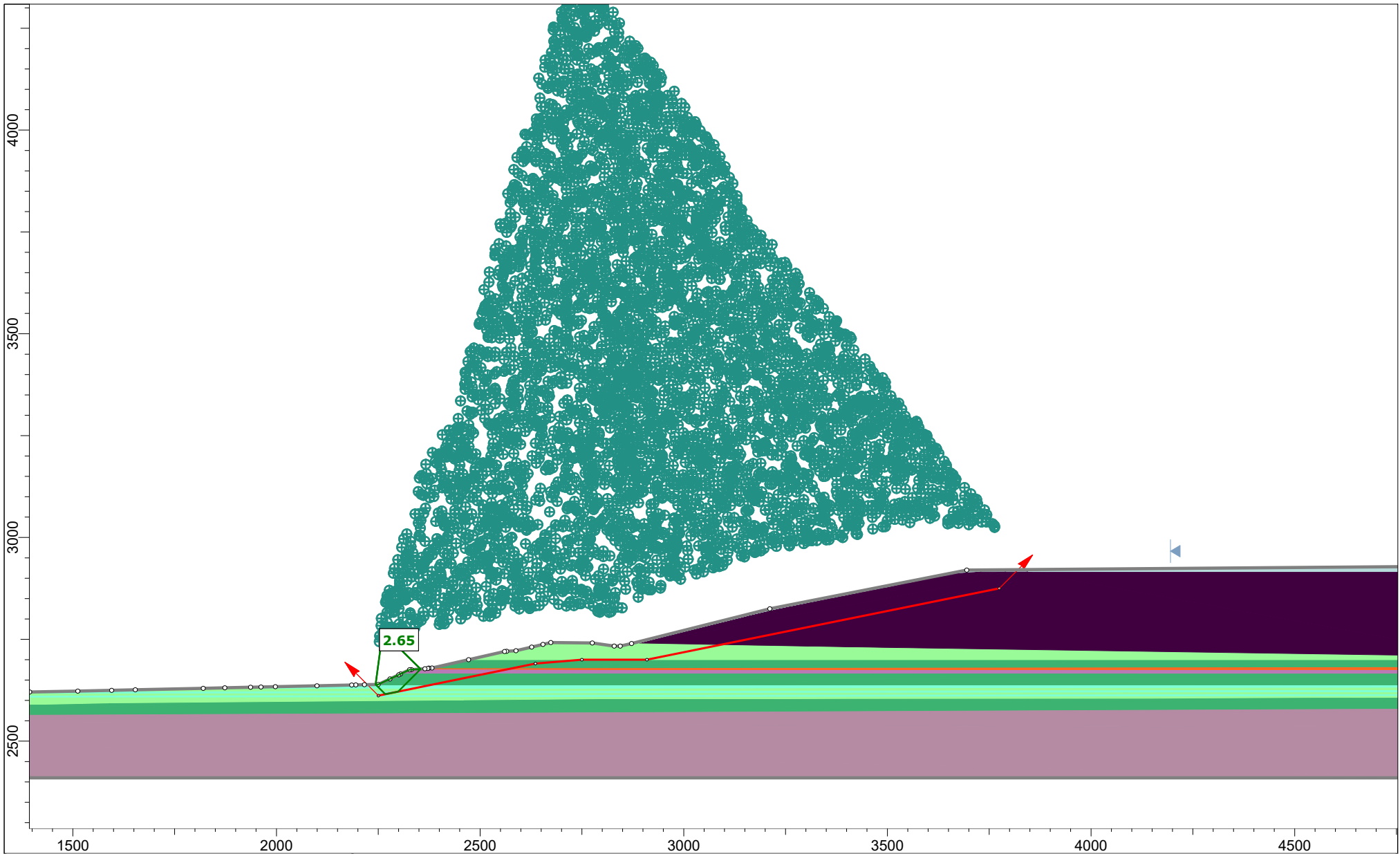
	Project		Pickles Butte		<b>Figure 33D</b>	
	Group		SECTION F	Scenario		Proposed Excavation 3H:1V
	Drawn By		SG	Company		Tetra Tech
	Date		7/28/2022	File Name		Seismic Loading
	SLIDEINTERPRET 9.023					




	Project	Pickles Butte		Figure 34D
	Group	SECTION G	Scenario	Proposed Excavation 2.6H:1V
	Drawn By	SG	Company	Tetra Tech
	Date	7/28/2022	File Name	Static Loading

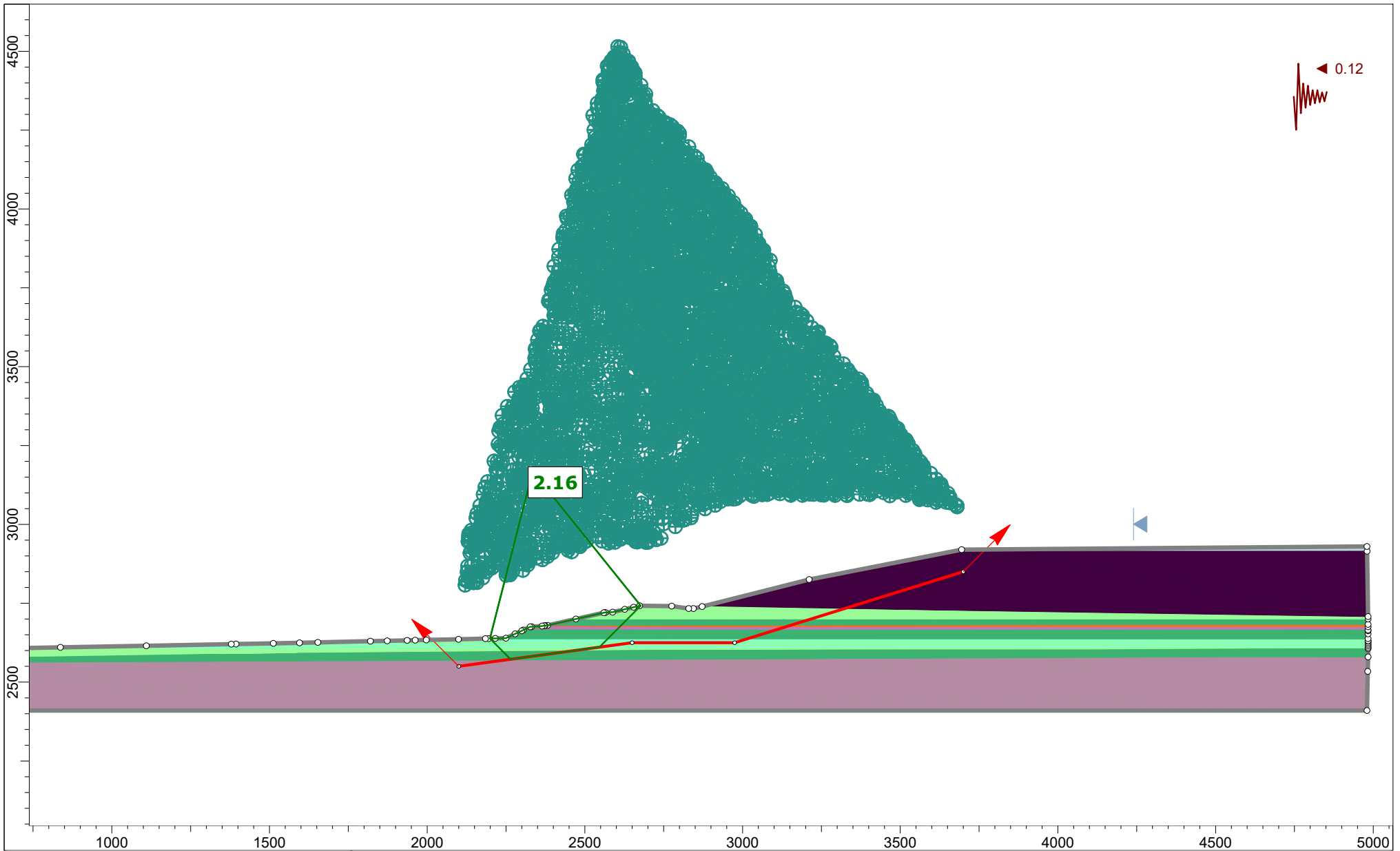



	Project		Pickles Butte		Figure 35D	
	Group		SECTION G		Scenario	
	Drawn By		SG		Company	
	Date		7/28/2022		File Name	
					Proposed Excavation 2.6H:1V	
				Tetra Tech		
				Seismic Loading		

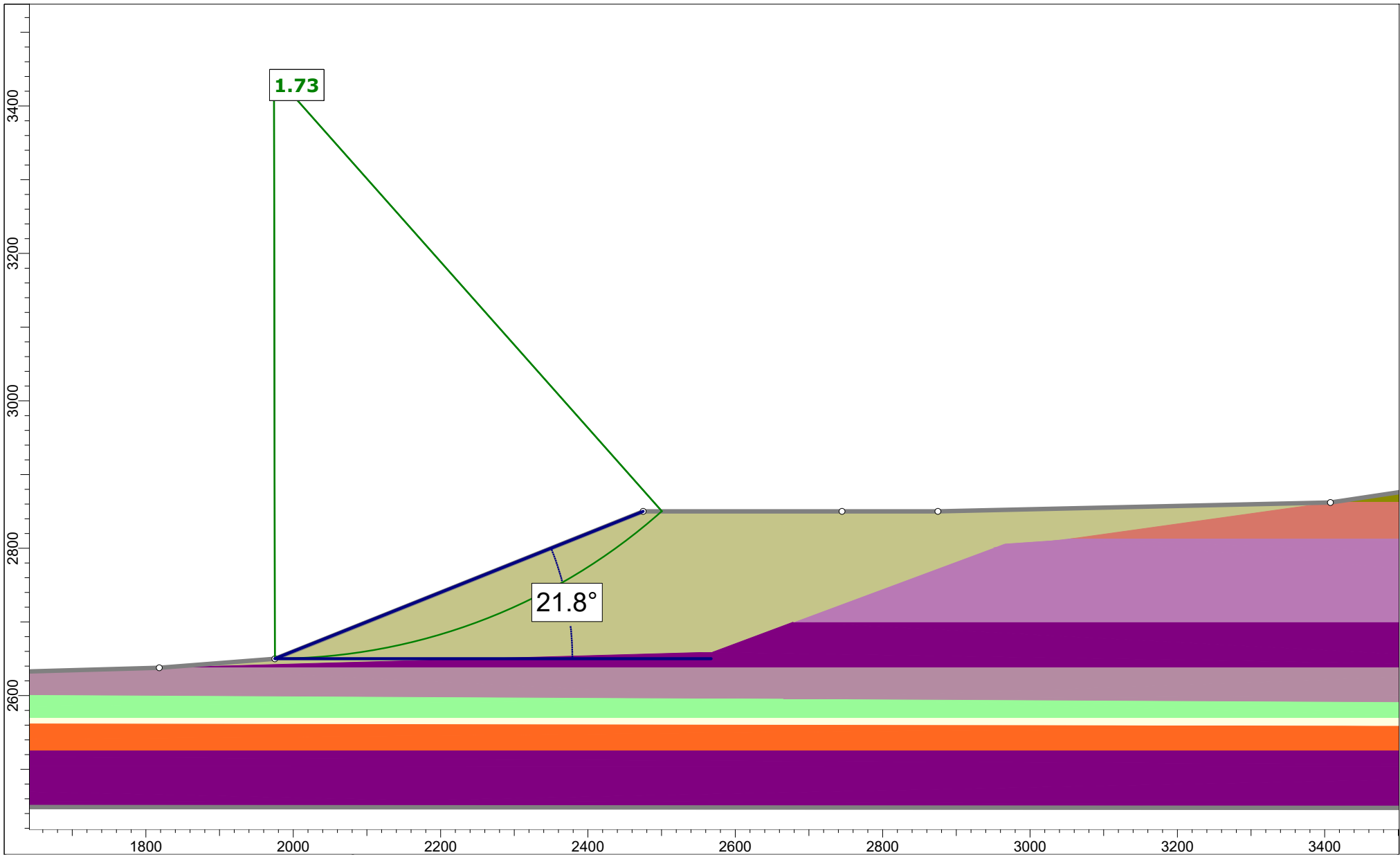



	Project		Pickles Butte		Figure 36D	
	Group		SECTION G	Scenario		Proposed Excavation 2.6H:1V
	Drawn By		SG	Company		Tetra Tech
	Date		7/28/2022	File Name		Static Loading - Block

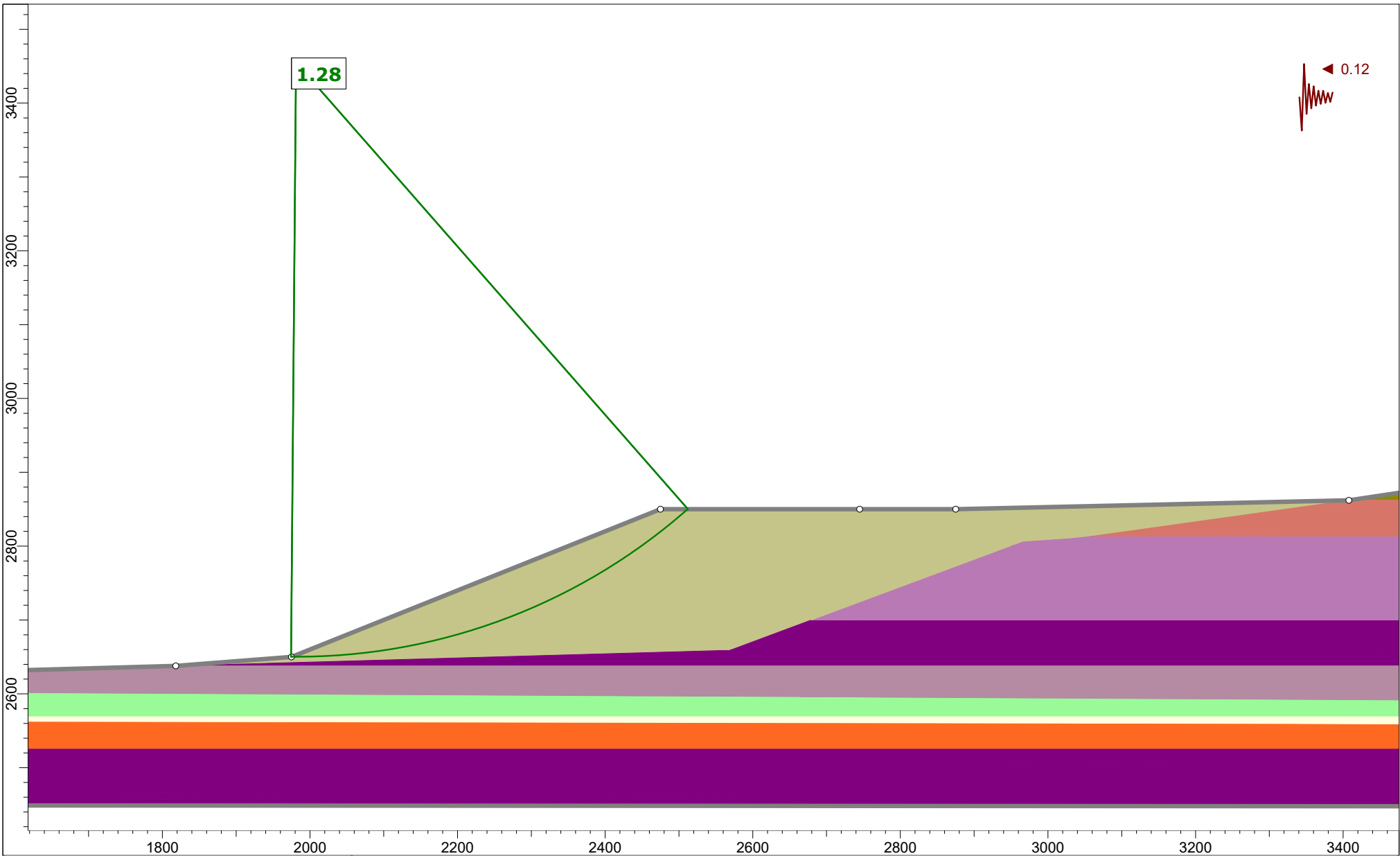





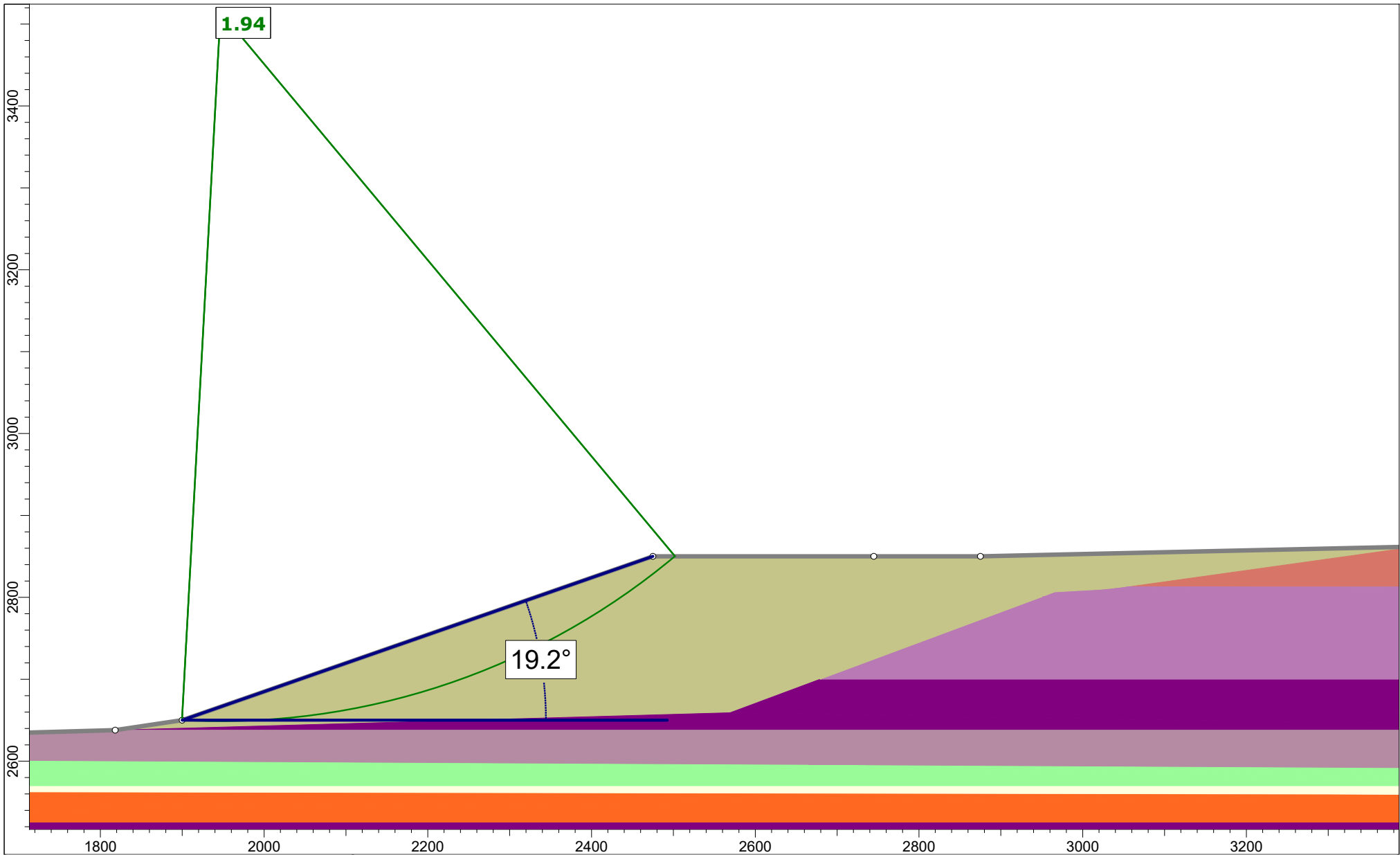
	Project		Pickles Butte		Figure 37D		
	Group		SECTION G		Scenario		
	Drawn By		SG		Company		
	Date		7/28/2022		File Name		
				Proposed Excavation 2.6H:1V		Tetra Tech	
				Seismic Loading - Block			




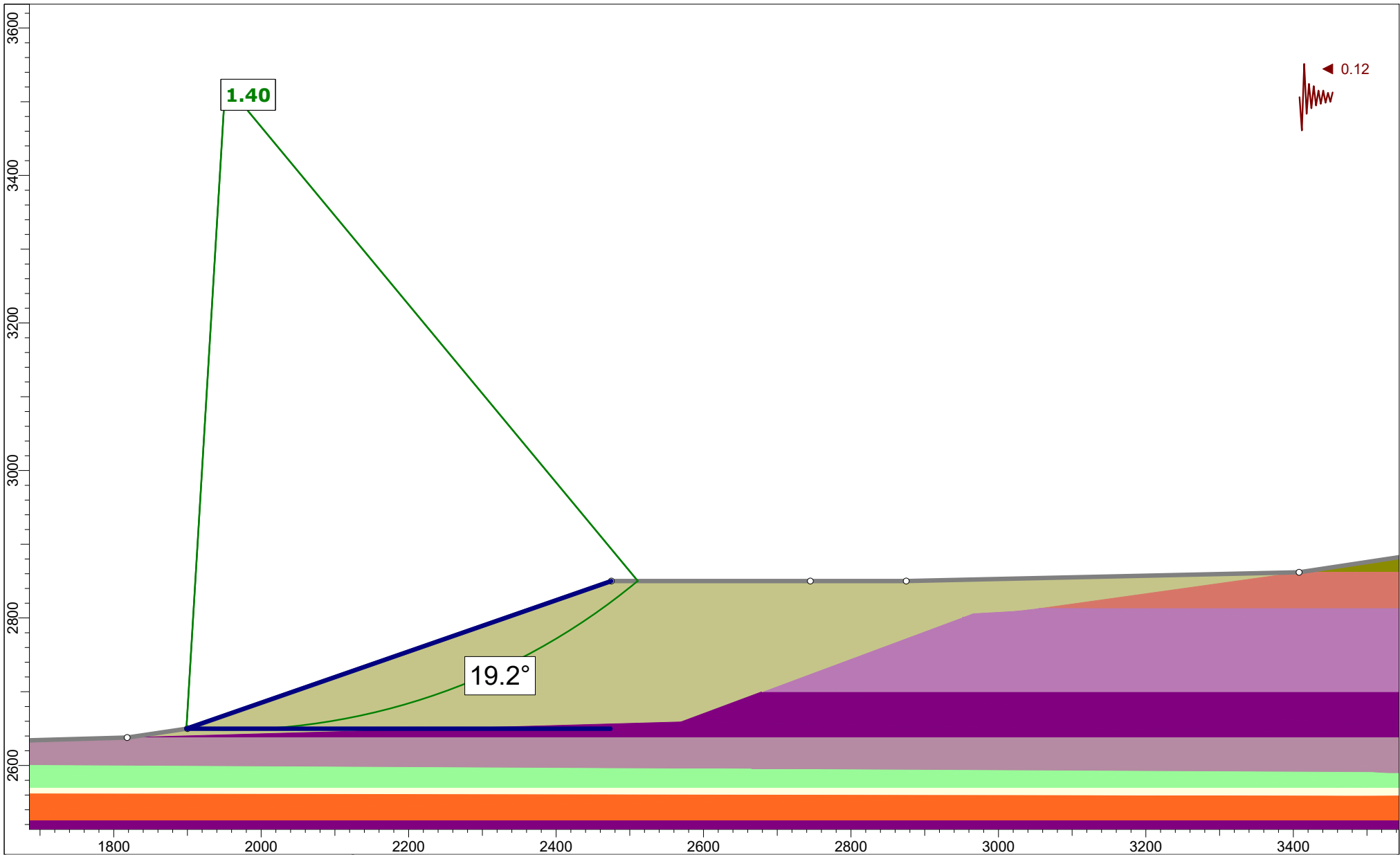
	<i>Project</i> Pickles Butte		<b>Figure 38D</b>	
	<i>Group</i> SECTION E		<i>Scenario</i> 2.75H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 8/4/2022		<i>File Name</i> Trash Backfill - Static	




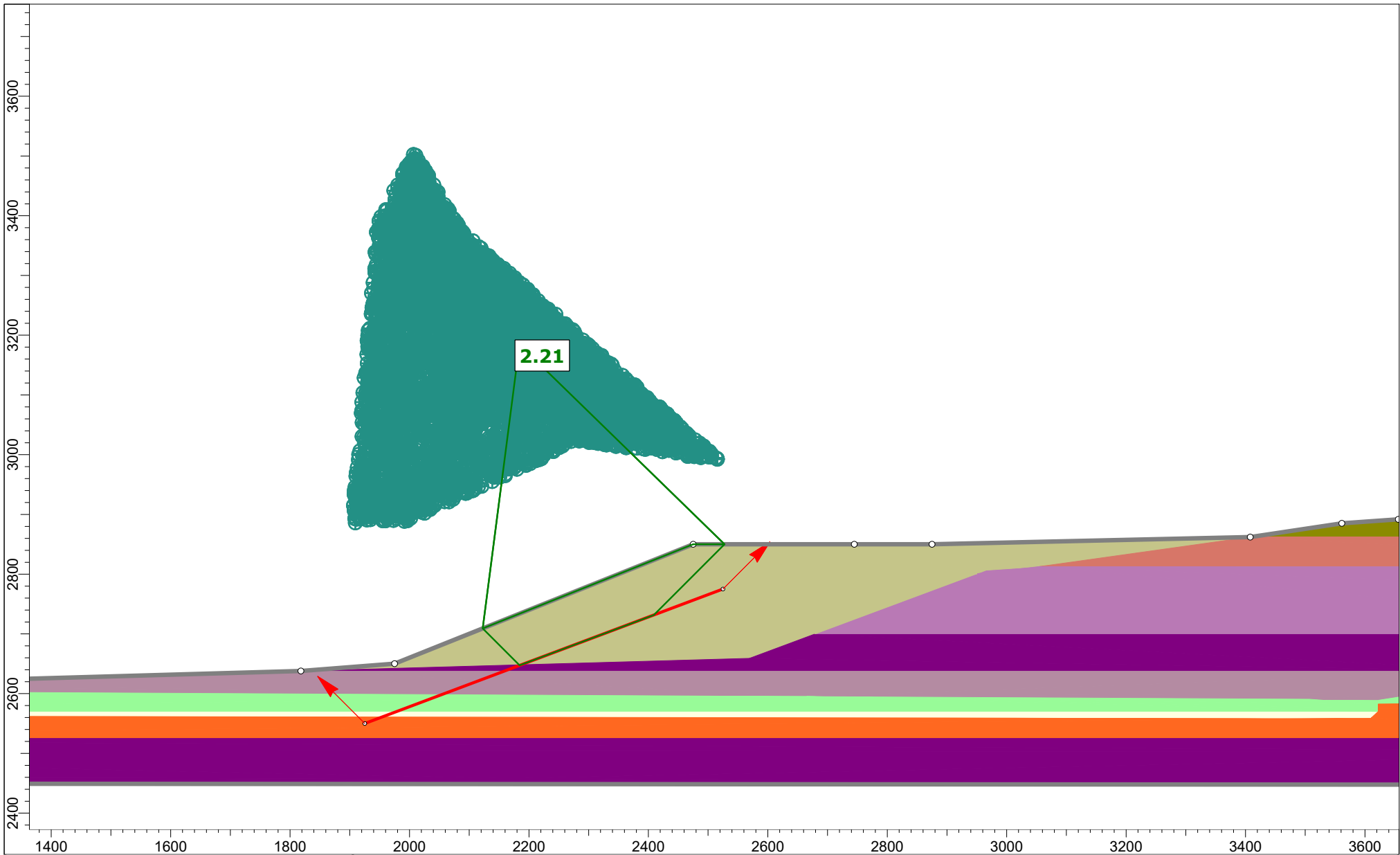
	<i>Project</i> Pickles Butte		<b>Figure 39D</b>
	<i>Group</i> SECTION E	<i>Scenario</i> 2.75H:1V Slope	
	<i>Drawn By</i> SG	<i>Company</i> Tetra Tech	
	<i>Date</i> 8/4/2022	<i>File Name</i> Trash Backfill - Seismic	




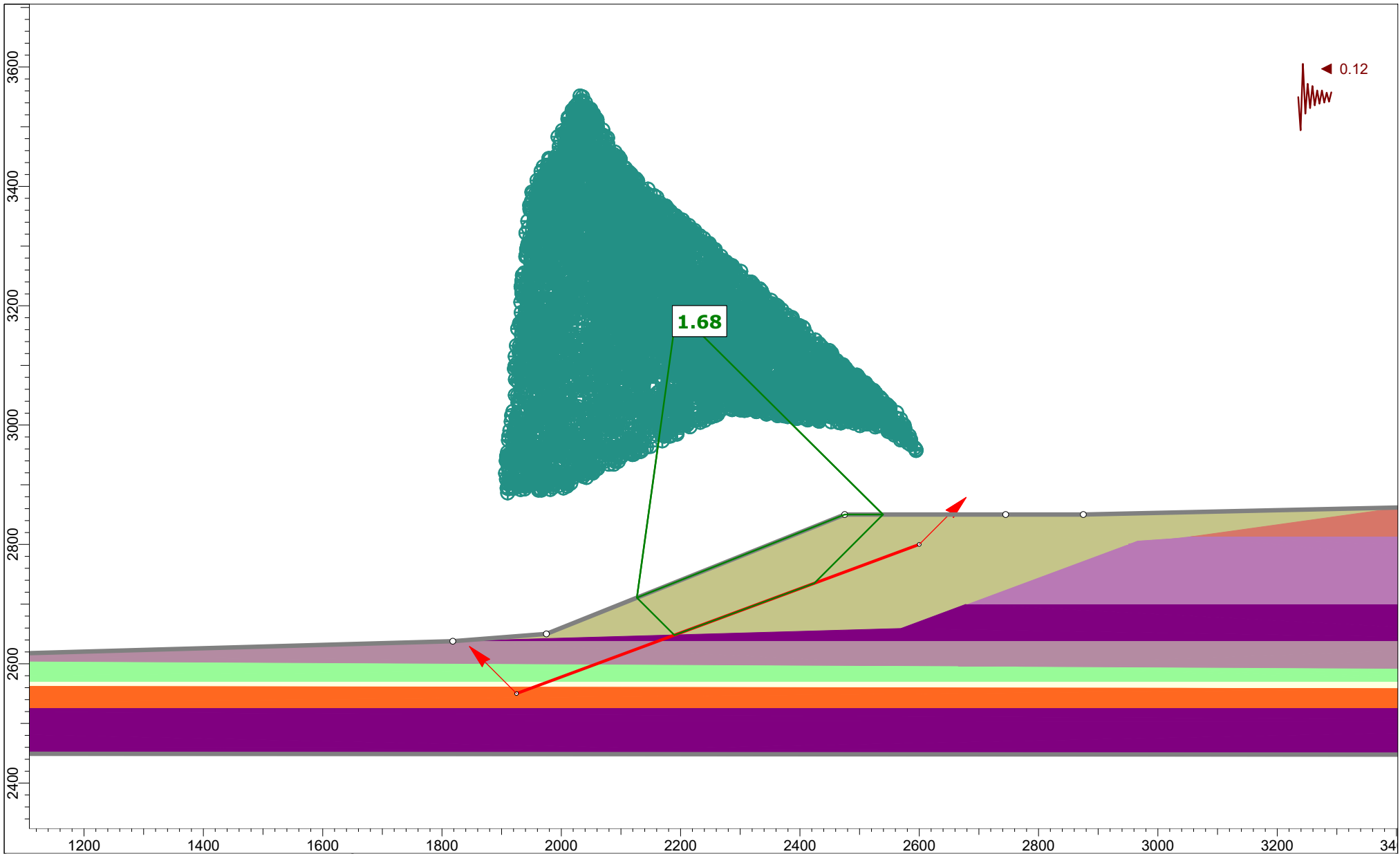
	Project		Pickles Butte		<b>Figure 40D</b>
	Group		SECTION E		
	Drawn By		SG		
	Date		8/4/2022		
	Scenario		3H:1V Slope		
		Company		Tetra Tech	
		File Name		Trash Backfill	




	<i>Project</i> Pickles Butte		<b>Figure 41D</b>	
	<i>Group</i> SECTION E		<i>Scenario</i> 3H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 8/4/2022		<i>File Name</i> Trash Backfill - Seismic	
	SLIDEINTERPRET 9.023			



	<i>Project</i> Pickles Butte		<b>Figure 42D</b>	
	<i>Group</i> SECTION E		<i>Scenario</i> 3H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 8/5/2022		<i>File Name</i> Trash Backfill Block Sliding- Static	
	<small>SLIDEINTERPRET 9.023</small>			












	<i>Project</i> Pickles Butte		<b>Figure 43D</b>	
	<i>Group</i> SECTION E		<i>Scenario</i> 3H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 8/5/2022		<i>File Name</i> Trash Backfill Block Sliding- Seismic	
	<small>SLIDEINTERPRET 9.023</small>			

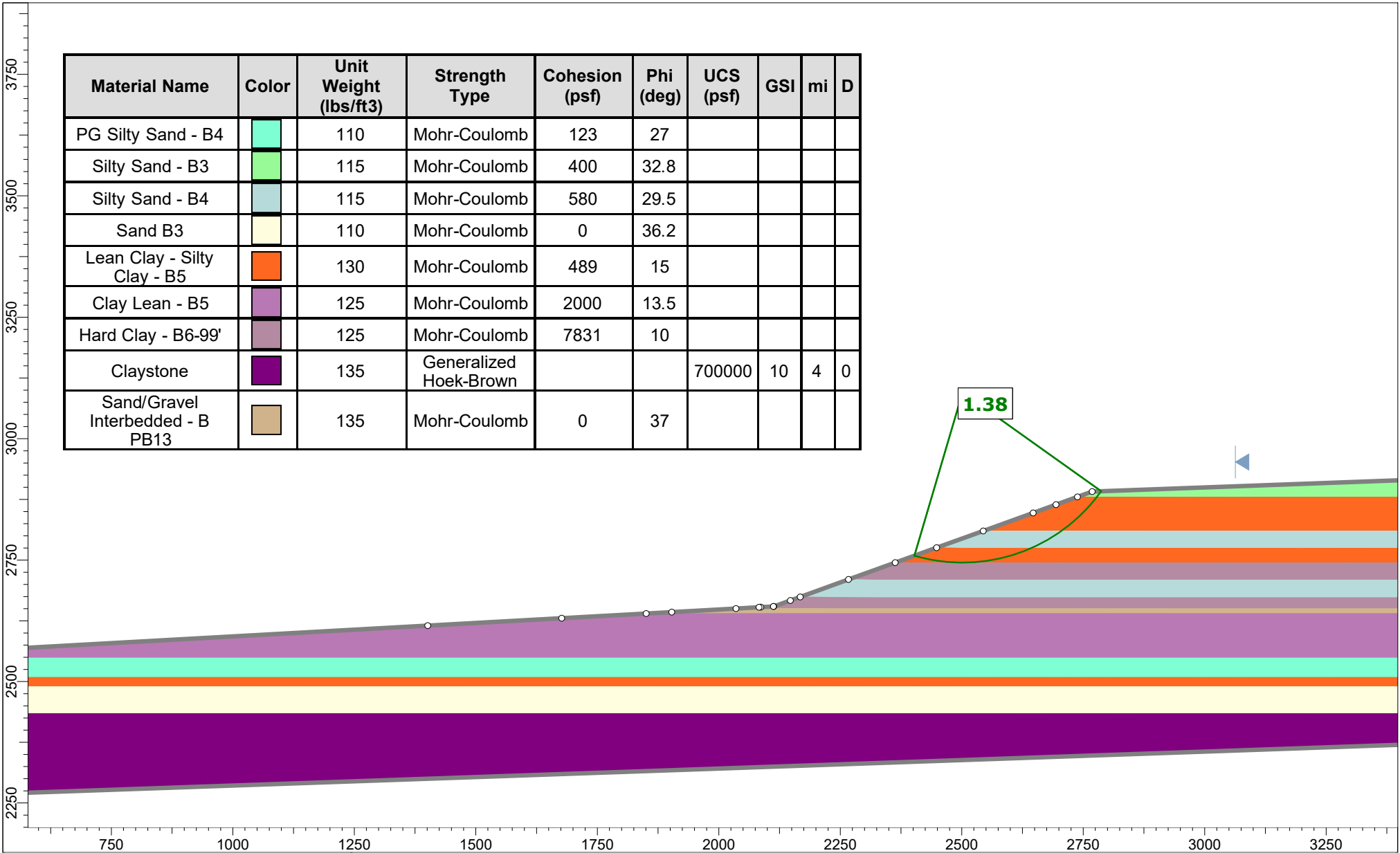
## APPENDIX E: Deformation Analysis


Static and Pseudo-Static Slope Stability Analyses with Associated Circular and Block Failure Factor of Safety, Newmark Displacement, and Critical Acceleration for Slope 3H:1V Figures 1E through 6E

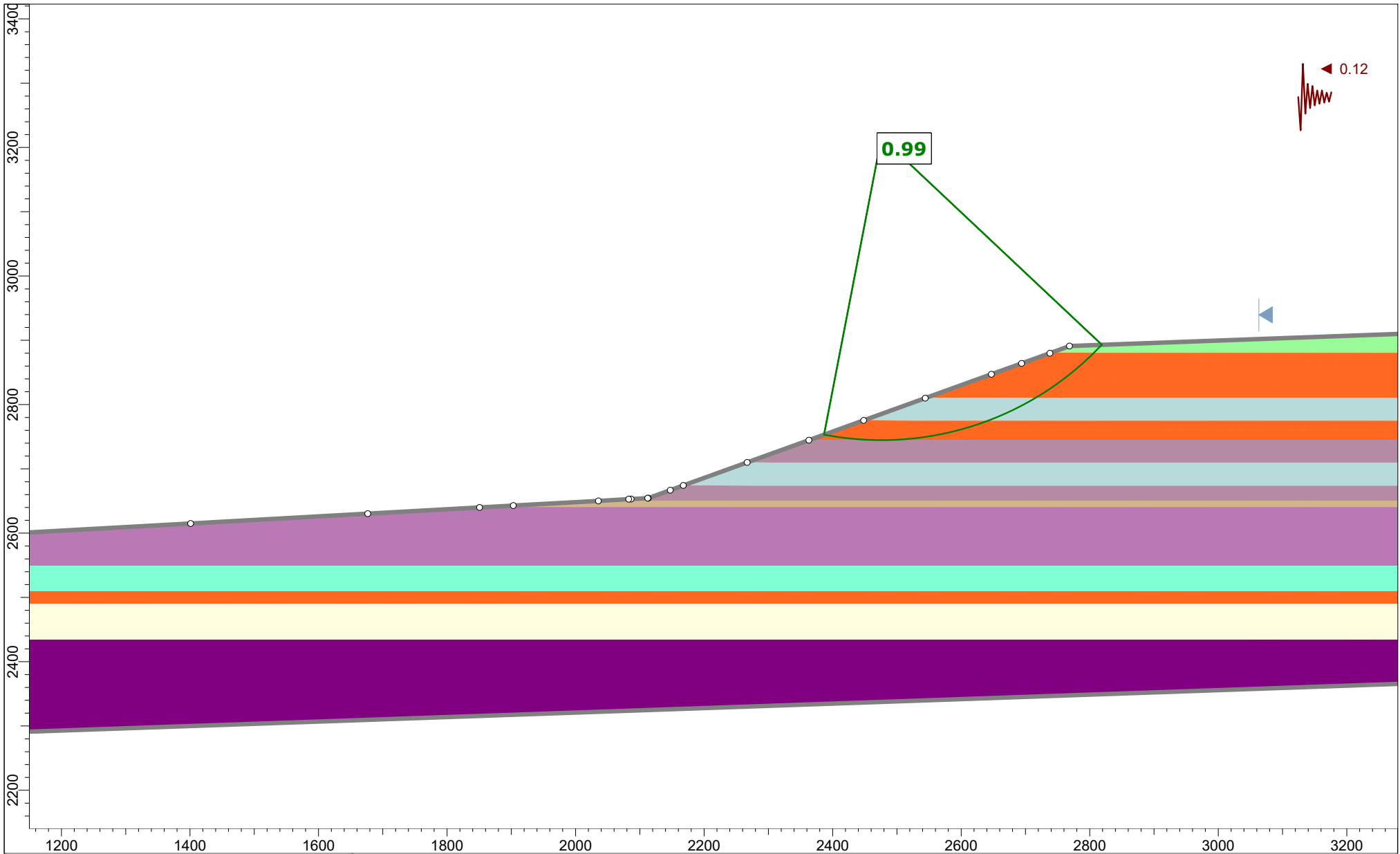
Static and Pseudo-Static Slope Stability Analyses with Associated Circular and Block Failure Factor of Safety, Newmark Displacement, and Critical Acceleration for Slope 4H:1V Figures 7E through 12E




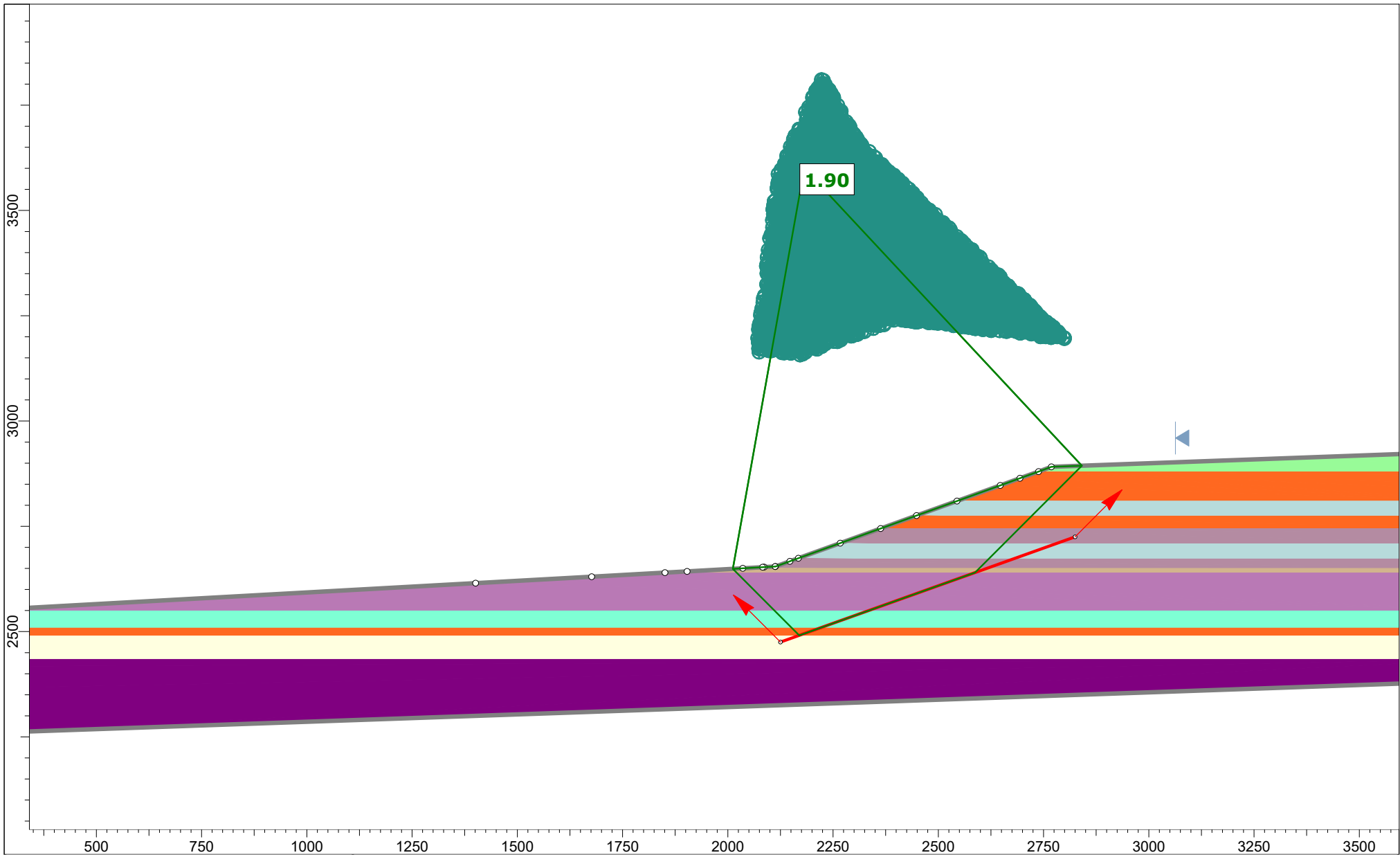
Material Name	Color	Unit Weight (lbs/ft <sup>3</sup> )	Strength Type	Cohesion (psf)	Phi (deg)	UCS (psf)	GSI	mi	D
PG Silty Sand - B4		110	Mohr-Coulomb	123	27				
Silty Sand - B3		115	Mohr-Coulomb	400	32.8				
Silty Sand - B4		115	Mohr-Coulomb	580	29.5				
Sand B3		110	Mohr-Coulomb	0	36.2				
Lean Clay - Silty Clay - B5		130	Mohr-Coulomb	489	15				
Clay Lean - B5		125	Mohr-Coulomb	2000	13.5				
Hard Clay - B6-99'		125	Mohr-Coulomb	7831	10				
Claystone		135	Generalized Hoek-Brown			700000	10	4	0
Sand/Gravel Interbedded - B PB13		135	Mohr-Coulomb	0	37				




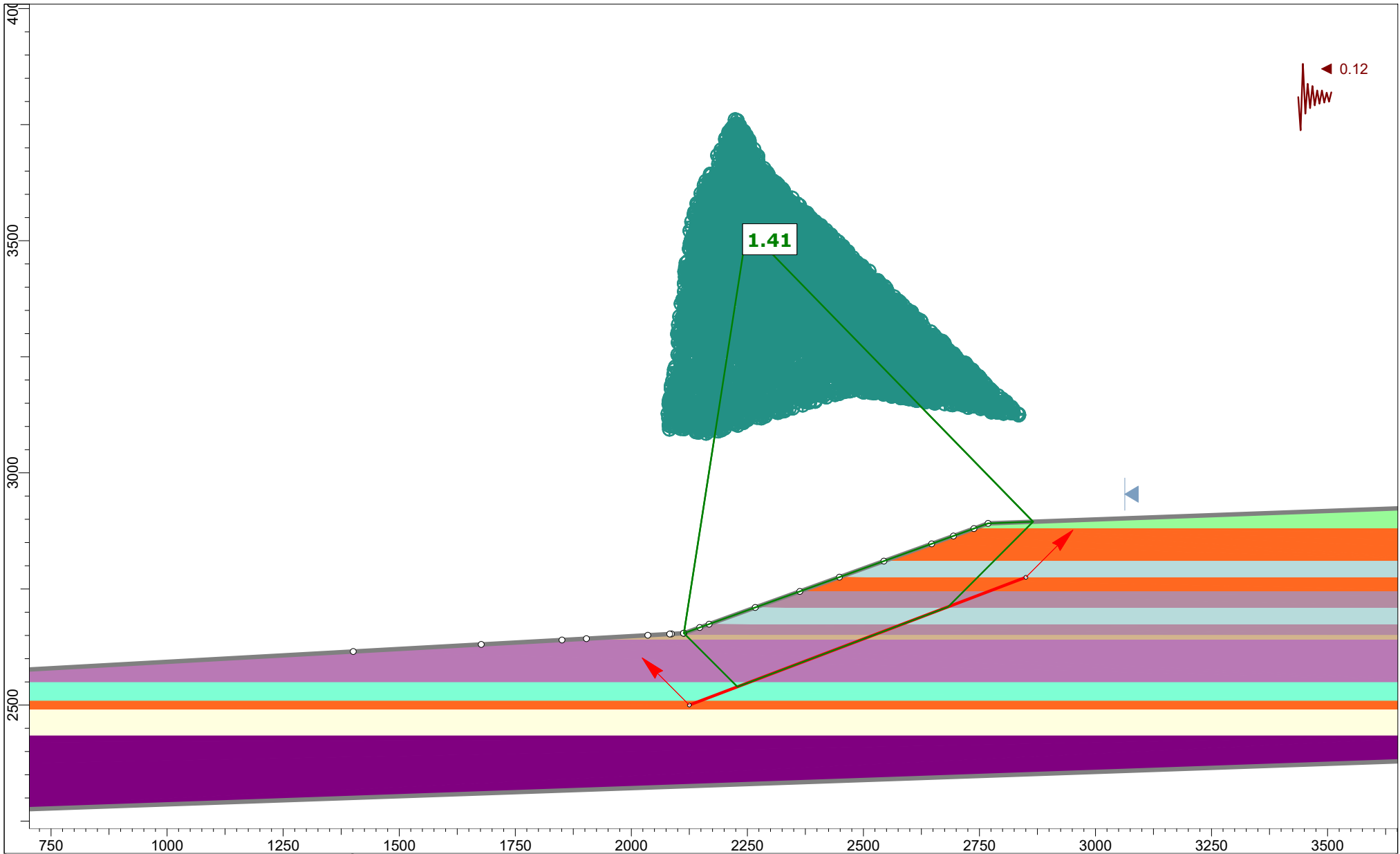
	Project	Pickles Butte	Figure 1E	
	Group	SECTION F	Scenario	3H:1V Slope
	Drawn By	SG	Company	Tetra Tech
	Date	7/29/2022	File Name	Static Loading




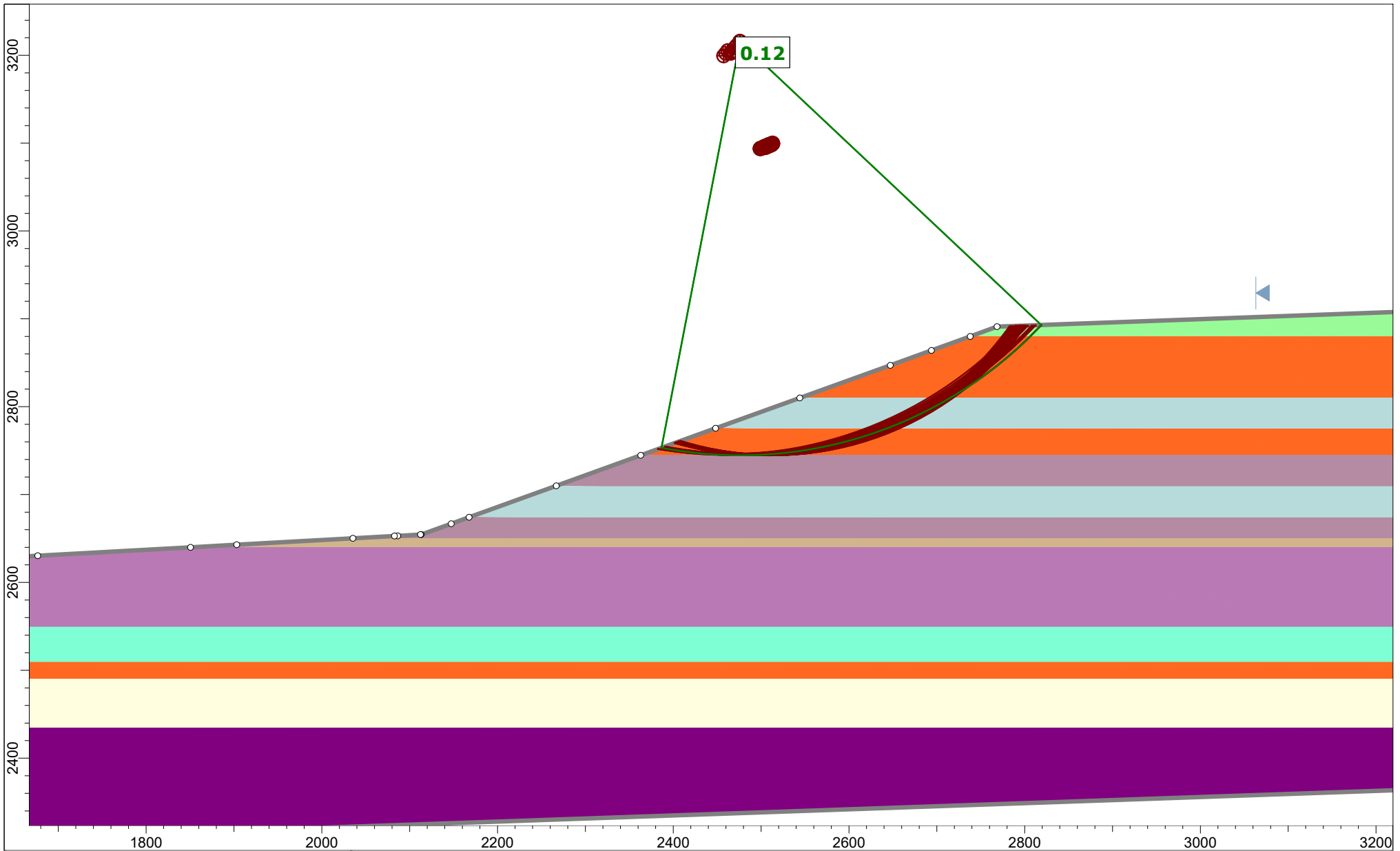
	<i>Project</i> Pickles Butte		Figure 2E	
	<i>Group</i> SECTION F		<i>Scenario</i> 3H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/29/2022		<i>File Name</i> Seismic Loading	




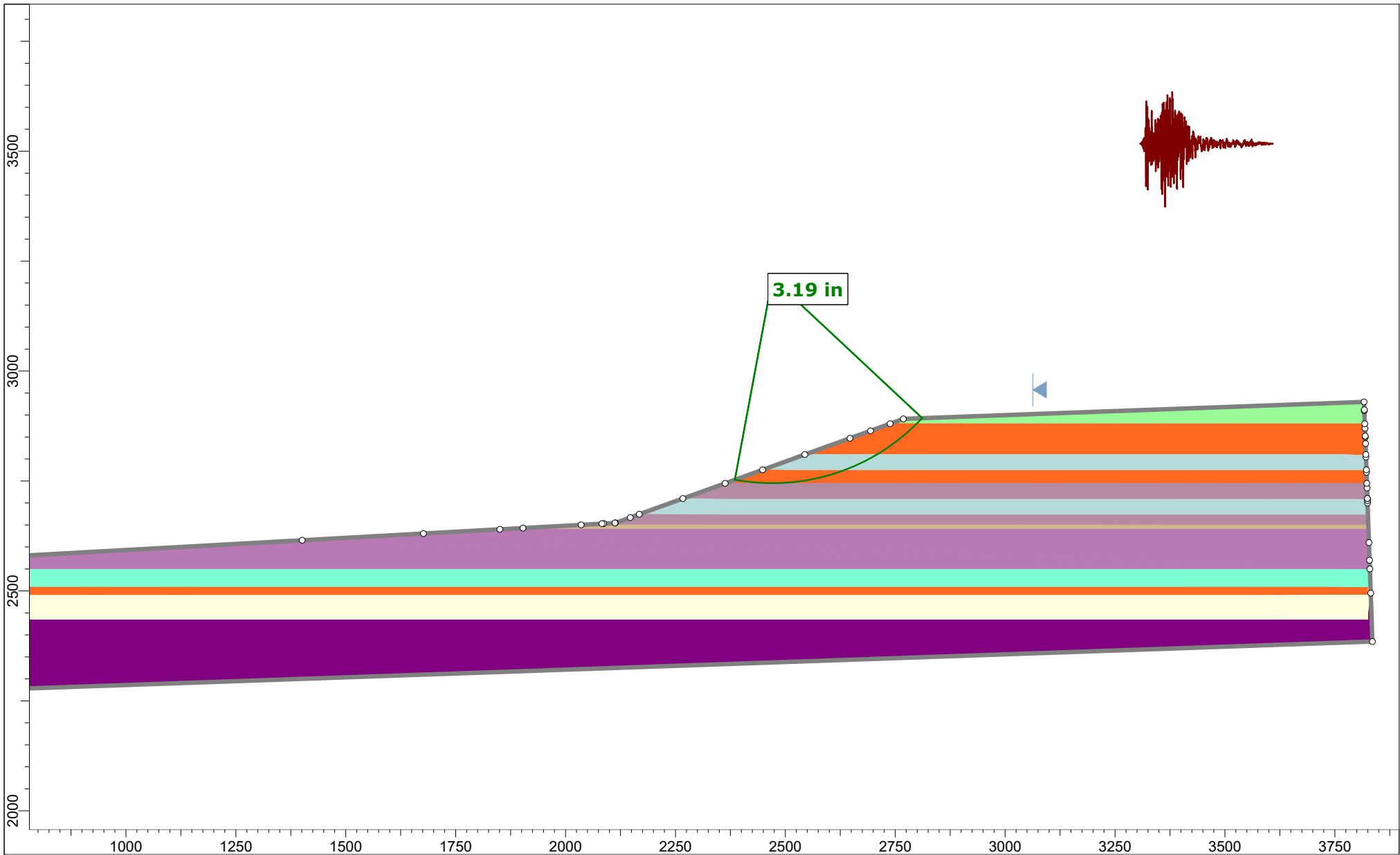
	<i>Project</i> Pickles Butte	Figure 3E
	<i>Group</i> SECTION F	<i>Scenario</i> 3H:1V Slope
	<i>Drawn By</i> SG	<i>Company</i> Tetra Tech
	<i>Date</i> 7/29/2022	<i>File Name</i> Static Loading




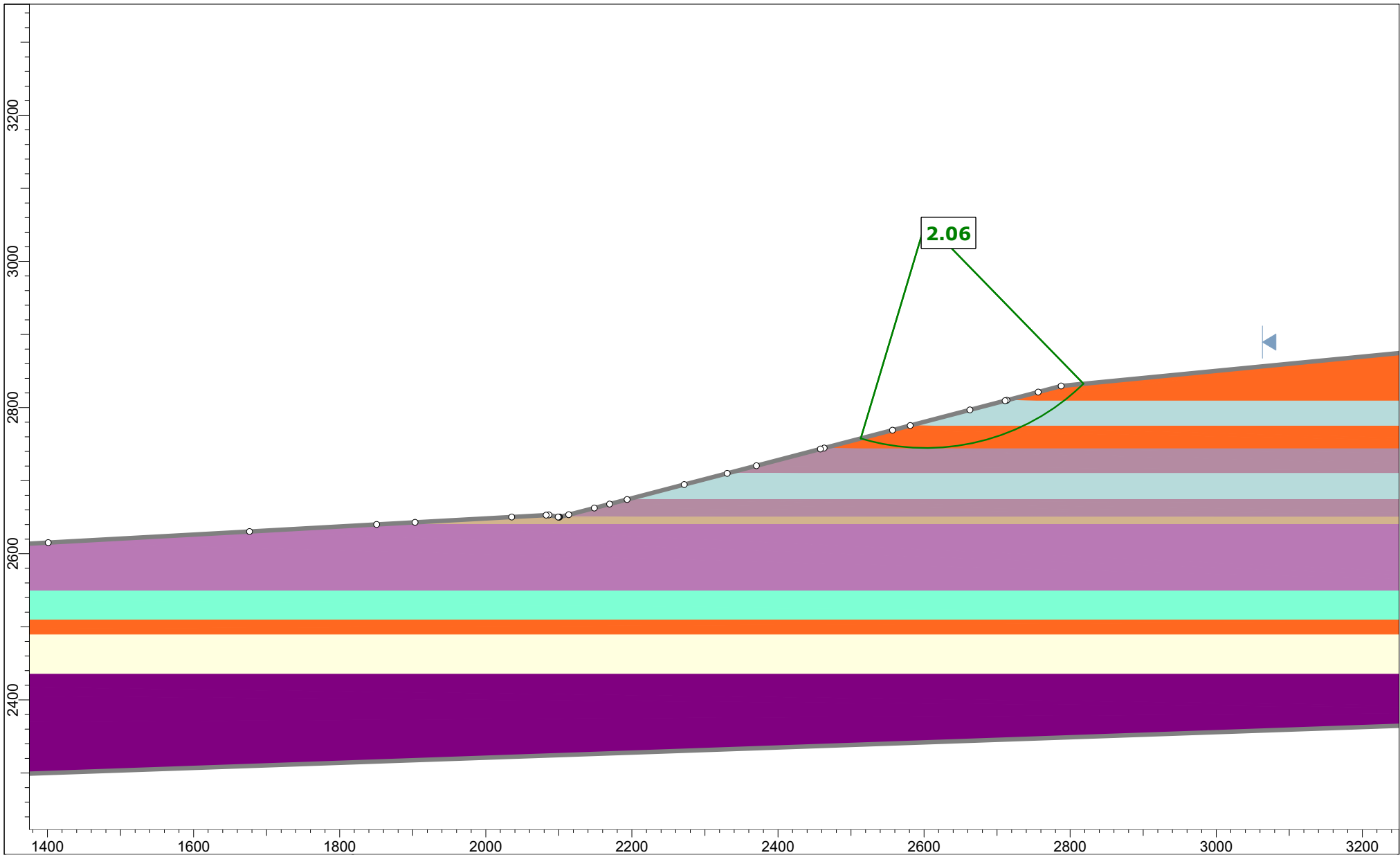
	Project		Pickles Butte	Figure 4E
	Group		SECTION F	Scenario
	Drawn By		SG	Company
	Date		7/29/2022	File Name
				Seismic Loading - Block Failure




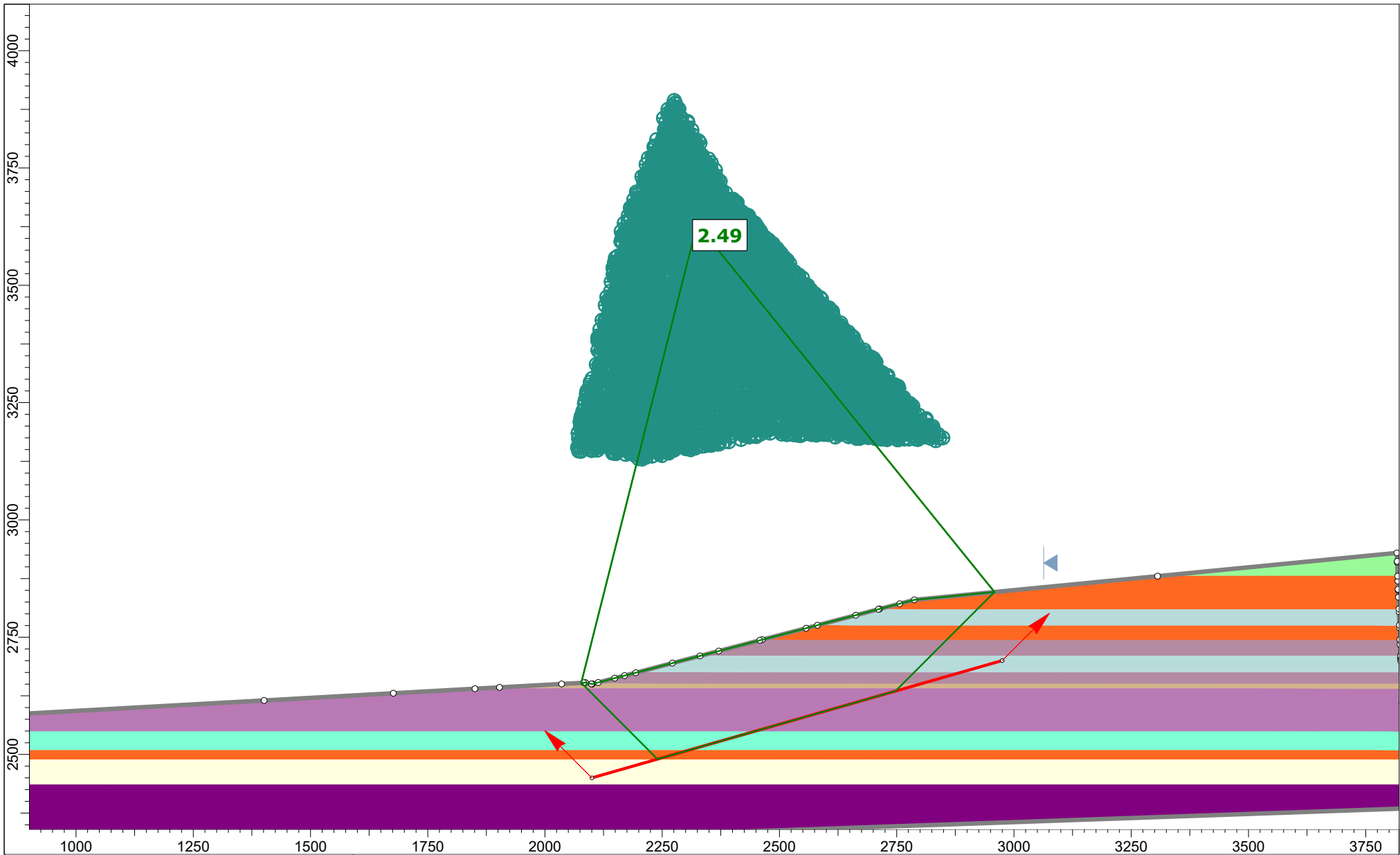
	<i>Project</i> Pickles Butte		Figure 5E	
	<i>Group</i> SECTION F		<i>Scenario</i> 3H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/29/2022		<i>File Name</i> Critical Acceleration	




	<i>Project</i> Pickles Butte		Figure 6E	
	<i>Group</i> SECTION F		<i>Scenario</i> 3H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/28/2022		<i>File Name</i> Seismic Loading - Newmark Displacement	

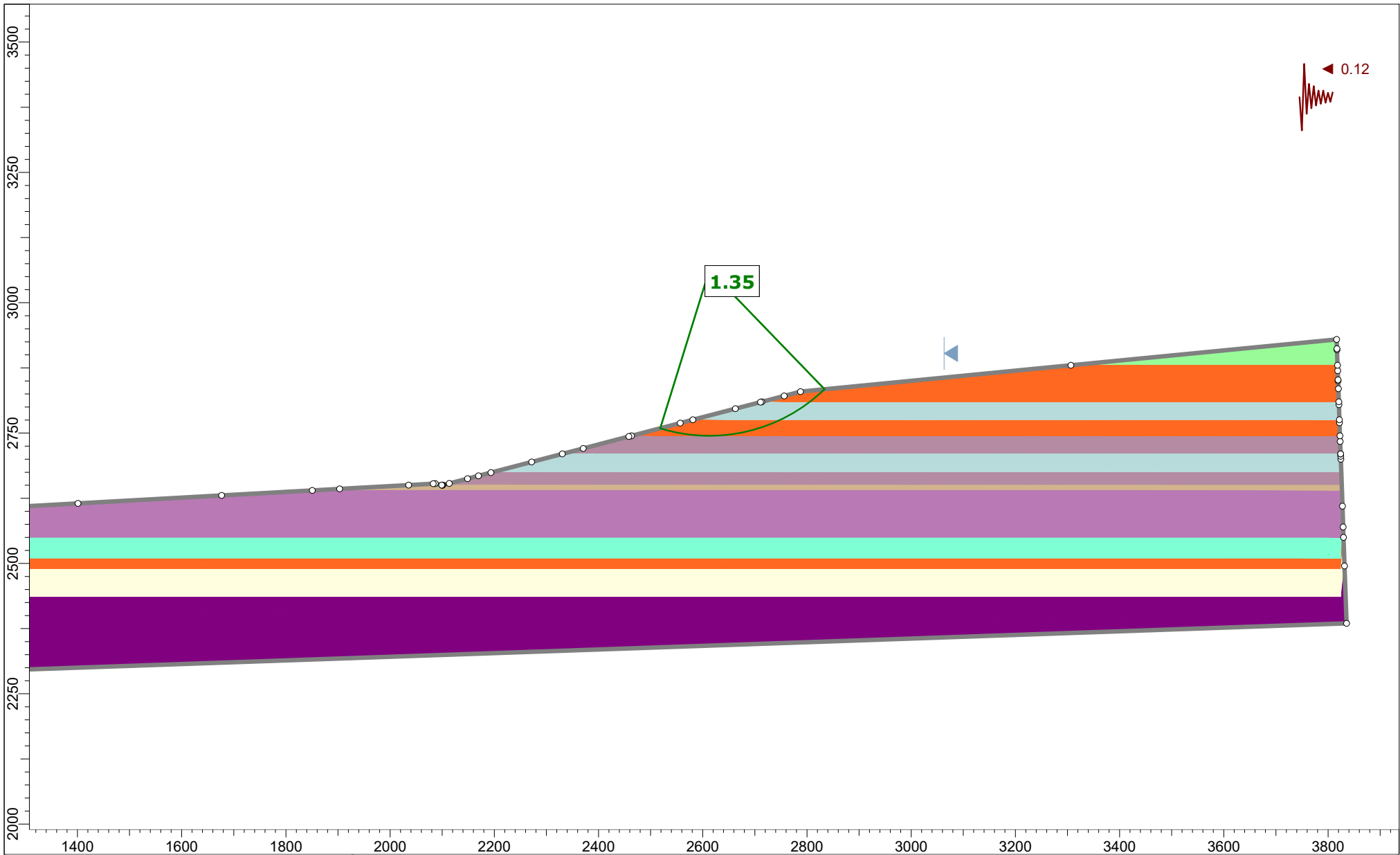



	<i>Project</i> Pickles Butte		Figure 7E	
	<i>Group</i> SECTION F		<i>Scenario</i> 4H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/29/2022		<i>File Name</i> Static Loading	

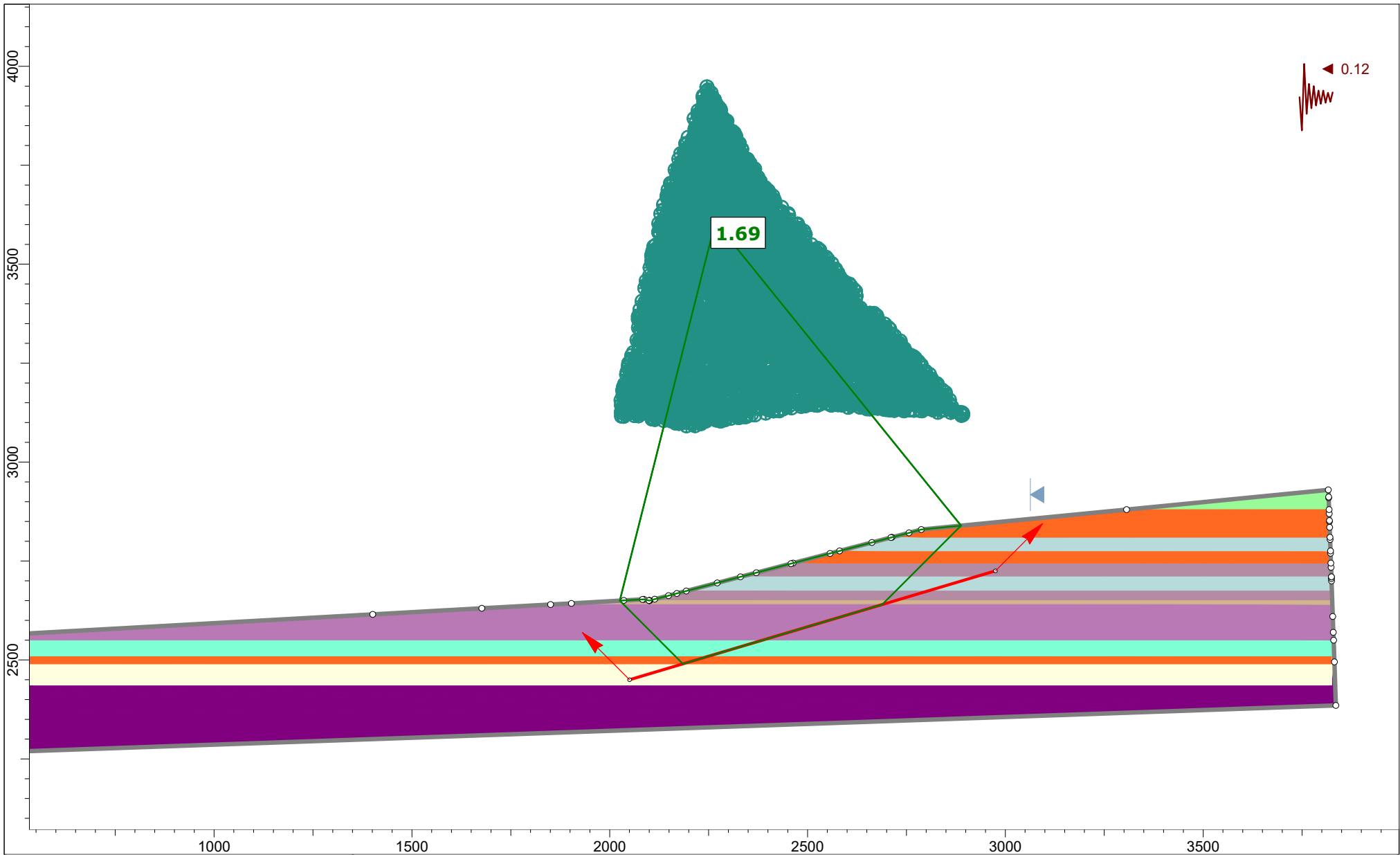



	Project		Pickles Butte	Figure 8E
	Group		SECTION F	4H:1V Slope
	Drawn By		SG	Tetra Tech
	Date		7/29/2022	Static Loading - Block Failure

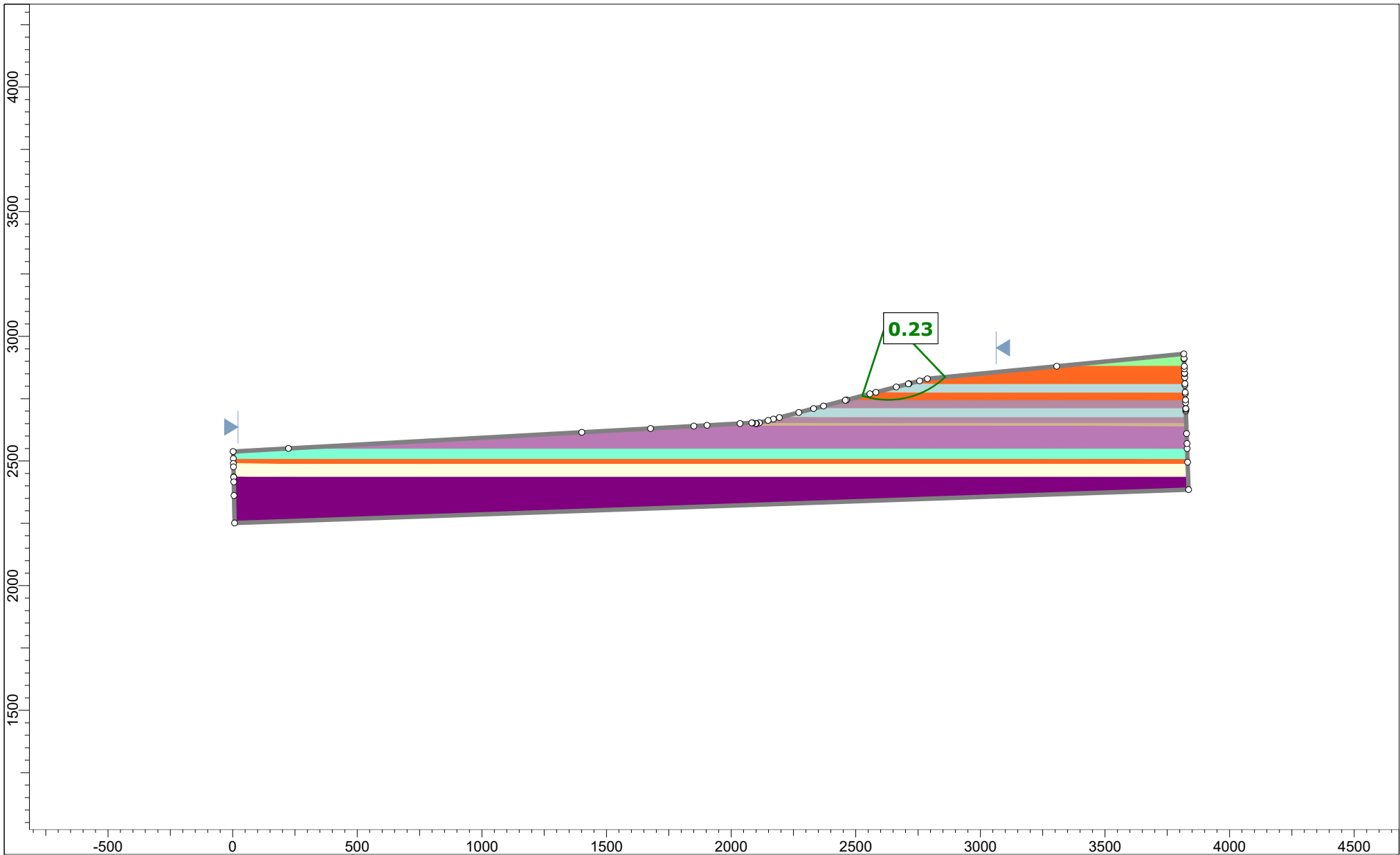





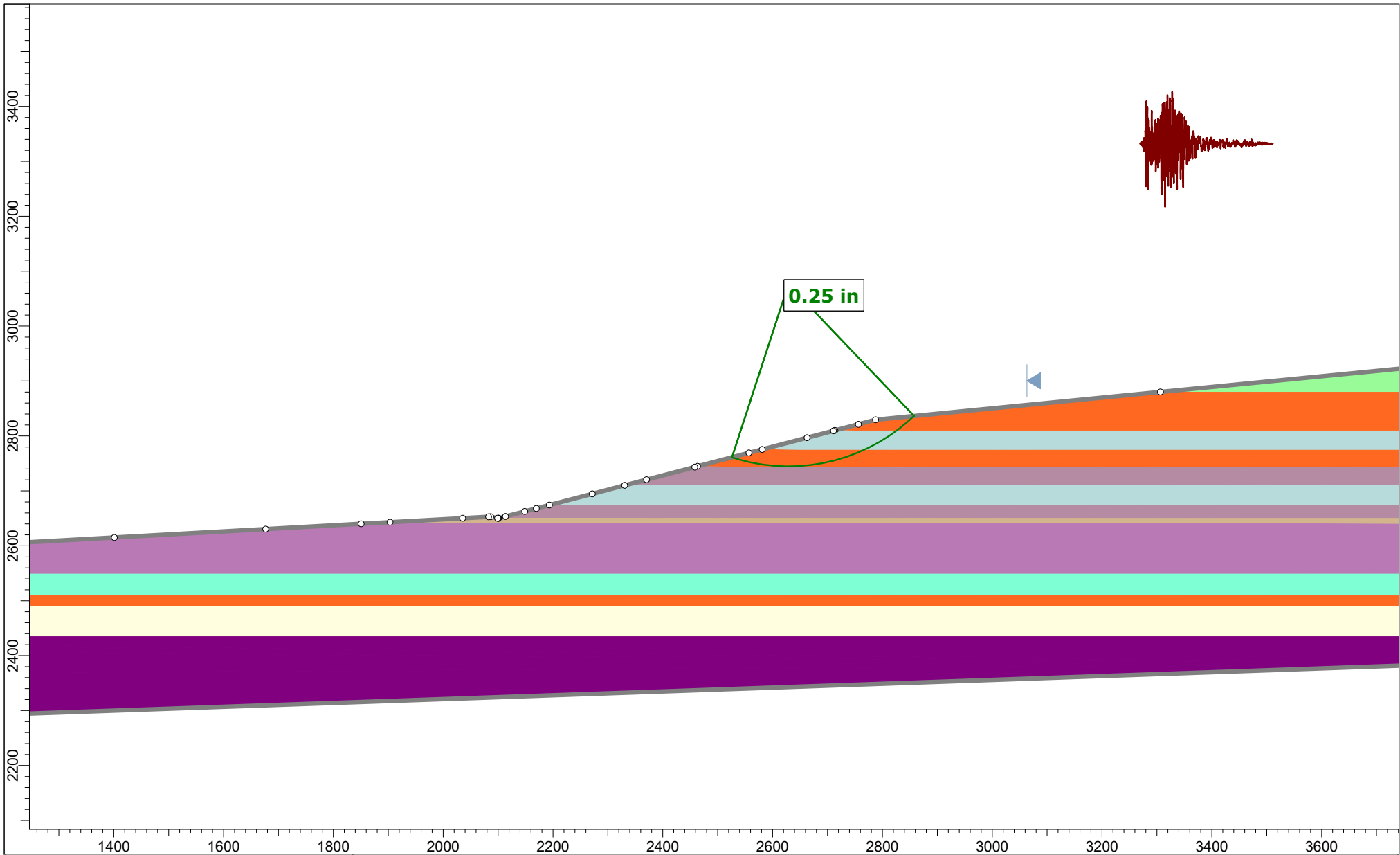
	<i>Project</i> Pickles Butte		Figure 9E	
	<i>Group</i> SECTION F		<i>Scenario</i> 4H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/29/2022		<i>File Name</i> Seismic Loading	




	<i>Project</i> Pickles Butte	Figure 10E
	<i>Group</i> SECTION F	<i>Scenario</i> 4H:1V Slope
	<i>Drawn By</i> SG	<i>Company</i> Tetra Tech
	<i>Date</i> 7/29/2022	<i>File Name</i> Seismic Loading - Block Failure



	<i>Project</i> Pickles Butte		Figure 11E	
	<i>Group</i> SECTION F		<i>Scenario</i> 4H:1V Slope	
	<i>Drawn By</i> SG		<i>Company</i> Tetra Tech	
	<i>Date</i> 7/29/2022		<i>File Name</i> Critical Acceleration	



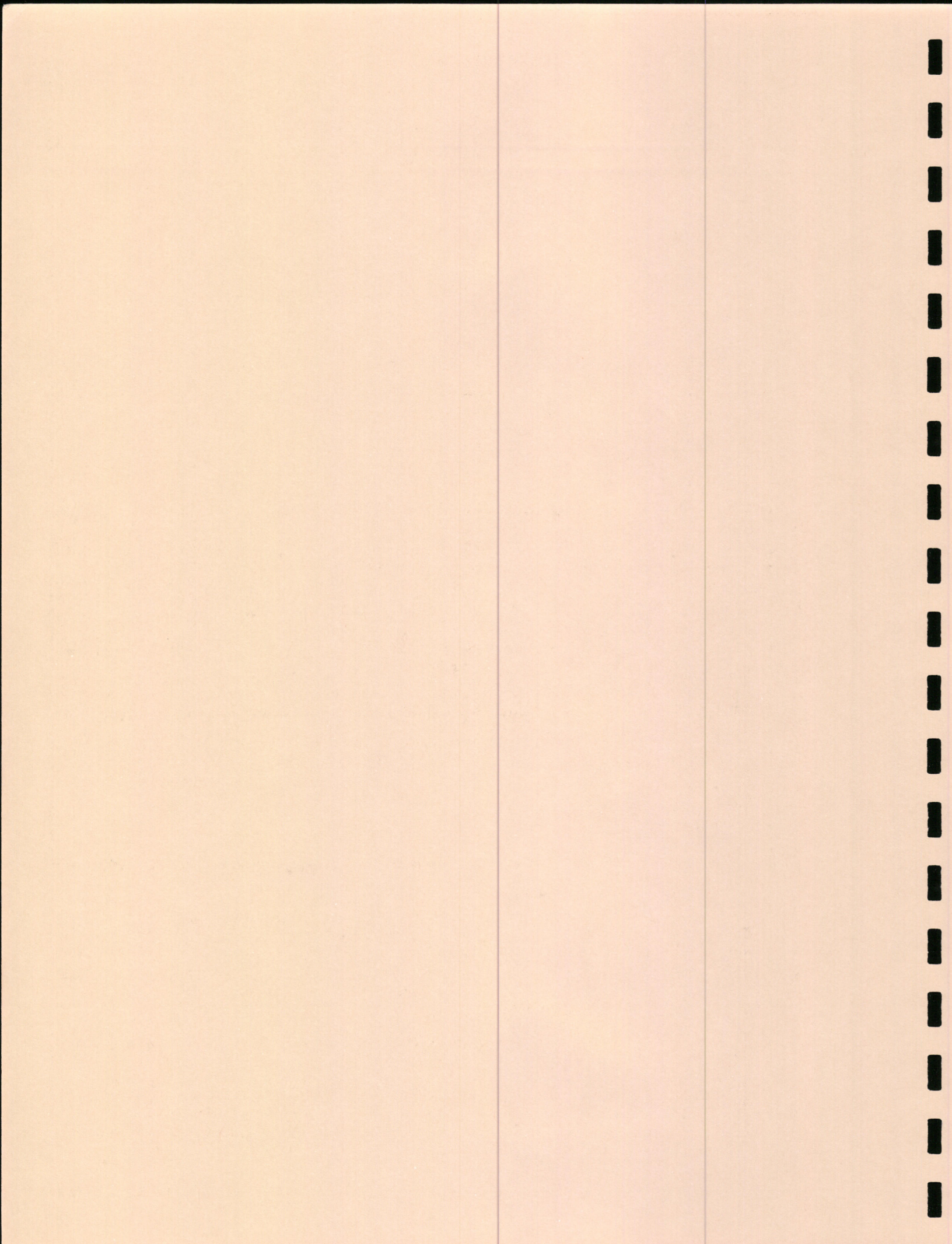
	Project		Pickles Butte	Figure 12E	
	Group		SECTION F	Scenario	
	Drawn By		SG	Company	Tetra Tech
	Date		7/28/2022	File Name	Seismic Loading - Newmark Displacement

## **APPENDIX F: Previous Reporting Logs of Boring**

LOGS GT-1 THROUGH GT-8 BY HOLIDAY ENGINEERING COMPANY(HOLIDAY)  
LOGS PB 5 THROUGH PB12 BY HOLIDAY and DANIEL B. STEPHENS &  
ASSOCIATES, INC.

**APPENDIX E: Borehole Logs**





$$*N' = N \cdot \sqrt{1/\theta}$$

Where  $\theta = .05 T / k^2$  per ft depth

( $\phi$  + stiffness based on table 13.A & 13.B) PAGE 1 OF 2

HOLE NUMBER GT-1 JOB NUMBER 090496 HOLLADAY ENGINEERING COMPANY

PROJECT Dirties Bitter Lebeck OWNER Prunus County LOCATION: CO Coconino SEC 1/4 OF 1/4 T N R W S 50'  
 LOGGED BY STP/WD DATE START 11/4/04 DATE FINISHED 11/4/04 HOLE DEPTH 20' 1/2 ANGLE 90 DRILL METHOD Hollow Stem Lucas DIAMETER 3/8" DRILL MODEL TK 81

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING			HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS	
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
																			Blow counts
4-5 1/2	11:50	tan	fine sand	[Graphic]															moist 2 2nd 3 4-5" 1" float removed (stamped) 2 1st 6" 3 2nd 6" N=12 3 3rd 6" (30°)
10-11 1/2		tan to live sand	fine sand	[Graphic]															moist 10-11 1/2 2, 3, 2 N=5 N'=7 (30°)
15-16 1/2		tan to live sand	fine sand	[Graphic]															moist 15-16 1/2 2, 3, 2 N=3, 3, 2 N'=6 (29°)
20-21 1/2	12:10	tan to live sand	fine sand	[Graphic]															moist 20-21 1/2 2, 3, 2 N=4, 3, 3 N'=5 (28°)
25-26 1/2	12:22	tan to live sand	fine sand	[Graphic]															moist 25-26 1/2 2, 3, 2 N=3, 3, 2 N'=5 (28°)
30-31 1/2	12:25	tan to live sand	fine sand	[Graphic]															moist 30-31 1/2 2, 3, 2 N=3, 3, 2 N'=8 (32°)
35-36 1/2	12:33	tan to live sand	fine sand fine sand fine sand + gravel	[Graphic]															moist 35-36 1/2 2, 3, 2 N=6, 7, 13 N'=15 (35°)
40-42																			dry 40-42 2, 3, 2 N=10, 10, 10 N'=15 (35°)
45-46 1/2																			dry 45-46 1/2 2, 3, 2 N=12, 23, 32 N'=37 (40°)

10'

10'

(40°)



HOLE NUMBER GT-1 JOB NUMBER 030496

HOLLADAY ENGINEERING COMPANY

PAGE 2 OF 4

PROJECT Dirkless F. Ho Gerbeck OWNER \_\_\_\_\_ LOCATION: CO \_\_\_\_\_ SEC \_\_\_\_\_ 1/4 \_\_\_\_\_ OF 1/4 \_\_\_\_\_ T \_\_\_\_\_ N \_\_\_\_\_ R \_\_\_\_\_ W

LOGGED BY SMOUD DATE START 11/4/96 DATE FINISHED 11/6/96 HOLE DEPTH 201 1/2 ANGLE -7° DRILL METHOD HOLLOW STEM AUGER DIAMETER 8" AUGER DRILL MODEL BK-81

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
50-51 1/2	11/4 1:20	gray	fine fine sand												med loose			dry, mostly moist	BLOW COUNTS N 18, 32, 41 N = 46 (42)
55-56 1/2	1:40		fine to med sand																13, 25, 34 N = 36 minor clay (40)
60-61 1/2	1:55	tan-gray	fine to med sand												med loose			dry	18, 30, 37 N = 37 (40)
65-66 1/2	2:20	tan/loose orange FeOx	fine sand												med loose			dry	25, 42, 41 N = 46 (42)
70-71 1/2	2:40	tan/loose orange FeOx	fine med sand												med loose			slightly moisture	25, 40, 44 N = 45 (42)
75-76 1/2	2:55	tan	fine sand												med loose			slightly moist	25, 37, 41 N = 40 (42)
80-81 1/2	3:05	tan	fine sand to very fine sand with silt/clay												ditto			ditto	26, 36, 50 N = 43 (42)
85-86 1/2	3:20	tan	fine sand to silt/clay												med loose			ditto	28, 47, 45 N = 42 (42)
90-91 1/2	4:05	tan	fine silt sand												med loose			slightly moist	13, 40, 50 N = 42 (42)
95-96 1/2	11:00	11/5	silt to clay @ 96'															very sticky clay	19, 28, 47 N = 34 (hard)

HOLE NUMBER GT-1 JOB NUMBER 030496

HOLLADAY ENGINEERING COMPANY

PAGE 3 OF 4

PROJECT Dickens Butte Geotech OWNER Canyon

LOCATION: CO \_\_\_\_\_ SEC \_\_\_\_\_ 1/4 \_\_\_\_\_ OF 1/4 \_\_\_\_\_ T \_\_\_\_\_ N \_\_\_\_\_ R \_\_\_\_\_ W \_\_\_\_\_

LOGGED BY STROWD DATE START 11-4-96 DATE FINISHED \_\_\_\_\_ HOLE DEPTH \_\_\_\_\_ ANGLE 90° DRILL METHOD Hollow Stem / 50T DIAMETER 8" Auger DRILL MODEL DJK-31

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC		
100-101 1/2	11-5	11:40	late tan	clay														stiff
	* BRASS RINGS		green															N = 11 18 27 N = 20 perhaps three clay & 2 brass ring samples
105-106 1/2	12:00	12:00	late tan	lt clay														12 32 34 N = 29 penetration unconfined 3.0 T/ft. conf. in brass ring d.o.T/ft =
	NO RINGS			1/2 fine sand														hard
	NO RINGS			3" clay														
110-111 1/2	12:25	12:25	tan	clay s														weakly moist 13 32 50 @ 6" N = 35 #1 brass ring sample clay penetration 1.5 for fine sand (T/ft) brass ring 4.0 T/ft for clayey silt
	* BRASS RINGS			fine sandy silt														
				10"														
115-116 1/2	12:45	12:45	light	interbedded fine														very weakly moist 11 41 50 N = 38 (40) confined ring penetrometer in clay > 4.5 Tons/ft
	NO BRASS RINGS		tan	clay														
				very fine sand														
				clay (bdw/s)														
				sample top														
				clay														
120-121 1/2	1:10	1:10	tan	silty clay														weakly moist 12 30 48 2-4 Tons @ N = 32 Very stiff
	NO RINGS																	
				clay contact														
125-126 1/2	2:50	2:50	first	very fine silty														moderately very add five gallons water 2.0 42 50 @ 5" slightly low N = 37 hard
	H <sub>2</sub> O added			and to 126														
	NO RINGS																	
130-131 1/2	2:25	2:25		clay														slightly to moderately damp 30 32 50 @ 5" #4 brass rings N = 32 Very stiff
	* RINGS			clayey silty														
				very fine sand														
				silty clay														
135-136 1/2	3:00	3:00	grayish	clay w/ traces														add water add five gallons water 11 21 37 N = 22 penetration 1.75-2.75 Very stiff
	NO RINGS		green	silt														
140-141 1/2	3:45	3:45	greenish	clay & silty														add water 19 27 38 N = 25 #4 rings (test both moderately clay & silty clay) moist (38?) Very stiff
	* RINGS		gray	clay interbed														
145-146 1/2	4:30	4:30	grn-gray	top 6" clay														moderate 23 23 28 N = 19 Very stiff
	NO RINGS			lower 12" silty														
	EDS	5:00		clay														

18

2 feet @ 33°

HOLE NUMBER GT-1 JOB NUMBER 030496 HOLLADAY ENGINEERING COMPANY PAGE 4 OF 4  
 PROJECT Packias Butte Geotech OWNER Carson County LOCATION: CO. Carson SEC. 1/4 OF 1/4 T. N R. W  
 LOGGED BY STROUD DATE START 11-4-92 DATE FINISHED 11-6-92 HOLE DEPTH 201 1/2 ANGLE -90 DRILL METHOD Hollow Stem Auger DIAMETER \_\_\_\_\_ DRILL MODEL BK-71

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
150-151 1/2	START 9:15 RINGS	grn-gry	clay w/ intrabdd silt/fine sand		1 Brass No Full														clay med damp silt ~ 1.5 T/ft in ring silt almost dry CLAY ~ 4-4.5 T/ft in ring * ONE BRASS RING CLAY SILT ADD 7 gal H.D. water PUGH 5 ft PUGH 2 gal 15 22 25 pure clay MOD. DAMP GOOD SOME SAMPLE N = 17 stiff
155-156 1/2	NO RINGS	grn-gry	clay d. 1/2																
160-161 1/2	RINGS	grn-gry	pure clay		3 Brass 1 almost 2 no full														ADD 5 gal MOD DAMP * 3 perfect samples in rings ~ 38-42% clay N = 16 stiff
165-166 1/2	NO RINGS	grn-gry	pure clay w/ 3" bd of med fine sand																ADD 5 gal MOD DAMP ~ 40% N = 33 Very stiff
170-171 1/2	NO RINGS	grn-gry	pure clay w/ 1" silt bed																~ 40% N = 22 Very stiff
175-176 1/2	NO RINGS	grn-gry	clayey silt																25% med N = 18 stiff
180-181 1/2	BRASS RINGS	grn-gry	SILTY CLAY		2 Brass No Full														~ 35% MOD DAMP 1.5 - 2.0 T/ft N = 17 stiff
185-186 1/2	NO RINGS	grn-gry	SILTY CLAY																~ 35% MOD DAMP 1.5 T/ft N = 23 Very stiff
190-191 1/2	RINGS	grn-gry	SILTY CLAY		1 Brass No Full														~ 35-38% N = 19 stiff
195-196 1/2	NO RINGS		clayey silt																~ 30-35% N = 13 stiff
200-201 1/2	ABANDON HOLE NO TOP		silt clay																12 17 20 1/4 1/2 N = 17 stiff

15

HOLE NUMBER GT-2 JOB NUMBER 030496

HOLLADAY ENGINEERING COMPANY

PAGE 1 OF 1

PROJECT Pickles Butte Geotech OWNER Canyon County LOCATION: CO. (see map) SEC. 1/4 OF 1/4 T. N R. W

LOGGED BY STAND DATE START 11-7-96 DATE FINISHED 11-7-96 HOLE DEPTH 25 1/2' ANGLE -90 DRILL METHOD HOLLOW STEM AUGER DIAMETER 2" DRILL MODEL 3K-81

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
5-6 1/2	START	11-7-96																
	12:25																	slightly damp check for methane - none smells
10-11 1/2		12:35																15 B T Dirt + trash
	BRASS RING																	
15-16 1/2	NO RINGS	12:55																BARELY DAMP 7.7.12 SAMP A - SOIL NO METHANE / BRASS - TRASH
	RINGS	1:05																OUTSIDE SPRITSPOON 17 14 10 WET 5% LEL in Area Slow quickly Drops to 10% LEL Two RINGS tripped together
20-21 1/2	NO RINGS	1:20																MODERATELY DAMP 8 8 14
	BRASS RINGS	1:35																19 13 12 DAMP 100% LEL METHANE SHUT RIG DOWN FLOOD HOLLOW STEM W/ WATER BACK OUT OF HOLE

HOLE NUMBER GT-3 JOB NUMBER 030496

HOLLADAY ENGINEERING COMPANY

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PAGE 1 OF 2

PROJECT Pickles Butte Geotech OWNER Canyon County LOCATION: CO. Canyon SEC. 1/4 OF 1/4 T. N R. W

LOGGED BY STREAND DATE START 11/8/76 DATE FINISHED 11/8/76 HOLE DEPTH 101' 1/2 ANGLE -90 DRILL METHOD SPT/AUGER DIAMETER 2 1/2" DRILL MODEL BK-81

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
	11-8-76	8:30																	
5-6 1/2	NO RINGS	8:40	tan	silty very fine sand												loose		slightly damp	2 3 2
10-12	2 HELIX TUBES	8:50	tan	fine sand												med loose		dry	200 lbs least 6"
15-16 1/2	NO RINGS	9:00	tan	fine sand												loose		medium damp	5 12 19 minor silt
20-21 1/2	BRASS RINGS	9:10	light brown	fine sand	3 BRASS NO-FILL											med loose		DAMP	13 21 23
25-26 1/2	NO RINGS	9:20	light brown	fine-med sand												loose		VERY DAMP	13 19 29
30-31 1/2	BRASS RINGS	9:30	light brown	fine-med sand	3 BRASS NO-FILL											med loose		VERY DAMP	14 21 33 #3 rings
35-36 1/2	NO RINGS	10:00	light grey-brown	fine to med. sand												loose med		almost saturated	23 37 39
40-41 1/2	BRASS RINGS	10:10	light grey-brown	fine sand some med. + orange cemented	3 BRASS NO-FILL											med loose		VERY DAMP	16 25 37
45-46 1/2	NO RINGS	10:20	light grey-brown	fine sand minor to med. silt												med loose		VERY DAMP	22 30 35

3:45

15

HOLE NUMBER GT-3 JOB NUMBER 130476

HOLLADAY ENGINEERING COMPANY

PROJECT PB Geotech OWNER Panjon Co. LOCATION: CO Cañon SEC 1/4 OF 1/4 T N R W

LOGGED BY Stowd DATE START 11/1/96 DATE FINISHED 11/2/96 HOLE DEPTH 101' 1/2" ANGLE -3° DRILL METHOD 4 1/2" (low) 3 1/2" Auger DIAMETER 8" 1/2" DRILL MODEL PK-81

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
50-51 1/2	11-8-96 RINGS	10:25	gray tan	very fine silty sand	3 - BASS 1 - Full 2 - NO Full											WK-MOD CONSOL		moderate damp	19 31 37 #3 BASS
55-56 1/2	NO RINGS	10:40	gray-tan	very fine silty sand												WK-MOD CONSOL		mod-stiff damp	16 29 40
60-61 1/2	RINGS	10:50	gray-tan	very fine sand w/ borderlines 2. ft	3 - BASS NO - Full											WK-MOD CONSOL		mod damp	20 35 44
65-66 1/2	NO RINGS	11:00	gray-tan	top 8" silty fine sand bottom non-gray 10" clay												SAND WK MOD-STIFF SAND/CLAY SOIL CLAY		MOD SAND	16 29 36
70-71 1/2	RINGS	11:15	gray	top 2" clay then very fine sand	2 - BASS NO Full											MOD CLY MOD SAND		WK-MOD SAND/CLAY	15 29 37 2 RINGS - 70% OF SAND
75-76 1/2	NO RINGS	11:30	gray-tan	silty clay w/ clay (various)												WK-CONSOL		WK DAMP	14 21 37 changes into silty clay & spread in brine
80-81 1/2	RINGS	11:45	gray-tan	interbedded sand-silt-silty clay	2 - BASS NO - Full											MOD-STIFF		slightly damp	15 44 50 @ 5" 2 RING clay / silty sand
85-86 1/2	NO RINGS	12:00	gray-tan	fine silty sand												MOD-STIFF		slightly damp	21 48 50 intermediate clay present 3" bed from 10' to 12' clay
90-91 1/2	RINGS	12:45	tan-gray	fine silty sand w/ clay in bot	2 - BASS NO - Full											MOD-STIFF		slightly damp	16 20 50
95-96 1/2	NO RINGS	1:00	tan-gray	10" silty clay w/ silty clay												MOD-CONSOL		slightly damp	22 36 46
100-101 1/2	RINGS	1:20	tan-gray	fine sand	2 - BASS NO - Full											MOD-CONSOL		very slightly damp	14 32 50 2100 HOLE

(21)

HOLE NUMBER GT-4 JOB NUMBER D30496

HOLLADAY ENGINEERING COMPANY

PAGE 1 OF 2

PROJECT Pickles Hill, Geokh OWNER Canyon County LOCATION: CO. Payson SEC. 1/4 OF 1/4 T N R W

LOGGED BY Stowd DATE START 11-11-96 DATE FINISHED 11-11-96 HOLE DEPTH 101 1/2 ANGLE -90 DRILL METHOD Yellow Stem Action DIAMETER 2 1/2" DRILL MODEL BK-91

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS	
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC				
5-6 1/2	11-11-96 Rings 10:00	tan	fine sand with minor clay silt															very loose low L. water pressure Balt. 10.11.96	non-saturated damp	2 1 1 2 rings
10-11 1/2	NO RINGS 10:07	tan	clayey silt with minor very fine sand															10.11.96	moist damp	3 2 1
15-16 1/2	Shallow tube 10:15	?	??																	
20-21 1/2	NO RINGS 10:25	tan	clean fine sand															10.11.96	somewhat damp	5, 6 & driven in first rings low L. water no sand still present in these same rings
25-26 1/2	NO RINGS 10:30	tan	silty fine sand															10.11.96	moist dampness	6 12 32
30-31 1/2	RINGS 10:40	dy. tan	silty fine sand															10.11.96	moist damp	15 20 37 2 rings
35-36 1/2	NO RINGS 10:50	gray-tan	fine sand															10.11.96	moist damp	12 21 32
40-40.75	Shallow tube 11:05	gray-tan	fine sand															10.11.96	moist damp	20.11.96 8" sample left good minor silt & clay
45-46 1/2	11:15	gray-tan	interbedded sand & silt															10.11.96	moist	ends 4-6 21.10 20 27 32

15-17

2-CRASS  
NO-FULL

HOLE NUMBER ST-4 JOB NUMBER D30496

HOLLADAY ENGINEERING COMPANY

PROJECT Dicks & Bullock OWNER Bayview Center LOCATION: CO. 2 SEC. 1/4 OF 1/4 T. N R. W

LOGGED BY SMOND DATE START 11/16/96 DATE FINISHED 11/16/96 HOLE DEPTH 101' 1/2 ANGLE -90 DRILL METHOD Hypodermic glass DIAMETER 3 1/2" DRILL MODEL 316-31

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING			HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAY	ANG	WK	MOD	WELL	EST.	MEAS.		
50-51 1/2	BRASS	11:25		filling w/1"	2-BRASS Almost.										MOD-STR	11-30 50	11-30 50 inner line hand
	RINGS			clay interbeds													
55-56 1/2	NO RINGS	11:40	dry-ten	fine sand 1/2"											MOD-MOD	11-18 31	11-18 31
				sand silt - 4"													
60-61 1/2	RINGS	11:55	dry-ten	fine sand silt	2-BRASS No Full										MOD SAND	23 37 50	2 RINGS
				interbedded 1" beds													
65-66 1/2	NO RINGS	12:10	dry-ten	fine sand silt											MOD SAND	19 34 45	19 34 45
				in 1/2" beds													
70-71 1/2	RINGS	12:25	dry-ten	fine sand silt	2-BRASS No Full										MOD SAND	21 42 50	21 42 50
75-76 1/2	NO RINGS	12:40	dry-ten	fine sand silt											MOD SAND	22 37 42	22 37 42
80-81 1/2	NO RINGS	1:10	dry-ten	fine sand silt											MOD SAND	22 37 42	22 37 42
85-86 1/2	NO RINGS	1:30	dry-ten	fine sand silt											MOD SAND	22 37 42	22 37 42
90-91 1/2	BRASS RINGS	1:45	dry-ten	fine sand silt	2-BRASS Almost.										MOD SAND	22 37 42	22 37 42
95-96 1/2	NO RINGS	2:10	dry-ten	fine sand silt											MOD SAND	22 37 42	22 37 42
100-101 1/2	RINGS	2:30	dry-ten	fine sand silt	3-BRASS										MOD SAND	23 47 50	END OF WELL

11



HOLE NUMBER GT-5 JOB NUMBER 030496 HOLLADAY ENGINEERING COMPANY. PAGE 1 OF 2  
 PROJECT Pinkas Butte Geotechowner Morgan Couder LOCATION: CO. Canon SEC. 1/4 OF 1/4 T. N R. W  
 LOGGED BY STRAWND DATE START 11/12/96 DATE FINISHED 11/14/96 HOLE DEPTH 101 1/2 ANGLE -90 DRILL METHOD Follow Spec. <sup>SPT</sup> ~~Lucas~~ DIAMETER 8 1/2" DRILL MODEL RK-91

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
0-1 1/2	11/12/96 10:05 SHELF		COVER & TRASH														MOIST	SHELF TUBE THRU INTER. TO COVER PLAYSILT & TRASH 1 1/2 FT @ 500 lbs wash end of tube
5-6 1/2	NO RINGS 10:15		COVER & TRASH														MOIST	15 5 4 MIST OF SAMPLE NAT RECORDED (SIDE BRIDGE)
10-11 1/2	NO RINGS 10:30		TRASH														MOIST	27 10 8 POOR RECOVERY (2.3-4" sample)
15-16 1/2	NO RINGS 10:40		TRASH														MOIST	70 @ 4 inches wood, plastic, paper
20-21 1/2	NO RINGS 10:55		TRASH														MOIST	12 9 19 GOOD RECOVERY ~ 20" NEED MORE CINDER (E.T.)
25-26 1/2	NO RINGS 11:10 EOS 11-13-96		TRASH														MOIST	50 @ 4 1/2" SHUT DOWN WAITING ON DELIVERY OF BRASS RINGS
30-31 1/2	BRASS RINGS 11:25		TRASH														MOIST	16 7 12 KIDNEY 2 BRASS RINGS
35-36 1/2	BRASS RINGS NO SAMPLE		TRASH														MOIST	MORE BLINDING BY HAZARD
40-41	BRASS RING 2:50		TRASH														MOIST	1 large brass ring
45	BRASS RING 3:15		TRASH														MOIST	~ 8" sample
50	BRASS RING 4:05		TRASH														MOIST	2 3/4" sample 1/2" in dia

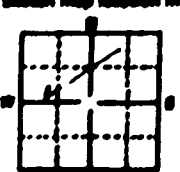


PB 1  
 2692 COLLAR  
 2353 Static  
 2097 Water Intercept (Top)

USE TYPEWRITER OR  
 BALL POINT PEN

State of Idaho  
 Department of Water Resources  
**WELL DRILLER'S REPORT**

State law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

<p><b>1. WELL OWNER</b></p> <p>Name <u>CAMPBELL COUNTY</u></p> <p>Address <u>Caldwell, Idaho</u></p> <p>Owner's Permit No. _____</p>	<p><b>7. WATER LEVEL</b></p> <p>Static water level <u>7.37</u> feet below land surface</p> <p>Flowing? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No G.P.M. flow _____</p> <p>Temperature _____ F. Quality _____</p> <p>Artesian closed-in pressure _____ p.s.i.</p> <p>Controlled by <input type="checkbox"/> Valve <input type="checkbox"/> Cap <input type="checkbox"/> Plug</p>																																																														
<p><b>2. NATURE OF WORK</b></p> <p><input checked="" type="checkbox"/> New well <input type="checkbox"/> Deepened <input type="checkbox"/> Replacement</p> <p><input type="checkbox"/> Abandoned (Describe method of abandoning) _____</p>	<p><b>8. WELL TEST DATA</b></p> <p><input checked="" type="checkbox"/> Pump <input type="checkbox"/> Bailor <input type="checkbox"/> Other</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Discharge (G.P.M.)</th> <th>Draw Down</th> <th>Hours Pumped</th> </tr> </thead> <tbody> <tr> <td><u>5 G.P.M.</u></td> <td><u>1.1</u></td> <td><u>3</u></td> </tr> </tbody> </table>	Discharge (G.P.M.)	Draw Down	Hours Pumped	<u>5 G.P.M.</u>	<u>1.1</u>	<u>3</u>																																																								
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<p><b>3. PROPOSED USE</b></p> <p><input checked="" type="checkbox"/> Domestic <input type="checkbox"/> Irrigation <input type="checkbox"/> Test <input type="checkbox"/> Other (Specify type) _____</p> <p><input type="checkbox"/> Municipal <input type="checkbox"/> Industrial <input type="checkbox"/> Stock <input type="checkbox"/> Waste Disposal or Injection</p>	<p><b>9. LITHOLOGIC LOG</b></p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th rowspan="2">Well Diam.</th> <th colspan="2">Depth</th> <th rowspan="2">Material</th> <th rowspan="2">Status Yes/No</th> </tr> <tr> <th>From</th> <th>To</th> </tr> </thead> <tbody> <tr> <td><u>20</u></td> <td><u>0</u></td> <td><u>3</u></td> <td><u>Till Soil</u></td> <td></td> </tr> <tr> <td><u>11</u></td> <td><u>3</u></td> <td><u>45</u></td> <td><u>SAND 20% CLAY</u></td> <td></td> </tr> <tr> <td><u>11</u></td> <td><u>48</u></td> <td><u>152</u></td> <td><u>SANDY CLAY</u></td> <td></td> </tr> <tr> <td><u>11</u></td> <td><u>152</u></td> <td><u>205</u></td> <td><u>Yellow Clay</u></td> <td></td> </tr> <tr> <td><u>11</u></td> <td><u>205</u></td> <td><u>251</u></td> <td><u>Grey Clay sticky</u></td> <td></td> </tr> <tr> <td><u>20</u></td> <td><u>251</u></td> <td><u>297</u></td> <td><u>Blue Shale</u></td> <td></td> </tr> <tr> <td><u>20</u></td> <td><u>297</u></td> <td><u>327</u></td> <td><u>Blue clay 10% sand</u></td> <td></td> </tr> <tr> <td><u>20</u></td> <td><u>327</u></td> <td><u>520</u></td> <td><u>Blue Clay (Shale)</u></td> <td></td> </tr> <tr> <td><u>18</u></td> <td><u>520</u></td> <td><u>595</u></td> <td><u>Grey Shale</u></td> <td></td> </tr> <tr> <td><u>16</u></td> <td><u>595</u></td> <td><u>640</u></td> <td><u>Shale sandy</u></td> <td></td> </tr> <tr> <td><u>16</u></td> <td><u>640</u></td> <td><u>658</u></td> <td><u>Blue clay</u></td> <td></td> </tr> </tbody> </table>	Well Diam.	Depth		Material	Status Yes/No	From	To	<u>20</u>	<u>0</u>	<u>3</u>	<u>Till Soil</u>		<u>11</u>	<u>3</u>	<u>45</u>	<u>SAND 20% CLAY</u>		<u>11</u>	<u>48</u>	<u>152</u>	<u>SANDY CLAY</u>		<u>11</u>	<u>152</u>	<u>205</u>	<u>Yellow Clay</u>		<u>11</u>	<u>205</u>	<u>251</u>	<u>Grey Clay sticky</u>		<u>20</u>	<u>251</u>	<u>297</u>	<u>Blue Shale</u>		<u>20</u>	<u>297</u>	<u>327</u>	<u>Blue clay 10% sand</u>		<u>20</u>	<u>327</u>	<u>520</u>	<u>Blue Clay (Shale)</u>		<u>18</u>	<u>520</u>	<u>595</u>	<u>Grey Shale</u>		<u>16</u>	<u>595</u>	<u>640</u>	<u>Shale sandy</u>		<u>16</u>	<u>640</u>	<u>658</u>	<u>Blue clay</u>	
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<p><b>4. METHOD DRILLED</b></p> <p><input checked="" type="checkbox"/> Cable <input type="checkbox"/> Rotary <input type="checkbox"/> Dug <input type="checkbox"/> Other</p>	<p><b>10. WELL CONSTRUCTION</b></p> <p>Diameter of hole <u>20</u> inches Total depth <u>658</u> feet</p> <p>Casing schedule: <input checked="" type="checkbox"/> Steel <input type="checkbox"/> Concrete</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Thickness</th> <th>Diameter</th> <th>From</th> <th>To</th> </tr> </thead> <tbody> <tr> <td><u>375</u> inches</td> <td><u>16</u> inches</td> <td><u>2</u> feet</td> <td><u>525</u> feet</td> </tr> <tr> <td><u>250</u> inches</td> <td><u>10</u> inches</td> <td><u>527</u> feet</td> <td><u>527</u> feet</td> </tr> <tr> <td><u>250</u> inches</td> <td><u>10</u> inches</td> <td><u>637</u> feet</td> <td><u>658</u> feet</td> </tr> </tbody> </table> <p>Was casing drive shoe used? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No</p> <p>Was a pecker or seal used? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No</p> <p>Perforated? <input type="checkbox"/> Yes <input type="checkbox"/> No</p> <p>How perforated? <input type="checkbox"/> Factory <input type="checkbox"/> Knife <input type="checkbox"/> Torch</p> <p>Size of perforation _____ inches by _____ inches</p> <p>Number _____ From _____ To _____</p> <p>_____ perforations _____ feet _____ feet</p> <p>_____ perforations _____ feet _____ feet</p> <p>_____ perforations _____ feet _____ feet</p> <p>Well screen installed? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No</p> <p>Manufacturer's name <u>JOHNSON</u></p> <p>Type <u>STAINLESS</u> Model No. _____</p> <p>Diameter <u>18</u> Slot size <u>25</u> Set from <u>527</u> feet to <u>637</u> feet</p> <p>Diameter _____ Slot size _____ Set from _____ feet to _____ feet</p> <p>Gravel packed? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No Size of gravel <u>NO. 10</u></p> <p>Placed from <u>527</u> feet to <u>658</u> feet</p> <p>Surface seal depth <u>20</u> Material used in seal <input checked="" type="checkbox"/> Cement grout</p> <p><input type="checkbox"/> Packing clay <input type="checkbox"/> Well fittings</p> <p>Sealing procedure used <input type="checkbox"/> Slurry pit <input checked="" type="checkbox"/> Temporary surface casing</p> <p><input type="checkbox"/> Overbars to seal depth</p>	Thickness	Diameter	From	To	<u>375</u> inches	<u>16</u> inches	<u>2</u> feet	<u>525</u> feet	<u>250</u> inches	<u>10</u> inches	<u>527</u> feet	<u>527</u> feet	<u>250</u> inches	<u>10</u> inches	<u>637</u> feet	<u>658</u> feet																																														
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<p><b>6. LOCATION OF WELL</b></p> <p>Sketch map location must agree with written location. <u>63</u></p>  <p>Substation Name _____</p> <p>Lot No. _____ Block No. _____</p> <p>County <u>CAMPBELL</u></p>	<p><b>11. DRILLER'S CERTIFICATION</b></p> <p>Work started <u>10/4/77</u> finished <u>2/16/78</u></p> <p>Firm Name <u>WITT Drilling Firm, Inc.</u></p> <p>Address <u>Caldwell, Idaho 83402</u></p> <p>Signed by (Firm Officer) <u>Kenneth Witt</u></p> <p>and <u>David Caldwell Dyfke</u></p>																																																														

HOLE NUMBER PB-2-CC JOB NUMBER I120491

HOLLADAY ENGINEERING COMPANY COLLAR ELV. ~ 2830'

PAGE 1 OF 2

PROJECT Pekles Butte OWNER Canyon Co:

LOCATION: CO. Canyon SEC. 21 1/4 SE OF 1/4 NW T. 2 N R. 3 W

LOGGED BY Srowd DATE START 4-15-92 DATE FINISHED 4-22-92 HOLE DEPTH 557' ANGLE 90° DRILL METHOD CORE ZEMM DIAMETER 2.4" DRILL MODEL Longyear 44

102  
45%  
8%  
0%

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS	
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.				GRAPHIC
0-1	4-15-92 2:00																		
2				silty sand										10-4		unconsolid.	ROAD		no core recovery/loose sand
3			lt gy br	"										"		"	F		sample collected in container
4			"	"										"		"	L		at collar - prob. rd fill
5	linear collar 2:50		"	"										"		"			no core rec. Rd fill head
6			"	"										10-3		"			
7			"	"										"		"			
8			"	"										"		"			
9			"	"										"		"			
10			"	"										"		"			
	3:30			"										"		"			
				gy wht silty sand & clay										"		"			
15	hole collar at 15'	5:20		"										10-4		min.			was sent to call office about collars, etc
				"										"		1-2 cm voids circular void			try drilling holes in layers
				"										10-2		mod consolidated			damp - 6%
				clay w/ mottled										10-7		wk consol.	massive		12.5 - 15 fines first core Rec.
	EOS 6:00			"										10-7		wk consol.			wk bedding
20	4-16-92 7:00		lt gy	sand										10-3		unconsolid			
	hole logs 7:30			mod sandstone										10-3		unconsolid			dry
	cuttings 9:15		lt gy to	frag silty sand										10-3		min. wk consol			coarse immature sandstone
	cuttings 9:45		"	silty fine sandy										10-5		cutting 7 P			bimodal grain size distrib.
			"	"										10-5		va - wk consol			dry
	11:30		"	"										10-5		wk consol.			no core sample coll. @ collar
			"	silty clay										10-5		"			sampled silty clay called Rec SEC
			"	clayey silt										10-5		"			sampling bias favors coarser
			"	"										10-6		"	massive		of collector catching cuttings
			"	"										10-6		"			
	1:00		"	"										10-6		"			
30			"	"										10-6		"			
			"	"										10-5		"			
			"	"										10-5		"			
33.5	EOS 4:30	1:45		"										10-5		"			
	4-17-92 8:00			olive tan gr. clayey silt										10-4		wk consol.			
	using H <sub>2</sub> O			"										10-4		wk mod consol.			1:50-3:00 Reaming stuck to bit cutting
90%				"										10-4		"			inject clear mud + water - hole bottom 78.5
	drilling rate 8:30			"										10-4		"			(physical) CORE ANAL. TOO SHORT FOR LEXAN TUBES
38.5				"										10-4		"			
				olive gyar										10-5		"			
				"										10-5		"			
100%	drilling fast			clayey silt										10-5		"			inject H <sub>2</sub> O + polymer
				"										10-5		"			
48.6	water run 9:05			"										10-5		"			
				"										10-5		"			
				"										10-6		"			
85%				"										10-6		"			
				"										10-5		"			
				"										10-5		"			
48.4		10:00		"										10-5		"			
90%				"										10-4		"			
				"										10-5		"			

HOLE NUMBER P8-2 JOB NUMBER T1120491

HOLLADAY ENGINEERING COMPANY

PAGE 2 OF 2

PROJECT Pickles Butte

OWNER Canyon Co.

LOCATION: CO. Canyon

SEC. 21

1/4 SE OF 1/4 NW T 2 N R 3 W

LOGGED BY Strand DATE START 4-15-92 DATE FINISHED 4-20-92 HOLE DEPTH \_\_\_\_\_

ANGLE 90°

DRILL METHOD core

DIAMETER 2.4"

DRILL MODEL Longer 44

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
902	fast drilling 4-17		gray-grn	silt/clay/sd										10-4		wkly consol.	massive	inject H <sub>2</sub> O + polymer
53'	10:50		"	siltstone and									10-4		"	"	(fluidail clear mud)	
652			olive-grn	"									10-5		mod. consol.	"		
			"	"									10-3		"	"		
			"	"									10-3		"	"		
58'	11:10		"	siltstone									10-3		"	"		
			"	"									10-4		"	"		
852			gray-grn	"									10-4		"	"		
63'	lost core 11:30		"	"									10-4		"	"	inject H <sub>2</sub> O	
802			"	fine sand									10-3		wk consol.	"	sand in hole bottom, losing circ.	
			"	coarse silt									10-4		"	"	cross beds	
			gray-tan	silty sand									10-4		"	"	x bedding	
			"	silt/clay									10-4		"	"	wk bed	
68'	Water run 12:15		"	sandy clay									10-4		mod. consol.	"		
	4-19 8:20		"	fine sand + silt									10-4		wet bed	"	quit for day EDS @ 2:00 high winds + dust storm	
	8:25		"	fine sand									10-4		"	"	inject H <sub>2</sub> O + polymer	
532			"	"									10-4		massive	"		
73'	8:25		"	silt									10-4		"	"		
			"	silt w/ minor clay									10-4		"	"		
100%			"	"									10-5		nk consol.	massive		
			"	"									10-5		"	"		
78'	9:05		"	clayey silt									10-5		"	"		
			"	silty clay									10-6		mod. consol.	"		
			"	"									10-7		"	"	coarse? clayey silt	
552			"	"									10-7		"	"		
83'	9:30		"	fine sand - silt									10-7		cross-bed	"	inject H <sub>2</sub> O + polymer	
	4-19 8:00 am		"	NO SAMPLE									10-6		"	"	CROSS	
070	check in hole		"	fine (fine sand) (small)									10-3		loose fine	"	water run core blurry @ casing	
	10:00		"	"									10-3		"	"	hole squeezed, re-venturing 15' get stuck in hole after 3 ft in	
	hole bottom		"	"									10-3		"	"	backs off hole, no flow	
88'	losing core 11:00		"	NO SAMPLE									10-3		"	"	fills w/ sand/air into foam	
			"	NO CORE SAMPLE									10-3		"	"	sample from sand blowing up casing	
	Try in		"	"									10-3		"	"	"	
090	chg bit		gray-tan	"									10-3		"	"	"	
			"	"									10-3		"	"	"	
93'	2:30		"	"									10-3		"	"	"	
	Try Air		tan-olive	silty fine sand									10-3		wk consol.	"	run quick + clear mud	
3%	Quick + Clear mud		"	"									10-4		"	"	2 inches of core recovery	
			"	"									10-4		"	"	last rest down hole	
			"	"									10-4		"	"	H <sub>2</sub> O inject trip out 4:30	
	3:10		"	"									10-4		"	"	"	
	trip in 7:30		olive	"									10-4		"	"	lose circ. Trip out + get stuck @ 56' ABOUT HOLE	

HOLE NUMBER DB-24 JOB NUMBER T1102491

HOLLADAY ENGINEERING COMPANY

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PROJECT Pickles butte

OWNER Canyon Co.

LOCATION: CO. Canyon SEC. 21 1/4 SE OF 1/4 NW T 2 N R 3 W

LOGGED BY Stroud DATE START 4-20-74 DATE FINISHED 5-15 HOLE DEPTH 557' ANGLE -90° DRILL METHOD Rotary/Cone DIAMETER \_\_\_\_\_ DRILL MODEL Longyear 44

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING			HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS	
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.				MEAS.
103'	4-22			no temp														
	9:20			silt														cuttings indicate silt but hardness + sand from up hole confounding does not allow further classification
				no temp														
113' 10% 114' 25%	10:00		grey-brown	silt														
	2:30			"									10-4					REPAIRING TO SET CASING - ON SYSTEM
				fine sand w/ silt										-4				Inject H <sub>2</sub> O
				silt										-4	minor bed			clear mud
				"	"									-4				CASING SET TO 113' TYP PUNCH
				"	"									-4				BORG CORE
170' 6% 123' 30% 127' 50%	3:30			silt w/ fine sand														
				no sample														core bedding / significant grain size changes
				no sample														
				no sample														
				no sample														
				no sample														
139' 136' 80% 133' 20% 139' 139'	3:45			SAMP														
				fine sand														
				clayey silt														
				clayey silt + sd														
				clay, minor silt														
				fine sand w/ silt														
131' 80% 133' 20% 139' 139'	4-23-74 8:30			silt minor clay														
				silt														
				fine sand w/ silt														
				no sample														
				"														
				"														
138' 139' 10% 445' 50% 146' 37% 148'	10:00			silt + minor clay														
				heavy sand about pure clay														
				clayey silt														
				no sample														
				"														
				"														
445' 50% 146' 37% 148'	11:20			"														
				"														
				silty fine sand														
				"														
				"														
				"														

HOLE NUMBER PB-2 JOB NUMBER T1120491 HOLLADAY ENGINEERING COMPANY PAGE 4 OF 12  
 PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO Canyon SEC. 21 1/4 SE OF 1/4 NW T 2 N R 3 W  
 LOGGED BY Stroud DATE START 4-26-92 DATE FINISHED 5-15 HOLE DEPTH 557' ANGLE -90° DRILL METHOD CORE DIAMETER 2.4" 10 DRILL MODEL Langyeer 44

Elev.	INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
				ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAY	ANG	WK	MOD	WELL	EST.	MEAS.			
812	153	4-23	gray-tan	fine silty sand										10-7				injected H <sub>2</sub> O	
		Trip out 2:15		clay										10-6	mod consol.				
				clayey silt										10-4				50% no. - trip out for loss - tube bit	
			lt gray tan	silty clay										-5					
			gray-tan	silty sand										-4					
	154	3:45	gray-tan	silty clay										-5	wt laminated				silty clays mod. consol. det. det
			lt gray tan	clayey fine sand										-5	bed in dgs				sands w/lt to unconsolidated
			"	"										-4	wt consol.				
			"	"										-4					
			"	"										-4					
	163	5:05 4-28-92	"	"										-4				injected H <sub>2</sub> O	trip back in hole, loss of H <sub>2</sub> O
		7:00 am	"	no samp.															
		no more	"	"															
	167	8:15	lt gray tan	silty fine sand										-4	specific gravel				access - HEAVY STEEL - GRABENT
			"	"										-4	some silt				up through consolidated zones
			"	clayey silt										-5	wt - unconsol.				mostly w/lt to unconsolidated
			"	"										-4	"				
	172	9:00	"	"										-4	"				some visible clay / binding sand
			"	"										-4	"				
			"	"										-4	"				
	177	9:45	"	silty fine sand										-4					
			"	"										-4					
			"	"										-4					
			"	"										-4					
	184	10:30	lt gray tan	sandy silt										-4	mod str consol				
			"	silty clay										-4	wt consol.				
			"	silty fine sand										-4					
			"	"										-4					
	188	11:15	lt gray tan	sandy silt w/ clay										-4	mod consol.				bedding structures
			"	"										-5					more clay less sand
			"	"										-5					
			"	"										-5					
	193	11:45	"	silty sand										-4	wt consol.			injected H <sub>2</sub> O	consolidation limited to zones within to a foot thick
			lt gray tan	clayey silt										-5					
			"	"										-5					
			"	silty fine sand										-4					
			"	"										-4					
	194	12:30	"	fine sand										-3					
			"	sandy silt										-4					
			"	"										-4					





HOLE NUMBER PA-72 WELL NUMBER T1120491

HOLLADAY ENGINEERING COMPANY

PROJECT Tricone

OWNER Canyon Co.

LOCATION: CO. Canyon SEC. 21

1/4 SE OF 1/4 NW 22

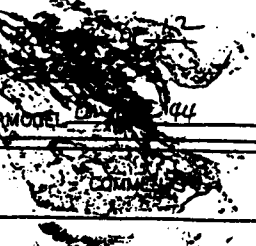
DATE START 4-20-92 DATE FINISHED 5-75

HOLE DEPTH 557 ANGLE 90 DRILL METHOD Core

DIAMETER 2 3/4 @ 4 DRILL MODEL 1944

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	GRAPHIC	
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.				
63% 252-253	10:30	lt gray tan	silty sand												10-4				
	2:50	lt gray tan	clay & silty sand												10-3				
		lt gray tan	silty fine sand												10-7				
			"	silty clay											10-4				
		4:45	"	silty clay/silt											10-7				
254	EDS 4:45	"	"											10-7					
	4:30-9:00	"	silty sand											10-7					
50% 257-268	Drill wet	"	sandy silt											10-4					
	UPD	gel. py. sp.	"											10-4					
	liner penetrates	"	"											10-3					
	slows down	"	"											10-3					
268	9:30	gray to	silty sandstone											10-5					
		"	silty sandstone											10-5					
85% 273-277		"	clayey siltstone											10-5					
		"	"											10-5					
		"	"											10-5					
273	10:00	gray to	silty claystone											10-5					
		"	"											10-5					
73% 277-279		"	"											10-5					
		"	"											10-5					
279	11:15	"	clayey siltstone											10-4					
		"	silty claystone											10-4					
96% 284-288		"	"											10-5					
		"	"											10-5					
		"	"											10-5					
284	12:40	"	"											10-5					
		"	"											10-5					
288	5-1-92		no sample											10-5					
	Tricone to set casing		"											10-5					
288	5-2-92	gray tan	clayey siltstone											10-5					
	Air.com	"	"											10-5					
28% 294		"	"											10-5					
	blow dry	10:15	"	clayey siltstone										10-5					
50% 297-298		"	silty claystone											10-5					
	clay	"	"											10-5					
297	4:30	"	"											10-7					
	4:30	"	"											10-7					
100% 299	10:00	"	"											10-7					
	12:45	"	" coarse clay											10-7					

Inject H<sub>2</sub>O  
blow dry hole  
NO GAS H<sub>2</sub>O  
after 3 1/2 hrs.  
AIR CORP  
INJECT H<sub>2</sub>O  
REWORKED  
SOL horiz. bdd.  
parting on bdd planes  
on well consol. material  
horizontal str on bdd plane  
material is "tight" and dense  
and has become more consistent  
consolidate since about 250'  
Decide to case in this zone  
and try air core again.  
Tricone beam hole 113'-  
288 - set casing to 287'  
damp from  
previous  
injected  
H<sub>2</sub>O??  
minor fossil wood stems?  
parting planes on bedding  
quartz "hercynite" spots?  
AIR CORP  
DRY MOST  
OF DAY  
FOURMAN H<sub>2</sub>O  
damp clay?  
INJECT H<sub>2</sub>O  
due to plugging up by air



HOLE NUMBER PB-2 JOB NUMBER T1120491

HOLLADAY ENGINEERING COMPANY

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PROJECT Pickles Butte

OWNER Canyon Co.

LOCATION: CO Canyon SEC 21

1/4 SE OF 1/4 NW T. 2 N R. 3 W

LOGGED BY Strawd DATE START 4-20-92 DATE FINISHED 5-15

HOLE DEPTH 557' ANGLE -90 DRILL METHOD C&E

DIAMETER 2 1/4" DRILL MODEL Longyear 44

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
100%			gray-prim	coarse clayst										10-7	fine fine		injected H <sub>2</sub> O	clay size fraction but not a plastic or patty type	
304	12:05		"	"										-7	hard subterr			a "coarse" boundary damp clay w/ minor silt fraction	
84%			"	clayey minor										-7	mod. str. consolidation	massive		perhaps silt siltier than prev. run.	
			"	"										-6					
310	1:20		"	"										-6				SAVED INTO TO CHECK SITUATION	
			"	"										-6					
			"	"										-6	6bd strat.			CRUSHED WHEN BLOCKING OFF	
84%			gray prim	silty claystone										-6				occasional bands, blebs	
			"	"										-6				and erratic zones of hematite stain are present in all of the clay.	
			"	"										-6				Minor fine plant debris, grass, the gastropod & animal bones present	
316	2:00		"	"										-6					
			"	"										-6	bed				
100%			"	"										-6					
			"	"										-6					
321	2:40		"	"										-6					
			gray prim	silty claystone										-6	mod strong induration	massive		same powdery damp clay	
			"	"										-6					
			"	"										-6					
326	3:15		"	"										-6					
			gray prim	silty claystone										-6					
			"	"										-6					
			"	"										-6					
			"	"										-6					
332	4:00		"	"										-6				blow hole dry	
			"	"										-6				Damp dry w/o air (28%mc)	
334	5:4/8:10		"	"										-6				INT. SAMPLE SAME DAMP BUT NOT SORTED	
			"	"										-6				INJECT H <sub>2</sub> O SAME MATERIAL MASSIVE CLAY BUT BECOMING HARDER	
			gray prim	silty claystone										-6	str. indur.				
			"	"										-6					
			"	"										-6					
			"	"										-6					
340	8:45		"	"										-6					
			"	"										-6	mod. horz.				
			"	"										-6					
			"	"										-6					
92%			"	"										-6					
			"	"										-6					
			"	"										-6					
345	9:30		"	"										-6					
			"	"										-6	bed strong induration			occasional hematite orange stains	
			"	"										-6					
			"	"										-6					
			"	"										-6					
350			"	"										-6					

HOLE NUMBER PB-2 JOB NUMBER T1120491

HOLLADAY ENGINEERING COMPANY

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PROJECT Pickles Butte

OWNER Canyon Co.

LOCATION: CO Canyon

SEC 21

1/4 SE OF 1/4 NW T 2 N R 3 W

LOGGED BY STROUD

DATE START 4-20-92

DATE FINISHED 5-15

HOLE DEPTH 557 ANGLE -90°

DRILL METHOD COLE

DIAMETER 2 1/4"

DRILL MODEL Longyear 44

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING			HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS	
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
832	351	10:30	grey-gn	silty glassstone										10-6				inject H <sub>2</sub> O	ABT GRASS THAN PREVIOUS
			CHANCE	draker										-6	mod str ind				heavy silty clay blocks but
			ADDITIVE	grey-grn										-6	parting on bedding				moist. damp becoming darker
				grey-grn										-6					Alaystone iron minimal in reduced form as metallic grey blocks
832	357	12:10												-6	mod indur				no lamellae / possible
			grey-brn											-6	CRACKLING				RED OX around 35 1/2'
														-6	PLANT TRASH				TRANSITIONAL OXIDATION
														-6	occass.				NO MATERIAL CHANGE OTHER THAN OXID.
717	363	12:35	blu-grey											-6	mod indur				NO REDUCTION PARTIAL REDUCTION HERE
				silty claystone										-6					REDUCED HERE
														-6	STRONG INDUR				ON DRYING CLAYSTONE BECOMES POWDERY BUT MOD. HARD
														-6					BECOMES LIGHT GRAY ON DRYING.
832	370	1:45												-6					CARBON PLANT TRASH COMMON SINCE REDUCED
			med. grey	silty claystone										-6					GOT STUCK 10 MINUTES BREAKING
														-6	fine bed				GOOD JOINT ABOVE HOLE BOTTOM.
														-6	MOD. STR. CONSOLIDATION				APPEARS SLIGHTLY MORE SILTY
872	376	2:20												-6					DRY CLAY
														-6					10-12%
														-6					MUSCOVITE MORE ABUNDANT
														-6					HOMOGENEOUS SILTY CLAY HAS NOT VARIED MUCH PHYSICALLY SINCE 270'
632	382	2:50	med. grey	silty claystone										-6					INJECTING H <sub>2</sub> O
														-6	platestone				SAME HARD SUFFICIENTLY
														-6	act hard				TO CRACK IN LINDER EVEN WHEN FLUID FILLED
														-6	mod str				
1002	390	3:30												-6					ADJACENT CARBON BED
			med. grey	silty claystone										-6					INTER H <sub>2</sub> O
														-6					THIS RUN DIDN'T HAVE MUCH INJECTED H <sub>2</sub> O IN SAMPLER LINER - GOOD TEST RUN
														-6	mod str				RUN DRY FOR 1 HR 4:15-5:15
1002	395	4:10												-6					less silty
		5-5-92		claystone										-6					sticks @ moisture 10-14%
		8:15												-7	10-11% H <sub>2</sub> O				NO H <sub>2</sub> O INT.
														-7	strong comp				" " " almost pure modeling clay

HOLE NUMBER PB-2 JOB NUMBER T1120491

HOLLADAY ENGINEERING COMPANY

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PROJECT Pickles Butte

OWNER Canyon Co.

LOCATION: CO. Canyon

SEC 21

1/4 SE OF 1/4 NW T 2 N R 3 W

LOGGED BY Strawel DATE START 4-20-92 DATE FINISHED 5-15 HOLE DEPTH 557' ANGLE 90 DRILL METHOD Core DIAMETER 2.4" DRILL MODEL Longyear 44

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
100%			MED. GRAY	Claystone										10-7	Strong consolidation		massive	Inject H <sub>2</sub> O sticky cly w/ minor silt
403	9:00 am		"	"										-7				EST. 10-14% formation
100%			"	"										-7				H <sub>2</sub> O MEDIUM GRAY BECOMES VERY LIGHT CEMENT GRAY ON DRYING OUT
408	9:30		"	"										-7				10-14% ~2% silt 98% cly
			MED. GRAY	CLAYSTONE										-7	STR. CONS.			water H <sub>2</sub> O INTERMEDIATE
80%			"	"										-7				
414	10:00		"	"										-7				
83%	1:00		MED. GRAY	Claystone										-7				
420	1:30		"	"										-7				
			"	"										-7				
58%	1:40		MED. GRAY	CLAYSTONE										-7				
			"	"										-7				
426	3:30		"	"										-7				
			"	"										-7				
	4:45		MED. GRAY	CLAYSTONE										-7	STRONG CONSOLIDATED			
71%			"	"										-7				
			"	"										-7				
433	5:30		"	"										-7	SUB-HORIZ. FOLD			
	7:00		MED. GRAY	CLAYSTONE										-7	STRONG CONSOLID.			
71%			"	"										-7				
			"	"										-7				
			"	"										-7				
440	8:45		"	"										-7				
			MED. GRAY	CLAYSTONE										-7	HORIZ. ADD. STR. CONS.			
70%			"	"										-7				
			"	"										-7				
447	9:15		"	"										-7				
70%			"	"										-7				
			"	"										-7				

HOLE NUMBER PC-2 JOB NUMBER T1120491

HOLLADAY ENGINEERING COMPANY

PAGE 10 OF 12

PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO. Canyon SEC. 21 1/4 SE OF 1/4 AW T 2 N R 3 W

LOGGED BY Stroud DATE START 4-20-93 DATE FINISHED 5-15-93 HOLE DEPTH 557' ANGLE -90° DRILL METHOD CORE DIAMETER 2.4" DRILL MODEL Longyear 44

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
100	454	9:45		MED. GRAY CLAYSTONE										10-7				INJECT H <sub>2</sub> O	MATERIAL BASICALLY UNCHANGED SINCE 395' OR EVEN 363'
				"										-7					
				"										-7					
				"										-7					
				"										-7					
712	460	10:00		MED. GRAY CLAYSTONE										-7					
				"										-7					
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				"										-7					
832	467	11:30		MED. GRAY CLAYSTONE										-7					
				"										-7					
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832	473	12:15		MED. GRAY CLAYSTONE										-7					
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832	479	12:45		MED. GRAY CLAYSTONE										-7					
				"										-7					
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832	485	1:30		MED. GRAY CLAYSTONE										-7					
		2:00		"										-7					
				"										-7					
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				"										-7					
832	491	7:45		MED. GRAY CLAYSTONE										-7					
				"										-7					
				"										-7					
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				"										-7					
070	496	3:45		"										-7					
	497	5-7-97	10:15		MED. GRAY CLAYSTONE									-7					
		5-15-97	10:00		NO SAMPLE									-7					

DRILL ONLY THIS ONE FOOT SAMPLE  
NO SAMP - DUCKER TRUCKED OVER TIME

INJECT WATER IN HOLE BOTTOM IN MORNING  
4:00 blow hole - return air coming from inside casing  
RESEAL casing + DRILL TUBING TO SET ABOVE CASING FROM 290' TO 295'

HOLE NUMBER PB2 JOB NUMBER T1120491

HOLLADAY ENGINEERING COMPANY

PROJECT Piedras Botte OWNER Canyon Co. LOCATION: CO. Canyon SEC 21 1/4 SE OF 1/4 NW T 2 N R 3 W

LOGGED BY STROWD DATE START 1/20/92 DATE FINISHED 5-15 HOLE DEPTH 55.7 ANGLE -90° DRILL METHOD CORE DIAMETER 2 1/4" DRILL MODEL Longyear 44

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS				
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.				GRAPHIC			
						CORE TRAE																
0%																						
505																						
507	10:45			MED GR CLAYSTONE																		INSTECT H2O TAKE RUBBER PACKER CHECK MUD DEBRIS MIXED IN SAMPLE
510				"																		NATIVE MOISTURE INSIDE CORE WETTING FRONT ~ 15% - 20%
512	11:30			MED GR CLAYSTONE																		1" MED GRAY CORE IS VERY LIGHT TAN-GRY UPON DRYING. THIS COLO CHARACTERISTIC APPLIES TO ALL GRAY CLAYSTONE ENCOUNTERED THRU FA.
517	12:00			"																		
520				LOST RECOVERED SAMPLE																		RUBBER PACKER DEBRIS IN SAMPLE
524	1:00	1:00		MED GR CLAYSTONE																		20-26% GUT MOLES IN LINEAR NATIVE RELEASED INT. H2O H2O RETAINED
530		1:15		"																		
536		2:00		MED GR CLAYSTONE																		20-25 GOOD SAMPLE FOR NATIVE UNDISTURBED SAMPLE MOISTURE NO PACKED IN INSTECT H2O (DRILLED INTO LEAKY LINER)
540		2:30		"																		
545		3:00		MED GR CLAYSTONE																		CLAYSTONE BEHIND BEDDING SLIGHTLY COARSER GRAINED
548				"																		
550				"																		
552				"																		
554				"																		
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HOLE NUMBER 2B-4 JOB NUMBER T2120491 HOLLADAY ENGINEERING COMPANY ELEV. 2930 PAGE 1 OF 13  
 PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE - 2 N R 3 W  
 LOGGED BY Smow DATE START 9-29-92 DATE FINISHED 10-21-92 HOLE DEPTH 440 ANGLE -90° DRILL METHOD Air Rotary E.C. DIAMETER 12 1/4" DRILL MODEL Schramm T68-DA

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY	GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT			GRAIN ROUNDING			HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
					CLY	SLT	SAND/GRV	ANG	WK	MOD	WELL	EST.			
	DRILL NOTES		ROCK TYPE GRAPHIC												
	Reverse Circ. 9-29-92														
	Air Rotary														
5	5:14	4:20	H gy-tan Road fill w/ fine sand + Grav								10-24	W/C CONSOLIDATION	~9%	GRAVEL FRACTION WELL ROUNDED MAY BE FORMATION GRAVEL IN PART OR GRAVEL FROM PAD CONSTRUCTION	
10	5:24	4:24	H tan-bn fine sand/GRV								10-24.3	W/C	~10%	GRAVEL CLASTS 1/4 TO 1/2" AND BRANAS LAGERS	
15		4:26	H tan-bn fine sand minor gravel								10-24.31	W/C-MOD	~12%	slightly damp	
20		4:30	H tan-bn fine sand minor GRAV.								10-24.3	W/C-MOD	~12%	slightly damp	
25		4:34	H tan-bn fine sand some silt								10-25	W/C	~10%	dry	
30		4:36	tan clayey silt w/ fine-med sand								10-24	W/C-MOD	~10%	dry	
35	5:01	4:40 02:30-21	tan clayey sandy clay								10-25	MOD	~15%	slightly damp	
40		7:30	tan clayey fine sand								10-25	MOD	~12%		
45		7:35	tan clayey fine sand w/ minor gravel								10-25	MOD	~15%	very poorly sorted material	
50			tan clayey silt								10-25	MOD	~12%	dry	



HOLE NUMBER PB-4 JOB NUMBER T2120491 HOLLADAY ENGINEERING COMPANY PAGE 2 OF 13  
 PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE T. 2 N R. 3 W  
 LOGGED BY STAND DATE START 9-27-92 DATE FINISHED 10-21 HOLE DEPTH 640 ANGLE -90° DRILL METHOD Air Rotary R.C. DIAMETER \_\_\_\_\_ DRILL MODEL Schram

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS.VOID.ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC		
	R.C. 9-30-92																	
	Air Rotary 5 1/4"																	
55	8:15	tan	silty clay											10 <sup>-6</sup>	mod.		~25%	clay is partially "balling up"
60	9:30	tan	silty clay w/ minor sand											10 <sup>-5</sup>	mod.		~20%	somewhat "clumpy" feeling
65	9:45	gy-tan	fin sandy silt											10 <sup>-4</sup>	wk-mud.		~15%	almost "dry + dusty" trace gravel
70	9:00	gy-tan	fin sandy silt											10 <sup>-5</sup>	mod-mud		~15%	minor gravel
75	9:02	gy-tan	silty fine sand											10 <sup>-4</sup>	wk-mud		~15%	"flowing sand" almost "dry"
80	9:05	tan	fin sandy silt											10 <sup>-5</sup>	wk-mud		~15%	
85	9:08	tan	clayey fine sand silt											10 <sup>-5</sup>	wk-mud		~15%	
90	9:10	gy-tan	fine sandy gravel											10 <sup>-4</sup>	wk-mud		~12%	
95	9:12	lt tan	silty fine sand											10 <sup>-5</sup>	wk-mud		~12%	
100	9:15	lt tan	silty fine sand											10 <sup>-4</sup>	wk		~15%	almost clumpy feeling

HOLE NUMBER PB-4 JOB NUMBER T2120491 HOLLADAY ENGINEERING COMPANY PAGE 3 OF 13  
 PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO. Canyon SEC 21 1/4 SW OF 1/4 SE T 2 N R 3 W  
 LOGGED BY Strand DATE START 9-29-92 DATE FINISHED 10-21 HOLE DEPTH 640 ANGLE -90 DRILL METHOD \_\_\_\_\_ DIAMETER \_\_\_\_\_ DRILL MODE Screens

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY	GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
					CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
			ROCK TYPE GRAPHIC														
	DRILL NOTES																
R.C. Air Rotary	D.C. 9-30-92																
	Air																
	Bottom																
105	9:18		H tan silty fine sand										10 <sup>-5</sup>	wk-mod		~12-15%	
110	9:20		H tan silty fine sand										10 <sup>-3</sup>	wk		~10%	D&Y, almost no clay fraction
115	9:25		H tan silty fine sand										10 <sup>-4</sup>	wk-mod		~12%	some clay again
120	9:30		H gy tan silty fine sand										10 <sup>-3</sup>	wk		~12%	less clay
125	9:32		H gy tan clayey silt w/ minor gravel										10 <sup>-5</sup>	wk mod		~12%	
130	START USING AVE. COMPRESS METER		H gy tan clayey silt w/ minor gravel										10 <sup>-5</sup>	wk mod		~12%	almost dry
135	Teeping up.		H gy tan silty fine sand										10 <sup>-4</sup>	wk		~10%	D&Y
140	9:45		H gy tan silty fine sand minor gravel										10 <sup>-4</sup>	wk		~12%	
145	9:50		H gy tan silty fine sand										10 <sup>-3/-4</sup>	wk		~15%	almost damp / almost some less clay
150	9:50		H tan silty fine sand										10 <sup>-4</sup>	wk-mod		~12%	

HOLE NUMBER PO-4 JOB NUMBER T2120491 HOLLADAY ENGINEERING COMPANY PAGE 4 OF 13  
 PROJECT Pickles Butte OWNER Camp Co. LOCATION: CO Camp SEC 21 1/4 SW OF 1/4 SE T 2 N R 3 W  
 LOGGED BY Stowd DATE START 9-29-72 DATE FINISHED 10-11 HOLE DEPTH 640 ANGLE -90 DRILL METHOD \_\_\_\_\_ DIAMETER \_\_\_\_\_ DRILL MODEL Schramm

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAY	ANG	WK	MOD	WELL	EST.	MEAS.			
155	10:00		tan-brn	sandy silt w/ minor gravel											10 <sup>-5</sup>	wk-med		12-15%
160	10:10		tan-brn	silty fine sand w/ gravel											10 <sup>-4</sup>	wk-med		~12-15%
165	10:20		tan-brn	silty fine sand											10 <sup>-3</sup>	wk		~12% ALMOST DRY
170	10:30		tan-brn	silty fine sand											10 <sup>-3</sup>	wk		~12% still "flowing" sand
175	10:40		tan-brn	fine sandy GRAVEL											10 <sup>-3</sup>	wk-med		~12-15% CLIMATE AIND ON MANY CLASTS CLASTS HAVE BEEN WELL ROUNDED
180	10:45		tan-brn	fine sandy gravel											10 <sup>-3</sup>	wk-med		~12%
185	10:50		tan-brn	fine sand											10 <sup>-3</sup>	wk		~12% fairly well sorted sand w/ possible few gravel clasts
190	10:55		tan-brn	fine sand											10 <sup>-3</sup>	wk		~12% clean sand
195	11:00		tan-brn	fine sand											10 <sup>-3</sup>	wk		~10% DRY
200	11:05		tan-brn	silty fine sand											10 <sup>-2</sup> /10 <sup>-4</sup>	wk		~12% finer sand more silt

HOLE NUMBER PB-4 JOB NUMBER T2120491 HOLLADAY ENGINEERING COMPANY PAGE 5 OF 13  
 PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE T 22 N R 3 W  
 LOGGED BY Steward DATE START 2-27-72 DATE FINISHED 10-21 HOLE DEPTH 640 ANGLE -90 DRILL METHOD \_\_\_\_\_ DIAMETER \_\_\_\_\_ DRILL MODE Screw

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS. VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC		
205	9-30-92 11:15		tan-brn	silty fine sand										10 <sup>-4</sup>	wk-mud		~12%	ALMOST DRY; "HUNT" OF MOTTLES
210	11:25		tan-brn	fine coarse sand										10 <sup>-3</sup>	wk		~12%	LESS SILT
215	11:30		tan-brn	silty sand										10 <sup>-4</sup>	wk		~12%	MORE SILT AS DEEPER
220	11:40		tan-brn	silty fine sand										10 <sup>-5</sup>	wk-mud		~12%	MORE CLAY
225	11:55		lt-brn	fine coarse sand w/ some gravel										10 <sup>-3</sup>	wk-mud		~10-12%	NO CLAY
230	12:10		br-tan	silty sand w/ gravel										10 <sup>-4</sup>	MUD		~12%	ALL GULLS Project Picked RDS STICKING ← silt binding + casing on RDS
235	12:30		br-tan	silty fine sand										10 <sup>-4</sup>	WK-MUD		~12%	
240	12:50		tan-brn	silty fine sand										10 <sup>-4</sup>	WK-MUD		~12%	
245	1:00		tan-brn	silty fine sand fine sandy silt										10 <sup>-4</sup> / <sub>10<sup>-5</sup></sub>	WK-MUD		~12%	GETTING FINER
250	1:30		tan-brn	fine sandy silt										10 <sup>-5</sup>	WK-MUD		~12%	

HOLE NUMBER PD-4 JOB NUMBER TU20491 HOLLADAY ENGINEERING COMPANY PAGE 6 OF 13  
 PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE T. 2 N R. 3 W  
 LOGGED BY Stowe DATE START 9-29-72 DATE FINISHED 10-21 HOLE DEPTH 640 ANGLE -90° DRILL METHOD \_\_\_\_\_ DIAMETER \_\_\_\_\_ DRILL MODEL Schramm

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
255	1:45	brn-tan	fine silty sand											10 <sup>-4</sup>	MOD		~12-15%	TRACE CLAY
260	2:00	brn-tan	fine sandy silt											10 <sup>-5</sup>	MOD		~12%	VIRTUALLY DRY + DUSTY
265	2:45	brn-tan	fine sandy silt minor gravel											10 <sup>-5</sup>	wk-MOD		~12%	
270	2:10	lt brn	claystone											10 <sup>-6</sup> /10 <sup>-7</sup>	MOD-STR			
275	2:15	lt brn	CLAYSTONE											10 <sup>-7</sup>	MOD-STR			
280	2:20	tan	CLAYSTONE											10 <sup>-7</sup>	MOD-STR		<20%	DUST @ DISCHARGE (DRY) MUCH OF SILT FRACTION BEING COLLECTED @ SAMPLE DISCHARGE AS DUST CLAY BLOWING AWAY
285	2:28	tan	CLAYSTONE											10 <sup>-7</sup>	MOD-STR		~25%	WETTED BY INJECTION SLIGHTLY
290	2:30	tan	CLAYSTONE											10 <sup>-7</sup>	MOD-STR		<20%	
295	2:35	tan	CLAYSTONE											10 <sup>-7</sup>	MOD-STR		<20%	TRIP OUT - CAN'T GO FURTHER R.C. AIR: WILL BEAM 12 3/4" MUD RUN BY 2-300 FT. END OF SHIFT @ 5:00
300	2:40	tan	CLAYSTONE											10 <sup>-7</sup>	MOD-STR		<20%	

HOLE NUMBER 2B-4 JOB NUMBER J1124091

HOLLADAY ENGINEERING COMPANY

PAGE 7 OF 13

PROJECT Pickles Butte OWNER Canyon Co LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE T 2 N R 3 W

LOGGED BY STWLD DATE START 9-29-92 DATE FINISHED 10-21 HOLE DEPTH 640 ANGLE 90° DRILL METHOD AIR ROTARY DIAMETER 8" DRILL MODEL Schramm

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
	DRILL NOTES																	
	8" AIR Rotary	10-13-92																NO H <sub>2</sub> O INJECT
305		7:40	LT-TAN	SILTY CLAY										10 <sup>-6</sup>	WK-MOD CONSOLID			REAMED 0-279' CHECK FOR WATER - FOUND POSSIBLE RETURN WATER ALLOW HOLE WAIT 2 HRS - ADD H <sub>2</sub> O used Med Low water in hole sample 30 is NOT REPRESENTATIVE - HOLE REQUIRES CLOSING
310	AIR CORE		LT-TAN	SILTY CLAY										10 <sup>-6</sup>	WK-MOD	LOOSE LOW DENSITY CLAY NOT NO OPEN VOIDS	~35%	
			"	"										-6	"		" ?	
			"	"										-6	"		" ?	POOR SAMPLE CORE
	↓	2:30	"	"										-6	"		" ?	309-311; 2 FT RECOVERABLE
315	AIR CORE AGAIN	5:	LT-TAN	SILTY CLAY										-6	"		>35%	CORE ATTEMPT AGAIN
	↓	5:30	"	"										-6	"		>35%	GOOD RECOVERY (311-315)
	AIR ROTARY	10-14-92	"	"										-6	"		>35%	SAMPLE VERY DAMP - RELEASE
	↓		"	"										-6	"		>35%	FILM OF MOISTURE ON CORE 312-313 Pulled for lab test
320		7:15	LT-TAN	SILTY CLAY										10 <sup>-5/10<sup>-6</sup></sup>	WK-MOD		>35%	SLIGHTLY DAMP FROM HOT COMPRESSOR. MIN. ROTARY
325		7:25	LT-TAN	SILTY CLAY										10 <sup>-6</sup>	WK-MOD		>35%	
330		7:50	LT-TAN	CLAYEY SILT										10 <sup>-5</sup>	WK		~35%	
335		8:05	LT-TAN	CLAYEY SILT										10 <sup>-5</sup>	WK		~32%	
340		8:15	LT-TAN	CLAYEY SILT										10 <sup>-5</sup>	WK		~35%	
345		8:30	LT-TAN	CLAYEY SILT										10 <sup>-5</sup>	WK		>35%	QUITE DAMP
350		8:45	LT-TAN	CLAYEY SILT										10 <sup>-5/4</sup>	WK		>35%	

HOLE NUMBER PA-4 JOB NUMBER T2120491

HOLLADAY ENGINEERING COMPANY

PAGE 8 OF 13

PROJECT Pickles Butte OWNER Canyon Co.

LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE T 2 N R 3 W

LOGGED BY Strawd DATE START 9-29-72 DATE FINISHED 10-21 HOLE DEPTH 646 ANGLE -90 DRILL METHOD \_\_\_\_\_ DIAMETER \_\_\_\_\_ DRILL MODEL Schram

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
	DRILL NOTES																	
	AIR																	No HD INJECTION
	8"																	↓
355	8:50	LT TAN	SILTY CLAY											10-6	WK-MOD		~35%	
360	9:00	LT TAN	SILTY CLAY											10-6	WK-MOD		~35%	
365	3:40	LT TAN	CLAYEY SILT											10-5	WK		~35%	LOST CORE SPREAD DOWN HOLE 11:45 - 2:00
370	3:50	LT TAN	SILTY CLAY											10-6	WK-MOD		~35%	MORE CLAY
375	3:55	LT TAN	SILTY CLAY											10-5	MOD		~35%	
380	4:00	LT TAN	SILTY CLAY											10-6	MOD		~35%	
385	4:05	LT TAN	SILTY CLAY											10-6	MOD		~35%	
390	4:10	LT TAN	CLAYSTONE											10-7	MOD		>35%	
395	4:15	LT TAN	CLAYSTONE											10-7	MOD		~35%	
400	4:20	LT TAN	CLAYSTONE											10-7	MOD		~35%	QUITE DAMP

HOLE NUMBER PD-4 JOB NUMBER T2120491 HOLLADAY ENGINEERING COMPANY PAGE 9 OF 13  
 PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO Canyon SEC 21 1/4 SW OF 1/4 SE T 2 N R 3 W  
 LOGGED BY Shaw DATE START 9-29-92 DATE FINISHED 10-21 HOLE DEPTH 640 ANGLE -90 DRILL METHOD AIR ROTARY DIAMETER 8" DRILL MODEL Schram

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	EST. WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC		
405	AIR	10-15-92	LT GRN	CLAY										10-9		WK-MOD	+35%	CHECK FOR WATER - PROBE COGE DOWN TO 388' (TD @ 400) NO WATER LEAKY LAYER CONDENSED SALT TUBE W/ CORE BARREL MARKING EXTRATION OF SPITTING NARROW CORE SAMPLE QUITE DAMP, SOME LAMINATED THIN BEDDING NO H <sub>2</sub> O INTERFERE IN HOLE 404-405 pulled for Lab tests
	COGE	7:45	DRY	"										-7	CONSOLIDATION	+35%		
				DRY	"										-7	"	+35%	
	V	10:20	GRN-BRN	"											-7	"	+35%	
	AIR																	
410	Rotary DRILLING																	
	DRY	12:05	GRN-BRN	CLAY											-7	MOD. CONS.	+35%	FORMS CLAY GULLS @ DEPTH DISCHARGE VERY DAMP feeling
415		12:10	LT GRN-BRN	CLAY											-7	MOD. CONS.	+35%	trace silt
420		12:25	GRN-BRN	CLAY											-7	MOD. CONS.	+35%	↑ OXIDIZED REDUCED
425		12:40	GRN-GRY	CLAY											-7	MOD. CONS.	+35%	↓
430		12:55	GRN-GRY	CLAY											-7	MOD. CONS.	+35%	TRACE SILT
435		1:05	GRY	CLAY											-7	MOD. CONS.	+35%	
440	EOS	1:20	GRY	CLAY											-7	MOD. CONS.	+35%	DRILLY LENSES
40%	11:00 AM	10-20-92	GRY-GRN	same silt											-7	MOD. CONS.	+35%	DRILLY LENSES
	FOR AIR		OXIDIZED	BRN	up clay											WK-CONS.		GRANDVIEW check after sitting 4-days - none VERY DAMP BUT (SAT TO WITHIN 3FT OF HOLE - ROTARY) HOLE MUDWATER CLEAR NOT WET - CORE SAMPLE 400-405
445	APPROX															WK		APPEARS to be hole shaft CORE BIT AVARAGE + FAILED HAVE TO REEL ANOTHER pull 444-449 for Lab tests
	SAMPLE	9:30													-5	?? silt??		
450		12:00		fine silt											-6	WK	+35%	PARTIALLY OXIDIZED

Broken  
AND  
LOOSE



HOLE NUMBER PP-4 JOB NUMBER TZ120491 HOLLADAY ENGINEERING COMPANY PAGE 10 OF 13  
 PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE T 2 N R 3 W  
 LOGGED BY Stowd DATE START 9-29-92 DATE FINISHED 10-21 HOLE DEPTH 640 ANGLE -90 DRILL METHOD AIR ROTARY DIAMETER 8" DRILL MODEL Schramm

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
	DRILL NOTES																	
	12:20-72																	
	12:20																	
455	12:20	GRAY-BRN	fin sandy silt											-5	WK		+35%	VERY DAMP PARTIALLY OXIDIZED
460	12:25	GRAY-BRN	clayey silt											-6	WK		+35%	BECOMING LESS OXIDIZED
465	12:25	GRAY-BRN	clayey silt											-6	WK		~35%	MORE OXIDIZED
470	12:30	DARK BRN	CLAYEY SILT											-5/-6	WK		~35%	
475	12:34	BRN-GRAY	CLAYEY SILT											-5/-6	WK		~35%	
480	12:34	BRN-GRAY	CLAYEY SILT											-6	WK		+35%	VERY DAMP
485	12:40	BRN-GRAY	CLAYEY SILT											-5/-6	WK		~35%	
490	12:45	BRN-GRAY	CLAYEY SILT											-6	WK		~35%	STILL PARTIALLY OXIDIZED
495	12:50	MED GRAY	SILTY CLAY											-6/-7	WK-MOD		+35%	QUITE DAMP - MORE CLAY
500	12:55	MED GRAY	SILTY CLAY											-7	WK-MOD		+35%	DAMP CLAY INCREASING

Temp at 500 - Check for water - more DAMP CLAY INCREASING

HOLE NUMBER 70-4 JOB NUMBER T2120491

HOLLADAY ENGINEERING COMPANY

PAGE 11 OF 13

PROJECT Pickles Butte OWNER Canyon Co.

LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE T 2 N R 3 W

LOGGED BY Shaw DATE START 9-29-92 DATE FINISHED 10-21 HOLE DEPTH 640 ANGLE -90° DRILL METHOD \_\_\_\_\_ DIAMETER \_\_\_\_\_ DRILL MODEL Schramm

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.		WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC			
505	10:20 NO RECOVERY 10:21-92																		
	AIR 10:35 Rotary	BRN GRAY	CLAY										10-7	WK-MOD CONSOLIDATION					Clear hole by Trip in + blow water @ 9:00 - 10:00 None (10-21-92) 10-20-92 - AIR CORZ MAD NO WATER NO RECOVERY DUE TO LOOSE FORMATION - NO BLOWING MATERIAL + 35% SW - SOUT OF THE TUBE. Rotary cutting. Sub-505 VERY DAMP
510	10:40	DRK GRAY	CLAY											-7	WK-MOD			+35%	MORE SILT - STILL "BALLING"
515	10:45	RED GRAY	SILTY CLAY											-6	WK-LOOSE			~35%	AIR LONGER IN HALL @ DISCARD
520	10:47	RED GRAY	CLAYEY SILT											-5/-6	WK			~35%	
525	10:50	GRAY	SILTY CLAY											-6/57	WK			~35%	Trace sand
530	10:52	GRAY	CLAY											-7	WK			+35%	
535	10:55	GRAY	SILTY CLAY											-7	WK-CONSIL			+35%	
540	10:59	GRAY	SILTY CLAY											-7	WK-MOD			+35%	TOO DAMP
545	11:01	GRAY	SILTY CLAY											-7	WK to MOD			+35%	
550	11:05	GRAY	SILTY CLAY											-7	WK-MOD			+35%	

HOLE NUMBER PB-4 JOB NUMBER T120491

HOLLADAY ENGINEERING COMPANY

PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO. Canyon SEC. 21 1/4 SW OF 1/4 SE T. 2 N R. 3 W

LOGGED BY Strawd DATE START 9-29-92 DATE FINISHED 10-21 HOLE DEPTH 646 ANGLE -90° DRILL METHOD \_\_\_\_\_ DIAMETER \_\_\_\_\_ DRILL MODEL Schramm

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VOIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.			
555	11:10	GRAY	CLAYSTONE											10-7	WK-MOD		+35%	
560	11:14	GRAY	CLAYSTONE											-7	WK-MOD		+35%	
565	11:16	GRAY	CLAYSTONE											-7	WK-MOD		+35%	VERY DAMP
570	11:20	GRAY	CLAYSTONE											-7	WK-MOD		+35%	VERY DAMP; TRACE SILT
575	11:24	GRAY	CLAYSTONE											-7	WK-MOD		+35%	VERY DAMP ZONE 565-575
580	11:28	GRAY	CLAYSTONE											-7	WK-MOD		+35%	ALSO 580 DRILL SCRAMBLE ALTHOUGH NO APPARENT YIELD EVIDENCE IN HOLE DURING DRILLING
585	11:30	GRAY	CLAYSTONE											-7	MOD CONSOLID		+35%	ABT HARDER MATERIAL
590	11:35	GRAY	CLAYSTONE											-7	MOD		+35%	
595	11:40	GRAY	CLAYSTONE											-7	MOD		+35%	

HOLE NUMBER PD-4 JOB NUMBER 7120491

HOLLADAY ENGINEERING COMPANY

PAGE 13 OF 13

PROJECT Pickles Butte OWNER Canyon Co. LOCATION: CO Canyon SEC 21 1/4 SW OF 1/4 SE T 2 N R 3 W

LOGGED BY STROWD DATE START 9-29-92 DATE FINISHED 10-21-92 HOLE DEPTH 640 ANGLE -90° DRILL METHOD Air Rotary DIAMETER 8" DRILL MODEL Schramm T65

INTERVAL (FT)	DATE TIME	COLOR	LITHOLOGY		GEOPHYSICS LOG	GRAIN SIZE REL. PERCENT				GRAIN ROUNDING				HYDRAULIC PROPERTIES		INDURATION & STRUCTURE FXS, VCIDS, ETC.	WATER	COMMENTS
			ROCK TYPE	GRAPHIC		CLY	SLT	SAND	GRAV	ANG	WK	MOD	WELL	EST.	MEAS.	GRAPHIC		
	DRILL NOTES																	
	AIR																	
	Rotary																	
	8'																	
605	11:50	GRAY	CLAYSTONE	=====										10-7		MOD CONSOLIDATED	+35%	VERY DAMP
610	11:55	GRAY	CLAYSTONE	=====										-7		MOD	+35%	VERY DAMP
615	12:00	GRAY	CLAYSTONE	=====										-7		MOD	+35%	
620	12:08	GRAY	CLAYSTONE	=====										-7		MOD	+35%	DRILLER FEELS POORLY SORTED BRACKEN ZONE
625	12:15	GRAY	CLAYSTONE	=====										-7		MOD	+35%	ABIT MORE SILT - DRILLER FEEL MAKING MUD & WATER 610-630 POSSIBLE SCREEN ZONE
630	12:20	GRAY	CLAYSTONE	=====										-7		MOD	~35%	ABIT DRIER FEELING
635	12:25	GRAY	CLAYSTONE	=====										-7		MOD	~30-35%	DISTINCTLY LESS MASSIVE PARTIALLY OXIDIZED CLAY CLASTS
640	TD	GRAY	CLAYSTONE	=====										-7		MOD	~30-35%	WATER CHECK - WATER IN THE PARTIALLY OXIDIZED CLAY CLASTS

STATE OF IDAHO  
DEPARTMENT OF WATER RESOURCES

USE TYPEWRITER OR  
BALLPOINT PEN

# WELL DRILLER'S REPORT

State law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

### 1. WELL OWNER

Name PICKLES BUTTE SANITARY LANDFILL  
Address 115 Albany, Caldwell, ID 83605  
Drilling Permit No. 63-93-W-0554-001004  
Water Right Permit No. \_\_\_\_\_

### 7. WATER LEVEL

Static water level 514 feet below land surface.  
Flowing?  Yes  No G.P.M. flow \_\_\_\_\_  
Artesian closed-in pressure \_\_\_\_\_ p.s.i.  
Controlled by:  Valve  Cap  Plug  
Temperature 77 °F. Quality Poor  
*Describe artesian or temperature zones below.*

### 2. NATURE OF WORK

- New well  Deepened  Replacement  
 Well diameter increase  Modification  
 Abandoned (describe abandonment or modification procedures such as liners, screen, materials, plug depths, etc. in lithologic log, section 9.)

### 8. WELL TEST DATA

Pump  Bailer  Air  Other \_\_\_\_\_

Discharge G.P.M.	Pumping Level	Hours Pumped

### 3. PROPOSED USE

- Domestic  Irrigation  Monitor  
 Industrial  Stock  Waste Disposal or Injection  
 Other \_\_\_\_\_ (specify type)

### 9. LITHOLOGIC LOG

**70568**

Bore Diam.	Depth		Material	Water	
	From	To		Yes	No
12 3/4"	0	40	tan fine sandy silt		
"	40	48	brown sandy gravel		
"	48	140	tan silty clay		
"	140	185	gray silty fine sand		
"	185	225	gray fine to med sand		
"	225	240	light gray clayey silt		
"	240	250	light gray silty fine sand		
"	250	275	tan clay		
"	275	320	fine to med sand		
"	320		mixed gray fine sand and		
"		400	tan clayey silts		
"	400	435	gray fine sand		
12 3/4"	435	455	no sample		
10"	455	485	tan gray silty claystone		
10"	485	560	gray brown silty fine sand		X
5 1/4"	560	620	clayey silt and fine sand		X
5 1/4"	620	660	blue gray claystone		

### 4. METHOD DRILLED

- Rotary  Air  Auger  Reverse rotary  
 Cable  Mud  Other \_\_\_\_\_  
(backhoe, hydraulic, etc.)

### 5. WELL CONSTRUCTION

Casing schedule:  Steel  Concrete  Other \_\_\_\_\_  
Thickness 2.5 inches Diameter 4 inches From 2.5 feet To 512.5 feet  
\_\_\_\_\_ inches \_\_\_\_\_ inches \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_\_ inches \_\_\_\_\_ inches \_\_\_\_\_ feet \_\_\_\_\_ feet  
Was casing drive shoe used?  Yes  No  
Was a packer or seal used?  Yes  No  
Perforated?  Yes  No  
How perforated?  Factory  Knife  Torch  Gun  
Size of perforation? \_\_\_\_\_ inches by \_\_\_\_\_ inches  
Number \_\_\_\_\_ From \_\_\_\_\_ To \_\_\_\_\_  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
Well screen installed?  Yes  No  
Manufacturer Houston Type Pre-pack  
Top Packer or Headpipe \_\_\_\_\_  
Bottom of Tailpipe \_\_\_\_\_

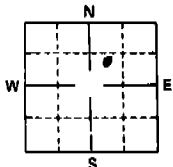
Diameter 4 Slot size .020 Set from 512.5 feet to 522.5 feet  
Diameter \_\_\_\_\_ Slot size \_\_\_\_\_ Set from \_\_\_\_\_ feet to \_\_\_\_\_ feet  
Gravel packed?  Yes  No  Size of gravel 10/20  
Placed from 496 feet to 535 feet

Surface seal depth 400-496 Material used in seal:  Cement grout  
 Bentonite  Puddling clay  \_\_\_\_\_  
Sealing procedure used:  Slurry pit  
 Temp. surface casing  Overbore to seal depth  
Method of joining casing:  Threaded  Welded  
 Solvent Weld  Cemented between strata

Describe access port Top of casing with locking cap and protective cover

### 6. LOCATION OF WELL

Sketch map location must agree with written location.



Subdivision Name Pickles Butte Landfill  
Lot No. \_\_\_\_\_ Block No. \_\_\_\_\_  
County Canyon  
Address of Well Site Perch Road, Pickles Butte  
(give at least name of road)  
SW 1/4 NE 1/4 Sec. 21 T. 2 N  or S   
R. 3 E  or W

### 10.

Work started 7-7-93 finished 11-23-93

### 11. DRILLER'S CERTIFICATION

I/We certify that all minimum well construction standards were complied with at the time the rig was removed.

Firm Name Boyles Brothers Firm No. 503  
Address Box 25608 Salt Lake, Date 11-23-93  
Ut  
Signed by Drilling Supervisor [Signature]  
and  
(Operator) [Signature]  
(If different than the Drilling Supervisor)

**WELL DRILLER'S REPORT**

State law requires that this report be filed with the Director, Department of Water Resources  
within 30 days after the completion or abandonment of the well.

**1. WELL OWNER**  
Name PICKLES BUTTE SANITARY LANDFILL  
Address 6284 Perch Road, Caldwell  
Drilling Permit No. 63-93-W-0554-001  
Water Right Permit No. \_\_\_\_\_

**7. WATER LEVEL**  
Static water level 491 feet below land surface.  
Flowing?  Yes  No G.P.M. flow \_\_\_\_\_  
Artesian closed-in pressure \_\_\_\_\_ p.s.i.  
Controlled by:  Valve  Cap  Plug  
Temperature 75 °F. Quality POOR  
*Describe artesian or temperature zones below.*

**2. NATURE OF WORK**  
 New well  Deepened  Replacement  
 Well diameter increase  Modification  
 Abandoned (describe abandonment or modification procedures such as liners, screen, materials, plug depths, etc. in lithologic log, section 9.)

**8. WELL TEST DATA**  
 Pump  Bailer  Air  Other \_\_\_\_\_

Discharge G.P.M.	Pumping Level	Hours Pumped

**3. PROPOSED USE**  
 Domestic  Irrigation  Monitor  
 Industrial  Stock  Waste Disposal or Injection  
 Other \_\_\_\_\_ (specify type)

**9. LITHOLOGIC LOG** **70567**

Bore Diam.	Depth		Material	Water	
	From	To		Yes	No
12 3/4"	0	17	silty sand		
"	17	18	sandy gravel		
"	18	60	tan silty clay		
"	60	95	med sand		
"	95	125	tan calyey silt		
"	125	160	tan clay		
12 3/4"	160	195	fine sand		
7 7/8"	195	220	silty clay		
"	220	360	fine and med sand		
"	360	380	tan clayey silt		
"	380	435	fine sand		
"	435	510	435-490 tan, 490-510 gray silt	x	
"	510	620	gray silty clay		
"	620	690	gray clay stone		
7 7/8"	690	700	gray silty clay		

**4. METHOD DRILLED**  
 Rotary  Air  Auger  Reverse rotary  
 Cable  Mud  Other \_\_\_\_\_  
(backhoe, hydraulic, etc.)

**5. WELL CONSTRUCTION**  
Casing schedule:  Steel  Concrete  Other \_\_\_\_\_  
Thickness Diameter From To  
25 inches 4 inches + 2.5 feet 487.5 feet  
\_\_\_\_ inches \_\_\_\_\_ inches \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_ inches \_\_\_\_\_ inches \_\_\_\_\_ feet \_\_\_\_\_ feet  
Was casing drive shoe used?  Yes  No  
Was a packer or seal used?  Yes  No  
Perforated?  Yes  No  
How perforated?  Factory  Knife  Torch  Gun  
Size of perforation? \_\_\_\_\_ inches by \_\_\_\_\_ inches  
Number From To  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
Well screen installed?  Yes  No  
Manufacturer Houston Type Stainless Steel  
Top Packer or Headpipe \_\_\_\_\_  
Bottom of Tailpipe \_\_\_\_\_  
Diameter 4 Slot size .020 Set from 487.5 feet to 497.5 feet  
Diameter \_\_\_\_\_ Slot size \_\_\_\_\_ Set from \_\_\_\_\_ feet to \_\_\_\_\_ feet  
Gravel packed?  Yes  No  Size of gravel \_\_\_\_\_  
Placed from 478 feet to 515 feet  
Surface seal depth 478 Material used in seal:  Cement grout  
 Bentonite  Puddling clay  \_\_\_\_\_  
Sealing procedure used:  Slurry pit  
 Temp. surface casing  Overbore to seal depth  
Method of joining casing:  Threaded  Welded  
 Solvent Weld  Cemented between strata  
Describe access port Top of casing with locking cap and protective cover.

RECEIVED  
NOV 30 1993

WATER RESOURCES  
WESTERN REGION

RECEIVED  
NOV 26 1993

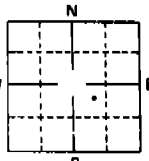
**10.** Work started 7-31-93 finished 11-20-93

**6. LOCATION OF WELL**  
Sketch map location must agree with written location.  
  
Subdivision Name Pickles Butte Landfill  
Lot No. \_\_\_\_\_ Block No. 09 **1994**  
County Canyon  
Address of Well Site 6284 Perch Road  
(give at least name of road)  
SE 1/4 NW 1/4 Sec. 21 T. 2 N.  or S   
R. 3 E  or W

**11. DRILLER'S CERTIFICATION**  
I/We certify that all minimum well construction standards were complied with at the time the rig was removed.  
Firm Name Boyles Brothers Firm No. 503  
Address \_\_\_\_\_ Date 11-23-93  
Signed by Drilling Supervisor [Signature]  
and  
(Operator) [Signature]  
(If different than the Drilling Supervisor)

# WELL DRILLER'S REPORT

State law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

<p><b>1. WELL OWNER</b>                  Name <u>PICKLES BUTTE SANITARY LANDFILL</u>                  Address <u>6284 Perch Road, Caldwell</u>                  Drilling Permit No. <u>63-93-w-0554-001 003</u>                  Water Right Permit No. _____</p>	<p><b>7. WATER LEVEL</b>                  Static water level <u>539'</u> feet below land surface.                  Flowing? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No G.P.M. flow _____                  Artesian closed-in pressure _____ p.s.i.                  Controlled by: <input type="checkbox"/> Valve <input type="checkbox"/> Cap <input type="checkbox"/> Plug                  Temperature <u>77</u> °F. Quality <u>Poor</u>  <small>Describe artesian or temperature zones below.</small></p>																																																																																																																																																																																																																																																																
<p><b>2. NATURE OF WORK</b>  <input checked="" type="checkbox"/> New well    <input type="checkbox"/> Deepened    <input type="checkbox"/> Replacement  <input type="checkbox"/> Well diameter increase    <input type="checkbox"/> Modification  <input type="checkbox"/> Abandoned (describe abandonment or modification procedures such as liners, screen, materials, plug depths, etc. in lithologic log, section 9.)</p>	<p><b>8. WELL TEST DATA</b></p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Discharge G.P.M.</th> <th>Pumping Level</th> <th>Hours Pumped</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	Discharge G.P.M.	Pumping Level	Hours Pumped																																																																																																																																																																																																																																																													
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<p><b>4. METHOD DRILLED</b>  <input checked="" type="checkbox"/> Rotary    <input checked="" type="checkbox"/> Air    <input type="checkbox"/> Auger    <input checked="" type="checkbox"/> Reverse rotary  <input type="checkbox"/> Cable    <input type="checkbox"/> Mud    <input type="checkbox"/> Other _____  <small>(backhoe, hydraulic, etc.)</small></p>	<p><b>10.</b>                  Work started <u>10-01-93</u> finished <u>11-20-93</u></p>																																																																																																																																																																																																																																																																
<p><b>5. WELL CONSTRUCTION</b>                  Casing schedule: <input checked="" type="checkbox"/> Steel    <input type="checkbox"/> Concrete    <input type="checkbox"/> Other _____  <small>Thickness Diameter From To</small>  <u>.25</u> inches <u>4</u> inches + <u>2.2</u> feet <u>535</u> feet                  _____ inches _____ inches _____ feet _____ feet                  _____ inches _____ inches _____ feet _____ feet                  Was casing drive shoe used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No                  Was a packer or seal used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No                  Perforated? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No                  How perforated? <input type="checkbox"/> Factory    <input type="checkbox"/> Knife    <input type="checkbox"/> Torch    <input type="checkbox"/> Gun                  Size of perforation? _____ inches by _____ inches  <small>Number From To</small>                  _____ perforations _____ feet _____ feet                  _____ perforations _____ feet _____ feet                  _____ perforations _____ feet _____ feet                  Well screen installed? <input checked="" type="checkbox"/> Yes    <input type="checkbox"/> No                  Manufacturer <u>Houston</u> Type <u>Wire Wrap</u>                  Top Packer or Headpipe _____                  Bottom of Tailpipe _____                  Diameter <u>4"</u> Slot size <u>.02'</u> Set from <u>535</u> feet to <u>555</u> feet                  Diameter _____ Slot size _____ Set from _____ feet to _____ feet                  Gravel packed? <input checked="" type="checkbox"/> Yes    <input type="checkbox"/> No    <input type="checkbox"/> Size of gravel <u>10/20</u>                  Placed from _____ <u>525</u> feet to _____ <u>566</u> feet                  Surface seal depth <u>520</u> Material used in seal: <input checked="" type="checkbox"/> Cement grout  <input type="checkbox"/> Bentonite    <input type="checkbox"/> Puddling clay    <input type="checkbox"/> _____                  Sealing procedure used: <input type="checkbox"/> Slurry pit  <input type="checkbox"/> Temp. surface casing    <input type="checkbox"/> Overbore to seal depth                  Method of joining casing: <input checked="" type="checkbox"/> Threaded    <input type="checkbox"/> Welded  <input type="checkbox"/> Solvent Weld    <input type="checkbox"/> Cemented between strata                  Describe access port <u>Top of casing with protective cover and lock</u></p>	<p><b>11. DRILLER'S CERTIFICATION</b>                  I/We certify that all minimum well construction standards were complied with at the time the rig was removed.                  Firm Name <u>Boyles Brothers</u> Firm No. <u>503</u>                  Address _____ Date <u>11-23-93</u>                  Signed by Drilling Supervisor <u>[Signature]</u>                  and _____                  (Operator) <u>[Signature]</u>  <small>(If different than the Drilling Supervisor)</small></p>																																																																																																																																																																																																																																																																
<p><b>6. LOCATION OF WELL</b>                  Sketch map location must agree with written location.                    Subdivision Name <u>Pickles Butte Landfill</u>                  Lot No. _____ Block No. _____                  County <u>Canyon</u>                  Address of Well Site <u>6284 Perch Road</u>  <small>(give at least name of road)</small>  <u>NW</u> 1/4 <u>SE</u> 1/4 Sec. <u>21</u> T. <u>2</u> N <input checked="" type="checkbox"/> or S <input type="checkbox"/>                  R. <u>3</u> E <input type="checkbox"/> or W <input checked="" type="checkbox"/></p>	<p><b>ADDITIONAL SHEETS</b> _____                  FORWARD THEM TO THE DEPARTMENT</p>																																																																																																																																																																																																																																																																

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WATER RESOURCES  
WESTERN REGION

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Department of Water Resources

FEB 09 1994

STATE OF IDAHO  
DEPARTMENT OF WATER RESOURCES  
**WELL DRILLER'S REPORT**

USE TYPEWRITER OR  
BALLPOINT PEN

State law requires that this report be filed with the Director, Department of Water Resources  
within 30 days after the completion or abandonment of the well.

1. WELL OWNER

Name CANYON COUNTY (PICKLES BUTTE LANDFILL)  
Address 115 Albany, Caldwell, ID 83605  
Drilling Permit No. 63-93-W-0554-001-002  
Water Right Permit No. \_\_\_\_\_

7. WATER LEVEL

Static water level 393' feet below land surface.  
Flowing?  Yes  No G.P.M. flow \_\_\_\_\_  
Artesian closed-in pressure \_\_\_\_\_ p.s.i.  
Controlled by:  Valve  Cap  Plug  
Temperature 74 °F. Quality Poor  
*Describe artesian or temperature zones below.*

2. NATURE OF WORK

New well  Deepened  Replacement  
 Well diameter increase  Modification  
 Abandoned (describe abandonment or modification procedures  
such as liners, screen, materials, plug depths, etc. in lithologic  
log, section 9.)

8. WELL TEST DATA

Pump  Bailer  Air  Other \_\_\_\_\_

Discharge G.P.M.	Pumping Level	Hours Pumped

3. PROPOSED USE

Domestic  Irrigation  Monitor  
 Industrial  Stock  Waste Disposal or Injection  
 Other \_\_\_\_\_ (specify type)

9. LITHOLOGIC LOG

**70566**

Bore Diam.	Depth		Material	Water	
	From	To		Yes	No
12 3/4"	0	10	tan silty sand		X
"	10	25	tan clayey silt		X
"	25	35	fine sand		X
"	35	50	tan clayey silt		X
"	50	70	tan clay		X
"	70	100	silty fine sand		X
"	100	105	clay		X
"	105	115	fine sand		X
"	115	120	tan clay		X
"	120	125	fine sand		X
"	125	145	tan silty clay		X
"	145	150	sand with cobbles		X
"	150	240	tan silty clay		X
"	240	365	gray clay		X
12 3/4"	365	424	gray clay	X	

4. METHOD DRILLED

Rotary  Air  Auger  Reverse rotary  
 Cable  Mud  Other \_\_\_\_\_  
(backhoe, hydraulic, etc.)

5. WELL CONSTRUCTION

Casing schedule:  Steel  Concrete  Other Stainless Steel  
Thickness Diameter From To  
.25 inches 4 inches + 2.5 feet 377 feet  
\_\_\_\_\_ inches \_\_\_\_\_ inches \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_\_ inches \_\_\_\_\_ inches \_\_\_\_\_ feet \_\_\_\_\_ feet  
Was casing drive shoe used?  Yes  No  
Was a packer or seal used?  Yes  No  
Perforated?  Yes  No  
How perforated?  Factory  Knife  Torch  Gun  
Size of perforation? .020 inches by \_\_\_\_\_ inches  
Number From To  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
\_\_\_\_\_ perforations \_\_\_\_\_ feet \_\_\_\_\_ feet  
Well screen installed?  Yes  No  
Manufacturer Houston Type Stainless Steel  
Top Packer or Headpipe \_\_\_\_\_  
Bottom of Tailpipe 10' S.S. Sump  
Diameter 4" Slot size .020 Set from 377 feet to 407 feet  
Diameter \_\_\_\_\_ Slot size \_\_\_\_\_ Set from \_\_\_\_\_ feet to \_\_\_\_\_ feet  
Gravel packed?  Yes  No  Size of gravel \_\_\_\_\_  
Placed from 299 feet to 424 feet

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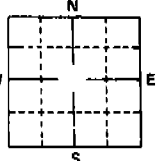
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Department of Water Resources

6. LOCATION OF WELL

Sketch map location must agree with written location  
  
Subdivision Name Pickles Butte Sanitary Landfill  
Lot No. \_\_\_\_\_ Block No. FEB 09 1994  
County Canyon  
Address of Well Site Perch Road, Pickle Butte  
(give at least name of road)  
SW 1/4 NW 1/4 Sec. 21, T. 2 N  or S   
R. 3 E  or W

10.

Work started 10-26-93 finished 11-20-93

11. DRILLER'S CERTIFICATION

I/We certify that all minimum well construction standards were  
Complied with at the time the rig was removed.

Firm Name Boyles Brothers Firm No. 503

Address \_\_\_\_\_ Date 11-23-93

Signed by Drilling Supervisor [Signature]

and

(Operator) [Signature]

(If different than the Drilling Supervisor)



WELL DRILLER'S REPORT

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or  
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WATER RESOURCES  
WESTERN REGION 1 OF 2

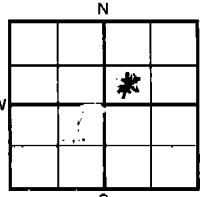
1. DRILLING PERMIT NO. 63-95-W-0564-001

Other IDWR No. \_\_\_\_\_

2. OWNER: County of Canyon  
Name HOLLADAY ENGINEERING  
Address 1431 BUS ALT HWY 95  
City PAYETTE State ID Zip 83661

3. LOCATION OF WELL by legal description:

Sketch map location must agree with written location.



Twp. 2 North  or South   
Rge. 3 East  or West   
Sec. 21 SW 1/4 NE 1/4  
Gov't Lot \_\_\_\_\_ County Canyon

Address of Well Site PICKLE BUTTE DUMP  
City \_\_\_\_\_  
(Give at least name of road + Distance to Road or Landmark)

Lt. \_\_\_\_\_ Blk. \_\_\_\_\_ Sub. Name \_\_\_\_\_

4. PROPOSED USE:

- Domestic  Municipal  Monitor  Irrigation  
 Thermal  Injection  Other \_\_\_\_\_

5. TYPE OF WORK

- New Well  Modify or Repair  Replacement  Abandonment

6. DRILL METHOD

- Mud Rotary  Air Rotary  Cable  Other \_\_\_\_\_

7. SEALING PROCEDURES

SEAL/FILTER PACK			AMOUNT		METHOD
Material	From	To	Sacks or Pounds		
BENTONITE	00	381	12000#		POUR

Was drive shoe used?  Y  N Shoe Depth(s) \_\_\_\_\_  
Was drive shoe seal tested?  Y  N  How? \_\_\_\_\_

8. CASING/LINER:

Diameter	From	To	Gauge	Material	Casing	Liner	Welded	Threaded
4"	+3	508		SMOOTH	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

Length of Headpipe \_\_\_\_\_ Length of Tailpipe 5'

9. PERFORATIONS/SCREENS

- Perforations Method \_\_\_\_\_  
 Screens Screen Type HUSTON

From	To	Slot Size	Number	Diameter	Material	Casing	Liner
508	543	.020		4"	SS	<input type="checkbox"/>	<input type="checkbox"/>

10. STATIC WATER LEVEL OR ARTESIAN PRESSURE:

513.11 ft. below ground Artesian pressure \_\_\_\_\_ lb.  
Depth flow encountered \_\_\_\_\_ ft. Describe access port or control devices: \_\_\_\_\_

11. WELL TESTS:

- Pump  Bailor  Air  Flowing Artesian

Yield gal./min.	Drawdown	Pumping Level	Time
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Water Temp. \_\_\_\_\_ Bottom hole temp. \_\_\_\_\_  
Water Quality test or comments: \_\_\_\_\_

12. LITHOLOGIC LOG: (Describe repairs or abandonment)

Bore Dia.	From	To	Remarks: Lithology, Water Quality & Temperature	Y	N
12	1	10	TOP SOIL: DUST		
	10	17	GRAVEL IN HARD PAN		
	17	28	LARGER GRAVEL + HARD PAN		
	28	30	CLAY + SMALL GRAVEL		
	30	32	MORE GRAVEL LOOSER		
	32	40	CLAY-TIGHT IN SMALL GRAVEL		
10	40	90	CLAY-TIGHT IN SMALL GRAVEL		
	90	95	COARSE SAND IN CLAY		
	95	112	SANDY CLAY		
	112	120	CLAY		
	120	135	CLAY W/ COARSE SAND		
	135	180	HARD CLAY		
	180	182	SUPER HARD CLAY		
	182	205	CLAY		
	205	210	COARSE SAND + CLAY		
	210	263	VERY HARD CLAY THRU REG		
	263	265	VERY HARD CLAY		
	265	305	SOFT CLAY/SANDY CLAY		
	305	315	SAND		
	315	375	CLAY		
	375	400	VERY HARD CLAY (CLAY ROCK)		
	400	405	SOFT SANDY CLAY/CLAY		
	405	430	REG CLAY		
	430	435	SOFT CLAY OR SANDY CLAY		
	435	445	CLAY REG TYPE		
	445	455	HARD CLAY w/ DARK PEA GRAVEL/COARSE SAND		
	455	465	SAME		
	465	470	SOFT CLAY LIKE SANDY CLAY		
	470	475	CLAY		
	475	480	CLAYSTONE + SANDSTONE LIKE PCS		
8	480	487	" " " " " "		
	487	510	GRAY BLUE CLAY		
			CONTINUED		

Completed Depth 544 Date: Started \_\_\_\_\_ Completed MAR 07 1996 (Measurable)

13. DRILLER'S CERTIFICATION

I/We certify that all minimum well-construction standards were complied with at the time the rig was removed.

Firm Name ADAMSON PUMP & DILLING Firm No. 0457

Firm Official Dave Adamson Date 11-17-95

and Supervisor or Operator Dave Adamson Date 11-17-95

(Sign once if Firm Official & Operator)



IDAHO DEPARTMENT OF WATER RESOURCES  
WELL DRILLER'S REPORT

Use Typewriter  
or  
Ball Point Pen

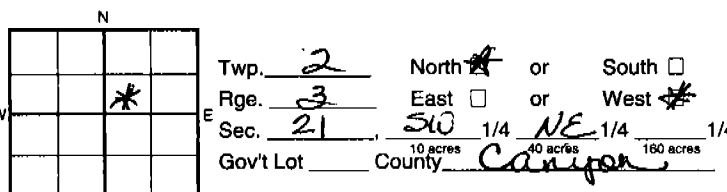
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Pg 1 of 2

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Other IDWR No. \_\_\_\_\_

2. OWNER: County of Canyon  
Name HOLLADAY ENGINEERING CO  
Address 1431 BUS. ALT HWY 95  
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Twp. 2 North  or South   
Rge. 3 East  or West   
Sec. 21 SW 1/4 NE 1/4  
Gov't Lot \_\_\_\_\_ County Canyon

Address of Well Site 15500 MISSOURI  
PICKLE BUTTE LANDFILL City \_\_\_\_\_  
(Give at least name of road + Distance to Road or Landmark)  
Lt. \_\_\_\_\_ Blk. \_\_\_\_\_ Sub. Name PB10

4. PROPOSED USE:  
 Domestic  Municipal  Monitor  Irrigation  
 Thermal  Injection  Other \_\_\_\_\_

5. TYPE OF WORK  
 New Well  Modify or Repair  Replacement  Abandonment

6. DRILL METHOD  
 Mud Rotary  Air Rotary  Cable  Other \_\_\_\_\_

7. SEALING PROCEDURES

SEAL/FILTER PACK		AMOUNT		METHOD
Material	From	To	Sacks or Pounds	
BENTONITE		20	12000	POUR

Was drive shoe used?  Y  N Shoe Depth(s) \_\_\_\_\_  
Was drive shoe seal tested?  Y  N  How? \_\_\_\_\_

8. CASING/LINER:

Diameter	From	To	Gauge	Material	Casing	Liner	Welded	Threaded
10	0	140	.125	STEEL	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
8	+2	500	.125	STEEL	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
4	+2	504		STAINLESS	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

Length of Headpipe \_\_\_\_\_ Length of Tailpipe \_\_\_\_\_

9. PERFORATIONS/SCREENS  
 Perforations Method \_\_\_\_\_  
 Screens Screen Type HOUSTON

From	To	Slot Size	Number	Diameter	Material	Casing	Liner
504	534	.020		4"	STAINLESS	<input type="checkbox"/>	<input type="checkbox"/>

10. STATIC WATER LEVEL OR ARTESIAN PRESSURE:  
\_\_\_\_\_ ft. below ground Artesian pressure \_\_\_\_\_ lb.  
Depth flow encountered \_\_\_\_\_ ft. Describe access port or control devices: \_\_\_\_\_

11. WELL TESTS: WATER RESOURCES WESTERN REGION  
 Pump  Bailer  Air  Flowing Artesian

Yield gal./min.	Drawdown	Pumping Level	Time
RECEIVED			
NOV 27 1995			

Water Temp. \_\_\_\_\_ Bottom hole temp. \_\_\_\_\_  
Water Quality test or comments: \_\_\_\_\_ Department of Water Resources

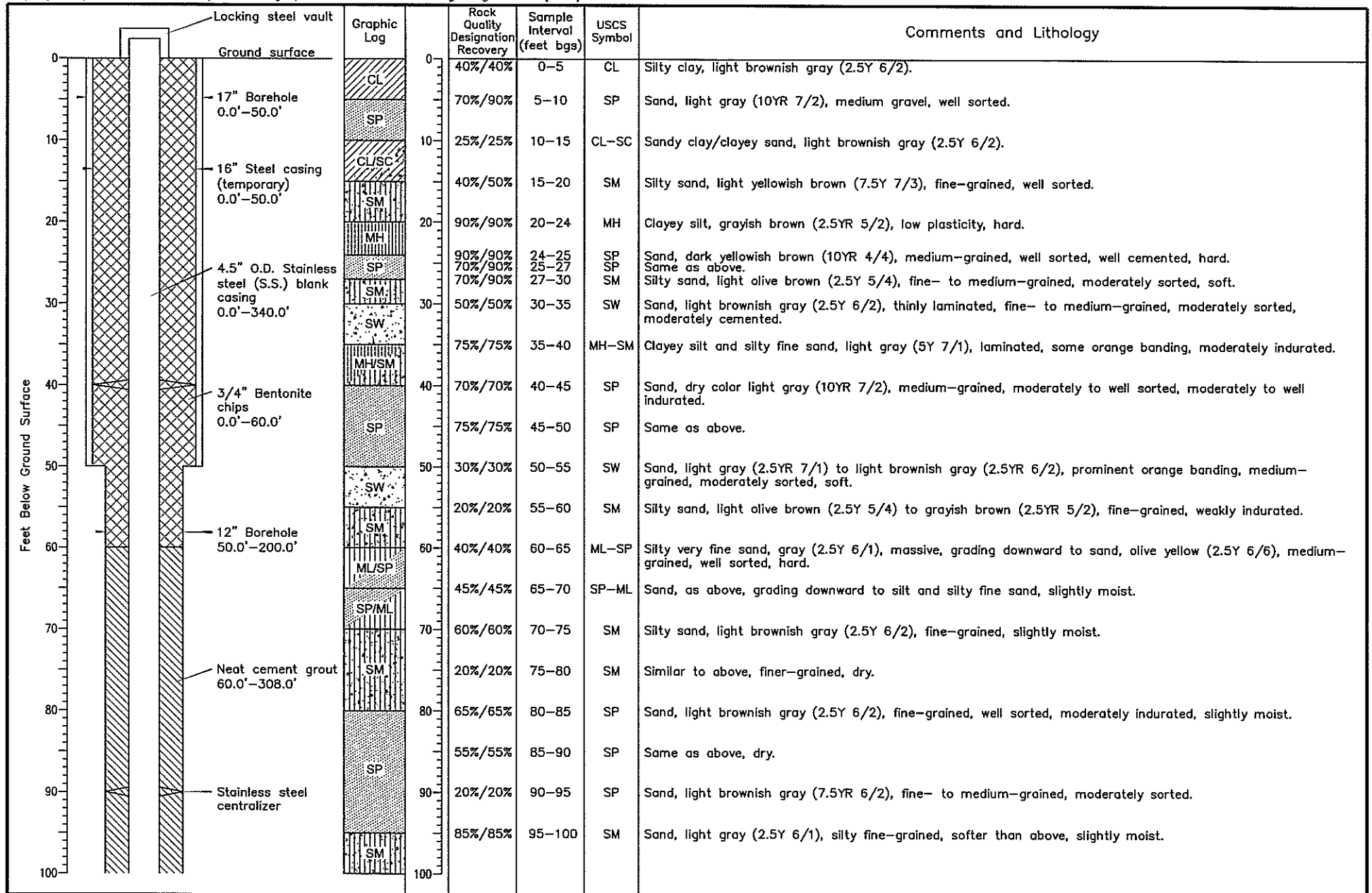
12. LITHOLOGIC LOG: (Describe repairs or abandonment) Water

Bore Dia.	From	To	Remarks: Lithology, Water Quality & Temperature	Y	N
10	1	5	TOP SOIL		
12	5	10	CLAY w/SMALL GRAVEL		
2	10	20	GRAVEL + SAND		
10	20	31	GRAVEL + SAND		
	31	45	CLAY w/SOME SMALL GRAVEL		
	45	55	" " " " COARSE SAND		
	55	73	COARSE SAND w/SOME CLAY (SLOW DRILLING)		
	73	100	CLAY		
	100	105	SAND		
	105	115	SAND (COARSE) w/CLAY SOFT + HARD		
	115	120	COARSE SAND / SMALL GRAVEL / CLAY		
	120	125	SAND w/ GRAVEL - SMALL + CLAY		
	125	130	SAND w/LITTLE CLAY		
	130	135	SAND + MORE CLAY		
	135	136	VERY HARD CLAY		
	136	205	REG CLAY		
8	205	210	SANDY CLAY		
	210	215	SANDY CLAY w/HARD Pcs CLAY		
	215	220	SANDY CLAY - VERY HARD DRILLING		
	220	275	SANDY CLAY - MORE CLAY		
	275	300	SANDY CLAY w/HARD Pcs OF CLAY TAGS FOR		
	300	305	SAND		
	305	339	CLAY		
	339	341	VERY HARD CLAY		
	341	430	CLAY		
	430	455	VERY HARD CLAY (DRILLING SLOWER)		
	455	467	"SUPER" VERY HARD CLAY		
	467	465	REG. CLAY		
	465	470	CLAY w/SMALL GRAVEL		
	470	515	CLAY w/IRON SPOTS		
	515	518	TURNOVER GR		
	518	525	BROWN CLAY		
	525	540	SAND COARSE w/CLAY		

Completed Depth CONTINUED (Measurable)  
Date: Started 8-25-95 Completed 9-29-95

13. DRILLER'S CERTIFICATION  
I/we certify that all minimum well construction standards were complied with at the time the rig was removed.  
Firm Name ADAMSON PUMP & DRILLING Firm No. 04157  
Firm Official Dave Adamson Date 11-17-95  
and  
Supervisor or Operator Dave Adamson Date 11-17-95  
(Sign once if Firm Official & Operator)





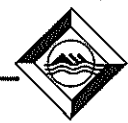
Geologist: J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 6-30-11

Drilling method: Core, air rotary  
 Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420')  
 Sampling device: HQ core, air rotary cuttings (400'-420')  
 Steel surface casing: 16" steel (0'-50')

Northing: 668731.199  
 Easting: 243735.206  
 Elevation: 2654.1 (TOC)

Note: TOC = top of casing

**PICKLES BUTTE  
 Well Log: PB-11**



		Graphic Log	Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
	100	ML	20%/20%	100-105	ML	Sandy silt, pale yellow (2.5Y 8/2), moderately indurated, dry.
	110	ML/SP	20%/20%	105-110	ML-SP	Same as above, interbedded with dark gray (2Y 3/1), medium-grained sandstone, very hard, CaCO3 cement.
	120	ML	20%/20%	110-115	ML	Sandy silt and silt, light olive gray (5Y 6/2), weakly indurated, slightly moist.
	130	ML/SP	20%/20%	115-120	ML-SP	Same as above, interbedded with dark gray medium-grained sandstone.
	140	SM/SP	50%/50%	120-125	SM-SP	Sandy silt, light olive gray, similar to above, slightly moist, with white fine-grained, well sorted sandstone, cross bedded, some yellow with orange banding, dry, hard.
	150	SM/SP	20%/20%	125-130	SM-SP	Same as above, interbedded with sandstone, dark gray (2Y 3/1), medium-grained.
	160	SM	60%/60%	130-135	SM-SP	Sandy silt, pale yellow (2.5Y 7/3), with white fine-grained sand with yellow color banding, dry.
	170	SM	30%/30%	135-140	SM	Silty sand, light gray (5Y 7/2), fine-grained, moist, reddish yellow color banding.
	180	ML	0%/30%	140-145	ML	Sandy silt, light gray (2.5Y 7/2), fine-grained, slightly moist with small (less than 1 inch) reddish yellow clay lenses.
	190	ML	55%/55%	145-150	ML	Siltstone, light gray (2.5Y 7/2), hard, dry.
	200	SM/CL	100%/100%	150-155	SM-CL	Interbedded, silty sand/sandy silt, light brownish gray (7.5Y 6/2) with clay, dark greenish gray (5GY 4/1), thin bands of reddish clay, fine-grained.
		SM	20%/20%	155-160	SM	Silty sand, light yellowish brown (2.5Y 6/4), laminated and color banded, cross bedded, fine-grained, weakly cemented, slightly moist.
		SM	50%/50%	160-165	SM	Silty sand, light brownish gray (2.5YR 6/2), otherwise as above, very fine-grained, borderline sandy silt.
		SP	100%/100%	165-168	SP	Similar to above, but dominantly fine sand.
		SP	100%/100%	168-170	SP	Sandstone, light olive brown (2.5Y 5/4), color banded, cross bedded, fine, soft, slightly moist.
		SM	50%/50%	170-175	SM	Silty sandstone, grayish brown (7.5Y 5/2), massive to laminated, color banding (yellow), trough cross bedded, fine-grained, organic material (?).
	SM	30%/50%	175-180	SM	Silty sandstone, light olive brown (7.5Y 5/3), fine-grained, similar to above, slightly moist.	
	SM/ML	100%/100%	180-185	SM-ML	Sandy silt and silty sand, gray (5Y 5/1) to grayish brown (2.5Y5/2), moderately indurated, slightly moist.	
	ML	85%/85%	185-190	ML	Siltstone, gray (5Y 5/1), moderately to strongly cemented, massive, slightly moist to dry.	
	CL	0%/0%	190-195	CL	Little recovery, clay, appears to be dark gray (5Y 4/1).	
	ML	65%/75%	195-200	ML	Siltstone, sandy silt and clayey silt intervals, gray (5Y 5/1), reddish brown color banding, moderately indurated, very slightly moist.	

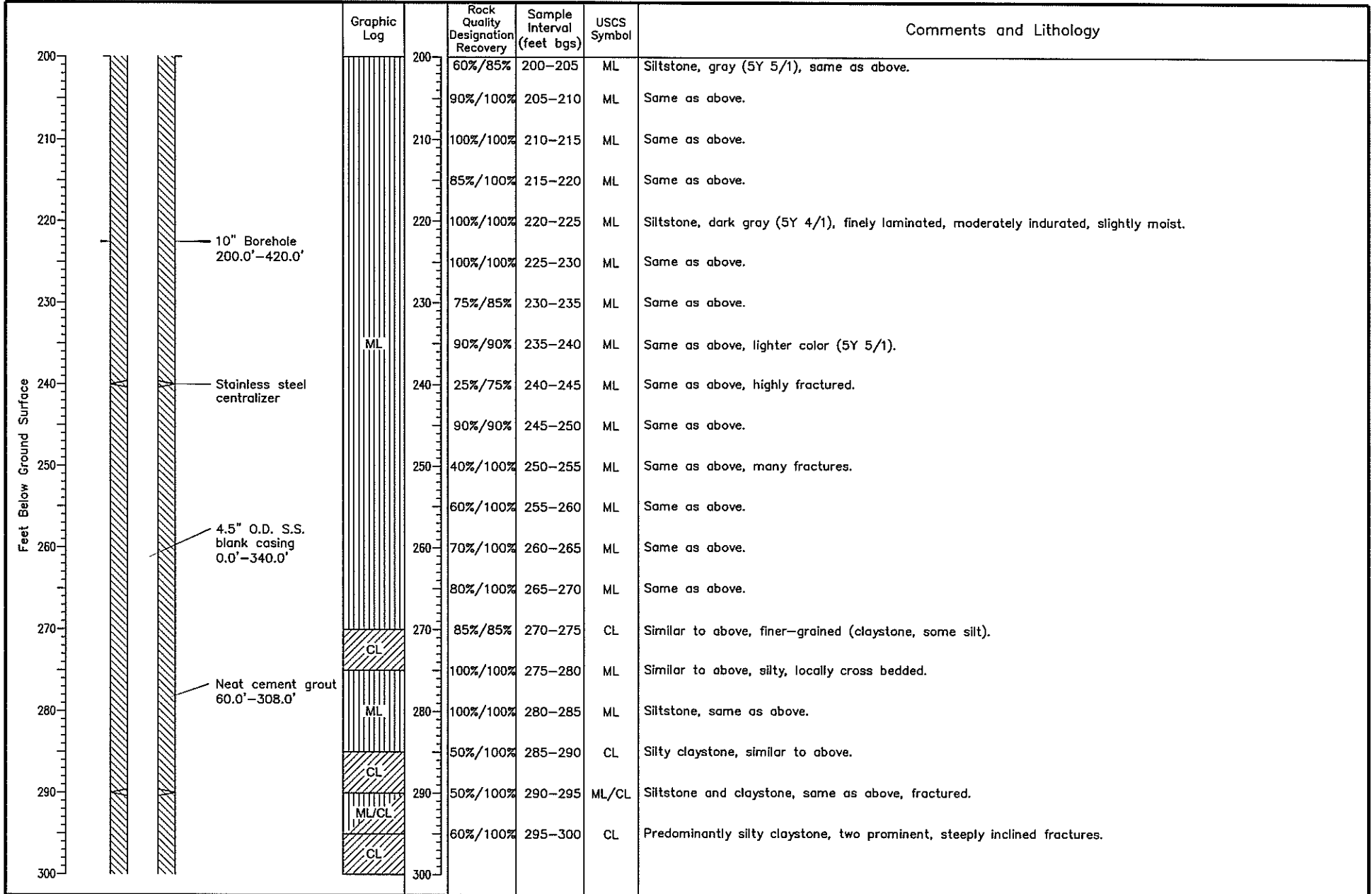
Geologist: J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 6-30-11

Drilling method: Core, air rotary  
 Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420')  
 Sampling device: HQ core, air rotary cuttings (400'-420')  
 Steel surface casing: 16" steel (0'-50')



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 6-05-2012 JN ES09.0154

PICKLES BUTTE  
 Well Log: PB-11



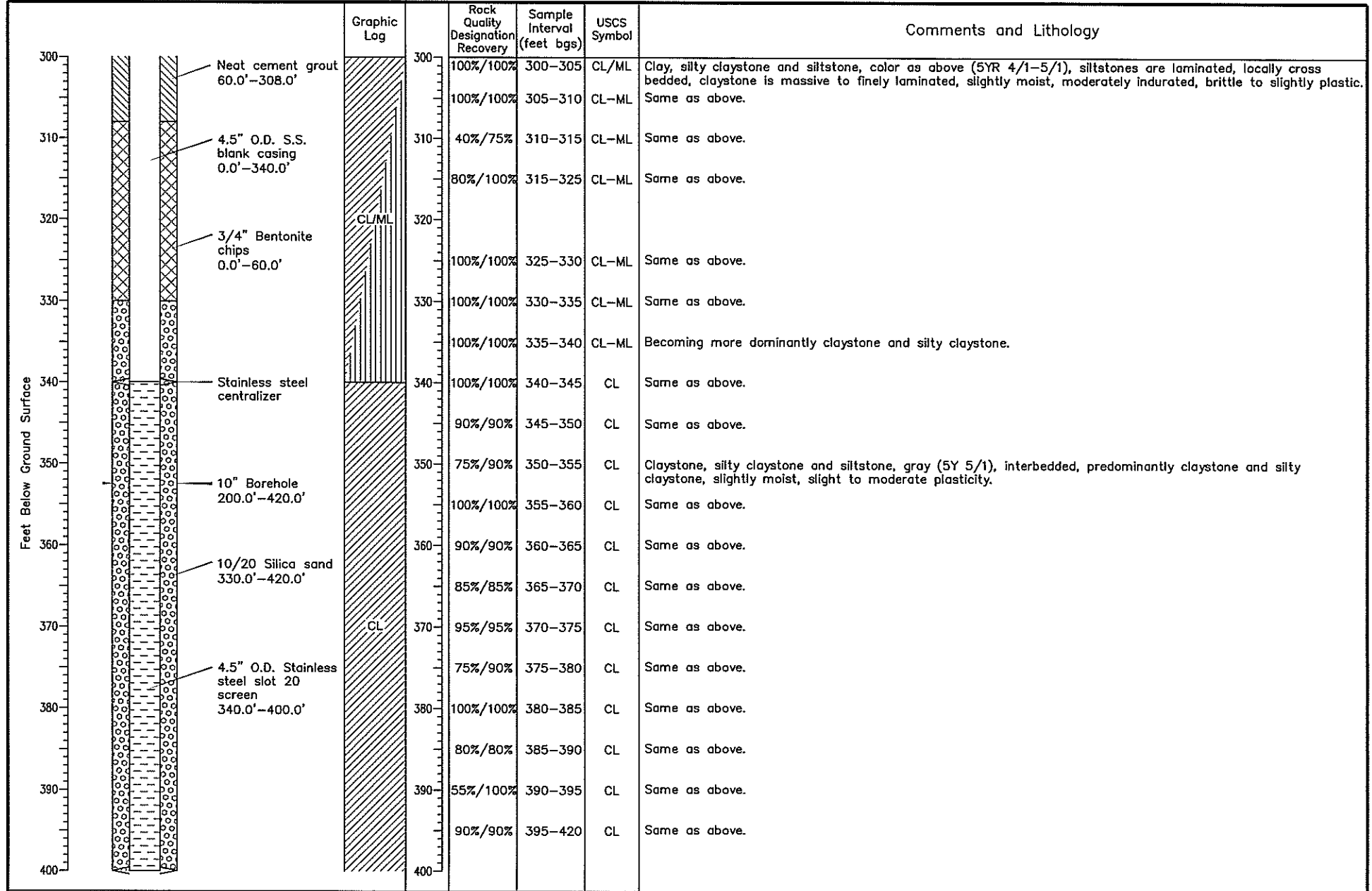
Geologist: J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 6-30-11

Drilling method: Core, air rotary  
 Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420')  
 Sampling device: HQ core, air rotary cuttings (400'-420')  
 Steel surface casing: 16" steel (0'-50')



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 6-05-2012 JN ES09.0154

PICKLES BUTTE  
 Well Log: PB-11



Geologist: J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 6-30-11

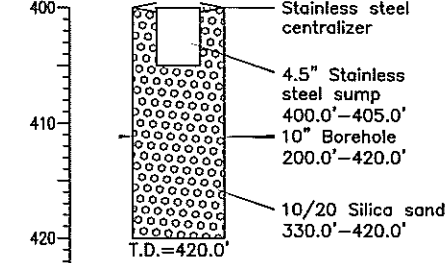

Drilling method: Core, air rotary  
 Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420')  
 Sampling device: HQ core, air rotary cuttings (400'-420')  
 Steel surface casing: 16" steel (0'-50')



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PICKLES BUTTE  
 Well Log: PB-11

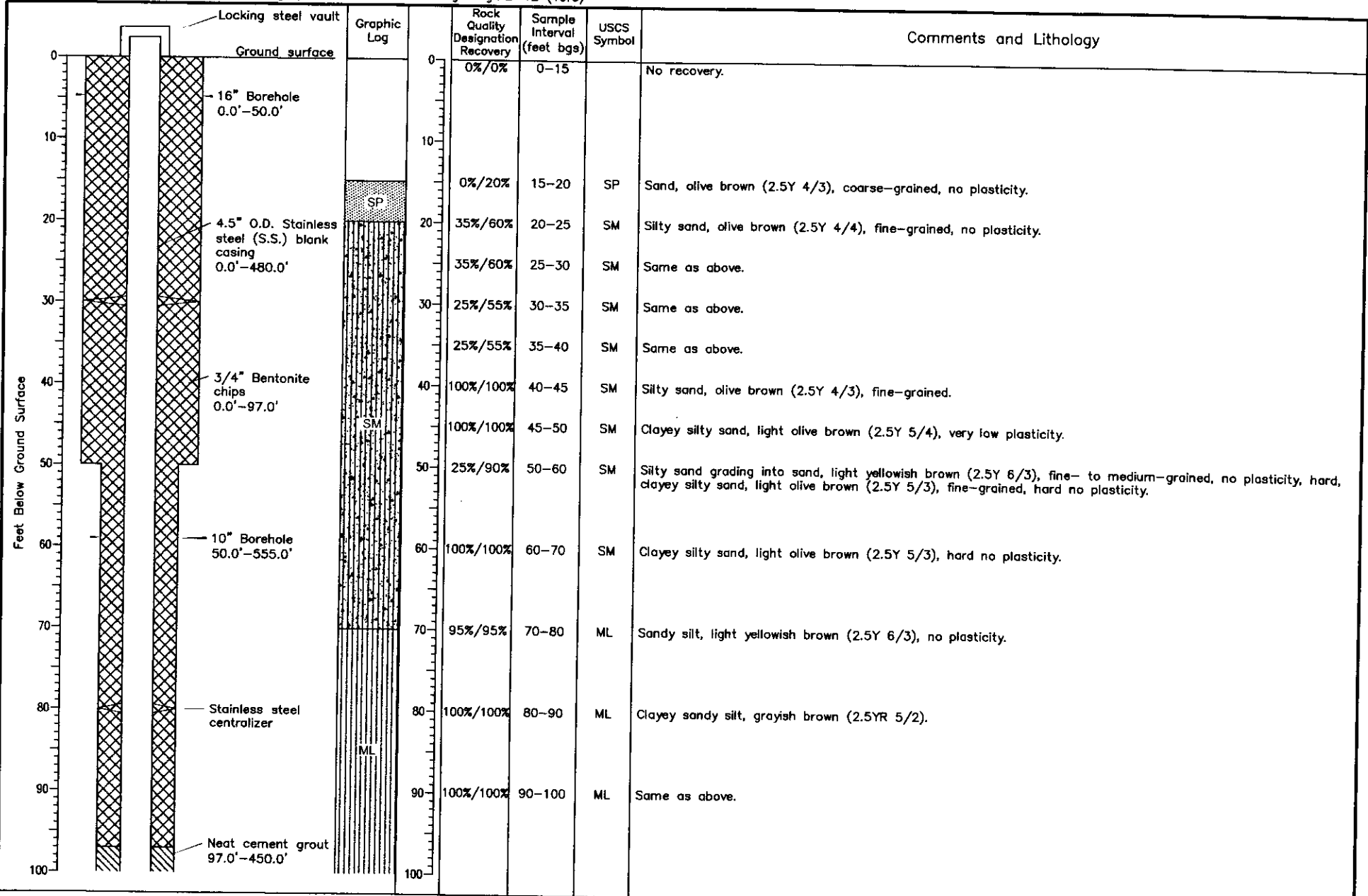


	Graphic Log	Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
 <p>Stainless steel centralizer 4.5" Stainless steel sump 400.0'-405.0' 10" Borehole 200.0'-420.0' 10/20 Silica sand 330.0'-420.0' T.D.=420.0'</p>				CL	Same as above, rotary cuttings.

Geologist: J. Raucci  
Driller: HAZ-Tech  
Date completed: 6-30-11

Drilling method: Core, air rotary  
Bit diameters: 19" (0'-50'), 12" (50'-200'), 9 7/8" (200'-420')  
Sampling device: HQ core, air rotary cuttings (400'-420')  
Steel surface casing: 16" steel (0'-50')





Geologist: M. Nauck  
 Driller: HAZ-Tech  
 Date completed: 7-15-11

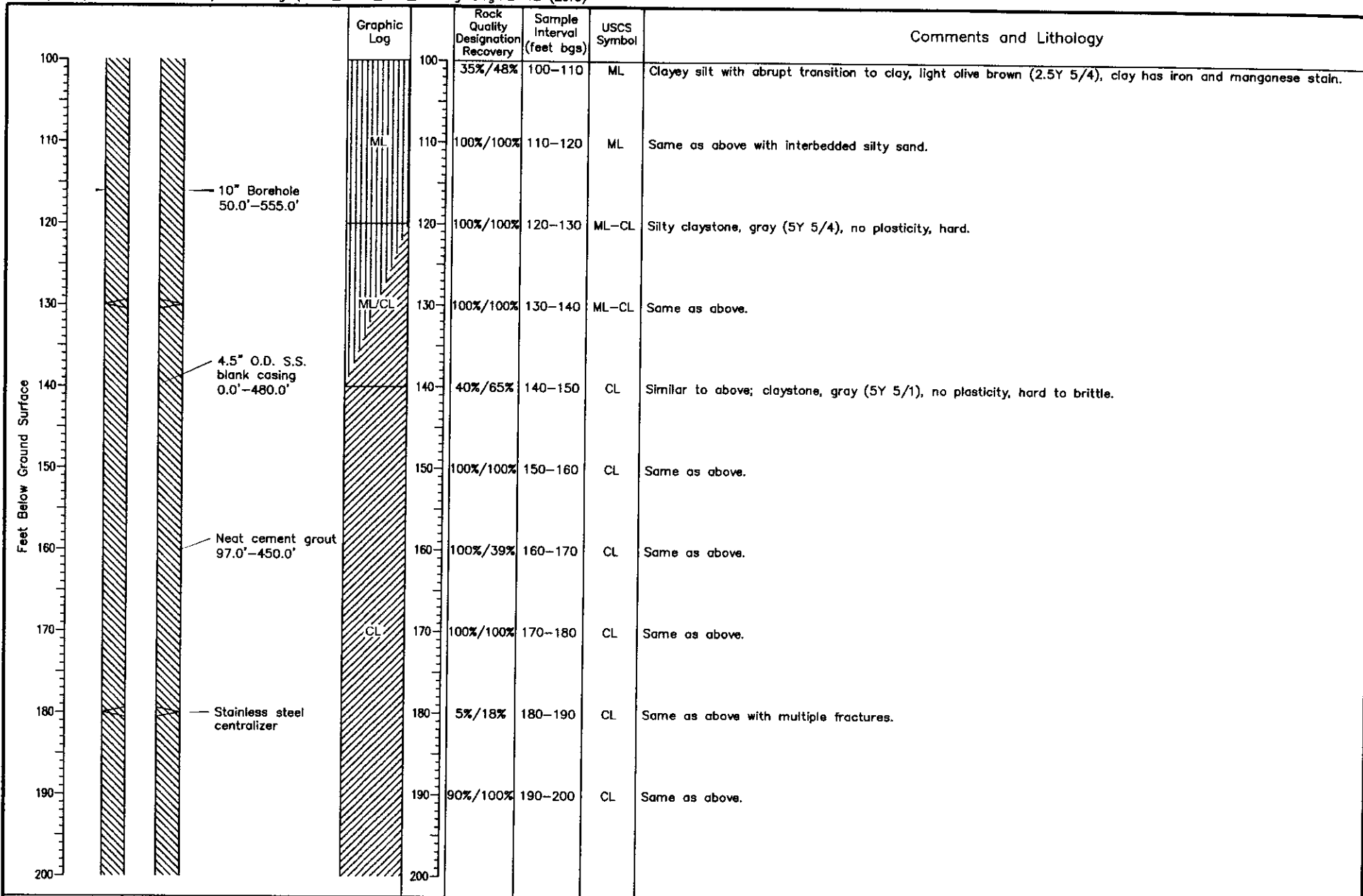
Drilling method: Core, air rotary  
 Bit diameters: 16" (0'-50'), 9 7/8" (50'-555')  
 Sampling device: HQ core (0'-350'), air rotary cuttings (350'-555')  
 Steel surface casing: None

Northing: 667697.966  
 Easting: 243653.665  
 Elevation: 2657.2 (TOC)

Note: TOC = top of casing

PICKLES BUTTE  
 Well Log: PB-12

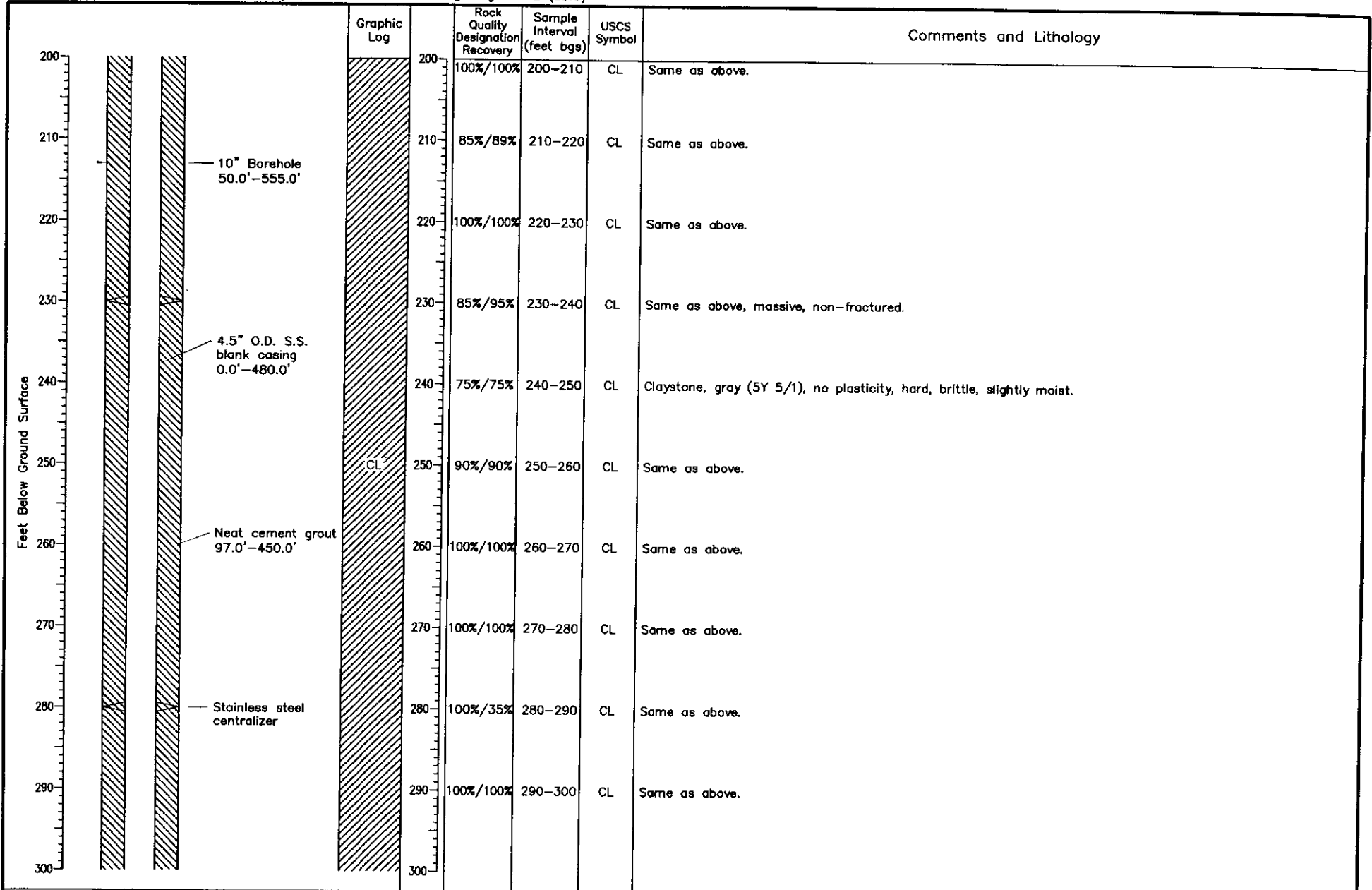




Geologist: M. Nauck  
 Driller: HAZ-Tech  
 Date completed: 7-15-11

Drilling method: Core, air rotary  
 Bit diameters: 16" (0'-50'), 9 7/8" (50'-555')  
 Sampling device: HQ core (0'-350'), air rotary cuttings (350'-555')  
 Steel surface casing: None





Geologist: M. Nauck

Driller: HAZ-Tech

Date completed: 7-15-11

Drilling method: Core, air rotary

Bit diameters: 16" (0'-50'), 9 7/8" (50'-555')

Sampling device: HQ core (0'-350'), air rotary cuttings (350'-555')

Steel surface casing: None

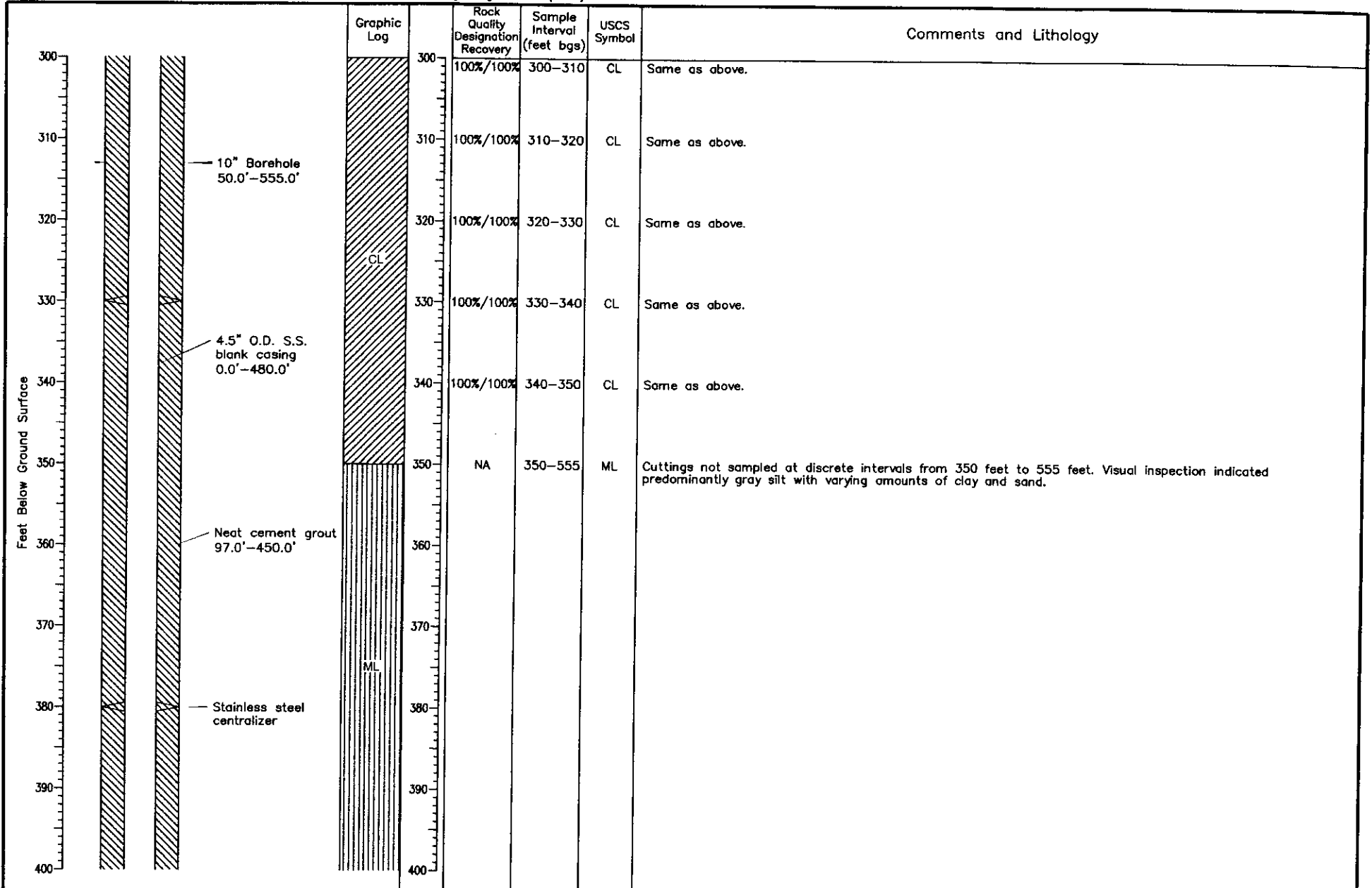


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6-05-2012

JN ES09.0154

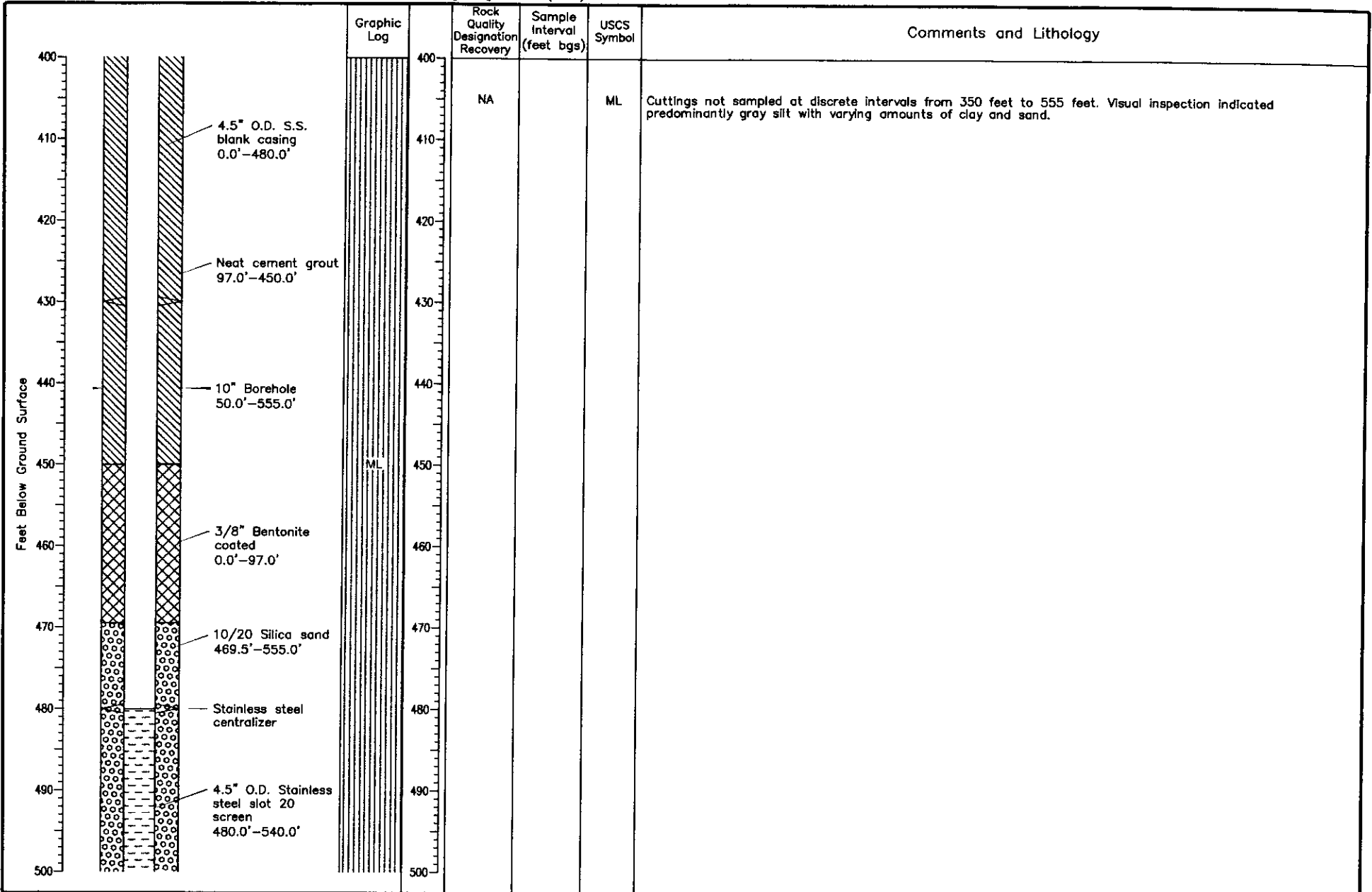
PICKLES BUTTE  
Well Log: PB-12



Geologist: M. Nauck  
 Driller: HAZ-Tech  
 Date completed: 7-15-11

Drilling method: Core, air rotary  
 Bit diameters: 16" (0'-50'), 9 7/8" (50'-555')  
 Sampling device: HQ core (0'-350'), air rotary cuttings (350'-555')  
 Steel surface casing: None

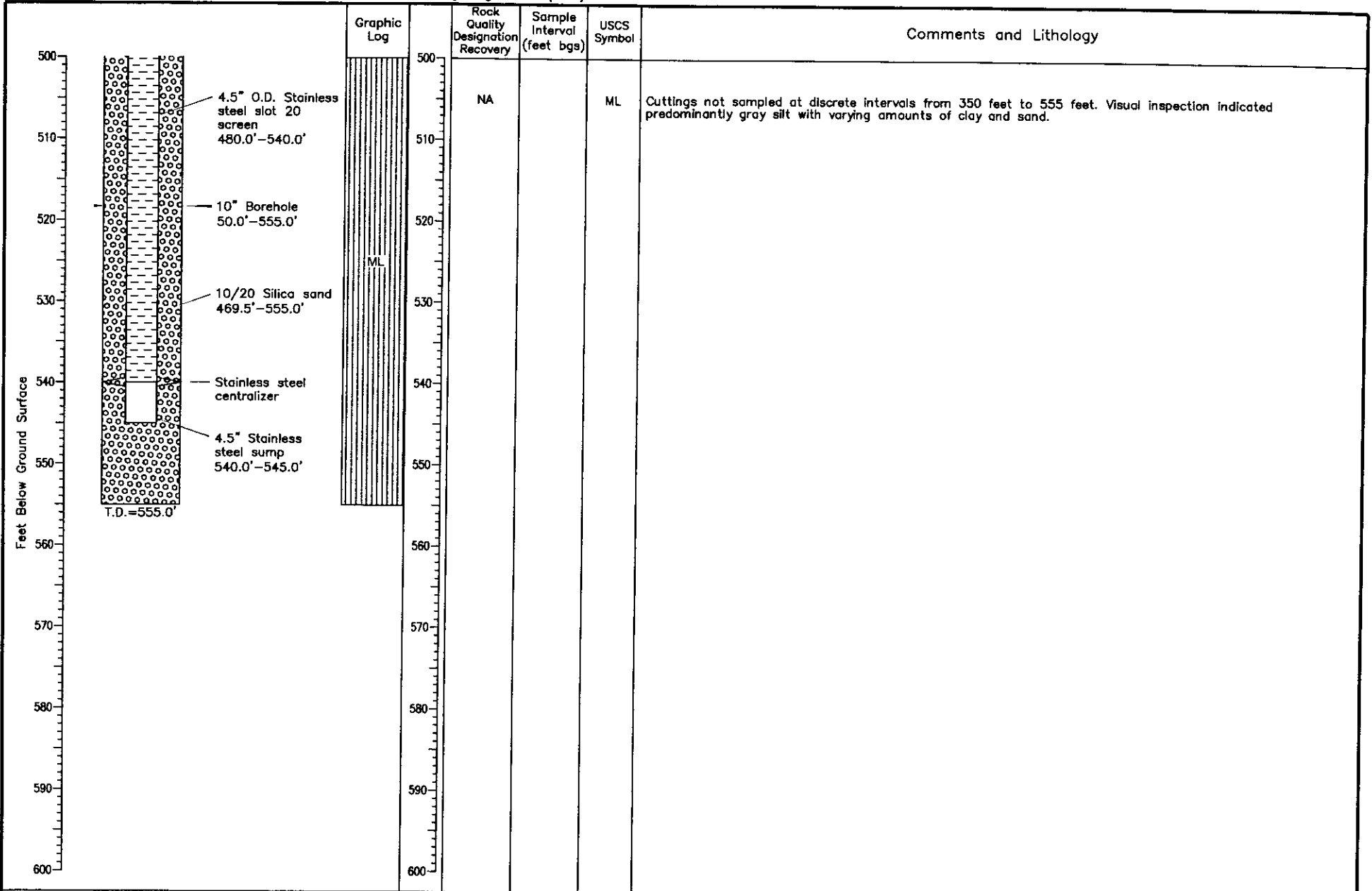




Geologist: M. Nauck  
 Driller: HAZ-Tech  
 Date completed: 7-15-11

Drilling method: Core, air rotary  
 Bit diameters: 16" (0'-50'), 9 7/8" (50'-555')  
 Sampling device: HQ core (0'-350'), air rotary cuttings (350'-555')  
 Steel surface casing: None





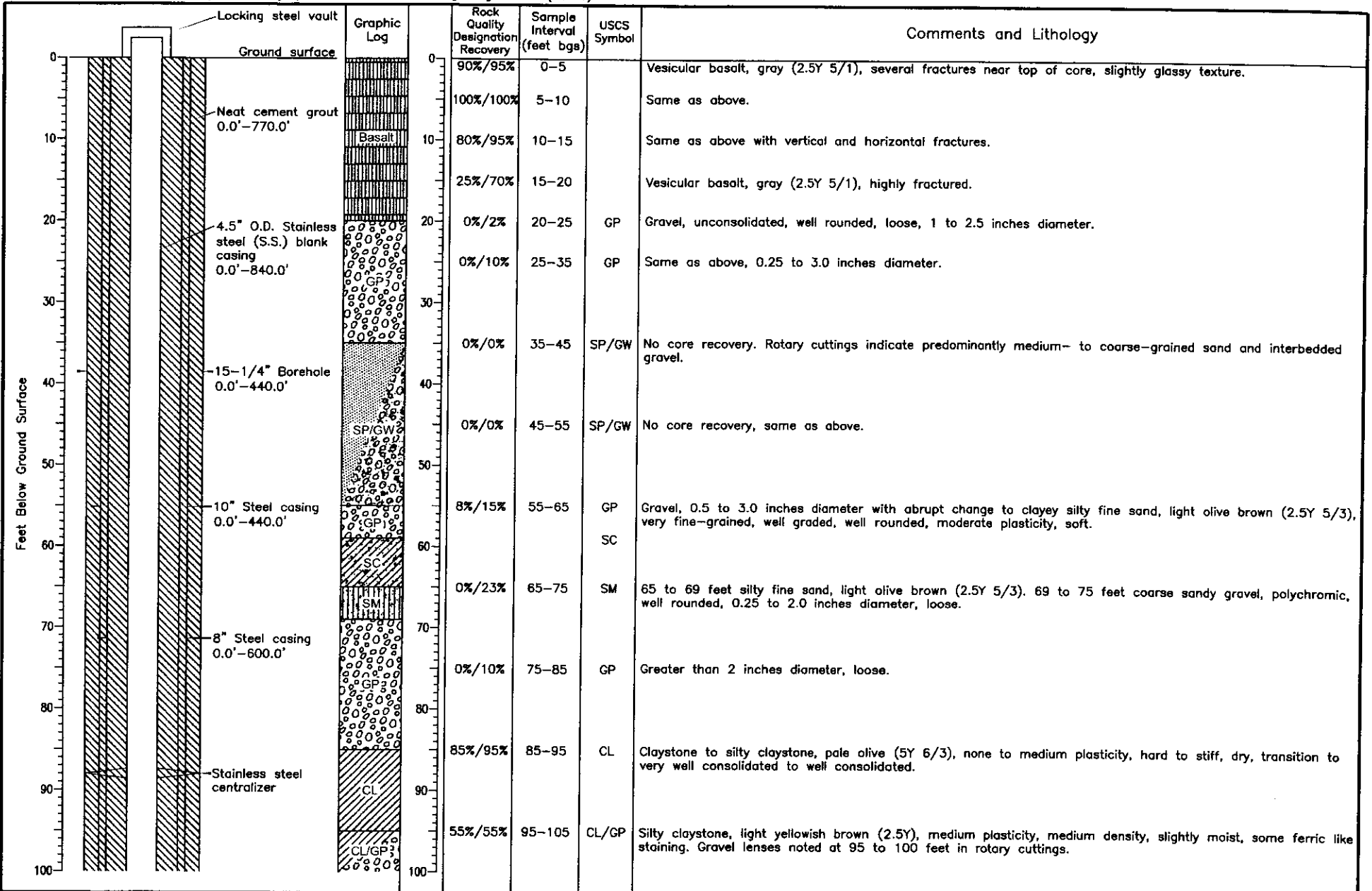
Geologist: M. Nauck  
 Driller: HAZ-Tech  
 Date completed: 7-15-11

Drilling method: Core, air rotary  
 Bit diameters: 16" (0'-50'), 9 7/8" (50'-555')  
 Sampling device: HQ core (0'-350'), air rotary cuttings (350'-555')  
 Steel surface casing: None



Daniel B. Stephens & Associates, Inc.  
 6-05-2012 JN ES09.0154

PICKLES BUTTE  
 Well Log: PB-12



Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

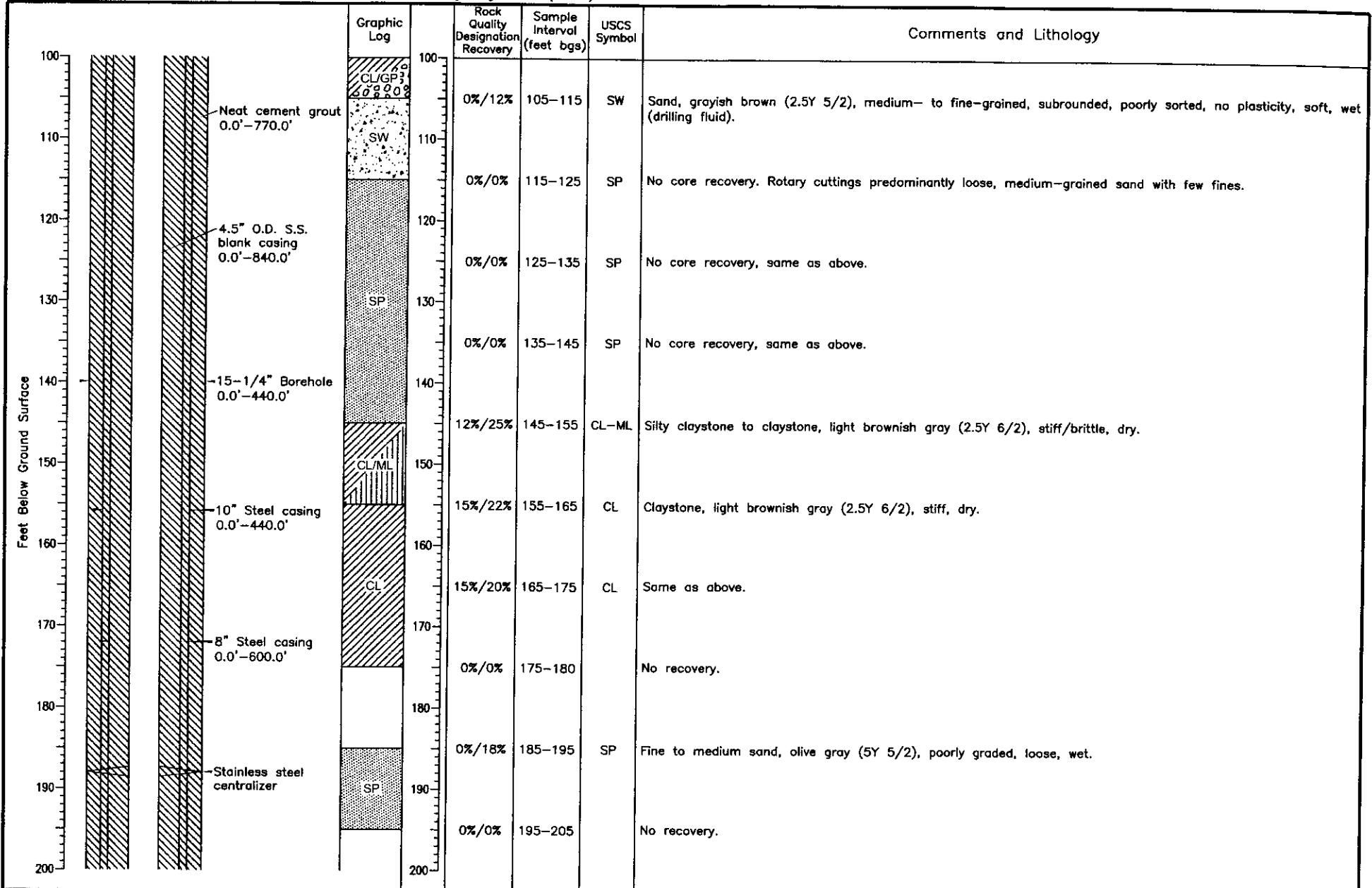
Northing: 666231.696  
 Easting: 243986.781  
 Elevation: 3073.9 (TOC)

Notes: HAZ-Tech core drilling 0'-666'; Adamson Pump and Drill air rotary drilling 666'-920'  
 TOC = top of casing

**PICKLES BUTTE**  
**Well Log: PB-13**





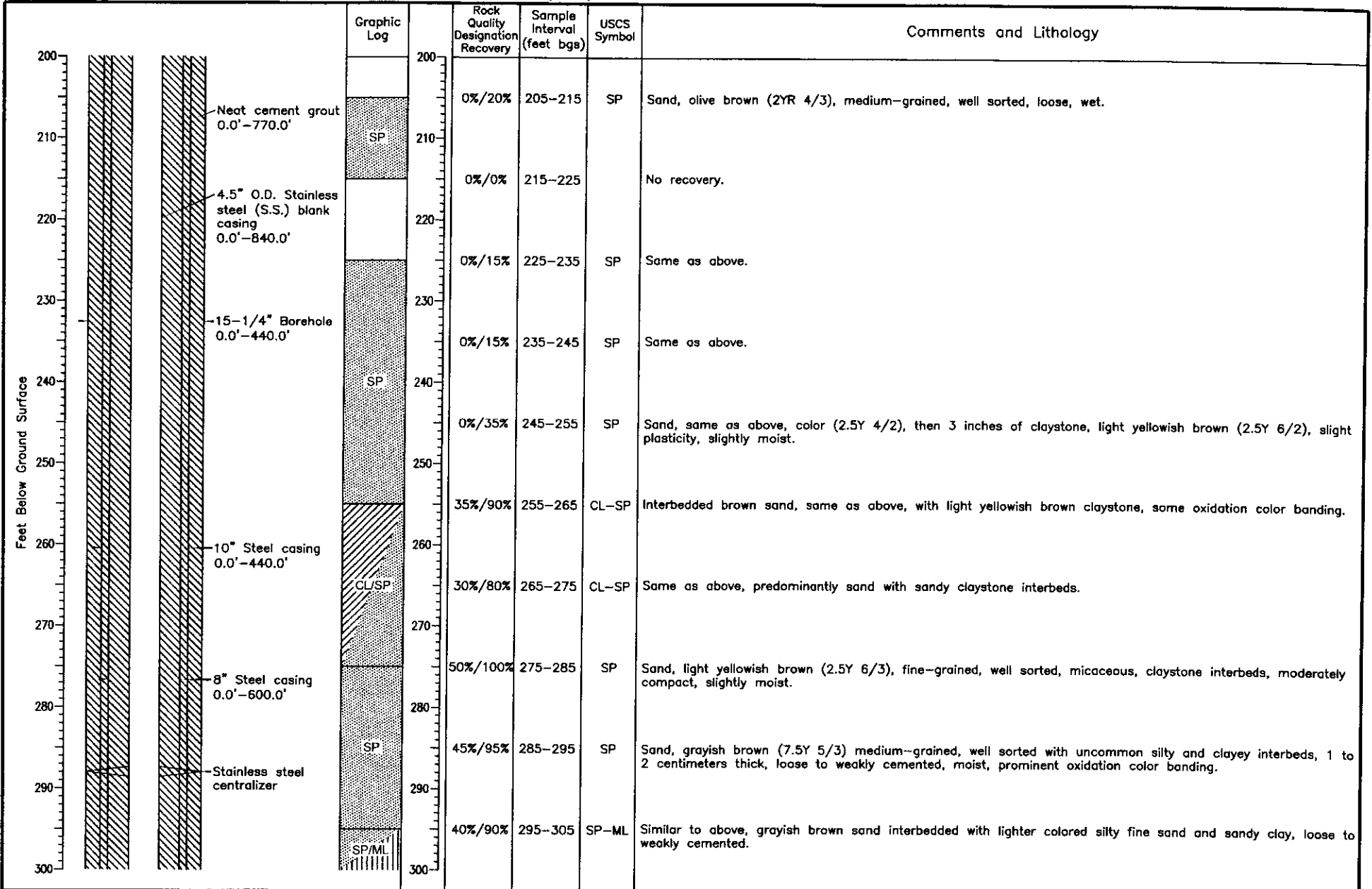


Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'



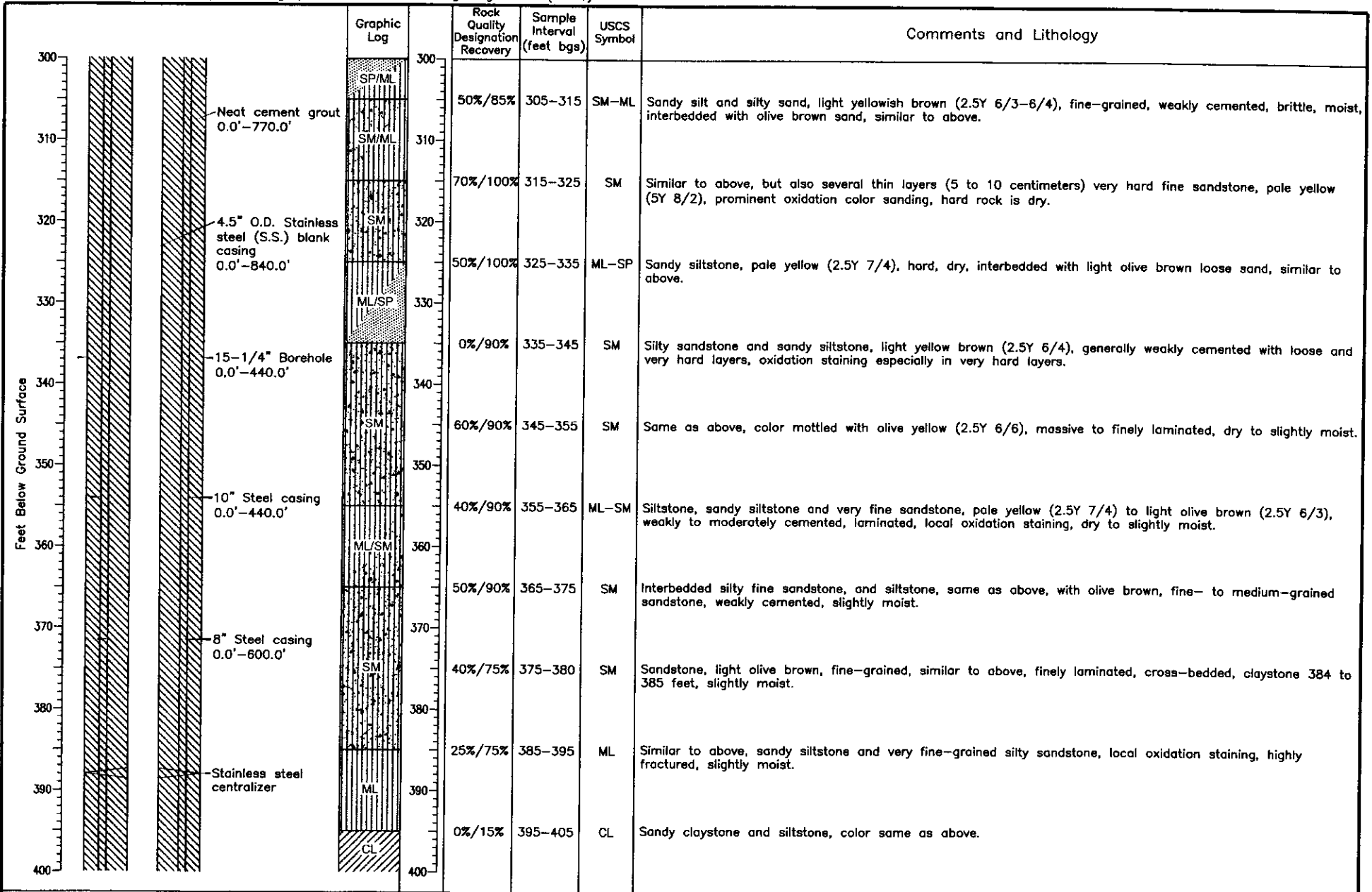


Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'



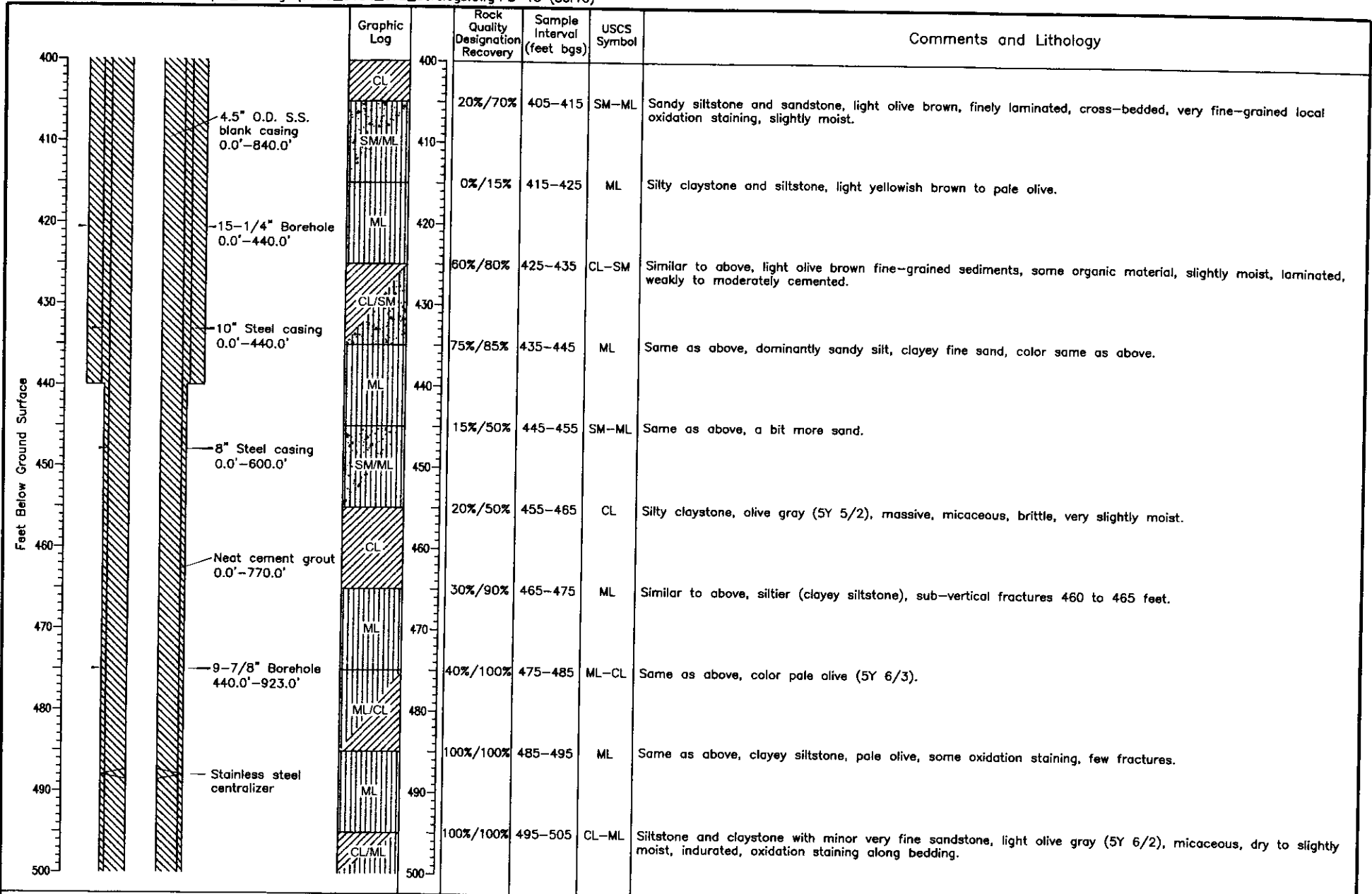


Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'



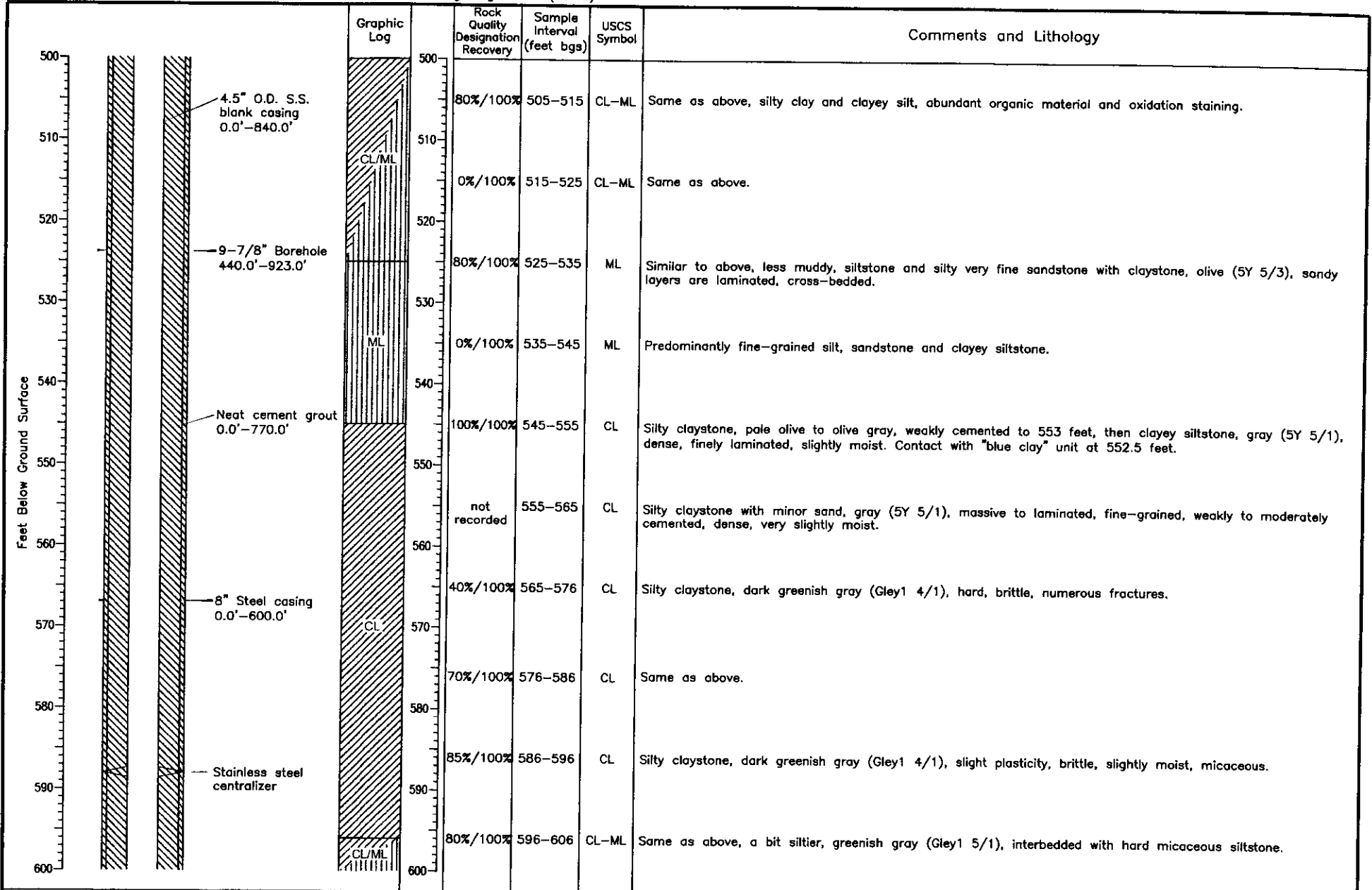


Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'



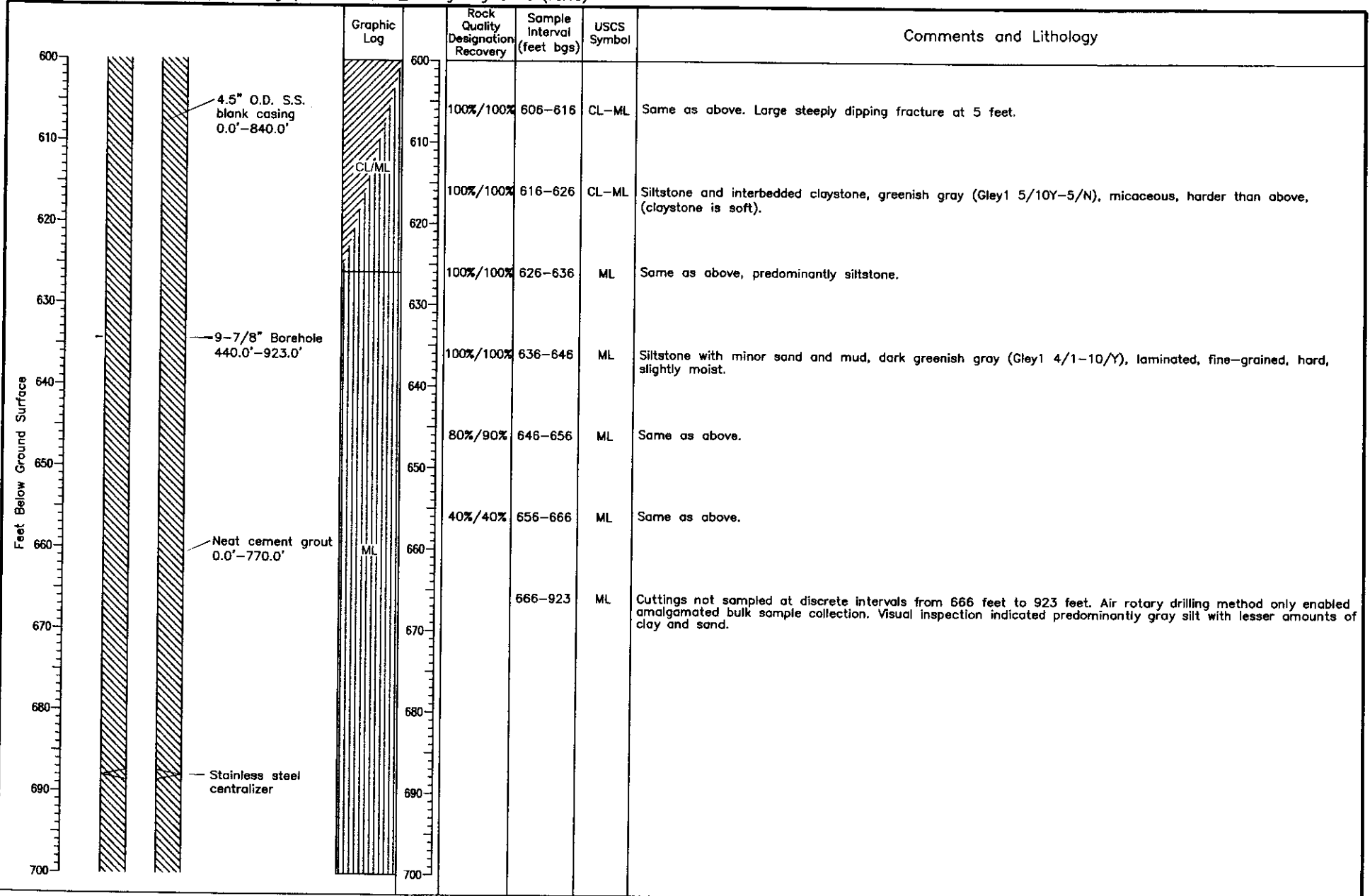


Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'





Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

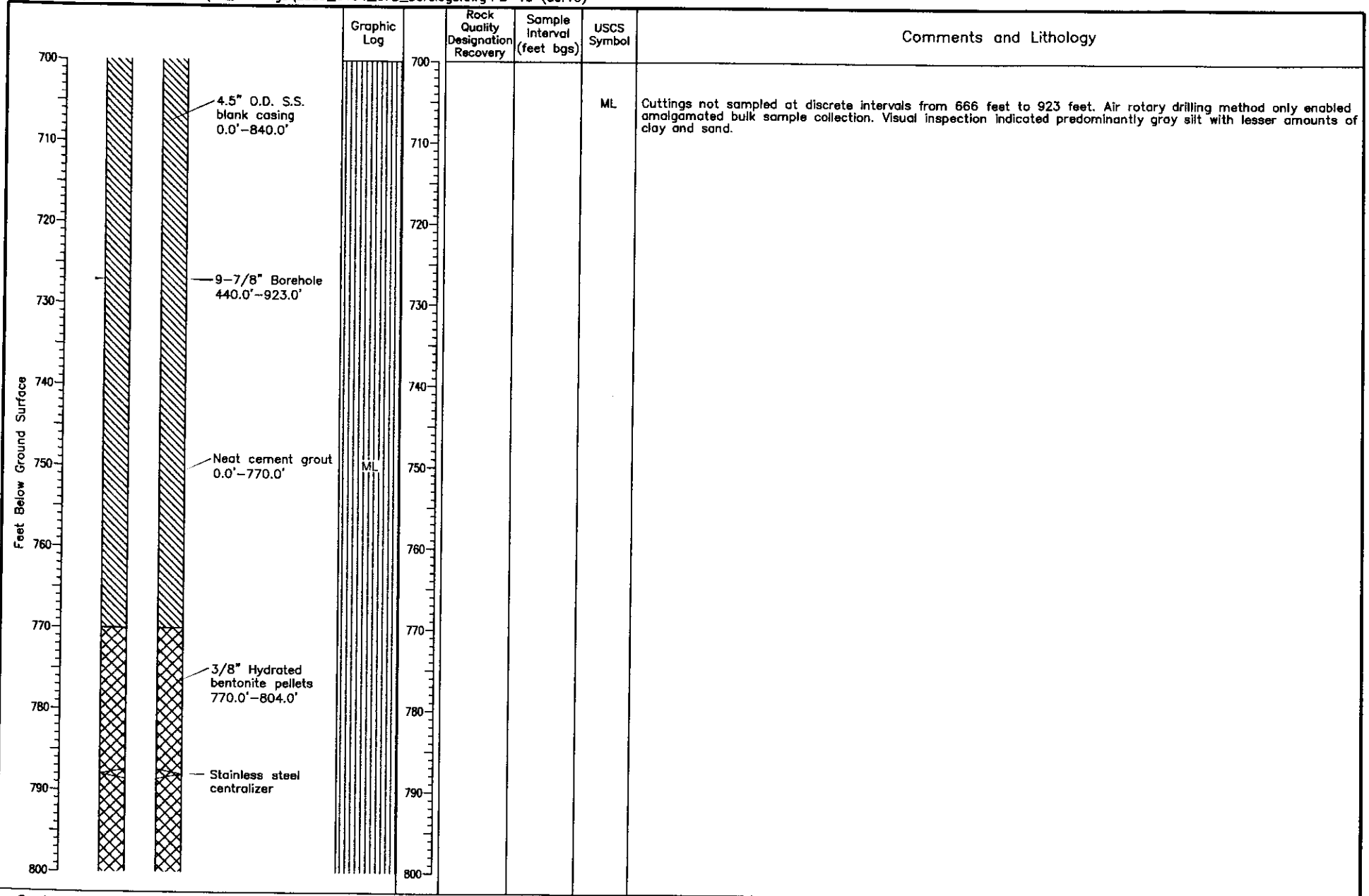
Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'



Daniel B. Stephens & Associates, Inc.  
 6-05-2012  
 JN ES09.0154

**PICKLES BUTTE  
 Well Log: PB-13**



Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

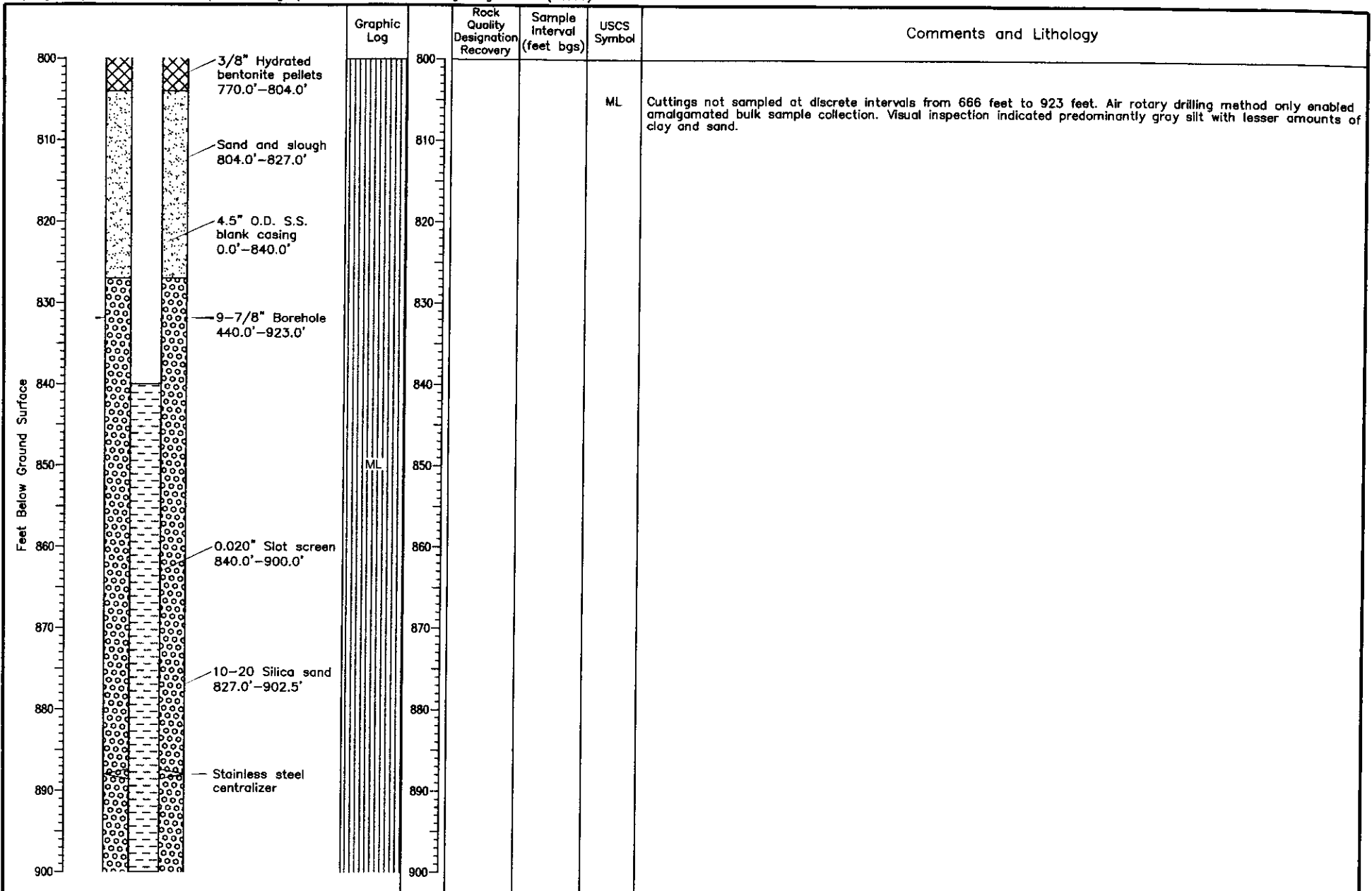
Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'



Daniel B. Stephens & Associates, Inc.  
 8-05-2012

JN ES09.0154

PICKLES BUTTE  
 Well Log: PB-13



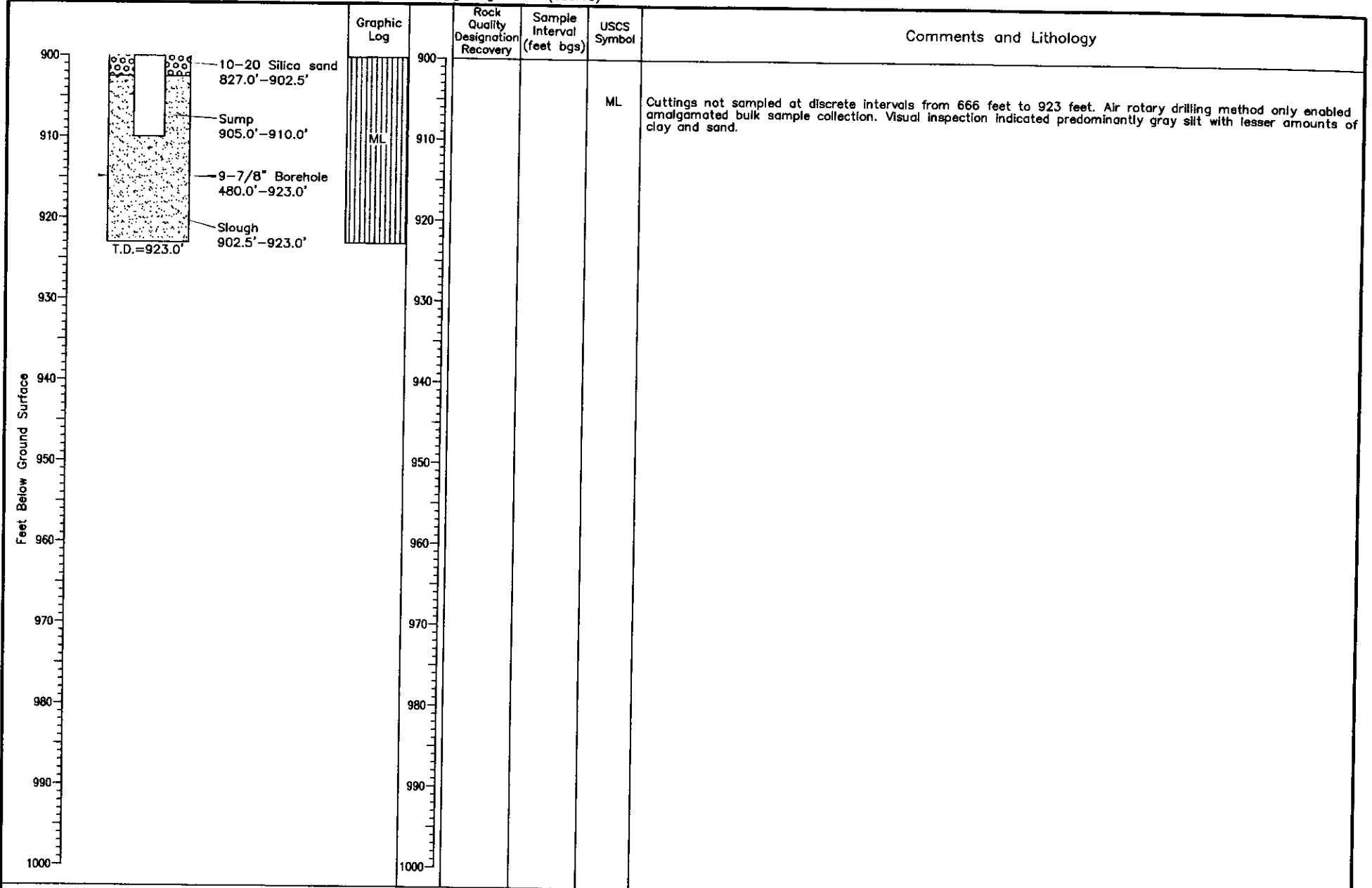
Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'





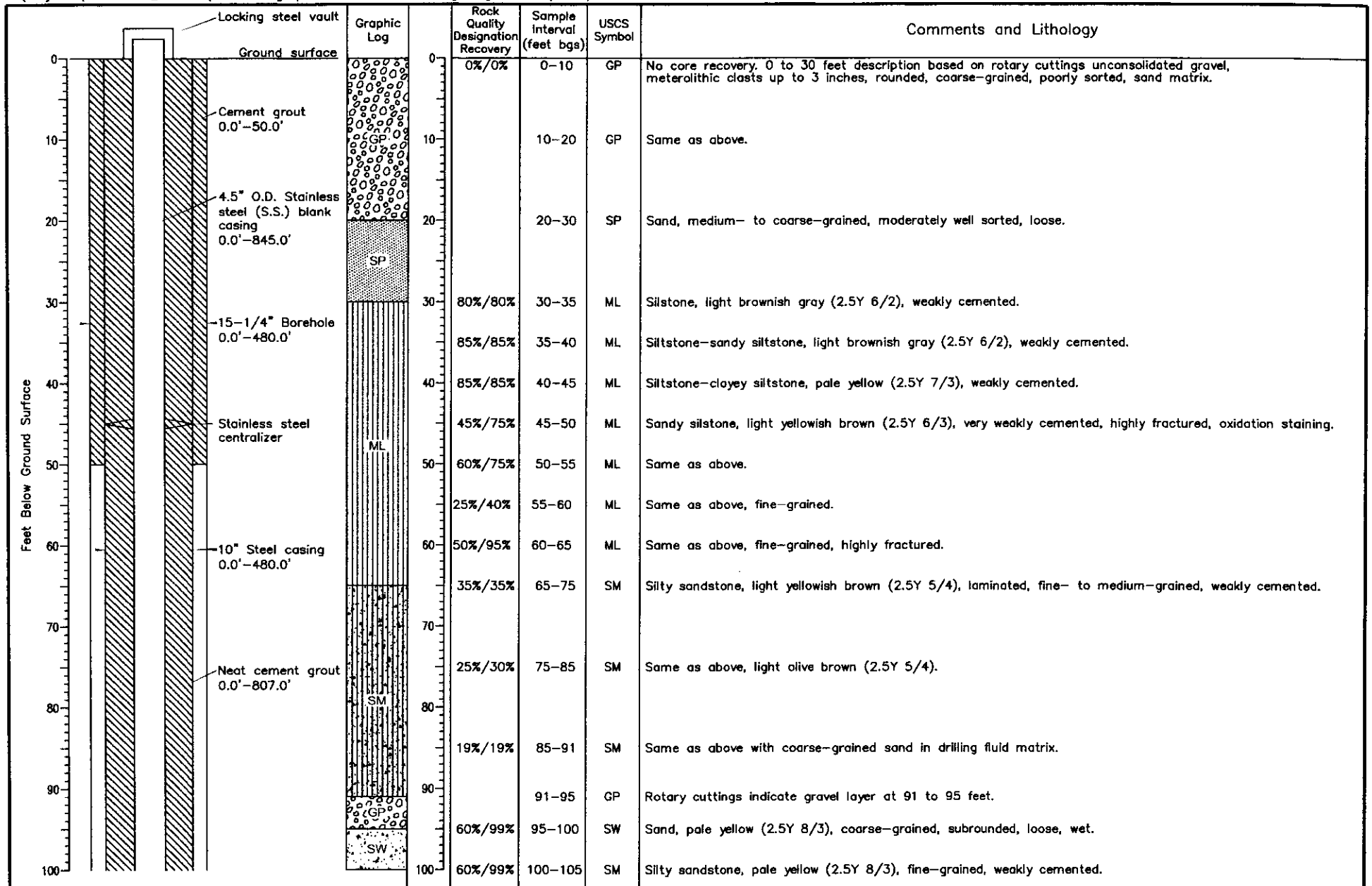


Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech  
 Date completed: 12-15-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15 1/4" (0'-440'), 9 7/8" (440'-923')  
 Sampling device: HQ core, air rotary cuttings  
 Steel surface casing: 8" (0'-600'), 10" (0'-440')

Note: HAZ-Tech core drilling 0'-666';  
 Adamson Pump and Drill air rotary drilling  
 666'-920'





Geologist: J. Fisher/M. Nauck/J. Raucchi  
 Driller: HAZ-Tech; Adamson Pump and Drill  
 Date completed: 10-11-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15-1/4" and 9-7/8"  
 Sampling device: HQ core, NQ core, rotary cuttings  
 Steel surface casing: 10"  
 Note: TOC = top of casing

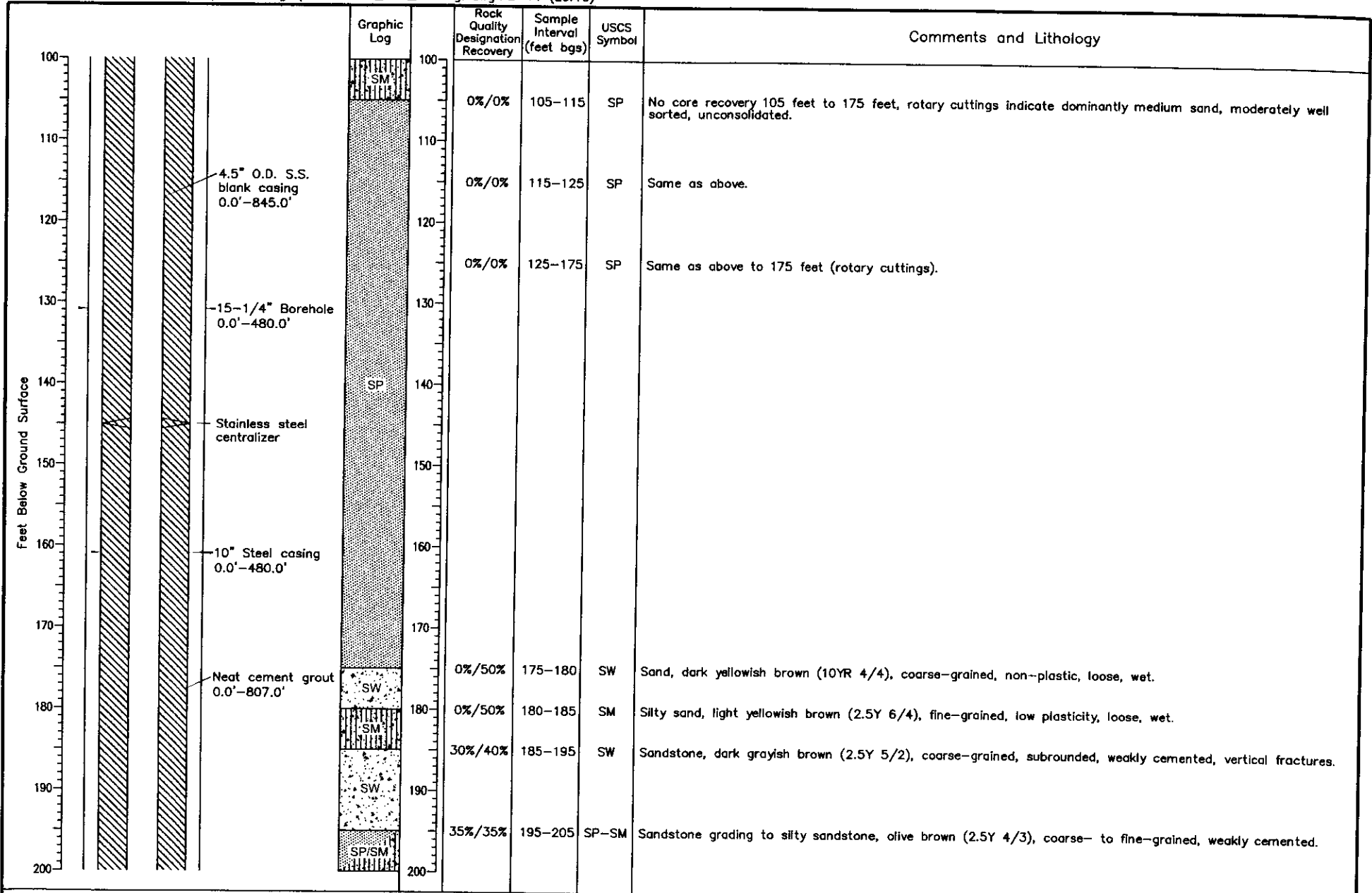
Northing: 665549.182  
 Easting: 244947.947  
 Elevation: 3080.9 (TOC)

Note: HAZ-Tech core drilling 0'-385', 520'-750' (NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923'

**PICKLES BUTTE  
 Well Log: PB-14**



Daniel B. Stephens & Associates, Inc.  
 6-05-2012



Geologist: J. Fisher/M. Nauck/J. Raucci  
 Driller: HAZ-Tech; Adamson Pump and Drill  
 Date completed: 10-11-11

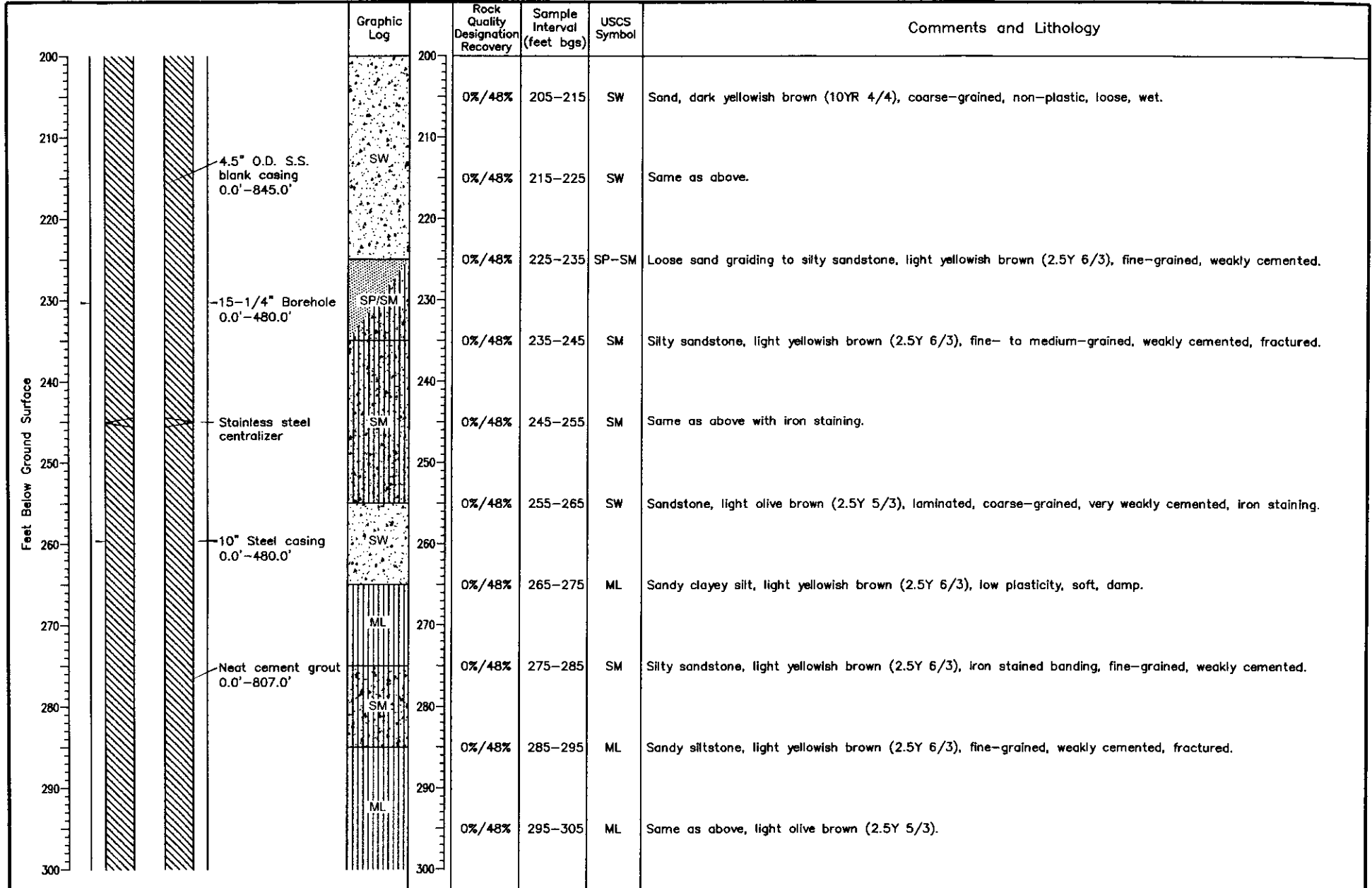
Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15-1/4" and 9-7/8"  
 Sampling device: HQ core, NQ core, rotary cuttings  
 Steel surface casing: 10"

Note: HAZ-Tech core drilling 0'-385', 520'-750' (NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923'



Daniel B. Stephens & Associates, Inc.  
 6-05-2012 JN ES09.0154

PICKLES BUTTE  
 Well Log: PB-14

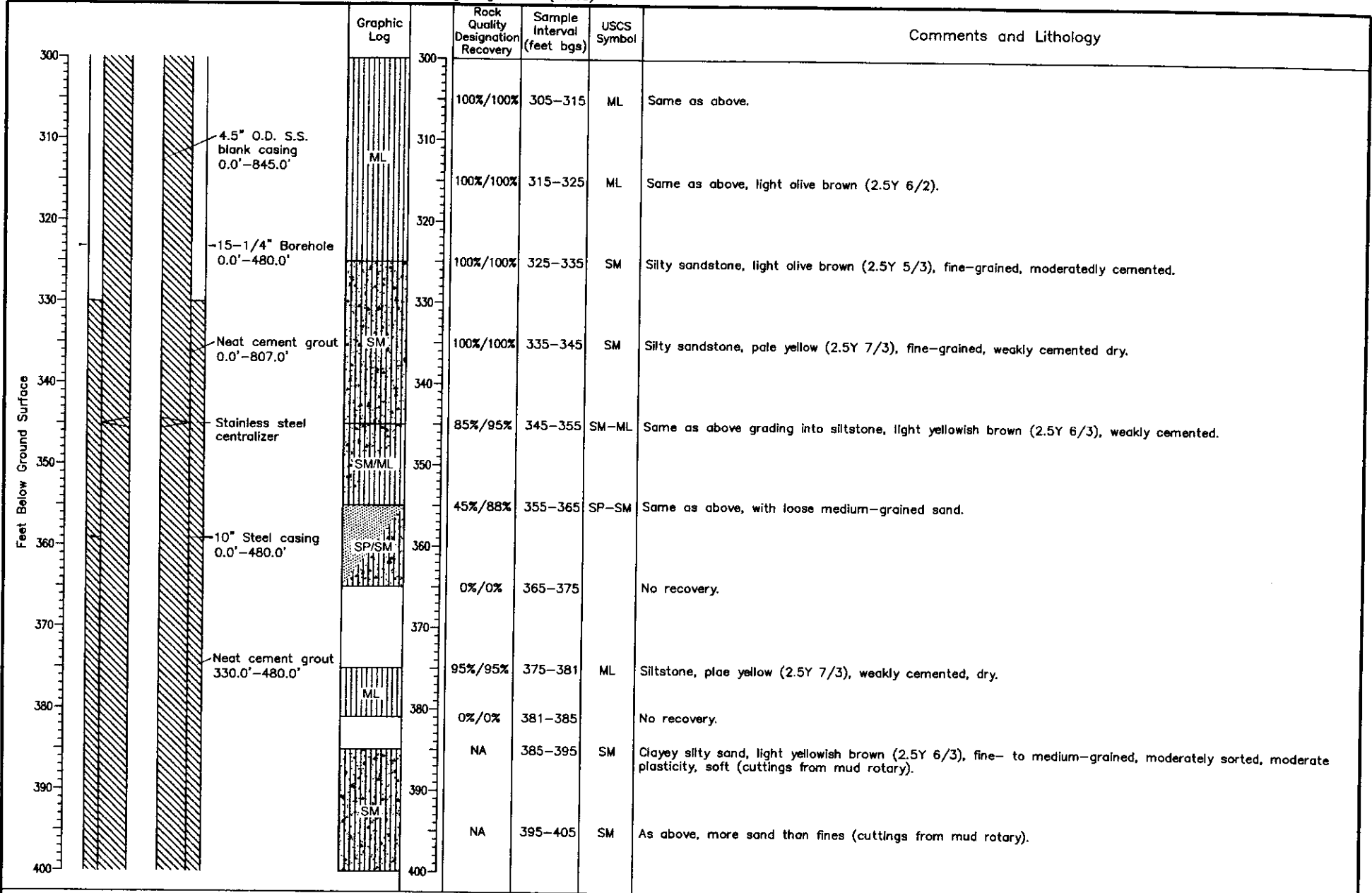


Geologist: J. Fisher/M. Nauck/J. Raucci  
 Driller: HAZ-Tech; Adamson Pump and Drill  
 Date completed: 10-11-11

Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15-1/4" and 9-7/8"  
 Sampling device: HQ core, NQ core, rotary cuttings  
 Steel surface casing: 10"

Note: HAZ-Tech core drilling 0'-385', 520'-750' (NQ core 600'-750'); Adamson Pump and Drill mud rotary drilling 385'-520', air rotary drilling 750'-923'





Geologist: J. Fisher/M. Nauck/J. Raucci  
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 6-05-2012 JN ES09.0154

PICKLES BUTTE  
 Well Log: PB-14

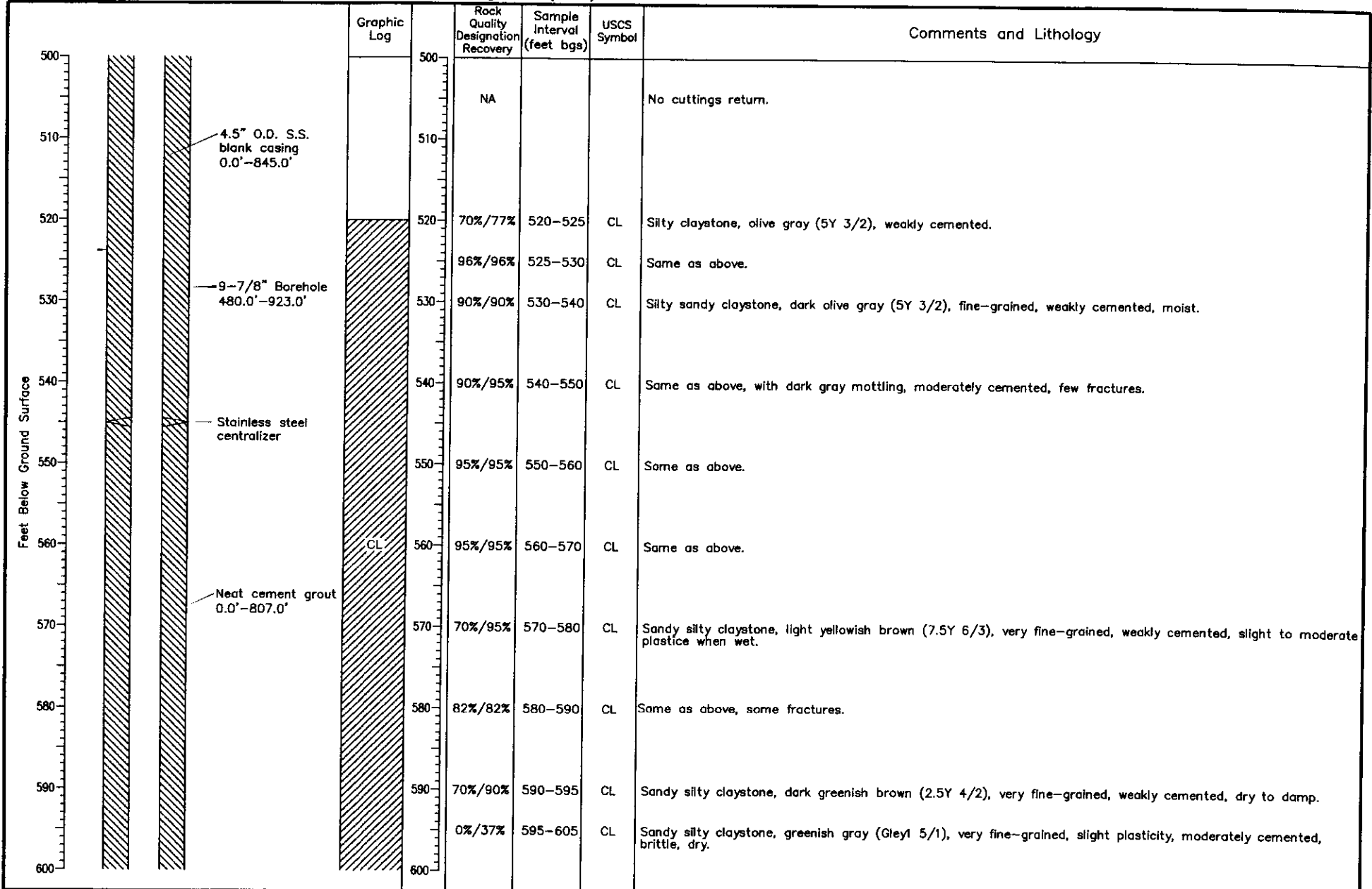
Graphic Log		Rock Quality Designation Recovery	Sample Interval (feet bgs)	USCS Symbol	Comments and Lithology
	4.5" O.D. S.S. blank casing 0.0'-845.0'	NA	405-415	ML	Same as above, clayey silt with sand, more fines than sand (cuttings from mud rotary).
	15-1/4" Borehole 0.0'-480.0'	NA	415-425	ML	Same as above (cuttings from mud rotary).
	Neat cement grout 330.0'-480.0'	NA	425-435	ML	Same as above (cuttings from mud rotary).
	Stainless steel centralizer	NA	435-445	ML	Same as above, few cutting returns (cuttings from mud rotary).
	10" Steel casing 0.0'-480.0'	NA	445-455	ML	Same as above (cuttings from mud rotary).
	Neat cement grout 0.0'-807.0'	NA	455-465	ML	Same as above (cuttings from mud rotary).
	9-7/8" Borehole 480.0'-923.0'	NA	465-475	ML	Same as above (cuttings from mud rotary).
		NA	475-485	ML	Same as above (cuttings from mud rotary).
		NA	485-520		No cuttings return.

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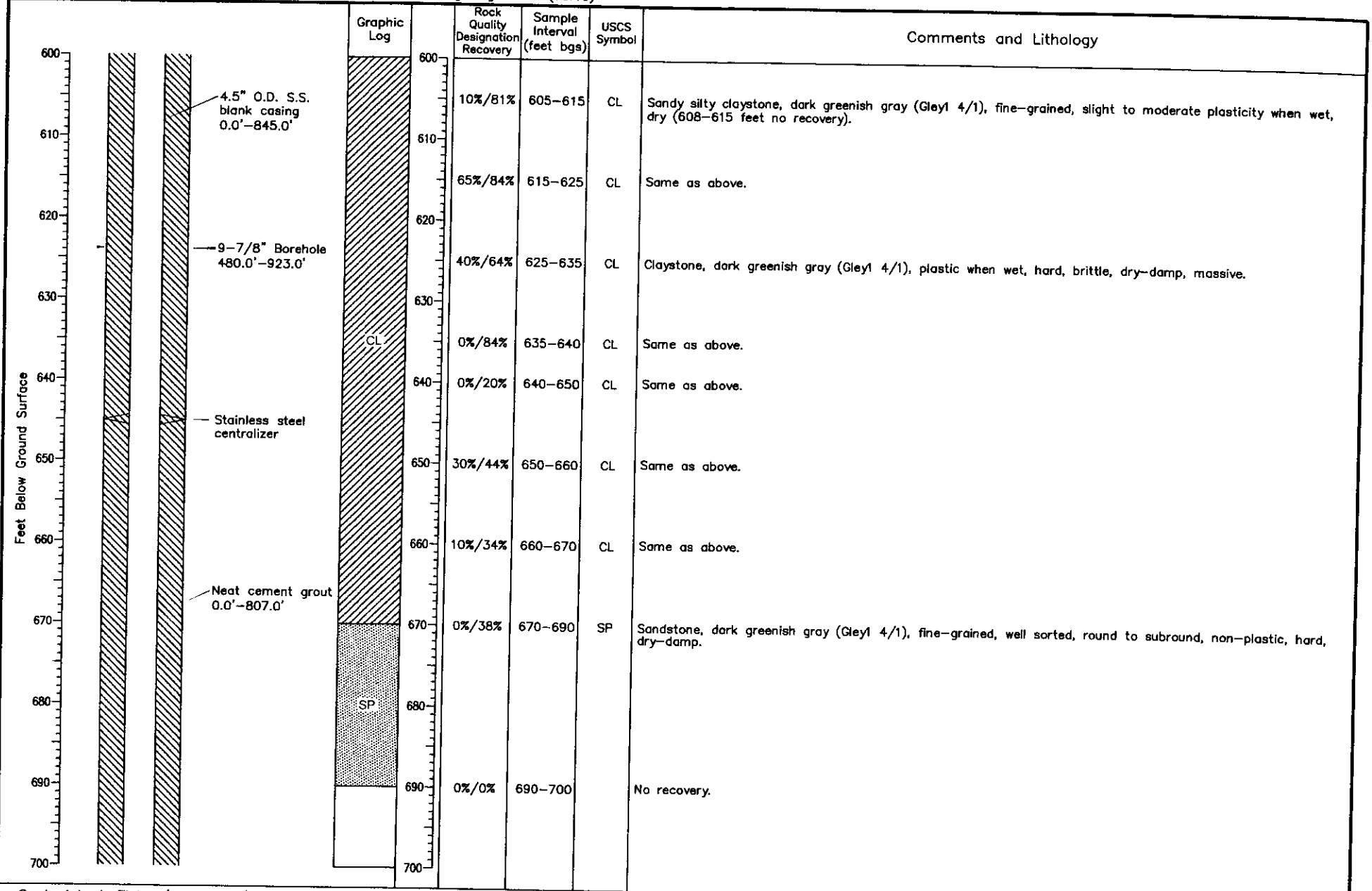
Drilling method: Core, mud rotary, air rotary  
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**PICKLES BUTTE  
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 Steel surface casing: 10"

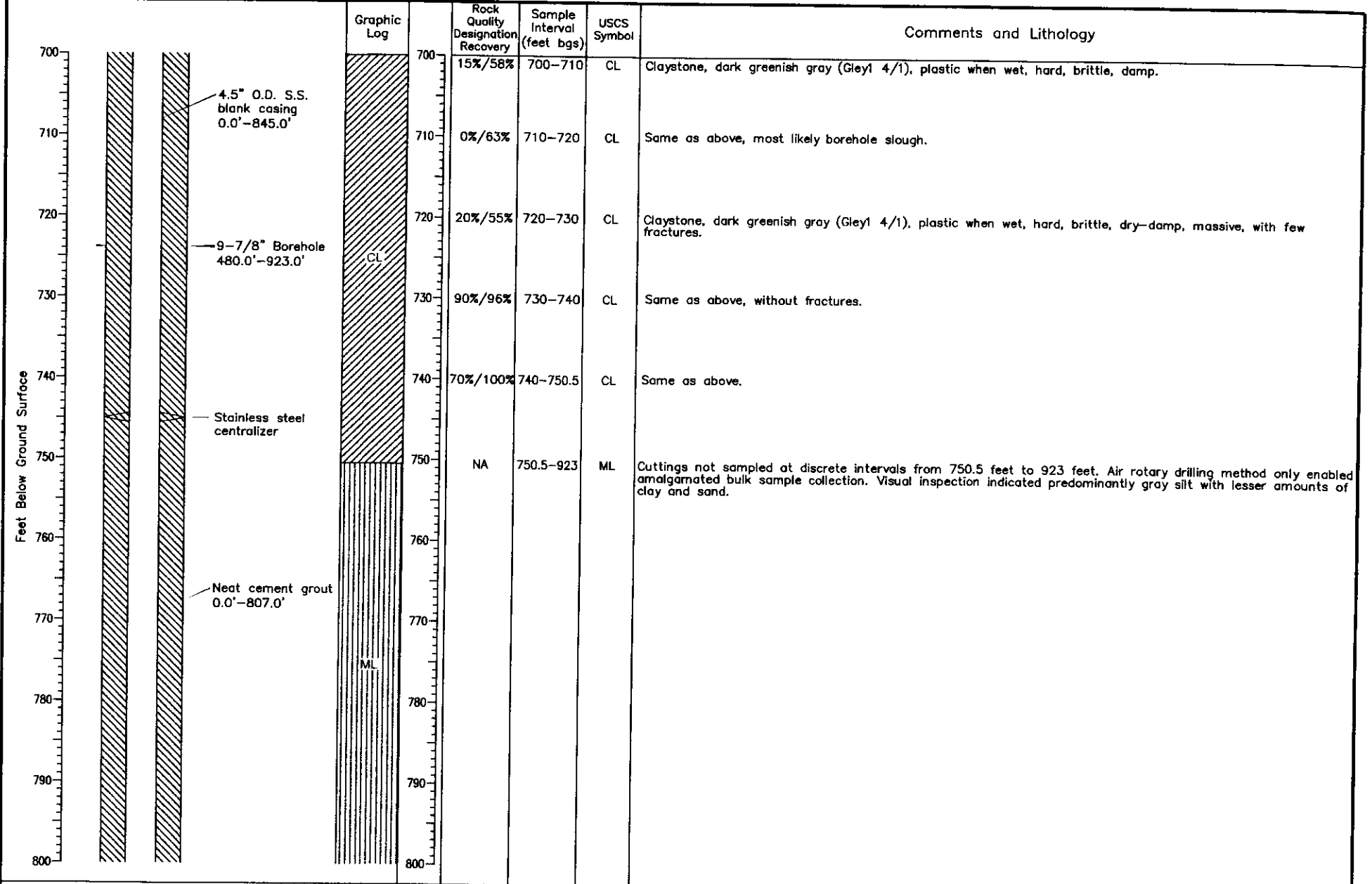
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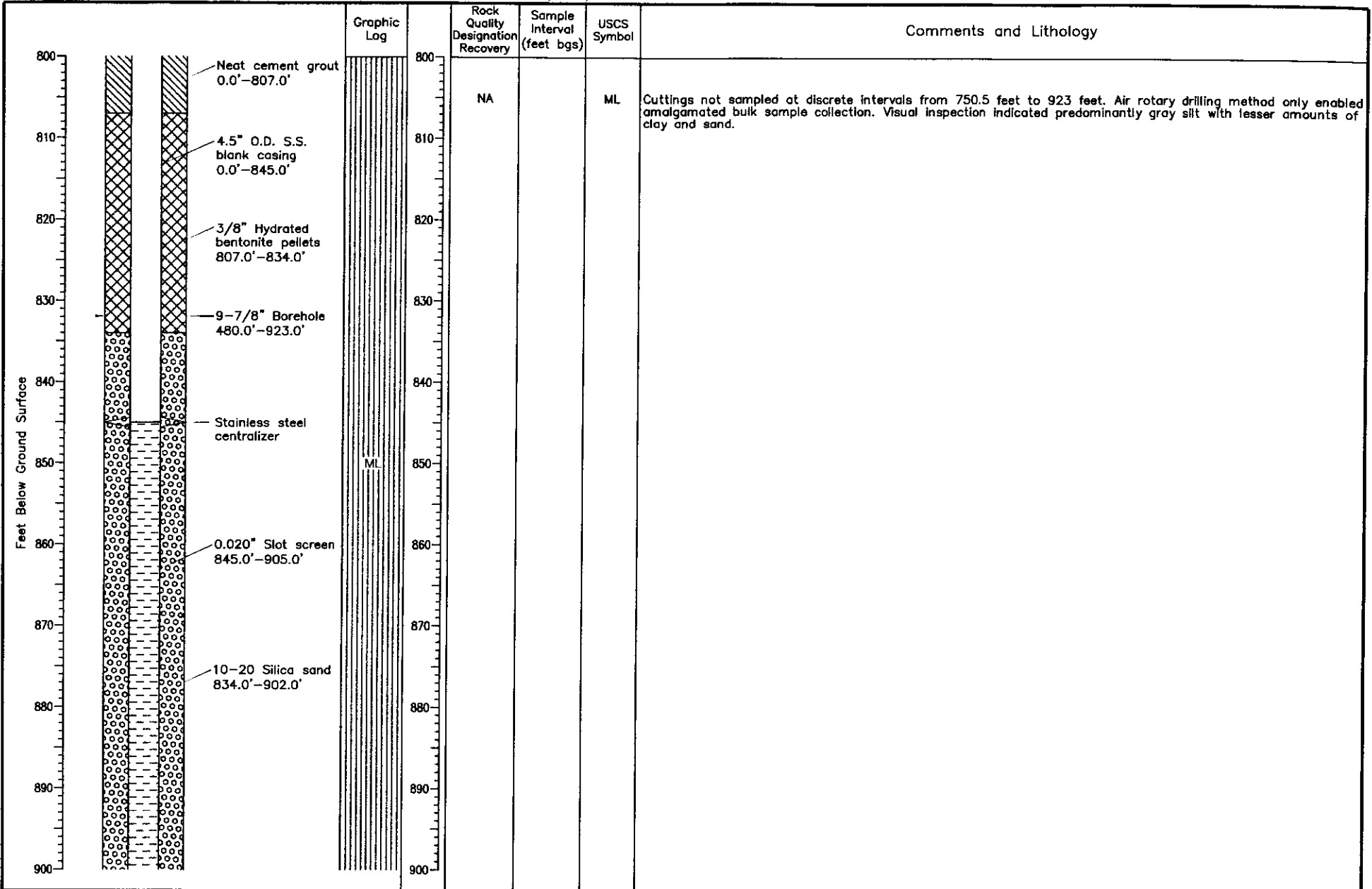
Drilling method: Core, mud rotary, air rotary  
 Bit diameters: 15-1/4" and 9-7/8"  
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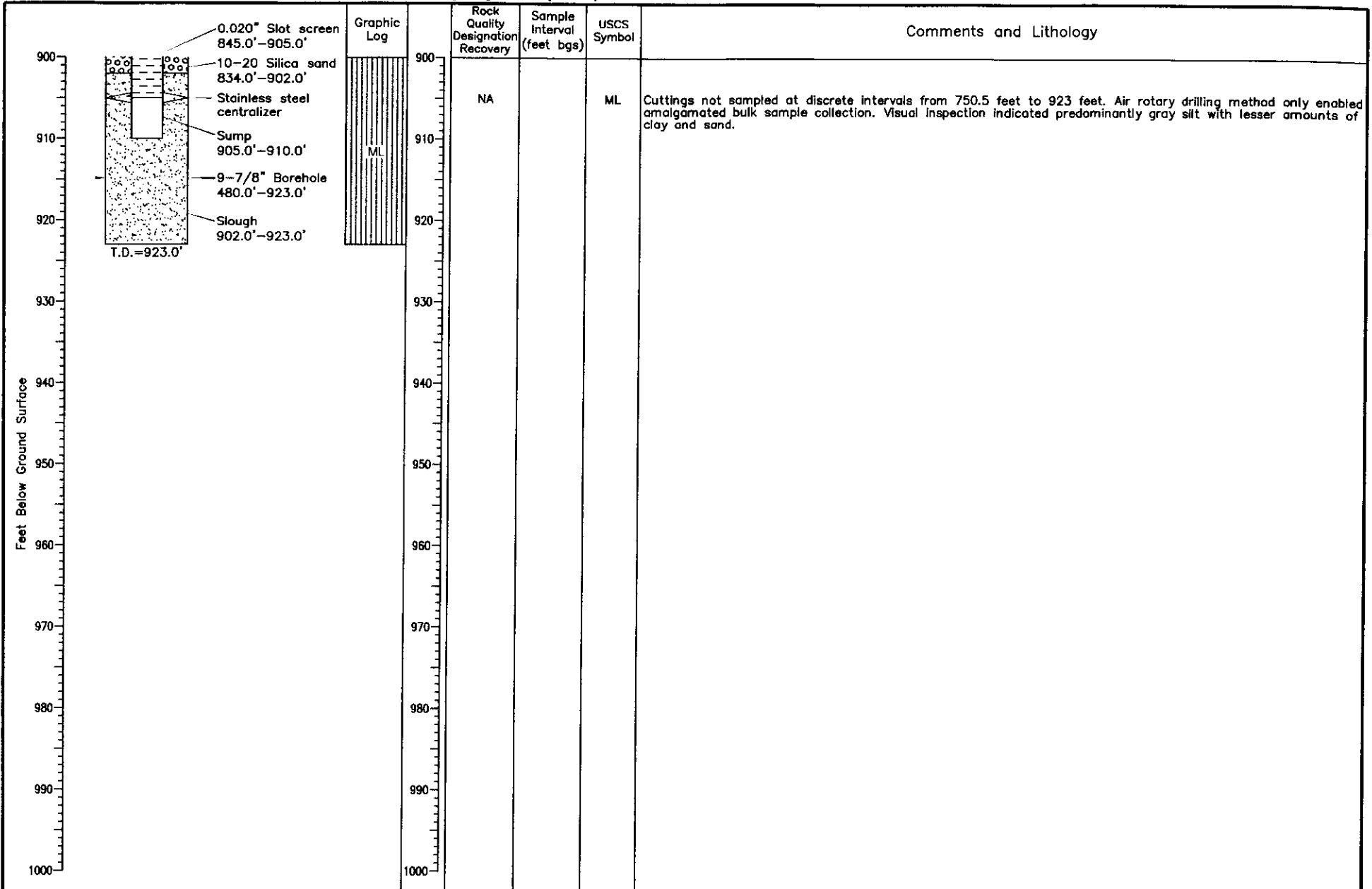
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 Well Log: PB-14

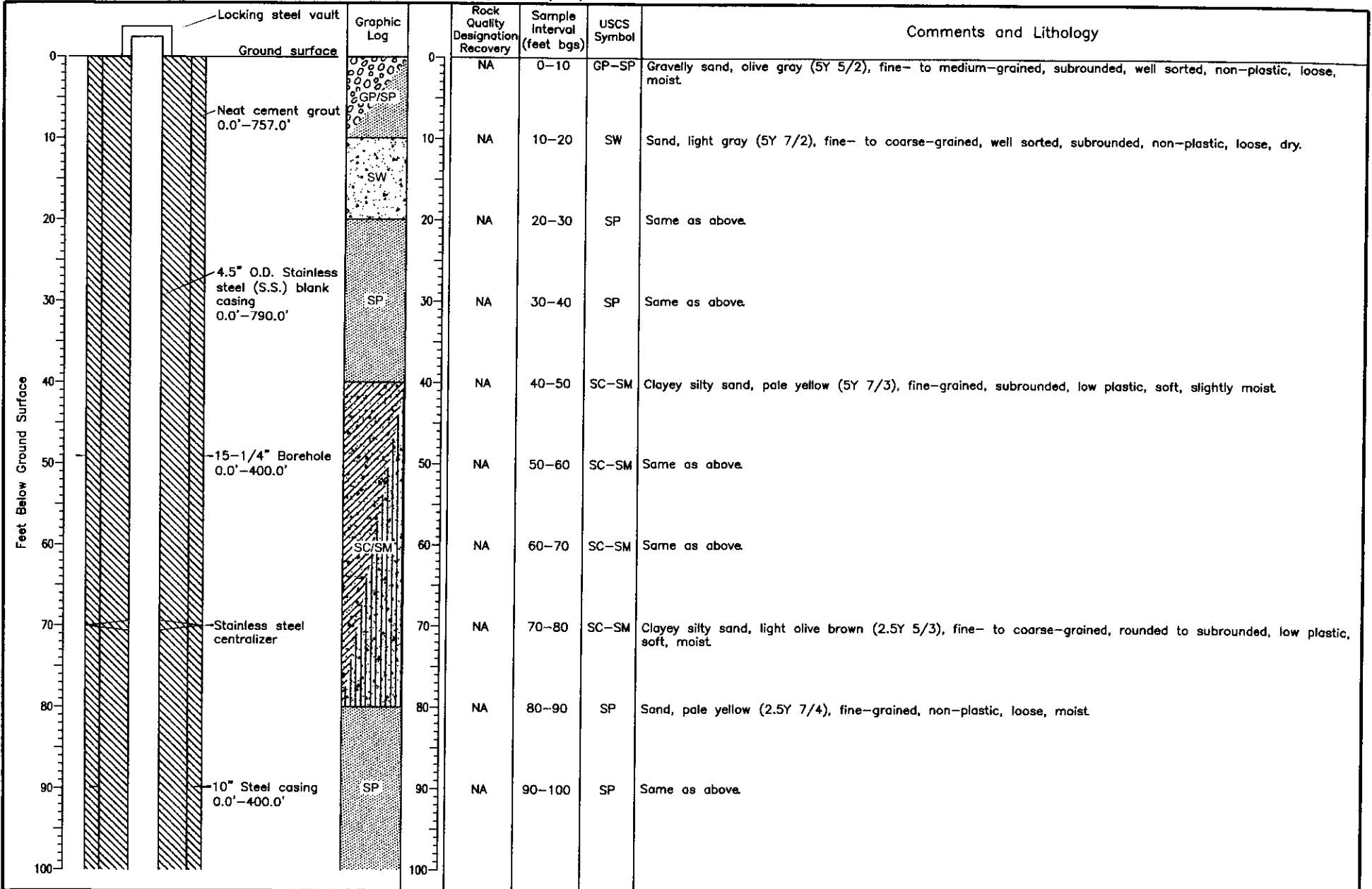


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 mud rotary drilling 385'-520', air rotary drilling  
 750'-923'





Geologist: M. Nauck/J. Raucci

Driller: HAZ-Tech; Adamson Pump and Drill

Date completed: 10-26-11

Drilling method: Core, mud rotary

Bit diameters: 15-1/4", 12" and 9-7/8"

Sampling device: HQ core, rotary cuttings

Steel surface casing: 10"

Note: TOC = top of casing

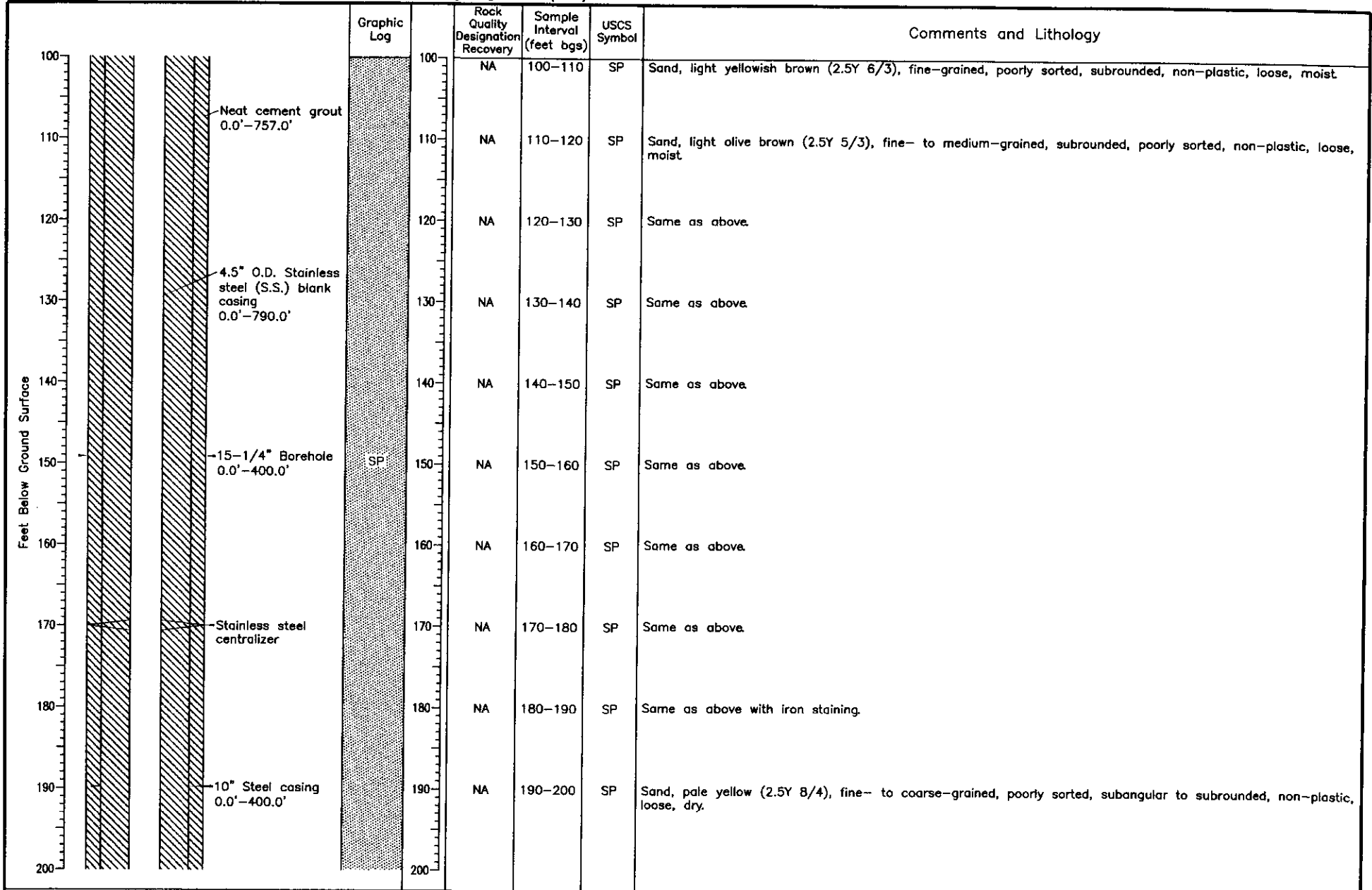
Northing: 665617.168

Easting: 246058.254

Elevation: 3023.3 (TOC)

Note: Adamson Pump and Drill mud rotary drilling 0'-425'; HAZ-Tech core drilling 425'-625'; air rotary drilling 625'-870'



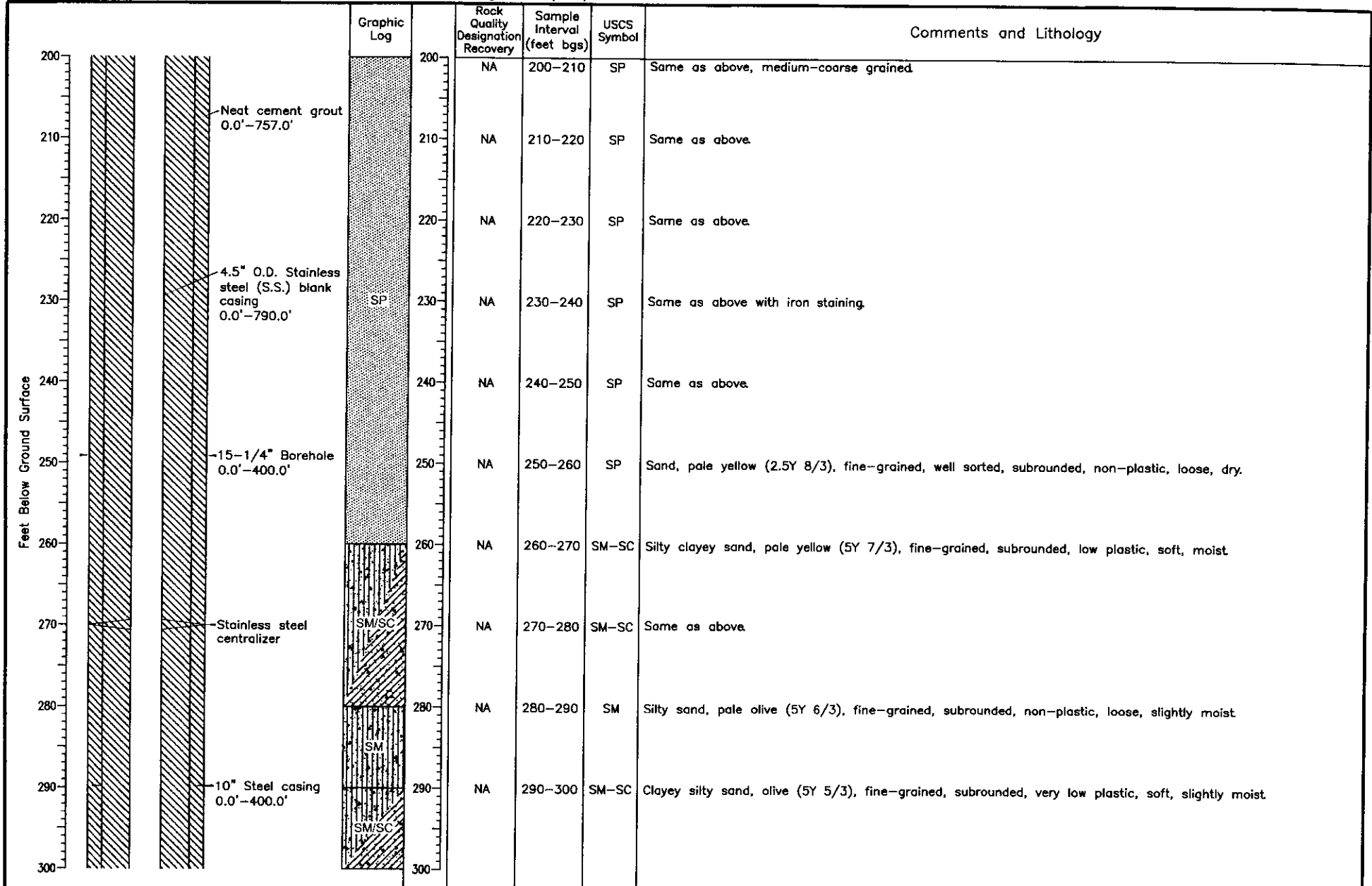


Geologist: M. Nauck/J. Raucci  
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 Date completed: 10-26-11

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 Bit diameters: 15-1/4", 12" and 9-7/8"  
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Note: Adamson Pump and Drill mud rotary drilling 0'-425'; HAZ-Tech core drilling 425'-625'; air rotary drilling 625'-870'



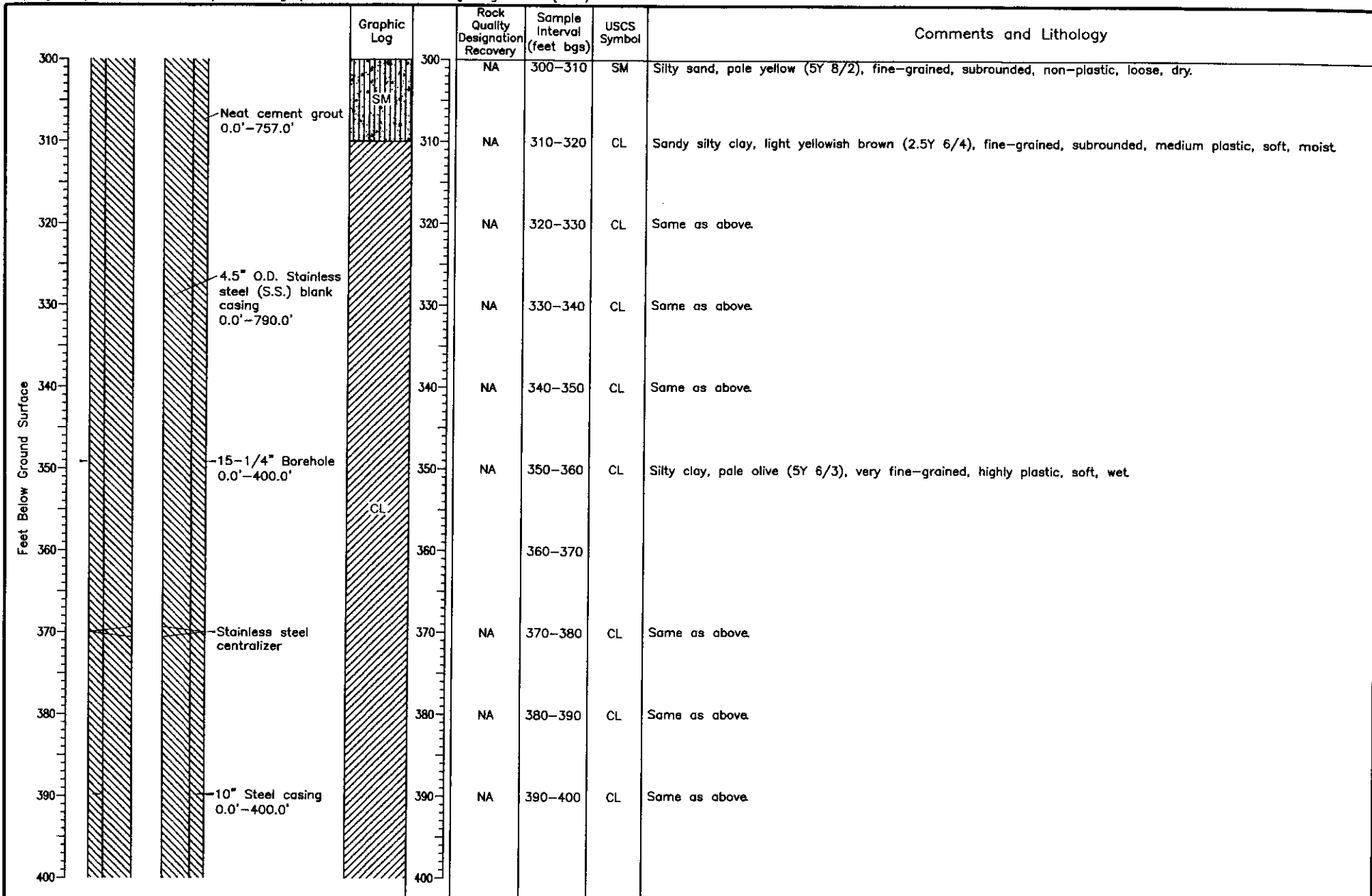


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 Date completed: 10-26-11

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 Bit diameters: 15-1/4", 12" and 9-7/8"  
 Sampling device: HQ core, rotary cuttings  
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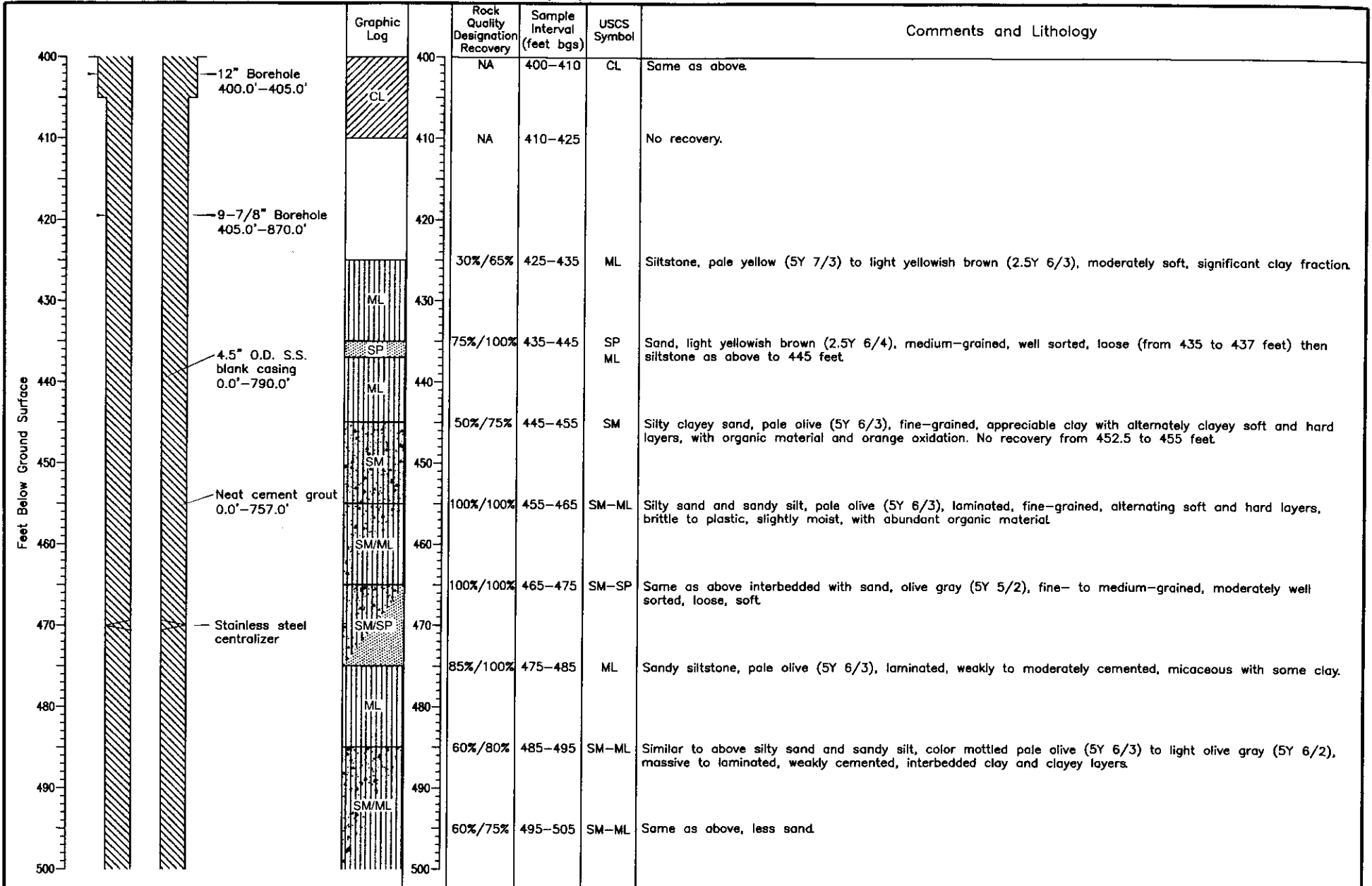


Geologist: M. Nauck/J. Raucci  
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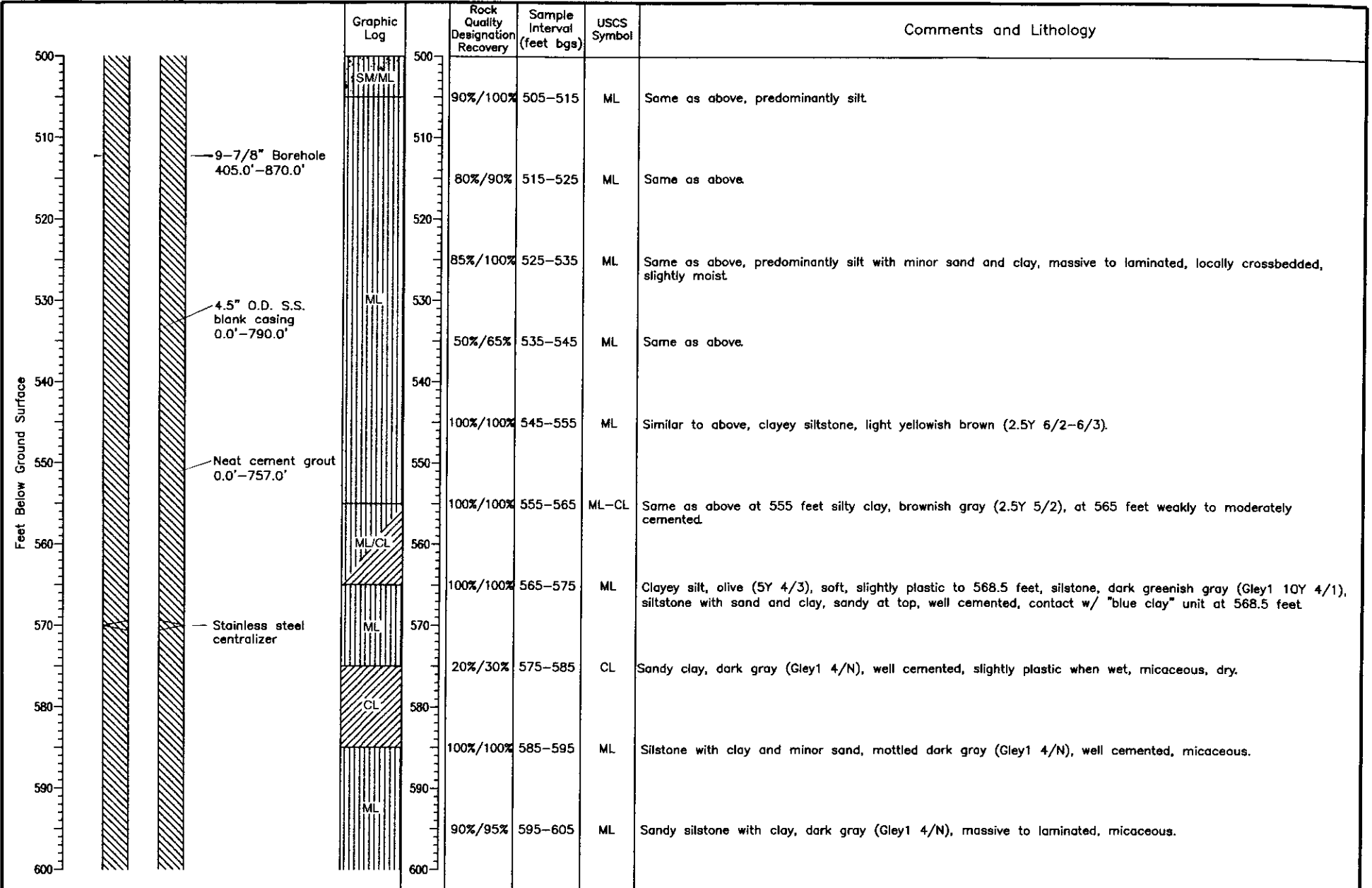
Geologist: M. Nauck/J. Raucci  
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Note: Adamson Pump and Drill mud rotary drilling 0'-425'; HAZ-Tech core drilling 425'-625'; air rotary drilling 625'-870'





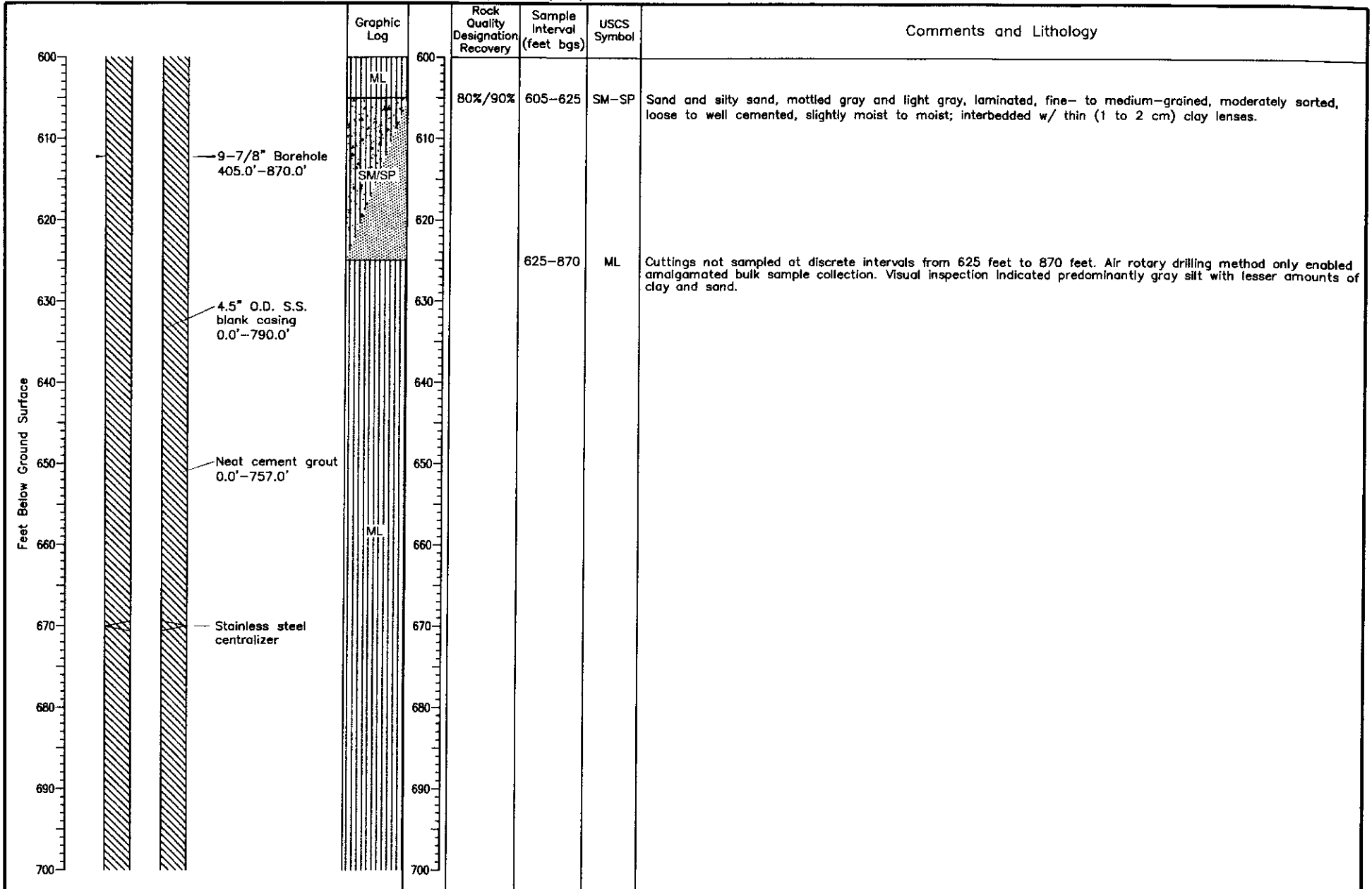


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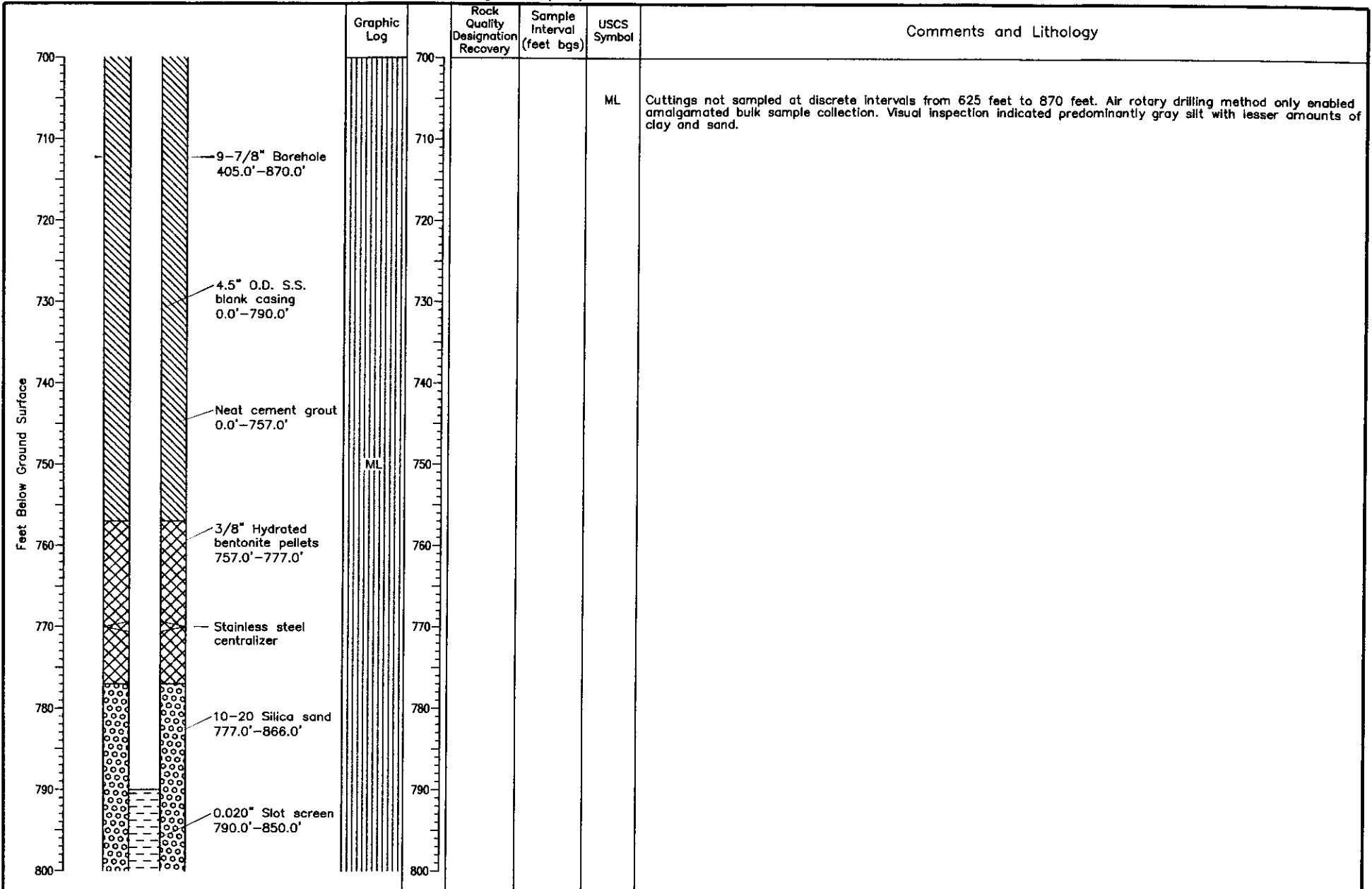


Geologist: M. Nauck/J. Raucci  
 Driller: HAZ-Tech; Adamson Pump and Drill  
 Date completed: 10-26-11

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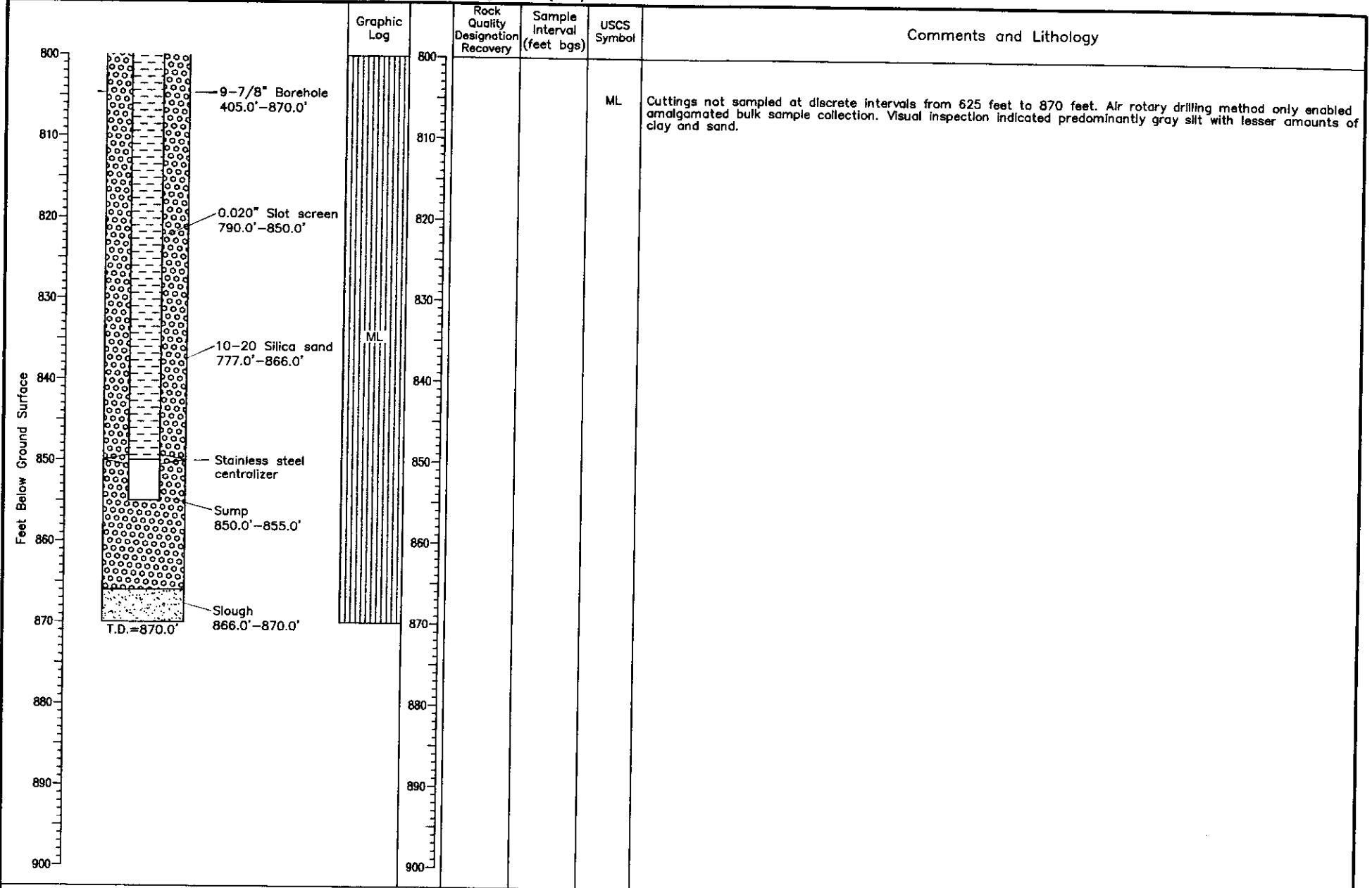


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Drilling method: Core, mud rotary  
 Bit diameters: 15-1/4", 12" and 9-7/8"  
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PICKLES BUTTE  
 Well Log: PB-15